

**NPDES PCSM MODULE 2/  
POST CONSTRUCTION  
STORM WATER MANAGEMENT REPORT**

FOR

**THE WESTTOWN SCHOOL  
OAK LANE PROJECT  
WESTTOWN TOWNSHIP  
CHESTER COUNTY, PA**

PROJECT NO: 1091-001



January 27, 2023

**Revised: March 17, 2023**

Prepared By:



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**NATIONAL POLLUTANT DISCHARGE ELIMINATION SYSTEM (NPDES)  
DISCHARGES OF STORMWATER ASSOCIATED WITH CONSTRUCTION ACTIVITIES  
POST-CONSTRUCTION STORMWATER MANAGEMENT (PCSM) MODULE 2**

Applicant: **The Westtown School**

Project Site Name: **The Westtown School - Oak Lane Projects**

Surface Water Name(s): **East Branch Chester Creek, Unt. to East Branch Chester Creek**

Surface Water Use(s): **TSF, MF**

**PCSM PLAN INFORMATION**

1. Identify all structural and non-structural PCSM BMPs that have been selected and provide the information requested.

Discharge Point(s)	BMP ID	BMP Name	BMP Manual	Latitude	Longitude	DA Treated (ac)
001	1	Infiltration Basin	6.4.2	39.944325	-75.539241	3.35
002	2	Subsurface Infiltration Bed	6.4.3	39.944787	-75.537636	2.22
002	3	Subsurface Infiltration Bed	6.4.3	39.945473	-75.537325	2.22
002	4	Infiltration Basin	6.4.2	39.946011	-75.535373	7.24

**Undetained Areas:** 3.85 acre(s)

The Project Qualifies as a Site Restoration Project (25 Pa. Code §102.8(n))

2. Describe the sequence of PCSM BMP implementation in relation to earth disturbance activities and a schedule of inspections for the critical stages of PCSM BMP installation.

**See plan sheet 4.**

3.  Plan drawings have been developed for the project and will be available on-site.

4.  Plan drawings have been developed for the project and are attached to the NOI/application.

5.  Recycling and proper disposal of materials associated with PCSM BMPs are addressed as part of long-term operation and maintenance of the PCSM BMPs.

6. Identify naturally occurring geologic formations or soil conditions that may have the potential to cause pollution after earth disturbance activities are completed and PCSM BMPs are operational and the applicant's plan to avoid or minimize potential pollution and its impacts.

**See plan sheet 4.**

7. Identify whether the potential exists for thermal impacts to surface waters from post-construction stormwater. If such potential exists, identify BMPs that will be implemented to avoid, minimize, or mitigate potential thermal impacts.

**See plan sheet 4.**

8.  The PCSM Plan has been planned, designed, and will be implemented to be consistent with the E&S Plan.

9.  A pre-development site characterization has been performed.

**STORMWATER ANALYSIS – RUNOFF VOLUME**

**Surface Water Name: East Branch Chester Creek**

**Discharge Point(s): 001**

1.  The design standard is based on volume management requirements in an Act 167 Plan approved by DEP within the past five years.
2.  The design standard is based on managing the net change for storms up to and including the 2-year/24-hour storm.
3.  An alternative design standard is being used.
4.  A printout of DEP's PCSM Spreadsheet – Volume Worksheet is attached.
5. 2-Year/24-Hour Storm Event: **3.26** inches Source of precipitation data: **NOAA Atlas 14**
6. Stormwater Runoff Volume, Pre-Construction Conditions: **8,045** CF  Calculations attached
7. Stormwater Runoff Volume, Post-Construction Conditions: **18,351** CF  Calculations attached
8. Net Change (Post-Construction – Pre-Construction Volumes): **10,307** CF
9. Identify all selected structural PCSM BMPs and provide the information requested.  Calculations attached

DP No.	BMP ID	Series	Vol. Routed to BMP (CF)	Inf. Area (SF)	Inf. Rate (in/hr)	Inf. Period (hrs)	Veg?	Media Depth (ft)	Storage Vol. (CF)	Inf. Credit (CF)	ET Credit (CF)
							<input type="checkbox"/>				
							<input type="checkbox"/>				
							<input type="checkbox"/>				
							<input type="checkbox"/>				
							<input type="checkbox"/>				
							<input type="checkbox"/>				
							<input type="checkbox"/>				
							<input type="checkbox"/>				
							<input type="checkbox"/>				

**Total Infiltration & ET Credits (CF): 15,322**

**Non-Structural BMP Volume Credits (CF) (Attach Calculations):**

**Managed Release Credits (CF) (Attach MRC Design Summary):**

**Volume Required to Reduce/Manage (CF): 10,307**

**Total Credits (CF): 15,322**

<b>INFILTRATION INFORMATION</b>	
<b>BMP ID:</b> 1	<input checked="" type="checkbox"/> Soil/geologic test results are attached.
1. No. of infiltration tests completed:	3
2. Method(s) used for infiltration testing:	double ring infiltrometer
3. Test Pit Identifiers (from PCSM Plan Drawings):	14A, 14B, & 16A
4. Avg Infiltration Rate:	0.81 in/hr
5. FOS:	2 : 1
6. Infiltration rate used for design:	0.41 in/hr
7. Separation distance between the BMP bottom and bedrock:	>3.5' feet
8. Separation distance between the BMP bottom and seasonal high-water table:	>3.5' feet
9. Comments:	
<b>BMP ID:</b>	<input type="checkbox"/> Soil/geologic test results are attached.
1. No. of infiltration tests completed:	
2. Method(s) used for infiltration testing:	
3. Test Pit Identifiers (from PCSM Plan Drawings):	
4. Avg Infiltration Rate:	in/hr
5. FOS:	: 1
6. Infiltration Rate Used for Design:	in/hr
7. Separation distance between the BMP bottom and bedrock:	feet
8. Separation distance between the BMP bottom and seasonal high-water table:	feet
9. Comments:	
<b>BMP ID:</b>	<input type="checkbox"/> Soil/geologic test results are attached.
1. No. of infiltration tests completed:	
2. Method(s) used for infiltration testing:	
3. Test Pit Identifiers (from PCSM Plan Drawings):	
4. Avg Infiltration Rate:	in/hr
5. FOS:	: 1
6. Infiltration Rate Used for Design:	in/hr
7. Separation distance between the BMP bottom and bedrock:	feet
8. Separation distance between the BMP bottom and seasonal high-water table:	feet
9. Comments:	

**STORMWATER ANALYSIS – RUNOFF VOLUME**

**Surface Water Name:**    **Unt. to East Branch Chester Creek**

**Discharge Point(s):**    **002**

1.     The design standard is based on volume management requirements in an Act 167 Plan approved by DEP within the past five years.
2.     The design standard is based on managing the net change for storms up to and including the 2-year/24-hour storm.
3.     An alternative design standard is being used.
4.     A printout of DEP's PCSM Spreadsheet – Volume Worksheet is attached.
5.    2-Year/24-Hour Storm Event:    **3.26**          inches          Source of precipitation data:    **NOAA Atlas 14**
6.    Stormwater Runoff Volume, Pre-Construction Conditions:          **23,930**    CF           Calculations attached
7.    Stormwater Runoff Volume, Post-Construction Conditions:          **74,053**    CF           Calculations attached
8.    Net Change (Post-Construction – Pre-Construction Volumes):          **50,123**    CF
9.    Identify all selected structural PCSM BMPs and provide the information requested.           Calculations attached

DP No.	BMP ID	Series	Vol. Routed to BMP (CF)	Inf. Area (SF)	Inf. Rate (in/hr)	Inf. Period (hrs)	Veg?	Media Depth (ft)	Storage Vol. (CF)	Inf. Credit (CF)	ET Credit (CF)
							<input type="checkbox"/>				
							<input type="checkbox"/>				
							<input type="checkbox"/>				
							<input type="checkbox"/>				
							<input type="checkbox"/>				
							<input type="checkbox"/>				
							<input type="checkbox"/>				
							<input type="checkbox"/>				
							<input type="checkbox"/>				
							<input type="checkbox"/>				

**Total Infiltration & ET Credits (CF):          67,633**

**Non-Structural BMP Volume Credits (CF) (Attach Calculations):**

**Managed Release Credits (CF) (Attach MRC Design Summary):**

**Volume Required to Reduce/Manage (CF):          50,123**

**Total Credits (CF):          67,633**

<b>INFILTRATION INFORMATION</b>	
<b>BMP ID: 2</b>	<input checked="" type="checkbox"/> Soil/geologic test results are attached.
1. No. of infiltration tests completed: <b>2</b>	
2. Method(s) used for infiltration testing: <b>double ring infiltrometer</b>	
3. Test Pit Identifiers (from PCSM Plan Drawings): <b>1A &amp; 3B</b>	
4. Avg Infiltration Rate: <b>4.65</b> in/hr	5. FOS: <b>2</b> : 1
6. Infiltration rate used for design: <b>2.32</b> in/hr	
7. Separation distance between the BMP bottom and bedrock: <b>&gt;4'</b> feet	
8. Separation distance between the BMP bottom and seasonal high-water table: <b>&gt;4'</b> feet	
9. Comments:	
<b>BMP ID: 3</b>	<input checked="" type="checkbox"/> Soil/geologic test results are attached.
1. No. of infiltration tests completed: <b>2</b>	
2. Method(s) used for infiltration testing: <b>double ring infiltrometer</b>	
3. Test Pit Identifiers (from PCSM Plan Drawings): <b>4A &amp; 5A</b>	
4. Avg Infiltration Rate: <b>2.02</b> in/hr	5. FOS: <b>2</b> : 1
6. Infiltration Rate Used for Design: <b>1.01</b> in/hr	
7. Separation distance between the BMP bottom and bedrock: <b>&gt;4'</b> feet	
8. Separation distance between the BMP bottom and seasonal high-water table: <b>&gt;4'</b> feet	
9. Comments:	
<b>BMP ID: 4</b>	<input type="checkbox"/> Soil/geologic test results are attached.
1. No. of infiltration tests completed: <b>2</b>	
2. Method(s) used for infiltration testing: <b>double ring infiltrometer</b>	
3. Test Pit Identifiers (from PCSM Plan Drawings): <b>6A &amp; 7B</b>	
4. Avg Infiltration Rate: <b>1.67</b> in/hr	5. FOS: <b>2</b> : 1
6. Infiltration Rate Used for Design: <b>0.84</b> in/hr	
7. Separation distance between the BMP bottom and bedrock: <b>&gt;2'</b> feet	
8. Separation distance between the BMP bottom and seasonal high-water table: <b>2'</b> feet	
9. Comments:	



**STORMWATER ANALYSIS – PEAK RATE**

**Surface Water Name:** East Branch Chester Creek **Discharge Point(s):** 001

1.  The design standard is based on rate requirements in an Act 167 Plan approved by DEP within the past five years.
2.  The design standard is based on managing the net change for 2-, 10-, 50-, and 100-year/24-hour storms.
3.  An alternative design standard is being used.
4.  A printout of DEP's PCSM Spreadsheet – Rate Worksheet is attached.
5.  Alternative rate calculations are attached.

6. Identify precipitation amounts. Source of precipitation data:

2-Year/24-Hour Storm: 10-Year/24-Hour Storm

50-Year/24-Hour Storm: 100-Year/24-Hour Storm

7. Report peak discharge rates, pre- and post-construction (without BMPs), based on a time of concentration analysis.

Design Storm	Pre-Construction Peak Rate (cfs)	Post-Construction Peak Rate (cfs)	Difference (cfs)
2-Year/24-Hour			
10-Year/24-Hour			
50-Year/24-Hour			
100-Year/24-Hour			

8. Identify all BMPs used to mitigate peak rate differences and provide the requested information.

BMP ID	Inflow to BMP (cfs)				Outflow from BMP (cfs)			
	2-Yr	10-Yr	50-Yr	100-Yr	2-Yr	10-Yr	50-Yr	100-Yr

9. Report peak rates for pre-construction and post-construction with BMPs and identify the differences.

Design Storm	Pre-Construction Peak Rate (cfs)	Post-Construction Peak Rate (with BMPs) (cfs)	Difference (cfs)
2-Year/24-Hour	4.26	1.23	-3.03
10-Year/24-Hour	11.81	22.86	-8.75
50-Year/24-Hour	22.86	7.66	-15.20
100-Year/24-Hour	28.81	12.60	-16.21

**STORMWATER ANALYSIS – PEAK RATE**

**Surface Water Name:** Unt. to East Branch Chester Creek **Discharge Point(s):** 002

1.  The design standard is based on rate requirements in an Act 167 Plan approved by DEP within the past five years.
2.  The design standard is based on managing the net change for 2-, 10-, 50-, and 100-year/24-hour storms.
3.  An alternative design standard is being used.
4.  A printout of DEP's PCSM Spreadsheet – Rate Worksheet is attached.
5.  Alternative rate calculations are attached.
6. Identify precipitation amounts. Source of precipitation data:

2-Year/24-Hour Storm: 10-Year/24-Hour Storm

50-Year/24-Hour Storm: 100-Year/24-Hour Storm

7. Report peak discharge rates, pre- and post-construction (without BMPs), based on a time of concentration analysis.

Design Storm	Pre-Construction Peak Rate (cfs)	Post-Construction Peak Rate (cfs)	Difference (cfs)
2-Year/24-Hour			
10-Year/24-Hour			
50-Year/24-Hour			
100-Year/24-Hour			

8. Identify all BMPs used to mitigate peak rate differences and provide the requested information.

BMP ID	Inflow to BMP (cfs)				Outflow from BMP (cfs)			
	2-Yr	10-Yr	50-Yr	100-Yr	2-Yr	10-Yr	50-Yr	100-Yr

9. Report peak rates for pre-construction and post-construction with BMPs and identify the differences.

Design Storm	Pre-Construction Peak Rate (cfs)	Post-Construction Peak Rate (with BMPs) (cfs)	Difference (cfs)
2-Year/24-Hour	7.08	2.33	-4.75
10-Year/24-Hour	22.59	6.13	-16.46
50-Year/24-Hour	45.85	17.54	-28.31
100-Year/24-Hour	58.42	26.76	-31.66

**STORMWATER ANALYSIS – WATER QUALITY**

A printout of DEP's PCSM Spreadsheet – Quality Worksheet is attached for all surface waters receiving discharges.

**LONG-TERM O&M**

Describe the long-term operation and maintenance (O&M) requirements for each selected PCSM BMP.

BMP ID	O&M Requirements
1	See plan sheet 5
2	See plan sheet 5
3	See plan sheet 5
4	See plan sheet 5

**PCSM PLAN DEVELOPER**

I am trained and experienced in PCSM methods.  I am a licensed professional.

Name:	<u>Tyler E. Hill, PE</u>	Title:	<u>Project Manager</u>
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City, State, ZIP:	<u>Lititz, PA 17543</u>	License No.:	<u>PE086960</u>
License Type:	<u>Professional Engineer</u>	Exp. Date	<u>09/30/2023</u>

  
\_\_\_\_\_  
PCSM Plan Developer Signature

1/9/2023  
\_\_\_\_\_  
Date

## **APPENDIX A**

### **STORMWATER MANAGEMENT NARRATIVE**

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## **STORMWATER MANAGEMENT NARRATIVE**

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### **SITE DESCRIPTION**

The project site is located near the center of the Westtown School campus, just south of Oak Lane. The existing site is largely comprised of existing grass athletic fields which are bordered to the north by a partially forested area and the school's academic centers; to the east by a baseball field and residential area; the south by agricultural fields (i.e. row crops) and a partially forested riparian area; and to the west by the school's working farm and agricultural area.

During the past 50 years, the site's primary use has been agricultural (i.e. row crops). The site is currently utilized primarily for athletic fields, with row crops along the southeastern portion of the project site. The site has been utilized as such for at least the past five years, with no significant improvements being constructed during that time.

### **SUMMARY OF PROPOSED IMPROVEMENTS**

The Westtown School is proposing to improve upon the existing athletic facilities on campus by constructing two new synthetic turf multipurpose fields, along with reconfiguring the remaining area to maximize field space. Additional components of the project involve the construction of a field house, parking lot and improved pedestrian access.

### **SOIL DESCRIPTIONS, LIMITATIONS AND RESOLUTIONS**

As per the USDA NRCS Web Soil Survey, the soils within the project area (Limit of Disturbance) are classified as follows:

- CaB – Califon Loam (3-8% slopes, Hydrologic Soil Group "D")
- GgC – Glenelg Silt Loam (8-15% slopes, Hydrologic Soil Group "B")
- MaA – Manor Loam (0-3% slopes, Hydrologic Soil Group "B")
- MaB – Manor Loam (3-8% slopes, Hydrologic Soil Group "B")
- MaC – Manor Loam (8-15% slopes, Hydrologic Soil Group "B")

See the *Supplemental Design Information* section for a summary of the Soil Facts, Use Limitations and Resolutions.

### **GEOTECHNICAL ASSESSMENT**

A geotechnical investigation was performed on site to evaluate the site for infiltration of post-construction stormwater. The investigation determined that the site is underlain by the polytuff schist of the Glenarm Wissahickon Formation. This formation includes lenticular amphibolite bodies having ocean-floor basalt chemistry and is not considered karst. Infiltration tests performed on site found suitable infiltration rates in nearly every test pit, but not at all depths. In general, the site was found to be well drained and suitable for infiltration.

The complete Stormwater Infiltration Feasibility Report, dated October 8, 2018, and Supplemental Infiltration Feasibility Report, dated November 9, 2018, has been provided as an attachment to this report.

## **NARRATIVE DESCRIPTION OF STORMWATER MANAGEMENT CONCEPT**

The project site generally sits along a watershed drainage boundary and thus has been analyzed as two drainage areas. The south/western portion of the site generally drains to the southwest towards East Branch Chester Creek (TSF, MF). In post development there is one proposed discharge point (DP001) in this watershed. The eastern portion of the site drains to an existing riparian area consisting of wetlands, forested area and the headwaters of an unnamed tributary to East Branch Chester Creek. In post development, there is one proposed discharge point (DP002) in this watershed. See the Pre and Post Watershed Mapping in this report for watershed delineation.

In order to address rate control, volume control, and water quality requirements the following structural and non-structural BMPs are being proposed:

### **Infiltration Basin (BMP 1 & BMP 4)**

- An infiltration basin is a constructed impoundment intended to capture and infiltrate stormwater runoff.
- Infiltration basin typically contains a layer of installed amended soils which typically contain a high percent of organic matter and additional large grained materials (such as sand) to provide an improved cation exchange rate and assure permeability.
- Infiltration basins are often planted with water-tolerant, native vegetation in order to increase water uptake via the vegetation's root system and increase pollutant removal.

### **Subsurface Infiltration Bed**

- A subsurface detention bed is a void space, typically angular stone and/or manufactured chamber system, constructed beneath the surface on virgin material with the intent to capture and infiltrate stormwater runoff.
- Infiltration Beds B-2 and B-3 are to be installed beneath the synthetic turf fields and consist of crushed angular stone with perforated distribution pipes

## **BMP DESIGN NOTES**

The proposed structural BMPs have been designed in general accordance with the PADEP Stormwater BMP Manual. Given the site topography and location of existing improvements, the design of Basin A required a slightly modified approach with minor deviations from the BMP Manual. First, as the only feasible location for infiltration within the East Branch Chester Creek watershed, impervious and overall loading ratios exceed the recommended values of 5:1 and 8:1, respectively. Loading ratios of approximately 7:1 and 28:1 are proposed. These loading ratios are acceptable as the contributing area does not present a high potential for pollution, the geology is not karst and thus sinkholes and groundwater contamination are not of concern, and the site is general well-drained.

Additionally, three (3) infiltration tests were performed within the infiltration footprint of BMP 1 at the infiltration invert elevation and yielded results of 0.0 in/hr, 1.0 in/hr, and 6.0 in/hr. Based on the results, and the general soil characteristics of the site the area is feasible for infiltration, however determination of a design infiltration rate is not straightforward due to the wide range and the presence of test with zero infiltration. As a result, the design infiltration rate has been determined by removing the highest and lowest recorded infiltration

rates and applying a safety factor of two (2) to the remaining infiltration rate. This approach is reasonable as the recorded infiltration rates in the other proposed infiltration facilities ranged from 1.00 in/hr to 6.00 in/hr, which suggests the site as a whole consists of relatively variable soils but is generally conducive for infiltration. The recorded rates of TP-14 and TP-16 of 1.00 in/hr and 6.00 in/hr are within the range of recorded values elsewhere onsite and thus utilizing the lower of the two would produce a conservative design rate. Additionally, notes have been added to the plan regarding the potentially unsuitable soils within BMP 1 which outline in-situ testing protocol to determine the extent of unsuitable soils and a remediation plan.

**VOLUME MANAGEMENT SUMMARY**

A geotechnical evaluation was performed by Advantage Engineers to determine the suitability of the site for infiltration practices. Based upon the analysis, the site is generally well-drained and suitable for infiltration. See the *Stormwater Infiltration Feasibility Report*, dated October 8, 2018 and the Supplemental Infiltration Feasibility Report, dated November 9, 2018, for more information and a complete list of infiltration test pit results.

**East Branch Chester Creek**

The increase in runoff for the 2-year/24-hour storm for East Branch Chester Creek is being fully mitigated within the Infiltration Basin (BMP 1). A summary of the volume calculatons can be seen in the following table:

**VOLUME SUMMARY**  
**East Branch Chester Creek**

PROJECT: The Westtown School - Oak Lane Project	JOB #: 1091-001
LOCATION: Westtown Township	DATE: 1/13/2023
COUNTY: Chester	REVISED:

Req'd Infiltration Volume						10,307 CF				
STRUCTURAL BMPS										
BMP ID	Infiltration Area (sf)	Impervious		Overall		2 YR Runoff Volume (cf)	Storage		Infiltration & ET Credit (CF)*	
		Area (sf)	LR	Area (sf)	LR		Vol. (cf) @	Elev.		
BMP 1	11,329	53,504	4.7:1	216,893	19:1	19,880	15,585	290.50	15,626	
<b>Total</b>	<b>11,329</b>	<b>53,504</b>	<b>4.7:1</b>	<b>216,893</b>	<b>19:1</b>	<b>19,880</b>	<b>15,585</b>		<b>15,626</b>	

\*See Infiltration Volume Worksheets

**Unt. to East Branch Chester Creek**

The increase in volume for the 2-year/24-hour storm for the Unnamed Tributary to East Branch Chester Creek is being controlled through two (2) subsurface infiltration beds (BMP's 2&3) and an infiltration basin (BMP 4). A summary of the volume calculatons can be seen in the following table:

## VOLUME SUMMARY UNT. TO EAST BRANCH CHESTER CREEK

PROJECT: The Westtown School - Oak Lane Project  
 LOCATION: Westtown Township  
 COUNTY: Chester

JOB #: 1091-001  
 DATE: 1/13/2023  
 REVISED:

Req'd Infiltration Volume (from WS 4)						50,123 CF			
STRUCTURAL BMPS									
BMP ID	Infiltration Area (sf)	Impervious		Overall		2 YR Runoff Volume (cf)	Storage		Infiltration Volume *
		Area (sf)	LR	Area (sf)	LR		Vol. (cf) @	Elev.	
2	75,725	96,824	1.3:1	96,824	1.3:1	24,426	23,035	316.75	24,426
3	26,795	96,824	3.6:1	96,824	3.6:1	24,426	21,916	321.00	24,357
4	18,641	15,823	0.8:1	424,430	22.8:1	25,095	21,724	311.00	18,850
<b>Total</b>	<b>121,161</b>	<b>209,471</b>	<b>1.7:1</b>	<b>618,078</b>	<b>5:1</b>	<b>73,947</b>	<b>66,675</b>		<b>67,633</b>

\*See Infiltration Volume Worksheets

See Appendix B for complete volume calculations.

### PEAK RATE SUMMARY CALCULATIONS

The following tables summarize the calculations for the pre-development peak flows, allowable post-development outflows, and the calculated outflow from each BMP and subdrainage area. Post development flows assume hydraulic routing through the proposed detention/infiltration facilities. All flows are in cfs. See Appendix E within this report for complete area calculations and hydrographs.

## SUMMARY OF FLOWS - NRCS Rainfall-Runoff East Branch Chester Creek

PROJECT: The Westtown School - Oak Lane Project  
 LOCATION: Westtown Township  
 COUNTY: Chester

JOB #: 1091-001  
 DATE: 1/13/2023  
 REVISED:

<u>WATERSHEDS</u>	2 yr	5 yr	10 yr	25 yr	50 yr	100 yr
<b>PRE-DEVELOPMENT</b>	Flows (cfs)					
POI 'A'	4.26	8.16	11.81	17.58	22.86	28.81
<b>Total Pre-Development</b>						
POI 'A' Onsite ( Reduction Factor)	3.15	6.04	8.75	13.02	16.93	21.34
50% Reduction	1.58	3.02	4.37	6.51	8.47	10.67
<b>Allowable Post-Development Flow (Pre-Dev. - 50% Reduction)</b>	<b>2.68</b>	<b>5.14</b>	<b>7.44</b>	<b>11.07</b>	<b>14.40</b>	<b>18.14</b>
<b>POST-DEVELOPMENT</b>						
A- Undetained	1.23	2.18	3.06	4.42	5.63	6.98
BMP 1 (Basin A)	0.13	0.54	1.41	3.93	6.91	12.69
<b>Total Post-Development(Combined Hydrographs)</b>	<b>1.23</b>	<b>2.18</b>	<b>3.06</b>	<b>4.51</b>	<b>7.66</b>	<b>13.69</b>



## SUMMARY OF FLOWS - NRCS Rainfall-Runoff Unt. to East Branch Chester Creek

PROJECT: The Westtown School - Oak Lane Project  
 LOCATION: Westtown Township  
 COUNTY: Chester

JOB #: 1091-001  
 DATE: 1/13/2023  
 REVISED:

<u>WATERSHEDS</u>	2 yr	5 yr	10 yr	25 yr	50 yr	100 yr
<b>PRE-DEVELOPMENT</b>	Flows (cfs)					
POI 'B'	7.08	14.94	22.59	34.79	45.85	58.42
<b>Total Pre-Development</b>						
POI 'B' Onsite ( Reduction Factor)	6.01	12.69	19.19	29.55	38.95	49.62
50% Reduction	3.01	6.35	9.60	14.78	19.48	24.81
<b>Allowable Post-Development Flow</b>	4.07	8.60	13.00	20.02	26.38	33.61
<b>POST-DEVELOPMENT</b>						
BMP 3	0.01	0.08	0.12	0.17	0.22	0.44
BMP 2	0.00	0.15	0.32	0.76	1.33	2.11
BMP 4	0.16	0.77	2.19	8.43	15.66	24.29
B- Undetained	2.33	4.30	6.13	8.99	11.55	14.48
<b>Total Post-Development(Combined Hydrographs)</b>	<b>2.33</b>	<b>4.30</b>	<b>6.13</b>	<b>9.78</b>	<b>17.54</b>	<b>26.76</b>

### OFFSITE DISCHARGE ANALYSIS

#### DP001

Discharge Point (DP)001 is considered to be the proposed outfall of BMP 1. In order to reduce the risk of downstream erosion a rip-rap apron will be employed to dissipate the energy and spread out the concentrated discharge of the endwall. The rip-rap has been designed using current design standards based on pipe size, outflow and anticipated velocity. Approximately 100 feet downslope of the discharge point the outflow enters and existing roadside swale. The flowpath between the discharge path and drainage swale is a well vegetated open area. The relatively short flowpath should reduce the amount of re-concentration of runoff. After the runoff enters the swale it continues on to an existing culvert which discharges to another reach of swale that enters the receiving surface water (refer to the Overall Drainage Map, sheet 44 of 44). Since the post-development rate and volume of runoff from the project site tributary to the existing drainage swale is being reduced from pre- to post development there is no risk of accelerated erosion to the downstream flowpath of runoff leaving the site at DP001. Further, mitigation is being provided in the form of a rip-rap apron to prevent erosion prior to runoff entering the existing drainage swale.

#### DP002

Discharge Point (DP)002 is considered to be the proposed outfall of BMP 4. DP002 discharges to an existing, well vegetated natural draw. This natural draw becomes the headwaters of the receiving watercourse approximately 350' downslope of DP002. In order to reduce the risk of downstream erosion a rip-rap apron will be employed to dissipate the energy and spread out the concentrated discharge of the endwall. The rip-

rap has been designed using current design standards based on pipe size, outflow and anticipated velocity. Given the mild slope of the draw, quality and density of the vegetation, and the proposed outlet protection (rip-rap) there is no anticipated risk of accelerated erosion to the downstream flowpath.

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## **APPENDIX B**

### **PADEP PCSM SPREADSHEETS**

**APPENDIX B**  
**PADEP PCSM SPREADSHEETS**  
**(EAST BRANCH CHESTER CREEK)**

## General Information

Instructions **General** Volume Rate Quality

Project Name:  Application Type:

County:  Municipality:

Project Type:   New Project  Minor / Major Amendment

Area:  acres Total Earth Disturbance:  acres  
*(In Watershed)* *(In Watershed)*

No. of Post-Construction Discharge Points:  Start DP Numbering at:

Discharge Point (DP) No.	Drainage Area (DA) (acres)	Earth Disturbance in DA (acres)	Existing Impervious in DA (acres)	Proposed Impervious in DA (acres)	Receiving Waters	Ch. 93 Class	Structural BMP(s)
001	4.98	3.35	0.35	1.23	Discharge to MS4	TSF, MF	Yes
Undetained Areas	1.46	1.42	0.08	0.14	Discharge to MS4	TSF, MF	
<b>Totals:</b>	<b>6.44</b>	<b>4.77</b>	<b>0.43</b>	<b>1.37</b>			

# Volume Management

Project: The Westtown School - Oak Lane Project

- Instructions
- General
- Volume
- Rate
- Quality

2-Year / 24-Hour Storm Event (NOAA Atlas 14):  inches      Alternative 2-Year / 24-Hour Storm Event  inches

Alternative Source:

**Pre-Construction Conditions:**      No. Rows:        Exempt from Meadow in Good Condition     Automatically Calculate CN, Ia, Runoff and Volume

Land Cover	Area (acres)	Soil Group	CN	Ia (in)	Q Runoff (in)	Runoff Volume (cf)
Impervious Areas: Paved Parking Lots, Roofs, Driveways, Etc. (Excluding ROW)	0.19	B	98	0.041	3.03	2,055
Pervious as Meadow	4.50	B	58	1.448	0.36	5,928
Impervious as Meadow	0.05	B	58	1.448	0.36	62
<b>TOTAL (ACRES):</b>	<b>4.74</b>				<b>TOTAL (CF):</b>	<b>8,045</b>

**Post-Construction Conditions:**      No. Rows:

Land Cover	Area (acres)	Soil Group	CN	Ia (in)	Q Runoff (in)	Runoff Volume (cf)
Impervious Areas: Paved Parking Lots, Roofs, Driveways, Etc. (Excluding ROW)	1.17	B	98	0.041	3.03	12,901
Open Space (Lawns, Parks, Golf Courses, Cemeteries, Etc.) - Good Condition (Grass Cover > 75%)	3.20	B	61	1.279	0.47	5,450
<b>TOTAL (ACRES):</b>	<b>4.38</b>				<b>TOTAL (CF):</b>	<b>18,351</b>

**NET CHANGE IN VOLUME TO MANAGE (CF):** 10,307

**Non-Structural BMP Volume Credits:**

Tree Planting Credit

Other (attach calculations):

**Structural BMP Volume Credits:**

No. Structural BMPs:

Start BMP Numbering at:

DP No.	BMP No.	BMP Name	MRC?	Discharge	Incremental BMP DA (acres)	Volume Routed to BMP (CF)	Infiltration / Vegetated Area (SF)	Infiltration Rate (in/hr)	Infiltration Period (hrs)	Vegetated?	Media Depth (ft)	Storage Volume (CF)	Infiltration Credit (CF)	ET Credit (CF)
001	1	Infiltration Basin		Off-Site	3.35	15,626	11,329	0.41	43	Yes	1.0	15,585	14,980	646

Totals: 14,980 646

INFILTRATION & ET CREDITS (CF):

NET CHANGE IN VOLUME TO MANAGE (CF):

TOTAL CREDITS (CF):

**VOLUME REQUIREMENT SATISFIED**

# Rate Control

Project: The Westtown School - Oak Lane Project

- Instructions
- General
- Volume
- Rate
- Quality

**Precipitation Amounts:**

NOAA 2-Year 24-Hour Storm Event (in):	<b>3.26</b>
NOAA 10-Year 24-Hour Storm Event (in):	<b>4.8</b>
NOAA 50-Year 24-Hour Storm Event (in):	<b>6.66</b>
NOAA 100-Year 24-Hour Storm Event (in):	<b>7.58</b>

Alternative 2-Year 24-Hour Storm Event (in):	
Alternative 10-Year 24-Hour Storm Event (in):	
Alternative 50-Year 24-Hour Storm Event (in):	
Alternative 100-Year 24-Hour Storm Event (in):	

**Report Summary of Peak Rates Only**

Attach model input and output data or other calculations to support the rates reported below.

	<i>Peak Discharge Rates (cfs)</i>			
	Pre-Construction	Post-Construction	Net Change	
2-Year Storm:	4.26	1.23	-3.03	<i>Rate Control Satisfied</i>
10-Year Storm:	11.81	3.06	-8.75	<i>Rate Control Satisfied</i>
50-Year Storm:	22.86	7.66	-15.20	<i>Rate Control Satisfied</i>
100-Year Storm:	28.81	13.69	-15.12	<i>Rate Control Satisfied</i>



# Water Quality

Project: The Westtown School - Oak Lane Project

PRINT

Instructions

General

Volume

Rate

Quality

## Pre-Construction Pollutant Loads:

Land Cover (from Volume Worksheet)	Land Cover for Water Quality	Area (acres)	Soil Group	Runoff Volume (cf)	Pollutant Conc. (mg/L)			Pollutant Loads (lbs)		
					TSS	TP	TN	TSS	TP	TN
Impervious Areas: Paved Parking Lots, Roofs, Driveways, Etc. (Excluding ROW)	Residential	0.19	B	2,055	65.0	0.29	2.05	8.34	0.04	0.26
Pervious as Meadow	Grassland/Herbaceous	4.50	B	5,928	48.8	0.22	2.30	18.06	0.08	0.85
Impervious as Meadow	Grassland/Herbaceous	0.05	B	62	48.8	0.22	2.30	0.19	0.00	0.01
<b>TOTAL (ACRES):</b>		<b>4.74</b>			<b>TOTALS:</b>			<b>26.59</b>	<b>0.12</b>	<b>1.12</b>

## Post-Construction Pollutant Loads (without BMPs):

Land Cover (from Volume Worksheet)	Land Cover for Water Quality	Area (acres)	Soil Group	Runoff Volume (cf)	Pollutant Conc. (mg/L)			Pollutant Loads (lbs)		
					TSS	TP	TN	TSS	TP	TN
Impervious Areas: Paved Parking Lots, Roofs, Driveways, Etc. (Excluding ROW)	Residential	1.17	B	12,901	65.0	0.29	2.05	52.36	0.23	1.65
Open Space (Lawns, Parks, Golf Courses, Cemeteries, Etc.) - Good Condition (Grass Cover > 75%)	Open Space	3.20	B	5,450	78.0	0.25	1.25	26.54	0.09	0.43

TOTAL (ACRES): 4.38

TOTALS: 78.91 0.32 2.08

POLLUTANT LOAD REDUCTION REQUIREMENTS (LBS): **52.31** **0.20** **0.95**

Characterize Undetained Areas (for Untreated Stormwater)

Land Cover	Area (acres)	Soil Group	CN	Ia (in)	Q Runoff (in)	Runoff Volume (cf)

**Non-Structural BMP Water Quality Credits:**

Pervious Undetained Area Credit

Other (attach calculations)

**Structural BMP Water Quality Credits:**

Use default BMP Outflows and Median BMP Outflow Concentrations

DP No.	BMP No.	BMP Name	MRC?	BMP DA (acres)	Vol. Routed to BMP (CF)	Inf. & ET Credits (CF)	Capture & Buffer Credits (CF)	Outflow (CF)	Outflow Conc. (mg/L)			Pollutant Loads (lbs)		
									TSS	TP	TN	TSS	TP	TN
001	1	Infiltration Basin		3.35	15,626	15,626		0	10.00	0.24	0.96	0.00	0.00	0.00

POLLUTANT LOADS FROM STRUCTURAL BMP (TREATED) OUTFLOWS (LBS):

POLLUTANT LOADS FROM UNTREATED STORMWATER (LBS):

NON-STRUCTURAL BMP WATER QUALITY CREDITS (LBS):

NET POLLUTANT LOADS FROM SITE, POST-CONSTRUCTION (LBS):

POLLUTANT LOADS FROM SITE, PRE-CONSTRUCTION (LBS):

TSS	TP	TN
0.00	0.00	0.00
11.72	0.05	0.31
11.72	0.05	0.31
26.59	0.12	1.12

**WATER QUALITY REQUIREMENT SATISFIED**

**CERTIFICATION**

I certify under penalty of law and subject to the penalties of 18 Pa.C.S. § 4904 (relating to unsworn falsification to authorities) that this document and all attachments were prepared under my direction or supervision in accordance with a system designed to assure that qualified personnel properly gathered and evaluated the information submitted. Based on my inquiry of the person or persons who manage the system, or those persons directly responsible for gathering the information, the information submitted is, to the best of my knowledge and belief, true, accurate, and complete. I further certify that the structure, function, and calculations contained in this spreadsheet have not been modified in comparison to the spreadsheet DEP has posted to its website or, if modifications were made, an explanation of the modifications made is attached to this spreadsheet.

**Tyler E. Hill, PE**

Spreadsheet User Name

**1/10/2023**

Date

**UNT. TO  
EAST BRANCH CHESTER CREEK**

## General Information

Instructions
General
Volume
Rate
Quality

Project Name:	<b>The Westtown School - Oak Lane Project</b>	Application Type:	<b>PAG-02 NOI</b>
County:	<b>Chester</b>	Municipality:	<b>Westtown Township</b>
Project Type:	<b>Other</b>	<input checked="" type="radio"/> New Project <input type="radio"/> Minor / Major Amendment	
Area: <i>(In Watershed)</i>	<b>16.93</b> acres	Total Earth Disturbance: <i>(In Watershed)</i>	<b>14.43</b> acres
No. of Post-Construction Discharge Points:	<b>1</b>	Start DP Numbering at:	<b>002</b>

Discharge Point (DP) No.	Drainage Area (DA) (acres)	Earth Disturbance in DA (acres)	Existing Impervious in DA (acres)	Proposed Impervious in DA (acres)	Receiving Waters	Ch. 93 Class	Structural BMP(s)
002	14.19	11.69	0.01	4.81	Unt. to E. Branch Chester Creek	TSF, MF	Yes
Undetained Areas	2.74	2.74	0.00	0.01	Unt. to E. Branch Chester Creek	TSF, MF	
<b>Totals:</b>	<b>16.93</b>	<b>14.43</b>	<b>0.01</b>	<b>4.82</b>			

# Volume Management

Project: The Westtown School - Oak Lane Project

Instructions General **Volume** Rate Quality

2-Year / 24-Hour Storm Event (NOAA Atlas 14):  inches

Alternative 2-Year / 24-Hour Storm Event  inches

Alternative Source:

**Pre-Construction Conditions:**

No. Rows:

Exempt from Meadow in Good Condition  Automatically Calculate CN, Ia, Runoff and Volume

Land Cover	Area (acres)	Soil Group	CN	Ia (in)	Q Runoff (in)	Runoff Volume (cf)
Impervious Areas: Paved Parking Lots, Roofs, Driveways, Etc. (Excluding ROW)	0.01	B	98	0.041	3.03	88
Pervious as Meadow	12.57	B	58	1.448	0.36	16,537
Impervious as Meadow	0.00	B	58	1.448	0.36	3
Pervious as Meadow	1.53	D	78	0.564	1.32	7,303
<b>TOTAL (ACRES):</b>		<b>14.10</b>			<b>TOTAL (CF):</b>	<b>23,930</b>

**Post-Construction Conditions:**

No. Rows:

Land Cover	Area (acres)	Soil Group	CN	Ia (in)	Q Runoff (in)	Runoff Volume (cf)
Impervious Areas: Paved Parking Lots, Roofs, Driveways, Etc. (Excluding ROW)	4.76	B	98	0.041	3.03	52,264
Open Space (Lawns, Parks, Golf Courses, Cemeteries, Etc.) - Good Condition (Grass Cover > 75%)	8.09	B	61	1.279	0.47	13,762
Open Space (Lawns, Parks, Golf Courses, Cemeteries, Etc.) - Good Condition (Grass Cover > 75%)	1.53	D	80	0.500	1.45	8,027
<b>TOTAL (ACRES):</b>		<b>14.37</b>			<b>TOTAL (CF):</b>	<b>74,053</b>

**IET CHANGE IN VOLUME TO MANAGE (CF):** 50,123

**Non-Structural BMP Volume Credits:**

- Tree Planting Credit
- Other (attach calculations):

**Structural BMP Volume Credits:**

No. Structural BMPs: 3

Start BMP Numbering at: 2

DP No.	BMP No.	BMP Name	MRC?	Discharge	Incremental BMP DA (acres)	Volume Routed to BMP (CF)	Infiltration / Vegetated Area (SF)	Infiltration Rate (in/hr)	Infiltration Period (hrs)	Vegetated?	Media Depth (ft)	Storage Volume (CF)	Infiltration Credit (CF)	ET Credit (CF)
002	2	Infiltration Bed		to BMP No. 4	2.22	24,426	75,725	2.32	12	No		23,035	24,426	
002	3	Infiltration Bed		to BMP No. 4	2.22	24,426	26,795	1.01	12	No		21,916	24,357	
002	4	Infiltration Basin		Off-Site	9.74	18,850	18,641	0.84	17	Yes	1.0	18,850	18,850	0

**Totals: 67,633**

**INFILTRATION & ET CREDITS (CF):** 67,633

**NET CHANGE IN VOLUME TO MANAGE (CF):** 50,123

**TOTAL CREDITS (CF):** 67,633

**VOLUME REQUIREMENT SATISFIED**

# Rate Control

Project: The Westtown School - Oak Lane Project

Instructions

General

Volume

**Rate**

Quality

### Precipitation Amounts:

NOAA 2-Year 24-Hour Storm Event (in):

**3.26**

Alternative 2-Year 24-Hour Storm Event (in):

NOAA 10-Year 24-Hour Storm Event (in):

**4.8**

Alternative 10-Year 24-Hour Storm Event (in):

NOAA 50-Year 24-Hour Storm Event (in):

**6.66**

Alternative 50-Year 24-Hour Storm Event (in):

NOAA 100-Year 24-Hour Storm Event (in):

**7.58**

Alternative 100-Year 24-Hour Storm Event (in):

Report Summary of Peak Rates Only

Attach model input and output data or other calculations to support the rates reported below.

	<i>Peak Discharge Rates (cfs)</i>			
	Pre-Construction	Post-Construction	Net Change	
2-Year Storm:	<b>7.08</b>	<b>2.33</b>	<b>-4.75</b>	<i>Rate Control Satisfied</i>
10-Year Storm:	<b>22.59</b>	<b>6.13</b>	<b>-16.46</b>	<i>Rate Control Satisfied</i>
50-Year Storm:	<b>45.85</b>	<b>17.54</b>	<b>-28.31</b>	<i>Rate Control Satisfied</i>
100-Year Storm:	<b>58.42</b>	<b>26.76</b>	<b>-31.66</b>	<i>Rate Control Satisfied</i>



# Water Quality

Project: The Westtown School - Oak Lane Project

[PRINT](#)

- Instructions
- General
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**Pre-Construction Pollutant Loads:**

Land Cover (from Volume Worksheet)	Land Cover for Water Quality	Area (acres)	Soil Group	Runoff Volume (cf)	Pollutant Conc. (mg/L)			Pollutant Loads (lbs)		
					TSS	TP	TN	TSS	TP	TN
Impervious Areas: Paved Parking Lots, Roofs, Driveways, Etc. (Excluding ROW)	Residential	0.01	B	88	65.0	0.29	2.05	0.36	0.00	0.01
Pervious as Meadow	Grassland/Herbaceous	12.57	B	16,537	48.8	0.22	2.30	50.39	0.23	2.38
Impervious as Meadow	Grassland/Herbaceous	0.00	B	3	48.8	0.22	2.30	0.01	0.00	0.00
Pervious as Meadow	Grassland/Herbaceous	1.53	D	7,303	48.8	0.22	2.30	22.25	0.10	1.05
<b>TOTAL (ACRES):</b>		<b>14.10</b>			<b>TOTALS:</b>			<b>73.01</b>	<b>0.33</b>	<b>3.44</b>

**Post-Construction Pollutant Loads (without BMPs):**

Land Cover (from Volume Worksheet)	Land Cover for Water Quality	Area (acres)	Soil Group	Runoff Volume (cf)	Pollutant Conc. (mg/L)			Pollutant Loads (lbs)		
					TSS	TP	TN	TSS	TP	TN
Impervious Areas: Paved Parking Lots, Roofs, Driveways, Etc. (Excluding ROW)	Residential	4.76	B	52,264	65.0	0.29	2.05	212.13	0.95	6.69

Open Space (Lawns, Parks, Golf Courses, Cemeteries, Etc.) - Good Condition (Grass Cover > 75%)	Open Space	8.09	B	13,762	78.0	0.25	1.25	67.03	0.21	1.07
Open Space (Lawns, Parks, Golf Courses, Cemeteries, Etc.) - Good Condition (Grass Cover > 75%)	Open Space	1.53	D	8,027	78.0	0.25	1.25	39.10	0.13	0.63

**TOTAL (ACRES): 14.37**

**TOTALS: 318.25 1.29 8.39**

**POLLUTANT LOAD REDUCTION REQUIREMENTS (LBS):** 245.24 0.96 4.96

**Characterize Undetained Areas (for Untreated Stormwater)**

Land Cover	Area (acres)	Soil Group	CN	Ia (in)	Q Runoff (in)	Runoff Volume (cf)

**Non-Structural BMP Water Quality Credits:**

- Pervious Undetained Area Credit
- Other (attach calculations)

**Structural BMP Water Quality Credits:**

*Use default BMP Outflows and Median BMP Outflow Concentrations*

DP No.	BMP No.	BMP Name	MRC?	BMP DA (acres)	Vol. Routed to BMP (CF)	Inf. & ET Credits (CF)	Capture & Buffer Credits (CF)	Outflow (CF)	Outflow Conc. (mg/L)			Pollutant Loads (lbs)		
									TSS	TP	TN	TSS	TP	TN
002	2	Infiltration Bed		2.22	24,426	24,426		0	-	-	-	-	-	-
002	3	Infiltration Bed		2.22	24,426	24,357		69	-	-	-	-	-	-
002	4	Infiltration Basin		9.74	18,850	18,850		0	10.00	0.24	0.96	0.00	0.00	0.00

	TSS	TP	TN
<b>POLLUTANT LOADS FROM STRUCTURAL BMP (TREATED) OUTFLOWS (LBS):</b>	<b>0.00</b>	<b>0.00</b>	<b>0.00</b>
<b>POLLUTANT LOADS FROM UNTREATED STORMWATER (LBS):</b>	<b>27.59</b>	<b>0.11</b>	<b>0.73</b>
<b>NON-STRUCTURAL BMP WATER QUALITY CREDITS (LBS):</b>			
<b>NET POLLUTANT LOADS FROM SITE, POST-CONSTRUCTION (LBS):</b>	<b>27.59</b>	<b>0.11</b>	<b>0.73</b>
<b>POLLUTANT LOADS FROM SITE, PRE-CONSTRUCTION (LBS):</b>	<b>73.01</b>	<b>0.33</b>	<b>3.44</b>

**WATER QUALITY REQUIREMENT SATISFIED**

### CERTIFICATION

I certify under penalty of law and subject to the penalties of 18 Pa.C.S. § 4904 (relating to unsworn falsification to authorities) that this document and all attachments were prepared under my direction or supervision in accordance with a system designed to assure that qualified personnel properly gathered and evaluated the information submitted. Based on my inquiry of the person or persons who manage the system, or those persons directly responsible for gathering the information, the information submitted is, to the best of my knowledge and belief, true, accurate, and complete. I further certify that the structure, function, and calculations contained in this spreadsheet have not been modified in comparison to the spreadsheet DEP has posted to its website or, if modifications were made, an explanation of the modifications made is attached to this spreadsheet.

**Tyler E. Hill, PE**

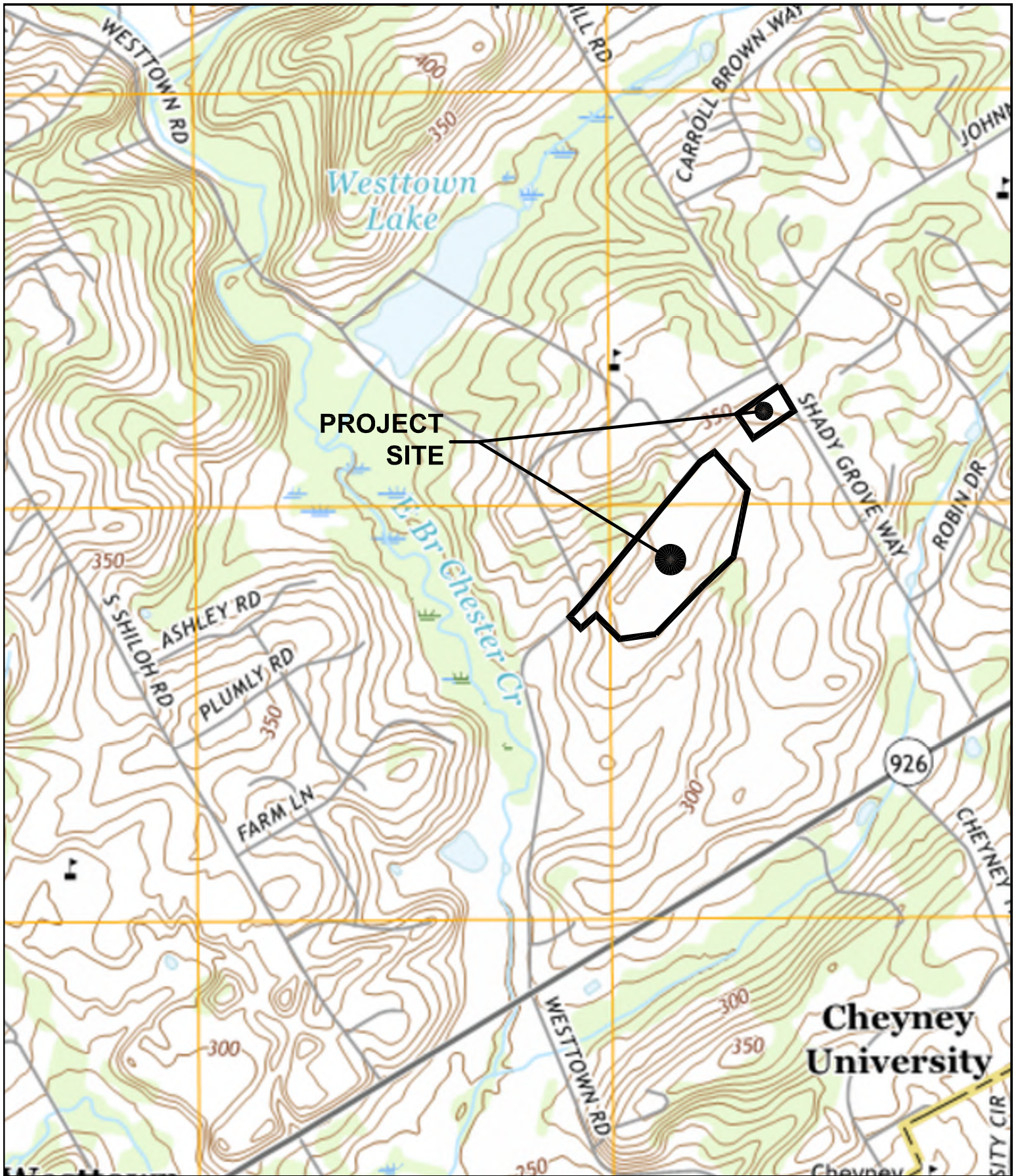
Spreadsheet User Name

**1/10/2023**

Date

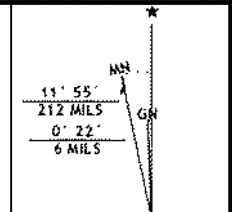
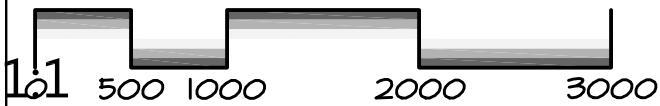
## **APPENDIX C**

### **REFERENCE & SUPPORTING DOCUMENTS**

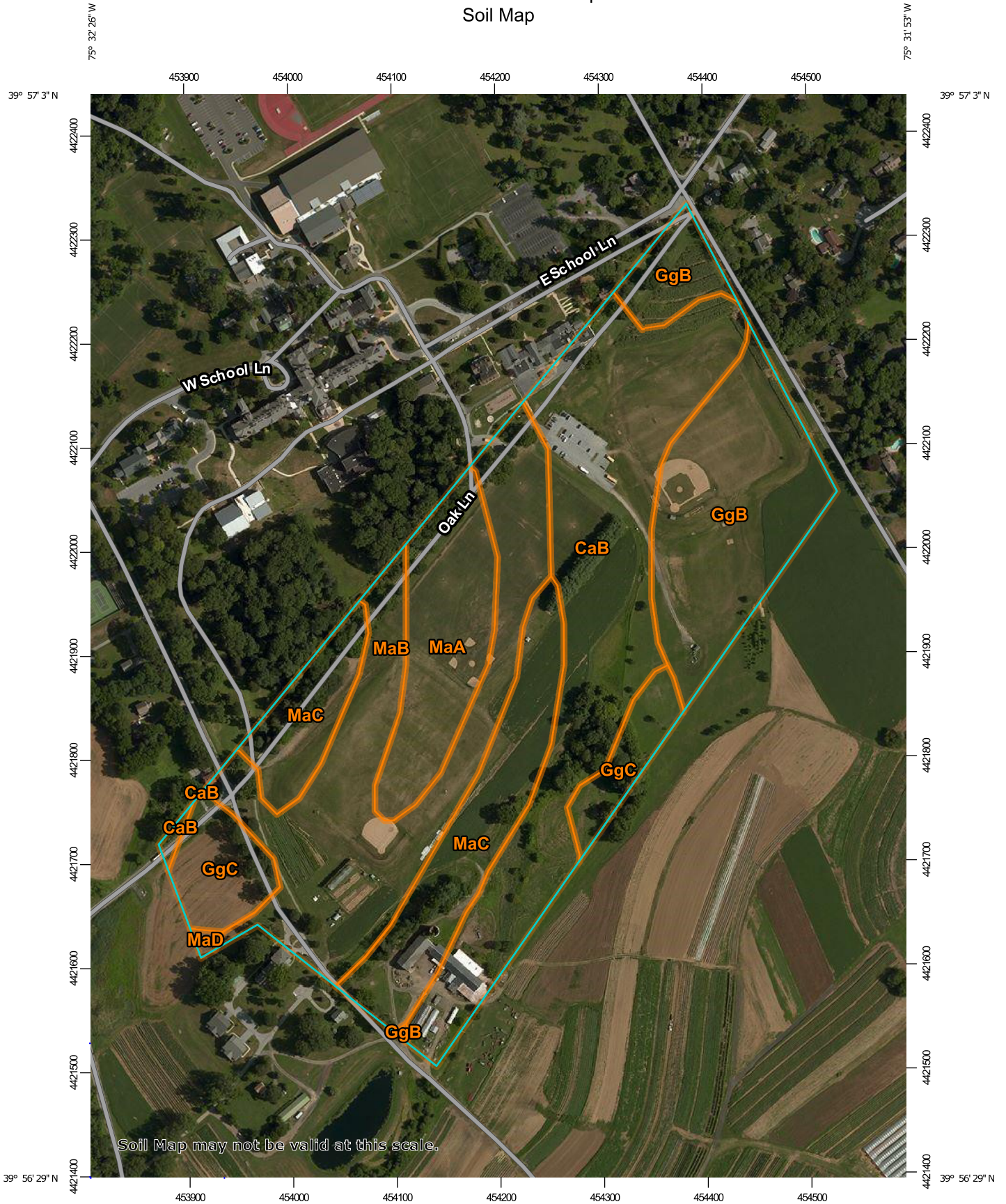


USGS 7.5 MINUTE  
WEST CHESTER, PA QUADRANGLE

SCALE IN FEET: 1" = 1000



# Custom Soil Resource Report Soil Map



Map Scale: 1:5,070 if printed on A portrait (8.5" x 11") sheet.

0 50 100 200 300 Meters

0 200 400 800 1200 Feet

Map projection: Web Mercator Corner coordinates: WGS84 Edge tics: UTM Zone 18N WGS84



## Map Unit Legend

Map Unit Symbol	Map Unit Name	Acres in AOI	Percent of AOI
CaB	Califon loam, 3 to 8 percent slopes	16.5	28.4%
GgB	Glenelg silt loam, 3 to 8 percent slopes	10.4	17.9%
GgC	Glenelg silt loam, 8 to 15 percent slopes	4.0	6.9%
MaA	Manor loam, 0 to 3 percent slopes	5.5	9.4%
MaB	Manor loam, 3 to 8 percent slopes	12.9	22.2%
MaC	Manor loam, 8 to 15 percent slopes	8.7	15.0%
MaD	Manor loam, 15 to 25 percent slopes	0.1	0.2%
<b>Totals for Area of Interest</b>		<b>58.1</b>	<b>100.0%</b>

## Map Unit Descriptions

The map units delineated on the detailed soil maps in a soil survey represent the soils or miscellaneous areas in the survey area. The map unit descriptions, along with the maps, can be used to determine the composition and properties of a unit.

A map unit delineation on a soil map represents an area dominated by one or more major kinds of soil or miscellaneous areas. A map unit is identified and named according to the taxonomic classification of the dominant soils. Within a taxonomic class there are precisely defined limits for the properties of the soils. On the landscape, however, the soils are natural phenomena, and they have the characteristic variability of all natural phenomena. Thus, the range of some observed properties may extend beyond the limits defined for a taxonomic class. Areas of soils of a single taxonomic class rarely, if ever, can be mapped without including areas of other taxonomic classes. Consequently, every map unit is made up of the soils or miscellaneous areas for which it is named and some minor components that belong to taxonomic classes other than those of the major soils.

Most minor soils have properties similar to those of the dominant soil or soils in the map unit, and thus they do not affect use and management. These are called noncontrasting, or similar, components. They may or may not be mentioned in a particular map unit description. Other minor components, however, have properties and behavioral characteristics divergent enough to affect use or to require different management. These are called contrasting, or dissimilar, components. They generally are in small areas and could not be mapped separately because of the scale used. Some small areas of strongly contrasting soils or miscellaneous areas are identified by a special symbol on the maps. If included in the database for a given area, the contrasting minor components are identified in the map unit

Job Number: 1091-001

Date: 10/25/2018

## SOILS INFORMATION FACT SHEET

SOIL						SUITABILITY				SOIL CONDITIONS FOR CONSTRUCTION			
SYMBOL NAME	TEXTURE	SLOPE, %	HYDRO. SOIL GROUP	HYDRIC (INCLUSIONS)	ERODIBILITY (K)	DEPTH OF WATER TABLE (IN)	DEPTH TO BEDROCK (IN)	WINTER GRADING	FROST ACTION	SURFACE WATER MANAGEMENT	BUILDING SITE	ROADFILL	TOPSOIL
CaB Califon	Loam	3 to 8	D		0.32	6 to 36	72 to 99	Limited	High	Somewhat Limited	Very Limited	Fair	Fair
GgC Glenelg	Silt Loam	8 to 15	B		0.37	80+	80+	Somewhat Limited	Moderate	Very Limited	Very Limited	Fair	Fair
MaA Manor	Loam	0 to 3	B		0.28	80+	72 to 99	Somewhat Limited	Moderate	Not Limited	Somewhat Limited	Poor	Fair
MaB Manor	Loam	3 to 8	B		0.28	80+	72 to 99	Somewhat Limited	Moderate	Very Limited	Somewhat Limited	Poor	Fair
MaC Manor	Loam	8 to 15	B		0.28	80+	59 to 100	Somewhat Limited	Moderate	Very Limited	Very Limited	Poor	Poor



SOIL LIMITATIONS & RESOLUTIONS					
SOIL	LIMITATIONS		CHARACTERISTICS	RESOLUTIONS	COMMENTS
CaB GgC MaA MaB Mac	Cutbanks Cave	Excavations	The walls of excavations tend to cave in or slough	It is imperative that appropriate precautions be taken to safeguard workers during all trenching and excavation operations.	All applicable OSHA standards and regulations must be implemented at all times.
CaB (C/S) GgC (C) MaA (C) MaB (C) MaC (C)	Corrosive to Concrete/ Steel	Foundation and other infrastructural materials that may contact the soil	Weakening or dissolution of concrete or uncoated steel caused by soil-induced electrochemical or chemical action.	Suitable precautions should be taken to protect all underground pipes, conduits, and storage tanks from concrete and steel corrosion. If potential corrosive properties are encountered during construction, impacted utilities in that area shall be backfilled with processed aggregate to reduce the potential of corrosion from soil backfill.	Refer to the Geotechnical Report
GgC MaA MaB MaC	Erodibility	Grassed Waterways Terraces Slopes Stabilization Landscaping	Easily Erodible Rill and/or Gully Erosion	Excavation should occur during low-rainfall periods when possible  Minimize duration of earth disturbance Immediately stabilize with erosion control matting, mulch, or sod.  Avoid concentrating runoff in disturbed areas	See Erosion and Sediment Control Plan
CaB	Depth to Saturated Zone/ Seasonal High Water Table	Buildings w/ basements Excavations Stormwater Facilities	High table Wetness Soil mottling	Suitable precautions should be taken if water is encountered Contractor is to utilize pumping techniques and other methods as recommended by a Geotechnical Engineer.	Contact Geotechnical Engineer if shallow groundwater is encountered
CaB GgC MaA MaB Mac	Frost Action	Winter Grading	Frost heaving or upward swelling of soil during freezing conditons.	Do not grade, fill, or backfill during periods of freezing temperatures.  Proper precautions should be taken to prevent damage, especially to roadways.	
GgC	Hydric/ Hydric Inclusions	unless authorized by DEP and/or ACOE if wetlands present	Wetlands Wetness	Delineate and Protect Wetlands Obtain all permits/authorizations Utilize pumping techniques where appropriate	See wetland delineation report
CaB GgC MaA MaB MaC	Low Strength/ Landslide Prone	Steep Slopes Structural Fill	Low strength soils are prone failure on steep slopes.	Precautions should be taken to prevent slope failures due to improper construction practices such as over-steepening and overloading of slopes, removal of lateral support, and failure to prevent saturation of slopes.  Setbacks should comply with the standards contained in Chapter 16 unless it can be shown that proposed cuts and fills do not pose a hazard to public safety or to surface waters.  Road fill/other structural fill material will likely need to be imported in areas where soils have low strength.	See geotechnical engineering report or consult the geotechnical professional on record
CaB GgC MaA MaB MaC	Slow Percolation	Stormwater Infiltration On-lot Sewage Facilities	Wetness Soil mottling Shallow groundwater	Soil testing should be performed if infiltration BMPs or on-lot sewage facilities are proposed.  Ammend soils with compost and/or sand.	See geotechnical engineering report or consult the geotechnical professional on record  See Appendix A of the PA Stormwater BMP Manual
GgC MaA MaB MaC	Piping		Formation of subsurface tunnels or pipelike cavities by water moving through the soil	Avoid concentrating runoff. Avoid infiltrating in areas with excessive infiltration rates. Install trench plugs, anti-seep collars, key trenches, etc.	See plans See geotechnical engineering report or consult the geotechnical professional on record
GgC MaA MaB MaC	Poor Source of Topsoil	Vegetative Growth/ Stabilization	Low Fertility Droughty or Wet High Acidity	Soil Testing and appropriate supplementation. Soil amendment/restoration practices	See plan notes
CaB GgC GgC	Wetness	Site work/grading Fill operations	Slow percolation Soil Mottling Shallow groundwater	Concrete stabilization Undercut and replace with suitable material Provide positive drainage	See geotechnical report or consult geotechnical engineer on record

## ORDINANCE APPENDIX C

### RUNOFF COEFFICIENTS AND CURVE NUMBERS

**TABLE C-1. RUNOFF CURVE NUMBERS**

*Source:* Table 2-2a, Table 2-2b, and Table 2-2c from U. S. Department of Agriculture, Natural Resources Conservation Service, June 1986, Urban Hydrology for Small Watersheds, Technical Release No. 55 (TR-55), Second Edition.

**TABLE C-2. RATIONAL RUNOFF COEFFICIENTS**

*Source:* Table F.2 from Delaware County Planning Department, December 2011, Crum Creek Watershed Act 167 Stormwater Management Plan.

**TABLE C-3. MANNING'S 'n' VALUES**

*Source:* Table 3-1 from United States Army Corps of Engineers, January 2010, HEC-RAS River Analysis System, Hydraulic Reference Manual, Version 4.1.

**FIGURE C-1. REDEVELOPMENT PROJECTS RUNOFF CRITERIA ADJUSTMENT FOR PRE-DEVELOPMENT CONDITIONS**

*Source:* Figure B-3 from the Delaware County Planning Department and Chester County Planning Commission, June 2002, Act 167 Stormwater Management Plan Chester Creek Watershed.

**TABLE C-1. RUNOFF CURVE NUMBERS**

(3 pages)

*Source:* Table 2-2a, Table 2-2b, and Table 2-2c from U. S. Department of Agriculture, Natural Resources Conservation Service, June 1986, Urban Hydrology for Small Watersheds, Technical Release No. 55 (TR-55), Second Edition.

**TABLE C-2. RATIONAL RUNOFF COEFFICIENTS**

(1 page)

*Source:* Table F.2 from Delaware County Planning Department, December 2011,  
*Crum Creek Watershed Act 167 Stormwater Management Plan.*

**TABLE C-3. MANNING'S 'n' VALUES**  
(3 pages)

*Source:* Table 3-1 from United States Army Corps of Engineers, January 2010,  
*HEC-RAS River Analysis System, Hydraulic Reference Manual*, Version 4.1.

**Table 2-2a** Runoff curve numbers for urban areas <sup>1/</sup>

Cover description	Average percent impervious area <sup>2/</sup>	Curve numbers for hydrologic soil group			
		A	B	C	D
<i>Fully developed urban areas (vegetation established)</i>					
Open space (lawns, parks, golf courses, cemeteries, etc.) <sup>3/</sup> :					
Poor condition (grass cover < 50%) .....		68	79	86	89
Fair condition (grass cover 50% to 75%) .....		49	69	79	84
Good condition (grass cover > 75%) .....		39	61	74	80
Impervious areas:					
Paved parking lots, roofs, driveways, etc. (excluding right-of-way) .....		98	98	98	98
Streets and roads:					
Paved; curbs and storm sewers (excluding right-of-way) .....		98	98	98	98
Paved; open ditches (including right-of-way) .....		83	89	92	93
Gravel (including right-of-way) .....		76	85	89	91
Dirt (including right-of-way) .....		72	82	87	89
Western desert urban areas:					
Natural desert landscaping (pervious areas only) <sup>4/</sup> .....		63	77	85	88
Artificial desert landscaping (impervious weed barrier, desert shrub with 1- to 2-inch sand or gravel mulch and basin borders) .....		96	96	96	96
Urban districts:					
Commercial and business .....	85	89	92	94	95
Industrial .....	72	81	88	91	93
Residential districts by average lot size:					
1/8 acre or less (town houses) .....	65	77	85	90	92
1/4 acre .....	38	61	75	83	87
1/3 acre .....	30	57	72	81	86
1/2 acre .....	25	54	70	80	85
1 acre .....	20	51	68	79	84
2 acres .....	12	46	65	77	82
<i>Developing urban areas</i>					
Newly graded areas (pervious areas only, no vegetation) <sup>5/</sup> .....		77	86	91	94
Idle lands (CN's are determined using cover types similar to those in table 2-2c).					

<sup>1</sup> Average runoff condition, and  $I_a = 0.2S$ .<sup>2</sup> The average percent impervious area shown was used to develop the composite CN's. Other assumptions are as follows: impervious areas are directly connected to the drainage system, impervious areas have a CN of 98, and pervious areas are considered equivalent to open space in good hydrologic condition. CN's for other combinations of conditions may be computed using figure 2-3 or 2-4.<sup>3</sup> CN's shown are equivalent to those of pasture. Composite CN's may be computed for other combinations of open space cover type.<sup>4</sup> Composite CN's for natural desert landscaping should be computed using figures 2-3 or 2-4 based on the impervious area percentage (CN = 98) and the pervious area CN. The pervious area CN's are assumed equivalent to desert shrub in poor hydrologic condition.<sup>5</sup> Composite CN's to use for the design of temporary measures during grading and construction should be computed using figure 2-3 or 2-4 based on the degree of development (impervious area percentage) and the CN's for the newly graded pervious areas.

**Table 2-2b** Runoff curve numbers for cultivated agricultural lands <sup>1/</sup>

Cover description			Curve numbers for hydrologic soil group			
Cover type	Treatment <sup>2/</sup>	Hydrologic condition <sup>3/</sup>	A	B	C	D
Fallow	Bare soil	—	77	86	91	94
	Crop residue cover (CR)	Poor	76	85	90	93
		Good	74	83	88	90
Row crops	Straight row (SR)	Poor	72	81	88	91
		Good	67	78	85	89
	SR + CR	Poor	71	80	87	90
		Good	64	75	82	85
	Contoured (C)	Poor	70	79	84	88
		Good	65	75	82	86
	C + CR	Poor	69	78	83	87
		Good	64	74	81	85
	Contoured & terraced (C&T)	Poor	66	74	80	82
		Good	62	71	78	81
C&T+ CR	Poor	65	73	79	81	
	Good	61	70	77	80	
Small grain	SR	Poor	65	76	84	88
		Good	63	75	83	87
	SR + CR	Poor	64	75	83	86
		Good	60	72	80	84
	C	Poor	63	74	82	85
		Good	61	73	81	84
	C + CR	Poor	62	73	81	84
		Good	60	72	80	83
	C&T	Poor	61	72	79	82
		Good	59	70	78	81
C&T+ CR	Poor	60	71	78	81	
	Good	58	69	77	80	
Close-seeded or broadcast legumes or rotation meadow	SR	Poor	66	77	85	89
		Good	58	72	81	85
	C	Poor	64	75	83	85
		Good	55	69	78	83
	C&T	Poor	63	73	80	83
Good	51	67	76	80		

<sup>1</sup> Average runoff condition, and  $I_a=0.2S$

<sup>2</sup> Crop residue cover applies only if residue is on at least 5% of the surface throughout the year.

<sup>3</sup> Hydraulic condition is based on combination factors that affect infiltration and runoff, including (a) density and canopy of vegetative areas, (b) amount of year-round cover, (c) amount of grass or close-seeded legumes, (d) percent of residue cover on the land surface (good  $\geq 20\%$ ), and (e) degree of surface roughness.

Poor: Factors impair infiltration and tend to increase runoff.

Good: Factors encourage average and better than average infiltration and tend to decrease runoff.

**Table 2-2c** Runoff curve numbers for other agricultural lands <sup>1/</sup>

Cover description	Hydrologic condition	Curve numbers for hydrologic soil group			
		A	B	C	D
Pasture, grassland, or range—continuous forage for grazing. <sup>2/</sup>	Poor	68	79	86	89
	Fair	49	69	79	84
	Good	39	61	74	80
Meadow—continuous grass, protected from grazing and generally mowed for hay.	—	30	58	71	78
Brush—brush-weed-grass mixture with brush the major element. <sup>3/</sup>	Poor	48	67	77	83
	Fair	35	56	70	77
	Good	30 <sup>4/</sup>	48	65	73
Woods—grass combination (orchard or tree farm). <sup>5/</sup>	Poor	57	73	82	86
	Fair	43	65	76	82
	Good	32	58	72	79
Woods. <sup>6/</sup>	Poor	45	66	77	83
	Fair	36	60	73	79
	Good	30 <sup>4/</sup>	55	70	77
Farmsteads—buildings, lanes, driveways, and surrounding lots.	—	59	74	82	86

<sup>1/</sup> Average runoff condition, and  $I_a = 0.2S$ .<sup>2/</sup> *Poor*: <50% ground cover or heavily grazed with no mulch.*Fair*: 50 to 75% ground cover and not heavily grazed.*Good*: > 75% ground cover and lightly or only occasionally grazed.<sup>3/</sup> *Poor*: <50% ground cover.*Fair*: 50 to 75% ground cover.*Good*: >75% ground cover.<sup>4/</sup> Actual curve number is less than 30; use CN = 30 for runoff computations.<sup>5/</sup> CN's shown were computed for areas with 50% woods and 50% grass (pasture) cover. Other combinations of conditions may be computed from the CN's for woods and pasture.<sup>6/</sup> *Poor*: Forest litter, small trees, and brush are destroyed by heavy grazing or regular burning.*Fair*: Woods are grazed but not burned, and some forest litter covers the soil.*Good*: Woods are protected from grazing, and litter and brush adequately cover the soil.



TABLE F-2

RATIONAL RUNOFF COEFFICIENTS

LAND USE DESCRIPTION	HYDROLOGIC SOIL GROUP			
	A	B	C	D
Cultivated land : without conservation treatment	.49	.67	.81	.88
: with conservation treatment	.27	.43	.61	.67
Pasture or range land: poor condition	.38	.63	.78	.84
: good condition	---*	.25	.51	.65
Meadow: good condition	---*	---*	.44	.61
Woods: thin stand, poor cover, no mulch	---*	.34	.59	.70
: good cover	---*	---*	.45	.59
Open spaces, lawns, parks, golf courses, cemeteries				
Good condition: grass cover on 75% or more of the area	---*	.25	.51	.65
Fair condition: grass cover on 50% to 75% of the area	---*	.45	.63	.74
Commercial and business areas (85% impervious)	.84	.90	.93	.96
Industrial districts (72% impervious)	.67	.81	.88	.92
Residential:				
Average lot size      Average % impervious				
1/8 acre or less      65	.59	.76	.86	.90
1/4 acre      38	.25	.49	.67	.78
1/3 acre      30	---*	.49	.67	.78
1/2 acre      25	---*	.45	.65	.76
1 acre      20	---*	.41	.63	.74
Paved parking lots, roofs, driveways, etc.	.99	.99	.99	.99
Streets and roads:				
Paved with curbs and storm sewers	.99	.99	.99	.99
Gravel	.57	.76	.84	.88
Dirt	.49	.69	.80	.84

Notes: Values are based on SCS definitions and are average values.

Values indicated by ---\* should be determined by the design engineer based on site characteristics.

Source : New Jersey Department of Environmental Protection, Technical Manual for Stream Encroachment, August 1984

Table 3-1 Manning's 'n' Values

Type of Channel and Description	Minimum	Normal	Maximum
<b>A. Natural Streams</b>			
<b>1. Main Channels</b>			
a. Clean, straight, full, no rifts or deep pools			
b. Same as above, but more stones and weeds	0.025	0.030	0.033
c. Clean, winding, some pools and shoals	0.030	0.035	0.040
d. Same as above, but some weeds and stones	0.033	0.040	0.045
e. Same as above, lower stages, more ineffective slopes and sections	0.035	0.045	0.050
f. Same as "d" but more stones	0.040	0.048	0.055
g. Sluggish reaches, weedy, deep pools	0.045	0.050	0.060
h. Very weedy reaches, deep pools, or floodways with heavy stands of timber and brush	0.050	0.070	0.080
	0.070	0.100	0.150
<b>2. Flood Plains</b>			
a. Pasture no brush			
1. Short grass	0.025	0.030	0.035
2. High grass	0.030	0.035	0.050
b. Cultivated areas			
1. No crop	0.020	0.030	0.040
2. Mature row crops	0.025	0.035	0.045
3. Mature field crops	0.030	0.040	0.050
c. Brush			
1. Scattered brush, heavy weeds	0.035	0.050	0.070
2. Light brush and trees, in winter	0.035	0.050	0.060
3. Light brush and trees, in summer	0.040	0.060	0.080
4. Medium to dense brush, in winter	0.045	0.070	0.110
5. Medium to dense brush, in summer	0.070	0.100	0.160
d. Trees			
1. Cleared land with tree stumps, no sprouts	0.030	0.040	0.050
2. Same as above, but heavy sprouts	0.050	0.060	0.080
3. Heavy stand of timber, few down trees, little undergrowth, flow below branches	0.080	0.100	0.120
4. Same as above, but with flow into branches	0.100	0.120	0.160
5. Dense willows, summer, straight	0.110	0.150	0.200
<b>3. Mountain Streams, no vegetation in channel, banks usually steep, with trees and brush on banks submerged</b>			
a. Bottom: gravels, cobbles, and few boulders	0.030	0.040	0.050
b. Bottom: cobbles with large boulders	0.040	0.050	0.070

Table 3-1 (Continued) Manning's 'n' Values

Type of Channel and Description	Minimum	Normal	Maximum
<b>B. Lined or Built-Up Channels</b>			
<b>1. Concrete</b>			
a. Trowel finish	0.011	0.013	0.015
b. Float Finish	0.013	0.015	0.016
c. Finished, with gravel bottom	0.015	0.017	0.020
d. Unfinished	0.014	0.017	0.020
e. Gunite, good section	0.016	0.019	0.023
f. Gunite, wavy section	0.018	0.022	0.025
g. On good excavated rock	0.017	0.020	
h. On irregular excavated rock	0.022	0.027	
<b>2. Concrete bottom float finished with sides of:</b>			
a. Dressed stone in mortar	0.015	0.017	0.020
b. Random stone in mortar	0.017	0.020	0.024
c. Cement rubble masonry, plastered	0.016	0.020	0.024
d. Cement rubble masonry	0.020	0.025	0.030
e. Dry rubble on riprap	0.020	0.030	0.035
<b>3. Gravel bottom with sides of:</b>			
a. Formed concrete	0.017	0.020	0.025
b. Random stone in mortar	0.020	0.023	0.026
c. Dry rubble or riprap	0.023	0.033	0.036
<b>4. Brick</b>			
a. Glazed	0.011	0.013	0.015
b. In cement mortar	0.012	0.015	0.018
<b>5. Metal</b>			
a. Smooth steel surfaces	0.011	0.012	0.014
b. Corrugated metal	0.021	0.025	0.030
<b>6. Asphalt</b>			
a. Smooth	0.013	0.013	
b. Rough	0.016	0.016	
<b>7. Vegetal lining</b>			
	0.030		0.500

Table 3-1 (Continued) Manning's 'n' Values

Type of Channel and Description	Minimum	Normal	Maximum
<i>C. Excavated or Dredged Channels</i>			
<b>1. Earth, straight and uniform</b>			
a. Clean, recently completed	0.016	0.018	0.020
b. Clean, after weathering	0.018	0.022	0.025
c. Gravel, uniform section, clean	0.022	0.025	0.030
d. With short grass, few weeds	0.022	0.027	0.033
<b>2. Earth, winding and sluggish</b>			
a. No vegetation	0.023	0.025	0.030
b. Grass, some weeds	0.025	0.030	0.033
c. Dense weeds or aquatic plants in deep channels	0.030	0.035	0.040
d. Earth bottom and rubble side	0.028	0.030	0.035
e. Stony bottom and weedy banks	0.025	0.035	0.040
f. Cobble bottom and clean sides	0.030	0.040	0.050
<b>3. Dragline-excavated or dredged</b>			
a. No vegetation	0.025	0.028	0.033
b. Light brush on banks	0.035	0.050	0.060
<b>4. Rock cuts</b>			
a. Smooth and uniform	0.025	0.035	0.040
b. Jagged and irregular	0.035	0.040	0.050
<b>5. Channels not maintained, weeds and brush</b>			
a. Clean bottom, brush on sides	0.040	0.050	0.080
b. Same as above, highest stage of flow	0.045	0.070	0.110
c. Dense weeds, high as flow depth	0.050	0.080	0.120
d. Dense brush, high stage	0.080	0.100	0.140

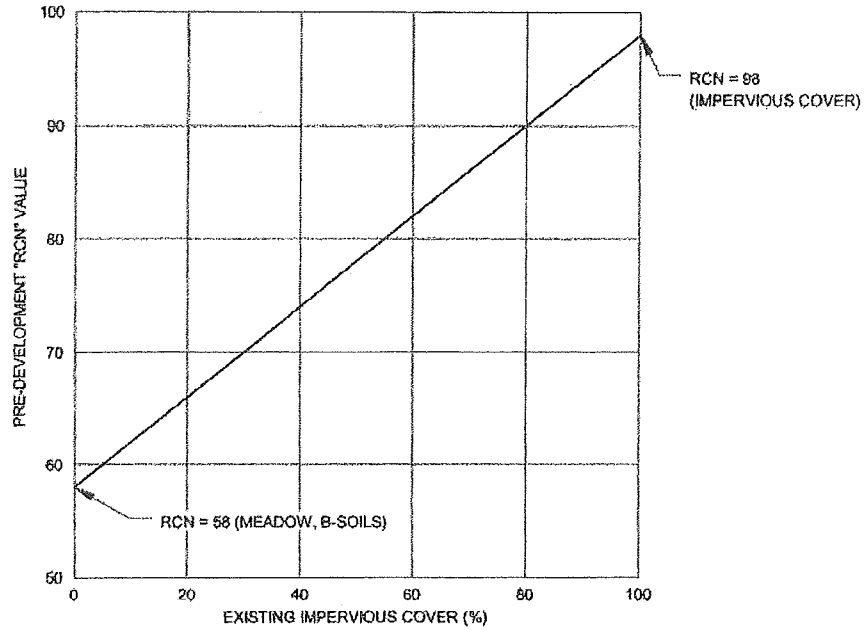
Other sources that include pictures of selected streams as a guide to n value determination are available (Fasken, 1963; Barnes, 1967; and Hicks and Mason, 1991). In general, these references provide color photos with tables of calibrated n values for a range of flows.

Although there are many factors that affect the selection of the n value for the channel, some of the most important factors are the type and size of materials that compose the bed and banks of a channel, and the shape of the channel. Cowan (1956) developed a procedure for estimating the effects of these factors to determine the value of Manning's n of a channel. In Cowan's procedure, the value of n is computed by the following equation:

FIGURE C-1

REDEVELOPMENT PROJECTS  
RUNOFF CRITERIA ADJUSTMENT FOR PRE-DEVELOPMENT CONDITIONS

NRCS METHODOLOGY  
RCN ADJUSTMENT



RATIONAL FORMULA  
C ADJUSTMENT

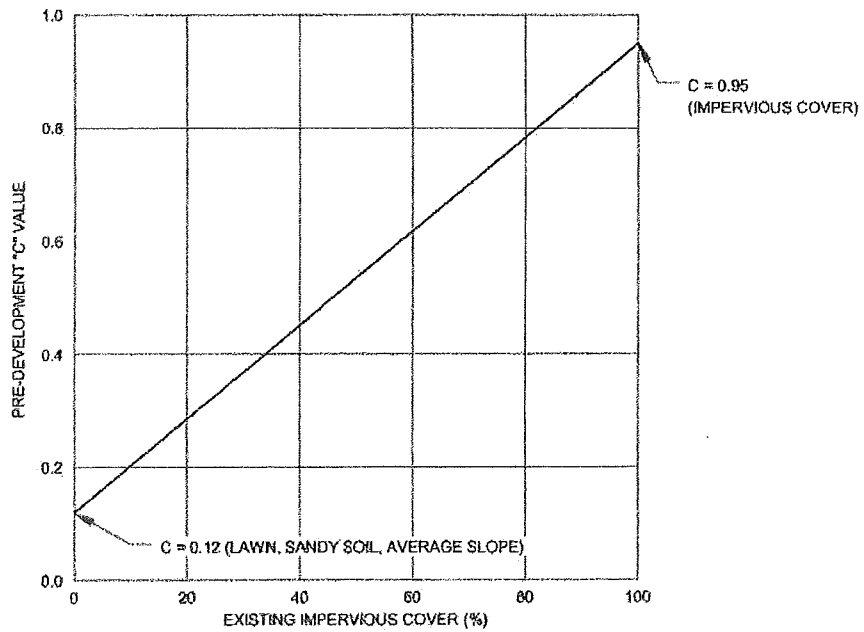
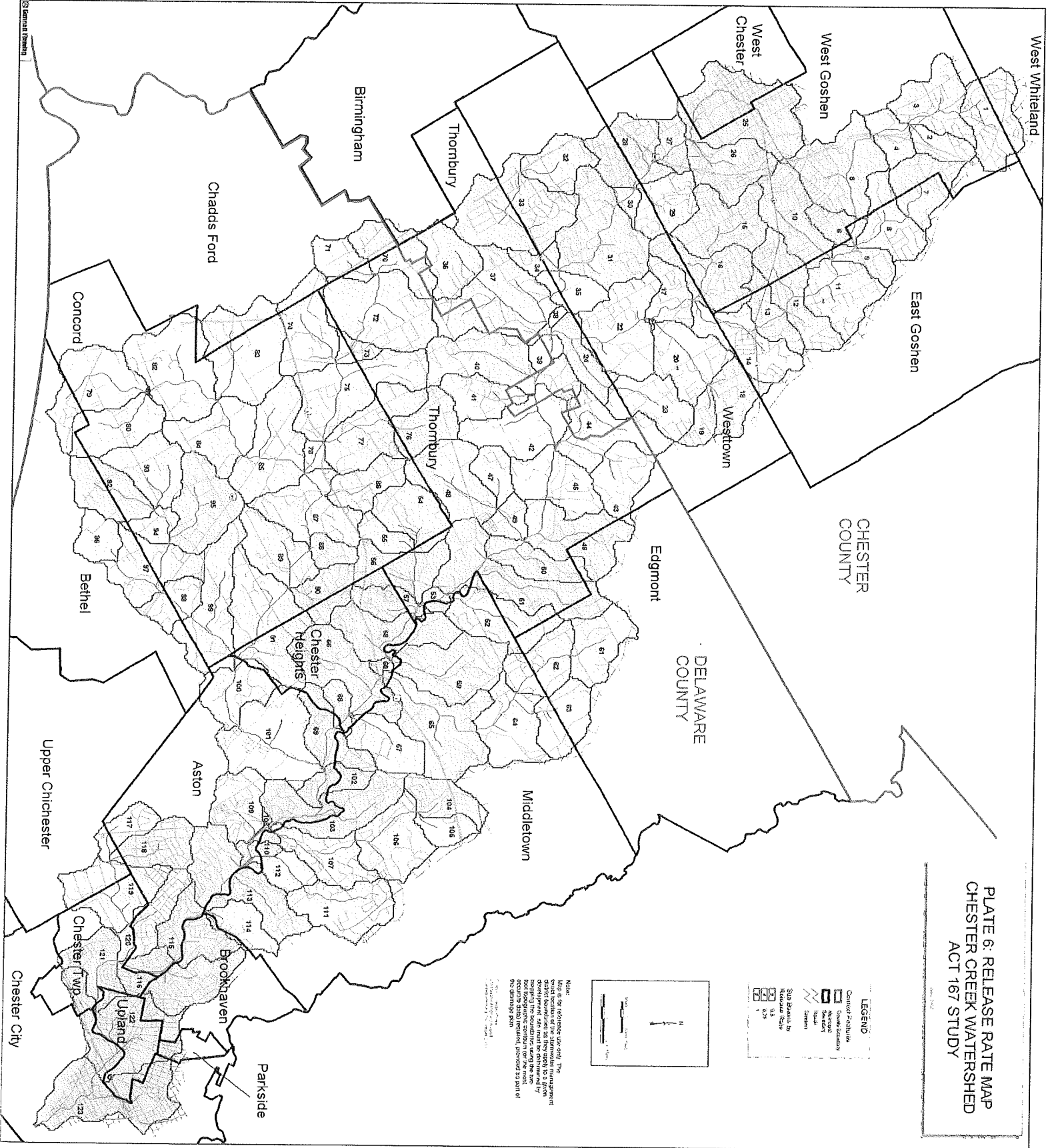


PLATE 6: RELEASE RATE MAP  
 CHESTER CREEK WATERSHED  
 ACT 167 STUDY



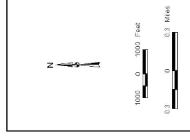
Note:  
 Map is for reference use only. The  
 actual location of the appropriate development  
 site must be determined by  
 the responsible authority. The use  
 of this map for any other purpose  
 requires data provided as part of  
 the strategy plan.

**PLATE 6: RELEASE RATE MAP  
CHESTER CREEK WATERSHED  
ACT 167 STUDY**

June, 2002

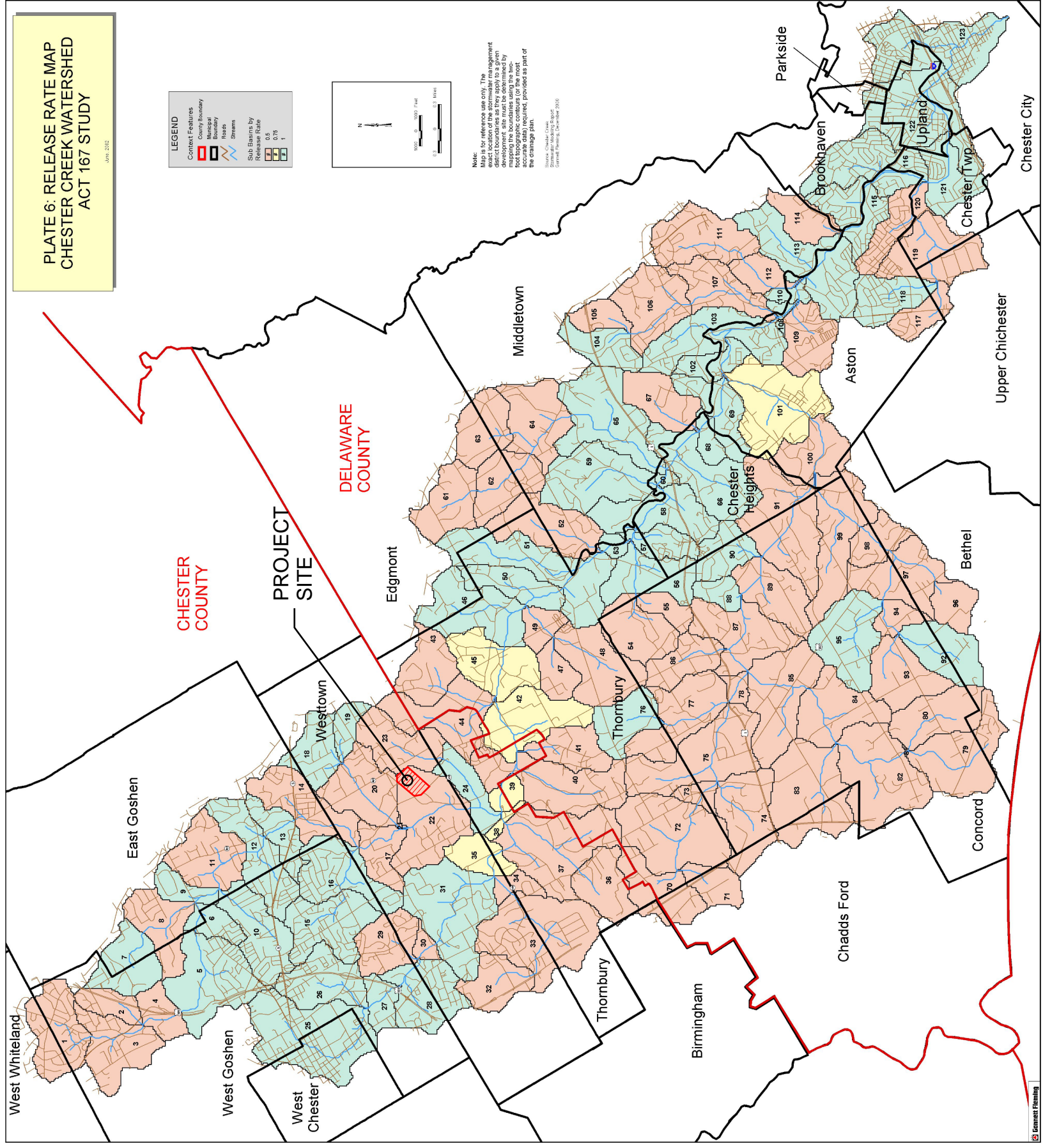
**LEGEND**

	Context Features
	County Boundary
	Municipal Boundary
	Streams
	Sub Basins by Release Rate
	0.5
	1
	1



**Note:** Map is for reference use only. The management district boundaries as they apply to a given development site must be determined by foot topographic contours (or the most accurate data) required, provided as part of the drainage plan.

Source: Chester Creek  
General Permit, December 2010





**NOAA Atlas 14, Volume 2, Version 3**  
**Location name: West Chester, Pennsylvania, USA\***  
**Latitude: 39.9456°, Longitude: -75.5371°**  
**Elevation: 319.37 ft\*\***



\* source: ESRI Maps  
 \*\* source: USGS

**POINT PRECIPITATION FREQUENCY ESTIMATES**

G.M. Bonnin, D. Martin, B. Lin, T. Parzybok, M.Yekta, and D. Riley

NOAA, National Weather Service, Silver Spring, Maryland

[PF tabular](#) | [PF graphical](#) | [Maps & aerials](#)

**PF tabular**

<b>PDS-based point precipitation frequency estimates with 90% confidence intervals (in inches)<sup>1</sup></b>										
<b>Duration</b>	<b>Average recurrence interval (years)</b>									
	<b>1</b>	<b>2</b>	<b>5</b>	<b>10</b>	<b>25</b>	<b>50</b>	<b>100</b>	<b>200</b>	<b>500</b>	<b>1000</b>
<b>5-min</b>	<b>0.353</b> (0.323-0.385)	<b>0.421</b> (0.386-0.459)	<b>0.492</b> (0.450-0.537)	<b>0.542</b> (0.495-0.591)	<b>0.600</b> (0.546-0.655)	<b>0.640</b> (0.578-0.699)	<b>0.679</b> (0.611-0.742)	<b>0.712</b> (0.637-0.781)	<b>0.750</b> (0.665-0.825)	<b>0.778</b> (0.684-0.860)
<b>10-min</b>	<b>0.563</b> (0.517-0.615)	<b>0.673</b> (0.617-0.734)	<b>0.788</b> (0.720-0.859)	<b>0.866</b> (0.791-0.946)	<b>0.957</b> (0.870-1.04)	<b>1.02</b> (0.921-1.11)	<b>1.08</b> (0.971-1.18)	<b>1.13</b> (1.01-1.24)	<b>1.19</b> (1.05-1.31)	<b>1.23</b> (1.08-1.36)
<b>15-min</b>	<b>0.704</b> (0.646-0.769)	<b>0.846</b> (0.775-0.923)	<b>0.996</b> (0.911-1.09)	<b>1.10</b> (1.00-1.20)	<b>1.21</b> (1.10-1.32)	<b>1.29</b> (1.17-1.41)	<b>1.36</b> (1.23-1.49)	<b>1.42</b> (1.27-1.56)	<b>1.49</b> (1.32-1.64)	<b>1.54</b> (1.35-1.70)
<b>30-min</b>	<b>0.966</b> (0.885-1.06)	<b>1.17</b> (1.07-1.27)	<b>1.42</b> (1.30-1.54)	<b>1.59</b> (1.45-1.73)	<b>1.80</b> (1.63-1.96)	<b>1.94</b> (1.76-2.12)	<b>2.09</b> (1.88-2.28)	<b>2.22</b> (1.98-2.43)	<b>2.38</b> (2.11-2.62)	<b>2.49</b> (2.19-2.75)
<b>60-min</b>	<b>1.20</b> (1.10-1.32)	<b>1.47</b> (1.34-1.60)	<b>1.82</b> (1.66-1.98)	<b>2.07</b> (1.89-2.26)	<b>2.39</b> (2.17-2.61)	<b>2.63</b> (2.38-2.88)	<b>2.88</b> (2.59-3.15)	<b>3.11</b> (2.78-3.41)	<b>3.41</b> (3.02-3.75)	<b>3.64</b> (3.20-4.02)
<b>2-hr</b>	<b>1.44</b> (1.31-1.59)	<b>1.75</b> (1.59-1.93)	<b>2.17</b> (1.97-2.40)	<b>2.50</b> (2.26-2.76)	<b>2.93</b> (2.63-3.22)	<b>3.27</b> (2.92-3.60)	<b>3.60</b> (3.20-3.97)	<b>3.94</b> (3.47-4.35)	<b>4.39</b> (3.83-4.86)	<b>4.74</b> (4.09-5.27)
<b>3-hr</b>	<b>1.56</b> (1.42-1.73)	<b>1.90</b> (1.73-2.09)	<b>2.37</b> (2.15-2.61)	<b>2.73</b> (2.47-3.01)	<b>3.20</b> (2.88-3.53)	<b>3.58</b> (3.20-3.94)	<b>3.96</b> (3.52-4.36)	<b>4.34</b> (3.82-4.79)	<b>4.86</b> (4.22-5.38)	<b>5.25</b> (4.51-5.83)
<b>6-hr</b>	<b>1.93</b> (1.75-2.14)	<b>2.33</b> (2.12-2.58)	<b>2.90</b> (2.63-3.21)	<b>3.36</b> (3.03-3.71)	<b>3.99</b> (3.58-4.41)	<b>4.51</b> (4.01-4.97)	<b>5.05</b> (4.45-5.57)	<b>5.61</b> (4.89-6.19)	<b>6.39</b> (5.48-7.09)	<b>7.01</b> (5.93-7.82)
<b>12-hr</b>	<b>2.35</b> (2.13-2.62)	<b>2.83</b> (2.57-3.16)	<b>3.55</b> (3.21-3.95)	<b>4.14</b> (3.73-4.60)	<b>4.99</b> (4.45-5.54)	<b>5.71</b> (5.05-6.33)	<b>6.48</b> (5.66-7.19)	<b>7.32</b> (6.30-8.14)	<b>8.53</b> (7.19-9.51)	<b>9.53</b> (7.89-10.7)
<b>24-hr</b>	<b>2.71</b> (2.49-2.96)	<b>3.26</b> (3.00-3.56)	<b>4.10</b> (3.76-4.48)	<b>4.80</b> (4.39-5.23)	<b>5.81</b> (5.29-6.33)	<b>6.66</b> (6.03-7.24)	<b>7.58</b> (6.82-8.23)	<b>8.57</b> (7.67-9.30)	<b>10.0</b> (8.87-10.9)	<b>11.2</b> (9.85-12.2)
<b>2-day</b>	<b>3.13</b> (2.87-3.43)	<b>3.78</b> (3.47-4.14)	<b>4.76</b> (4.36-5.20)	<b>5.55</b> (5.08-6.07)	<b>6.69</b> (6.09-7.31)	<b>7.63</b> (6.92-8.33)	<b>8.64</b> (7.79-9.42)	<b>9.71</b> (8.70-10.6)	<b>11.3</b> (9.99-12.3)	<b>12.5</b> (11.0-13.7)
<b>3-day</b>	<b>3.30</b> (3.03-3.62)	<b>3.98</b> (3.66-4.36)	<b>5.00</b> (4.59-5.46)	<b>5.83</b> (5.33-6.37)	<b>7.00</b> (6.38-7.65)	<b>7.98</b> (7.24-8.70)	<b>9.02</b> (8.14-9.83)	<b>10.1</b> (9.08-11.0)	<b>11.7</b> (10.4-12.8)	<b>13.0</b> (11.5-14.2)
<b>4-day</b>	<b>3.47</b> (3.19-3.80)	<b>4.19</b> (3.85-4.58)	<b>5.24</b> (4.81-5.73)	<b>6.10</b> (5.59-6.66)	<b>7.32</b> (6.67-7.99)	<b>8.33</b> (7.56-9.08)	<b>9.40</b> (8.49-10.2)	<b>10.5</b> (9.46-11.5)	<b>12.2</b> (10.8-13.3)	<b>13.5</b> (11.9-14.7)
<b>7-day</b>	<b>4.06</b> (3.77-4.41)	<b>4.87</b> (4.51-5.29)	<b>6.03</b> (5.58-6.55)	<b>6.98</b> (6.45-7.57)	<b>8.34</b> (7.68-9.04)	<b>9.47</b> (8.67-10.2)	<b>10.7</b> (9.72-11.5)	<b>12.0</b> (10.8-12.9)	<b>13.8</b> (12.4-14.9)	<b>15.3</b> (13.6-16.6)
<b>10-day</b>	<b>4.62</b> (4.30-4.98)	<b>5.52</b> (5.14-5.95)	<b>6.73</b> (6.26-7.26)	<b>7.71</b> (7.16-8.31)	<b>9.08</b> (8.40-9.77)	<b>10.2</b> (9.40-11.0)	<b>11.3</b> (10.4-12.2)	<b>12.5</b> (11.4-13.5)	<b>14.2</b> (12.9-15.3)	<b>15.6</b> (14.0-16.8)
<b>20-day</b>	<b>6.24</b> (5.84-6.69)	<b>7.41</b> (6.94-7.93)	<b>8.84</b> (8.27-9.47)	<b>9.97</b> (9.31-10.7)	<b>11.5</b> (10.7-12.3)	<b>12.7</b> (11.8-13.6)	<b>13.9</b> (12.9-14.9)	<b>15.1</b> (13.9-16.2)	<b>16.8</b> (15.4-18.0)	<b>18.0</b> (16.4-19.4)
<b>30-day</b>	<b>7.77</b> (7.32-8.24)	<b>9.16</b> (8.63-9.72)	<b>10.7</b> (10.1-11.3)	<b>11.9</b> (11.2-12.6)	<b>13.4</b> (12.6-14.3)	<b>14.6</b> (13.7-15.5)	<b>15.8</b> (14.8-16.8)	<b>17.0</b> (15.8-18.0)	<b>18.5</b> (17.1-19.6)	<b>19.6</b> (18.1-20.9)
<b>45-day</b>	<b>9.86</b> (9.35-10.4)	<b>11.6</b> (11.0-12.2)	<b>13.3</b> (12.6-14.1)	<b>14.6</b> (13.9-15.5)	<b>16.3</b> (15.4-17.2)	<b>17.6</b> (16.6-18.5)	<b>18.7</b> (17.7-19.8)	<b>19.8</b> (18.7-21.0)	<b>21.2</b> (19.9-22.4)	<b>22.2</b> (20.8-23.5)
<b>60-day</b>	<b>11.8</b> (11.2-12.4)	<b>13.8</b> (13.2-14.6)	<b>15.8</b> (15.0-16.6)	<b>17.3</b> (16.4-18.2)	<b>19.1</b> (18.1-20.1)	<b>20.4</b> (19.4-21.5)	<b>21.7</b> (20.5-22.8)	<b>22.8</b> (21.6-24.0)	<b>24.2</b> (22.9-25.5)	<b>25.2</b> (23.8-26.6)

<sup>1</sup> Precipitation frequency (PF) estimates in this table are based on frequency analysis of partial duration series (PDS). Numbers in parenthesis are PF estimates at lower and upper bounds of the 90% confidence interval. The probability that precipitation frequency estimates (for a given duration and average recurrence interval) will be greater than the upper bound (or less than the lower bound) is 5%. Estimates at upper bounds are not checked against probable maximum precipitation (PMP) estimates and may be higher than currently valid PMP values. Please refer to NOAA Atlas 14 document for more information.

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**NOAA Atlas 14, Volume 2, Version 3**  
**Location name: West Chester, Pennsylvania, USA\***  
**Latitude: 39.9456°, Longitude: -75.5371°**  
**Elevation: 319.37 ft\*\***



\* source: ESRI Maps  
 \*\* source: USGS

**POINT PRECIPITATION FREQUENCY ESTIMATES**

G.M. Bonnin, D. Martin, B. Lin, T. Parzybok, M. Yekta, and D. Riley

NOAA, National Weather Service, Silver Spring, Maryland

[PF\\_tabular](#) | [PF\\_graphical](#) | [Maps & aerials](#)

**PF tabular**

<b>PDS-based point precipitation frequency estimates with 90% confidence intervals (in inches/hour)<sup>1</sup></b>										
Duration	Average recurrence interval (years)									
	1	2	5	10	25	50	100	200	500	1000
5-min	4.24 (3.88-4.62)	5.05 (4.63-5.51)	5.90 (5.40-6.44)	6.50 (5.94-7.09)	7.20 (6.55-7.86)	7.68 (6.94-8.39)	8.15 (7.33-8.90)	8.54 (7.64-9.37)	9.00 (7.98-9.90)	9.34 (8.21-10.3)
10-min	3.38 (3.10-3.69)	4.04 (3.70-4.40)	4.73 (4.32-5.15)	5.20 (4.75-5.68)	5.74 (5.22-6.26)	6.11 (5.53-6.68)	6.47 (5.83-7.08)	6.77 (6.06-7.43)	7.12 (6.31-7.84)	7.35 (6.46-8.13)
15-min	2.82 (2.58-3.08)	3.38 (3.10-3.69)	3.98 (3.64-4.35)	4.38 (4.00-4.78)	4.85 (4.41-5.29)	5.16 (4.66-5.64)	5.46 (4.91-5.96)	5.70 (5.10-6.25)	5.97 (5.29-6.57)	6.15 (5.41-6.80)
30-min	1.93 (1.77-2.11)	2.34 (2.14-2.55)	2.83 (2.59-3.09)	3.17 (2.90-3.47)	3.59 (3.27-3.92)	3.89 (3.51-4.24)	4.18 (3.76-4.57)	4.43 (3.97-4.86)	4.75 (4.21-5.23)	4.98 (4.38-5.51)
60-min	1.20 (1.10-1.32)	1.47 (1.34-1.60)	1.82 (1.66-1.98)	2.07 (1.89-2.26)	2.39 (2.17-2.61)	2.63 (2.38-2.88)	2.88 (2.59-3.15)	3.11 (2.78-3.41)	3.41 (3.02-3.75)	3.64 (3.20-4.02)
2-hr	0.719 (0.652-0.792)	0.874 (0.794-0.964)	1.09 (0.986-1.20)	1.25 (1.13-1.38)	1.47 (1.32-1.61)	1.63 (1.46-1.80)	1.80 (1.60-1.99)	1.97 (1.74-2.17)	2.20 (1.91-2.43)	2.37 (2.04-2.63)
3-hr	0.521 (0.474-0.575)	0.632 (0.575-0.697)	0.789 (0.716-0.869)	0.908 (0.822-1.00)	1.07 (0.959-1.17)	1.19 (1.07-1.31)	1.32 (1.17-1.45)	1.45 (1.27-1.60)	1.62 (1.40-1.79)	1.75 (1.50-1.94)
6-hr	0.322 (0.293-0.357)	0.389 (0.354-0.431)	0.484 (0.439-0.536)	0.560 (0.507-0.620)	0.667 (0.598-0.736)	0.752 (0.670-0.830)	0.843 (0.743-0.930)	0.937 (0.817-1.03)	1.07 (0.915-1.18)	1.17 (0.990-1.31)
12-hr	0.195 (0.177-0.218)	0.235 (0.213-0.262)	0.294 (0.267-0.328)	0.343 (0.309-0.382)	0.415 (0.370-0.460)	0.474 (0.419-0.525)	0.538 (0.470-0.597)	0.607 (0.523-0.675)	0.708 (0.597-0.789)	0.791 (0.655-0.885)
24-hr	0.113 (0.104-0.123)	0.136 (0.125-0.149)	0.171 (0.157-0.187)	0.200 (0.183-0.218)	0.242 (0.220-0.264)	0.277 (0.251-0.302)	0.316 (0.284-0.343)	0.357 (0.319-0.388)	0.418 (0.370-0.453)	0.468 (0.410-0.508)
2-day	0.065 (0.060-0.071)	0.079 (0.072-0.086)	0.099 (0.091-0.108)	0.116 (0.106-0.127)	0.139 (0.127-0.152)	0.159 (0.144-0.173)	0.180 (0.162-0.196)	0.202 (0.181-0.221)	0.234 (0.208-0.256)	0.261 (0.230-0.284)
3-day	0.046 (0.042-0.050)	0.055 (0.051-0.061)	0.069 (0.064-0.076)	0.081 (0.074-0.088)	0.097 (0.089-0.106)	0.111 (0.101-0.121)	0.125 (0.113-0.137)	0.141 (0.126-0.153)	0.163 (0.145-0.177)	0.181 (0.159-0.197)
4-day	0.036 (0.033-0.040)	0.044 (0.040-0.048)	0.055 (0.050-0.060)	0.064 (0.058-0.069)	0.076 (0.070-0.083)	0.087 (0.079-0.095)	0.098 (0.088-0.107)	0.110 (0.099-0.120)	0.127 (0.113-0.138)	0.141 (0.124-0.153)
7-day	0.024 (0.022-0.026)	0.029 (0.027-0.031)	0.036 (0.033-0.039)	0.042 (0.038-0.045)	0.050 (0.046-0.054)	0.056 (0.052-0.061)	0.064 (0.058-0.069)	0.071 (0.064-0.077)	0.082 (0.074-0.089)	0.091 (0.081-0.099)
10-day	0.019 (0.018-0.021)	0.023 (0.021-0.025)	0.028 (0.026-0.030)	0.032 (0.030-0.035)	0.038 (0.035-0.041)	0.042 (0.039-0.046)	0.047 (0.043-0.051)	0.052 (0.048-0.056)	0.059 (0.054-0.064)	0.065 (0.058-0.070)
20-day	0.013 (0.012-0.014)	0.015 (0.014-0.017)	0.018 (0.017-0.020)	0.021 (0.019-0.022)	0.024 (0.022-0.026)	0.026 (0.025-0.028)	0.029 (0.027-0.031)	0.032 (0.029-0.034)	0.035 (0.032-0.037)	0.038 (0.034-0.040)
30-day	0.011 (0.010-0.011)	0.013 (0.012-0.013)	0.015 (0.014-0.016)	0.016 (0.016-0.017)	0.019 (0.018-0.020)	0.020 (0.019-0.022)	0.022 (0.020-0.023)	0.024 (0.022-0.025)	0.026 (0.024-0.027)	0.027 (0.025-0.029)
45-day	0.009 (0.009-0.010)	0.011 (0.010-0.011)	0.012 (0.012-0.013)	0.014 (0.013-0.014)	0.015 (0.014-0.016)	0.016 (0.015-0.017)	0.017 (0.016-0.018)	0.018 (0.017-0.019)	0.020 (0.018-0.021)	0.021 (0.019-0.022)
60-day	0.008 (0.008-0.009)	0.010 (0.009-0.010)	0.011 (0.010-0.012)	0.012 (0.011-0.013)	0.013 (0.013-0.014)	0.014 (0.013-0.015)	0.015 (0.014-0.016)	0.016 (0.015-0.017)	0.017 (0.016-0.018)	0.018 (0.016-0.018)

<sup>1</sup> Precipitation frequency (PF) estimates in this table are based on frequency analysis of partial duration series (PDS). Numbers in parenthesis are PF estimates at lower and upper bounds of the 90% confidence interval. The probability that precipitation frequency estimates (for a given duration and average recurrence interval) will be greater than the upper bound (or less than the lower bound) is 5%. Estimates at upper bounds are not checked against probable maximum precipitation (PMP) estimates and may be higher than currently valid PMP values. Please refer to NOAA Atlas 14 document for more information.

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**APPENDIX D**  
**SUPPORTING VOLUME CALCULATIONS**  
**(EAST BRANCH CHESTER CREEK)**

## BMP Volume Calculation Worksheet

**PROJECT:** The Westtown School - Oak Lane Project  
**2-Year Rainfall:** 3.26 in

**Drainage Area Name:** Infiltration BMP 1

Cover Type/Condition	Soil Type	Area (sf)	Area (ac)	CN	S	Ia ((0.2*S)	Q Runoff <sup>1</sup> (in)	Runoff Volume <sup>2</sup> (ft <sup>3</sup> )
<b>Disturbed Area</b>								
Lawn (Good condition)	B	99155	2.28	61	6.39	1.28	0.47	3,873
Paved/Impervious Areas	B	46588	1.07	98	0.20	0.04	3.03	11,753
<b>TOTAL ONSITE:</b>		<b>145743</b>	<b>3.35</b>					<b>15,626</b>
<b>Undisturbed Area</b>								
Lawn (Good condition)	B	64234	1.47	61	6.39	1.28	0.47	2,509
Paved/Impervious Areas	B	6916	0.16	98	0.20	0.04	3.03	1,745
<b>TOTAL:</b>		<b>216893</b>	<b>4.98</b>					<b>19,880</b>

**Drainage Area Name:**

Cover Type/Condition	Soil Type	Area (sf)	Area (ac)	CN	S	Ia ((0.2*S)	Q Runoff <sup>1</sup> (in)	Runoff Volume <sup>2</sup> (ft <sup>3</sup> )
<b>Disturbed Area</b>								
Lawn (Good condition)	B			61	6.39	1.28	0.47	0
Paved/Impervious Areas	B			98	0.20	0.04	3.03	0
<b>Undisturbed Area</b>								
Lawn (Good condition)	B			61	6.39	1.28	0.47	0
Paved/Impervious Areas	B			98	0.20	0.04	3.03	0
<b>TOTAL:</b>		<b>0</b>	<b>0.00</b>				<b>6.99</b>	<b>0</b>

**Drainage Area Name:**

Cover Type/Condition	Soil Type	Area (sf)	Area (ac)	CN	S	Ia ((0.2*S)	Q Runoff <sup>1</sup> (in)	Runoff Volume <sup>2</sup> (ft <sup>3</sup> )
<b>Disturbed Area</b>								
Lawn (Good condition)	B			61	6.39	1.28	0.47	0
Paved/Impervious Areas	B			98	0.20	0.04	3.03	0
<b>Undisturbed Area</b>								
Lawn (Good condition)	B			61	6.39	1.28	0.47	0
Paved/Impervious Areas	B			98	0.20	0.04	3.03	0
<b>TOTAL:</b>		<b>0</b>	<b>0.00</b>				<b>6.99</b>	<b>0</b>

1. Runoff (in) =  $Q = (P - 0.2S)^2 / (P + 0.8S)$  where  
 P = 2-Year Rainfall (in)  
 S =  $(1000 / CN) - 10$
2. Runoff Volume (CF) = Q x Area x 1/12  
 Q = Runoff (in)

## Infiltration BMP 1 Calculations

### Infiltration Volume

Inf Rate:	0.41 in/hr
Inf Area:	11,329 sf

Storage Volume = 15,585 cf at elev: 290.50

Infiltration Volume = Inf. Rate x Inf Area X Inf Period  
 = 0.41 in/hr x 11,329 sf x 2 hr x (1ft/12in)  
 = 769 CF

Total Inf. Volume = Storage Volume + Infiltration Volume  
 = 16,354 cf at elev: 290.5

Volume Captured = 19,880 cf

\* Includes runoff from disturbed and undisturbed areas

**Volume Infiltrated = 16,354 cf<sup>1</sup>**  
**Infiltration Credit = 14,980 cf<sup>2</sup>**  
**ET Credit = 646 cf<sup>2</sup>**

Test Pit	Infiltration Rate (in/hr)
TP-14A	0.20
TP-14B	1.00
TP-15A*	<del>0.00</del>
TP-15B*	<del>0.00</del>
TP-16A	2.70
TP-16B*	<del>6.00</del>
Geomean	0.81
Safety Factor	2.00
Adjusted Rate	0.41

\*The highest and lowest recorded rates were removed from the calculation.

### Loading Ratios

Total Drainage Area = 216,893 sf  
 Impervious Area = 53,504 sf  
 Infiltration Area = 11,329 sf  
 Impervious Loading Ratio = 4.7:1  
 Overall Loading Ratio = 19.1:1

### Dewatering Time (After Rainfall Event)

$T = \frac{\text{Infiltration Volume}}{(\text{Inf. Rate}/12 \times \text{Inf. Area})}$   
 = 42.5 hrs

<sup>1</sup> For dewatering calculation analysis

<sup>2</sup> See PADEP PCSM Volume Spreadsheet

**UNT. TO  
EAST BRANCH CHESTER CREEK**

## BMP Volume Calculation Worksheet

**PROJECT:** The Westtown School - Oak Lane Project

**2-Year Rainfall:** 3.26 in

**Drainage Area Name:** Infiltration Bed - BMP 2

Cover Type/Condition	Soil Type	Area (sf)	Area (ac)	CN	S	Ia ((0.2*S)	Q Runoff <sup>1</sup> (in)	Runoff Volume <sup>2</sup> (ft <sup>3</sup> )
<b>Disturbed Area</b>								
Paved/Impervious Areas	B	96824	2.22	98	0.20	0.04	3.03	24,426
Lawn (Good condition)	B			61	6.39	1.28	0.47	0
Lawn (Good condition)	D			80	2.50	0.50	1.45	0
<b>TOTAL ONSITE:</b>		96824	2.22					24,426

**Drainage Area Name:** Infiltration Bed - BMP 3

Cover Type/Condition	Soil Type	Area (sf)	Area (ac)	CN	S	Ia ((0.2*S)	Q Runoff <sup>1</sup> (in)	Runoff Volume <sup>2</sup> (ft <sup>3</sup> )
<b>Disturbed Area</b>								
Paved/Impervious Areas	B	96824	2.22	98	0.20	0.04	3.03	24,426
Lawn (Good condition)	B			61	6.39	1.28	0.47	0
Lawn (Good condition)	D			80	2.50	0.50	1.45	0
<b>TOTAL ONSITE:</b>		96824	2.22					24,426
<b>Volume Infiltrated ( from DEP PCSM Spreadsheet)</b>								24,357
<b>Overflow volume to BMP 4</b>								69

1. Runoff (in) =  $Q = (P-0.2S)^2 / (P+0.8S)$  where  
 P = 2-Year Rainfall (in)  
 S=(1000 / CN) - 10

## BMP Volume Calculation Worksheet

**PROJECT:** The Westtown School - Oak Lane Project  
**2-Year Rainfall:** 3.26 in

**Drainage Area Name:** Infiltration Basin - BMP 4

Cover Type/Condition	Soil Type	Area (sf)	Area (ac)	CN	S	Ia ((0.2*S)	Q Runoff <sup>1</sup> (in)	Runoff Volume <sup>2</sup> (ft <sup>3</sup> )
<b>Disturbed Area</b>								
Paved/Impervious Areas	B	15823	0.36	98	0.20	0.04	3.03	3,992
Lawn (Good condition)	B	261948	6.01	61	6.39	1.28	0.47	10,232
Lawn (Good condition)	D	37761	0.87	80	2.50	0.50	1.45	4,557
<b>TOTAL ONSITE:</b>		<b>315532</b>	<b>7.24</b>					<b>18,781</b>
							Additional Volume from BMP 3	69
							Volume Routed to BMP	18,850
<b>Undisturbed Area</b>								
Paved/Impervious Areas	B			98	0.20	0.04	3.03	0
Lawn (Good condition)	B	84498	1.94	61	6.39	1.28	0.47	3,301
Lawn (Good condition)	D	24400	0.56	80	2.50	0.50	1.45	2,945
<b>TOTAL:</b>		<b>424430</b>	<b>9.74</b>					<b>25,026</b>

**Drainage Area Name:**

Cover Type/Condition	Soil Type	Area (sf)	Area (ac)	CN	S	Ia ((0.2*S)	Q Runoff <sup>1</sup> (in)	Runoff Volume <sup>2</sup> (ft <sup>3</sup> )
<b>Disturbed Area</b>								
Paved/Impervious Areas	B			98	0.20	0.04	3.03	0
Lawn (Good condition)	B	0	0.00	61	6.39	1.28	0.47	0
Lawn (Good condition)	D			80	2.50	0.50	1.45	0
<b>TOTAL ONSITE:</b>		<b>0</b>	<b>0.00</b>					<b>0</b>
<b>Undisturbed Area</b>								
Paved/Impervious Areas	B			98	0.20	0.04	3.03	0
Lawn (Good condition)	B	0	0.00	61	6.39	1.28	0.47	0
Lawn (Good condition)	D			80	2.50	0.50	1.45	0
<b>TOTAL:</b>		<b>0</b>	<b>0.00</b>					<b>0</b>

1. Runoff (in) =  $Q = (P-0.2S)^2 / (P+0.8S)$  where

P = 2-Year Rainfall (in)

S=(1000 / CN) - 10

2. Runoff Volume (CF) = Q x Area x 1/12

Q=Runoff (in)

Area = Land use area (sq. ft)

$$S=(1000 / CN) - 10$$

2. Runoff Volume (CF) = Q x Area x 1/12

$$Q=\text{Runoff (in)}$$

$$\text{Area} = \text{Land use area (sq. ft)}$$



## Infiltration Bed - BMP 2 Calculations

### Subsurface Infiltration Bed Volume

Inf Rate:	2.32 in/hr
Inf Area:	75,725 sf

Storage Volume = 23,035 cf at elev: 316.75

Infiltration Volume = Inf. Rate x Inf Area X Inf Period  
 = 2.32 in/hr x 75,725 sf x 2 hr x (1ft/12in)  
 = 29328 CF

Total Inf. Volume = Storage Volume + Infiltration Volume  
 = 52,363 cf at elev: 316.75

Volume Captured = 24,426 cf

**Volume Infiltrated = 24,426 cf**

Test Pit	Infiltration Rate (in/hr)
TP-1A	1.80
TP-3B	12.00
Geomean	4.65
Safety Factor	2.00
Adjusted Rate	2.32

### Loading Ratios

Total Drainage Area = 96824 sf  
 Impervious Area = 96824 sf  
 Infiltration Area = 75,725 sf  
 Impervious Loading Ratio = 1.3:1  
 Overall Loading Ratio = 1.3:1

### Dewatering Time (After Rainfall Event)

$T = \frac{\text{Infiltration Volume}}{(\text{Inf. Rate}/12 \times \text{Inf. Area})}$   
 = 1.7 hrs

## Synthetic Turf Field Storage Calculations

### BMP 2

WATER SURFACE ELEVATION (FEET)	SUBGRADE AREA (SQ.FT.)	AVERAGE AREA (SQ.FT.)	Δ ELEV. (FEET)	STORAGE VOLUME	x 0.40 (40% Void space)	Σ (CU.FT.)	(AC. FT.)
316	75725					0	0
		75725	0.67	50,736	20294		
316.67	75725					20,294	0.4659
		85638	0.08	6,851	2740		
316.75	95550					23,035	0.5288
		95550	0.75	71,663	28665		
317.5	95550					51,700	1.1869
		0	0.00	0	0		
						0	0.0000
		0	0.00	0	0		
						0	0.0000
		0	0.00	0	0		
						0	0.0000

## Infiltration Bed - BMP 3 Calculations

### Subsurface Infiltration Bed Volume

Inf Rate:	1.01 in/hr
Inf Area:	26,795 sf

$$\text{Storage Volume} = 21,916 \text{ cf at elev: } 321.00$$

$$\begin{aligned} \text{Infiltration Volume} &= \text{Inf. Rate} \times \text{Inf Area} \times \text{Inf Period} \\ &= 1.01 \text{ in/hr} \times 26,795 \text{ sf} \times 2 \text{ hr} \times (1\text{ft}/12\text{in}) \\ &= 4510 \text{ CF} \end{aligned}$$

$$\begin{aligned} \text{Total Inf. Volume} &= \text{Storage Volume} + \text{Infiltration Volume} \\ &= 26,426 \text{ cf at elev: } 321 \end{aligned}$$

$$\text{Volume Captured} = 24,426 \text{ cf}$$

$$\text{Volume Infiltrated} = 24,357 \text{ cf}$$

Test Pit	Infiltration Rate (in/hr)
TP-4A	1.20
TP-5A	3.40
Geomean	2.02
Safety Factor	2.00
Adjusted Rate	1.01

### Loading Ratios

$$\begin{aligned} \text{Total Drainage Area} &= 96824 \text{ sf} \\ \text{Impervious Area} &= 96824 \text{ sf} \\ \text{Infiltration Area} &= 26,795 \text{ sf} \\ \text{Impervious Loading Ratio} &= 3.6:1 \\ \text{Overall Loading Ratio} &= 3.6:1 \end{aligned}$$

### Dewatering Time (After Rainfall Event)

$$\begin{aligned} T &= \frac{\text{Infiltration Volume}}{(\text{Inf. Rate}/12 \times \text{Inf. Area})} \\ &= 10.8 \text{ hrs} \end{aligned}$$

## Synthetic Turf Field Storage Calculations

### BMP 3

WATER SURFACE ELEVATION (FEET)	SUBGRADE AREA (SQ.FT.)	AVERAGE AREA (SQ.FT.)	Δ ELEV. (FEET)	STORAGE VOLUME	x 0.40 (40% Void space)	Σ (CU.FT.)	(AC. FT.)
319	26795					0	0
		27195	1.00	27,195	10878		
320	27595					10,878	0.2497
		27595	1.00	27,595	11038		
321	27595					21,916	0.5031
		56028	0.65	36,418	14567		
321.65	84460					36,483	0.8375
		90005	0.10	9,001	3600		
321.75	95550					40,083	0.9202
		95550	0.75	71,663	28665		
322.5	95550					68,748	1.5782
		0	0.00	0	0		
						0	0.0000

## Infiltration Basin - BMP 4 Calculations

### Infiltration Volume

Inf Rate:	0.84 in/hr
Inf Area:	18,641 sf

Storage Volume = 21,724 cf at elev: 311.00

Infiltration Volume = Inf. Rate x Inf Area X Inf Period  
 = 0.84 in/hr x 18,641 sf x 2 hr x (1ft/12in)  
 = 2599 CF

Total Inf. Volume = Storage Volume + Infiltration Volume  
 = 24,323 cf at elev: 311.00

Volume Captured = 25,026 cf

\*Includes runoff from disturbed and undisturbed area

Overflow volume from BMP 3 = 69

Total Volume Captured<sup>1</sup> = 25,095

**Volume Infiltrated = 18,850 cf<sup>2</sup>**

**ET Credit = 0 cf<sup>2</sup>**

Test Pit	Infiltration Rate (in/hr)
TP-6A	1.00
TP-7B	2.80
Geomean	1.67
Safety Factor	2.00
Adjusted Rate	0.84

### Loading Ratios

Total Drainage Area = 424430 sf  
 Impervious Area = 15823 sf  
 Infiltration Area = 18,641 sf  
 Impervious Loading Ratio = 0.8:1  
 Overall Loading Ratio = 22.8:1

### Dewatering Time (After Rainfall Event)

T =  $\frac{\text{Storage Volume}}{\text{Inf. Rate}/12 \times \text{Inf. Area}}$   
 = **16.7 hrs**

<sup>1</sup> For dewatering calculation analysis

<sup>2</sup> See PADEP PCSM Volume Spreadsheet

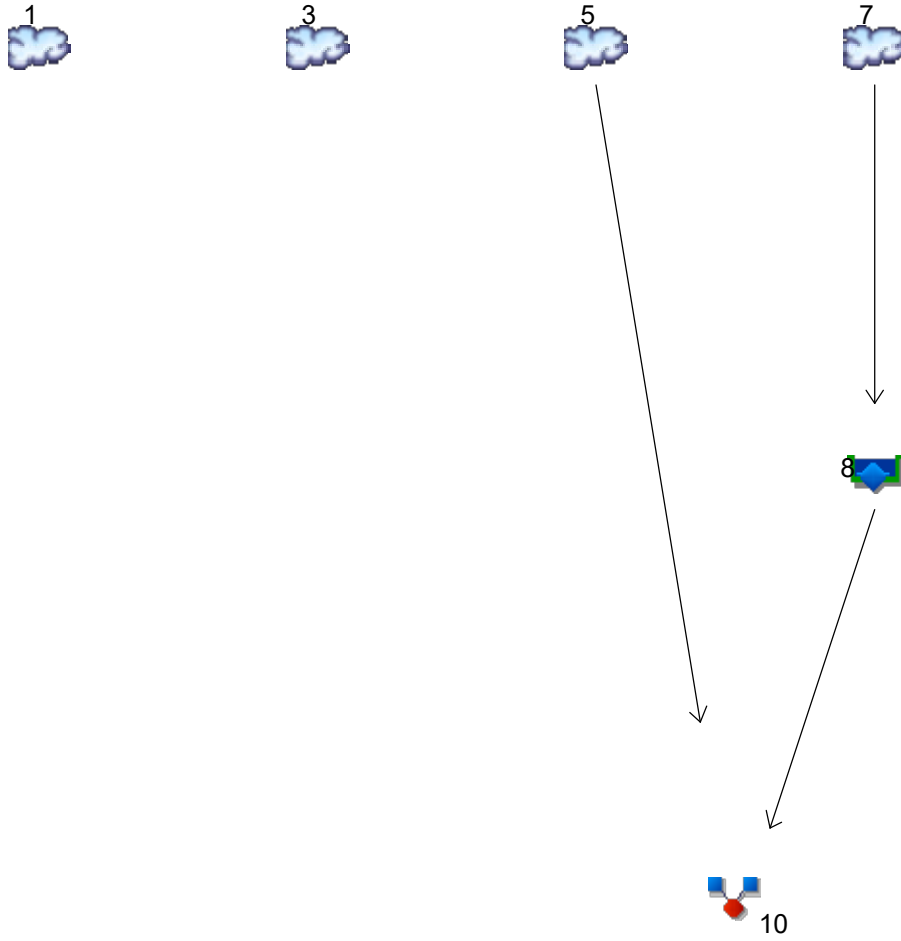
## **APPENDIX E**

### **RATE CONTROL ANALYSIS**

## OVERALL HYDROLOGY

# Watershed Model Schematic

Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2022





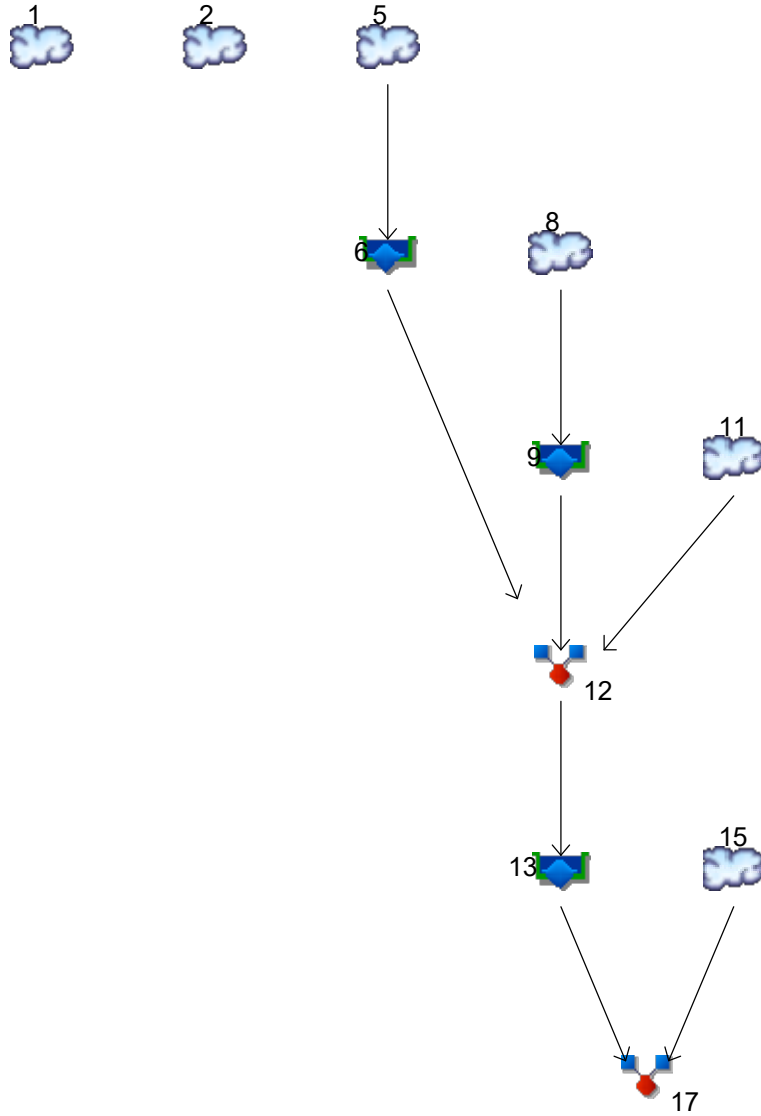
# Hydrograph Return Period Recap

Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2022

Hyd. No.	Hydrograph type (origin)	Inflow hyd(s)	Peak Outflow (cfs)								Hydrograph Description
			1-yr	2-yr	3-yr	5-yr	10-yr	25-yr	50-yr	100-yr	
1	SCS Runoff	-----	2.123	4.257	-----	8.156	11.81	17.58	22.86	28.81	Pre-Dev. Area A
3	SCS Runoff	-----	1.573	3.153	-----	6.041	8.748	13.02	16.93	21.34	Area 'A-ONSITE'
5	SCS Runoff	-----	0.683	1.225	-----	2.179	3.059	4.420	5.626	6.983	A-Undetained
7	SCS Runoff	-----	3.512	5.820	-----	9.799	13.41	19.00	23.98	29.52	BMP 1 (Basin A)
8	Reservoir	7	0.000	0.134	-----	0.542	1.405	3.929	6.906	12.69	Basin A Routed
10	Combine	5, 8,	0.683	1.225	-----	2.179	3.059	4.506	7.657	13.69	A-COMBINED

# Watershed Model Schematic

Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2022



# Hydrograph Return Period Recap

Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2022

Hyd. No.	Hydrograph type (origin)	Inflow hyd(s)	Peak Outflow (cfs)								Hydrograph Description
			1-yr	2-yr	3-yr	5-yr	10-yr	25-yr	50-yr	100-yr	
1	SCS Runoff	-----	3.209	7.080	-----	14.94	22.59	34.79	45.85	58.42	Pre-Dev. POI B
2	SCS Runoff	-----	2.726	6.014	-----	12.69	19.19	29.55	38.95	49.62	B-Onsite (Reduction)
5	SCS Runoff	-----	8.084	9.771	-----	12.34	14.48	17.55	20.14	22.94	BMP 3 IN
6	Reservoir	5	0.000	0.006	-----	0.076	0.116	0.165	0.219	0.435	BMP 3 Routed
8	SCS Runoff	-----	8.084	9.771	-----	12.34	14.48	17.55	20.14	22.94	BMP 2 IN
9	Reservoir	8	0.000	0.000	-----	0.148	0.319	0.762	1.333	2.110	BMP 2 Routed
11	SCS Runoff	-----	2.582	5.169	-----	10.17	14.91	22.37	29.07	36.71	BMP 4 DA
12	Combine	6, 9, 11	2.582	5.169	-----	10.17	14.91	22.92	30.34	38.87	BMP 4 IN
13	Reservoir	12	0.000	0.155	-----	0.772	2.194	8.434	15.66	24.29	BMP 4 Routed
15	SCS Runoff	-----	1.222	2.328	-----	4.298	6.130	8.988	11.55	14.48	B-Undetained
17	Combine	13, 15,	1.222	2.328	-----	4.298	6.130	9.782	17.54	26.76	B-Combined

## **PRE-DEVELOPMENT HYDROLOGY (EAST BRANCH CHESTER CREEK)**

**ELA SPORT**  
**ATHLETIC FACILITIES**  
**DESIGN & CONSULTING**

737 S. BROAD STREET  
 LITITZ, PA 17543  
 (717) 626-72713

**NRCS (SCS) TR-55- WATERSHED WEIGHTED**  
**CURVE NUMBER**  
**PRE-DEVELOPMENT SUMMARY**

PROJECT: The Westtown School - Oak Lane Project  
 LOCATION: Westtown Township  
 COUNTY: Chester



LAND USE	Area (ac)				Total Area (ac.)	Composite 'CN' Value	Tc Min.
	Row Crops (C+CR)	Open Space	Open Space	Woods/Forest			
HSG	B	D	B	D	77	65	15
"CN" Value	98	74	61	80			
WATERSHED							
POI 'A'	0.42	0.77	0.00	0.00	6.44	65	15
POI 'A-Onsite' (Reduction Factor)	0.23	0.77	0.00	0.00	4.77	65	15



**ELA SPORT**  
**ATHLETIC FACILITIES**  
**DESIGN & CONSULTING**

737 S. BROAD STREET  
 LITITZ, PA 17543  
 (717) 626-72713

**SUMMARY - SUBAREAS TIME OF CONCENTRATION PRE-DEVELOPMENT CONDITIONS**

PROJECT: The Westtown School - Oak Lane Project  
 LOCATION: Westtown Township  
 COUNTY: Chester

Time of concentration (Tc) or travel time (Tt)																						
overland					Shallow Concentrated					Channel or Pipe										Total		
Watershed	Length L <sub>1</sub> ft.	Slope S <sub>1</sub> ft./ft.	Manning's n	2 yr rainfall in.	Tc Min.	Flow Path U/P	Length L <sub>2</sub> ft.	Slope S <sub>2</sub> ft./ft.	Average Velocity ft./s	Min.	Tt	Channel or Pipe C/P	Flow Area sq.ft.	Wetted Perimeter ft.	Pipe Diameter in.	Slope S <sub>3</sub> ft./ft.	Manning's n	Length L <sub>3</sub> ft.	Tt Min.	Min.	Hrs.	
A	89	0.017	0.24	3.26	14	U	234	0.090	4.8	0.8	0.0	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0	0	0	0.00
					0				0	0	0	0.00	0.00	0.00	0	0	0	0	0	0	0	0.00
					0				0	0	0	0.00	0.00	0.00	0	0	0	0	0	0	0	0.00
					0				0	0	0	0.00	0.00	0.00	0	0	0	0	0	0	0	0.00
					13.7					0.8									0.0	0.0	15	0.25

# Hydrograph Report

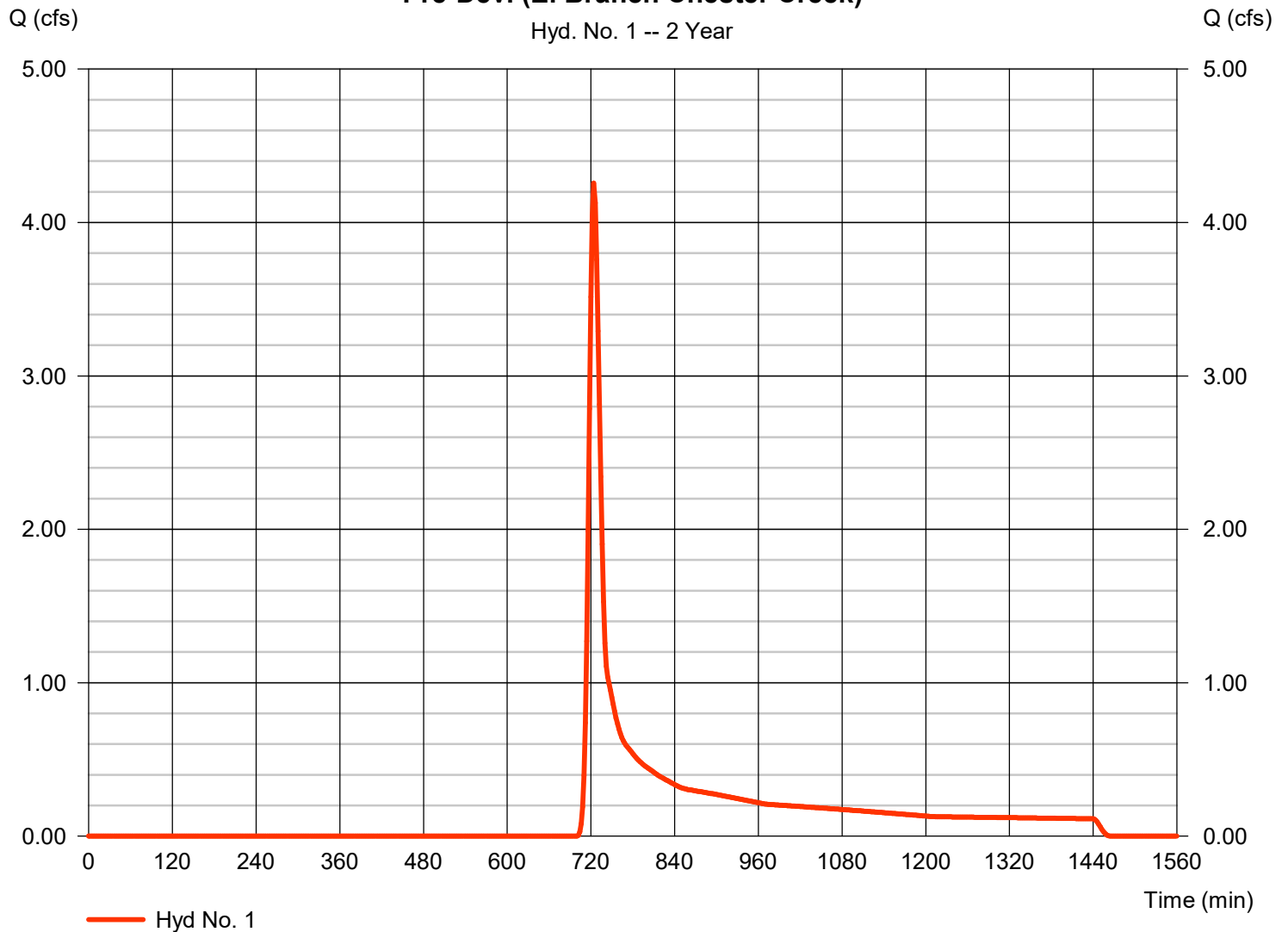
## Hyd. No. 1

Pre-Dev. (E. Branch Chester Creek)

Hydrograph type	= SCS Runoff	Peak discharge	= 4.257 cfs
Storm frequency	= 2 yrs	Time to peak	= 724 min
Time interval	= 2 min	Hyd. volume	= 14,353 cuft
Drainage area	= 6.440 ac	Curve number	= 65
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 15.00 min
Total precip.	= 3.26 in	Distribution	= Type II
Storm duration	= 24 hrs	Shape factor	= 484

### Pre-Dev. (E. Branch Chester Creek)

Hyd. No. 1 -- 2 Year



# Hydrograph Report

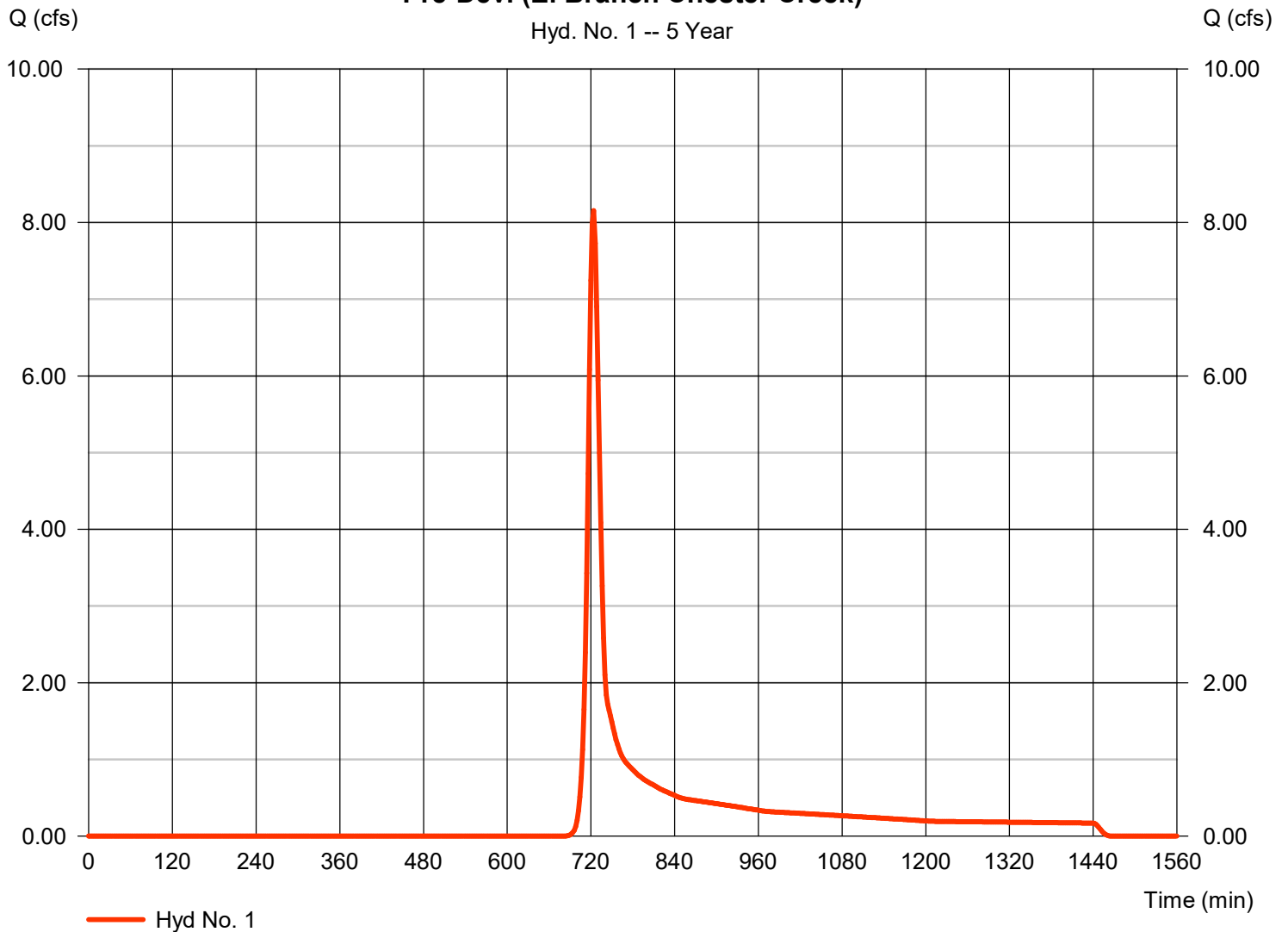
## Hyd. No. 1

Pre-Dev. (E. Branch Chester Creek)

Hydrograph type	= SCS Runoff	Peak discharge	= 8.156 cfs
Storm frequency	= 5 yrs	Time to peak	= 724 min
Time interval	= 2 min	Hyd. volume	= 24,775 cuft
Drainage area	= 6.440 ac	Curve number	= 65
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 15.00 min
Total precip.	= 4.10 in	Distribution	= Type II
Storm duration	= 24 hrs	Shape factor	= 484

### Pre-Dev. (E. Branch Chester Creek)

Hyd. No. 1 -- 5 Year





# Hydrograph Report

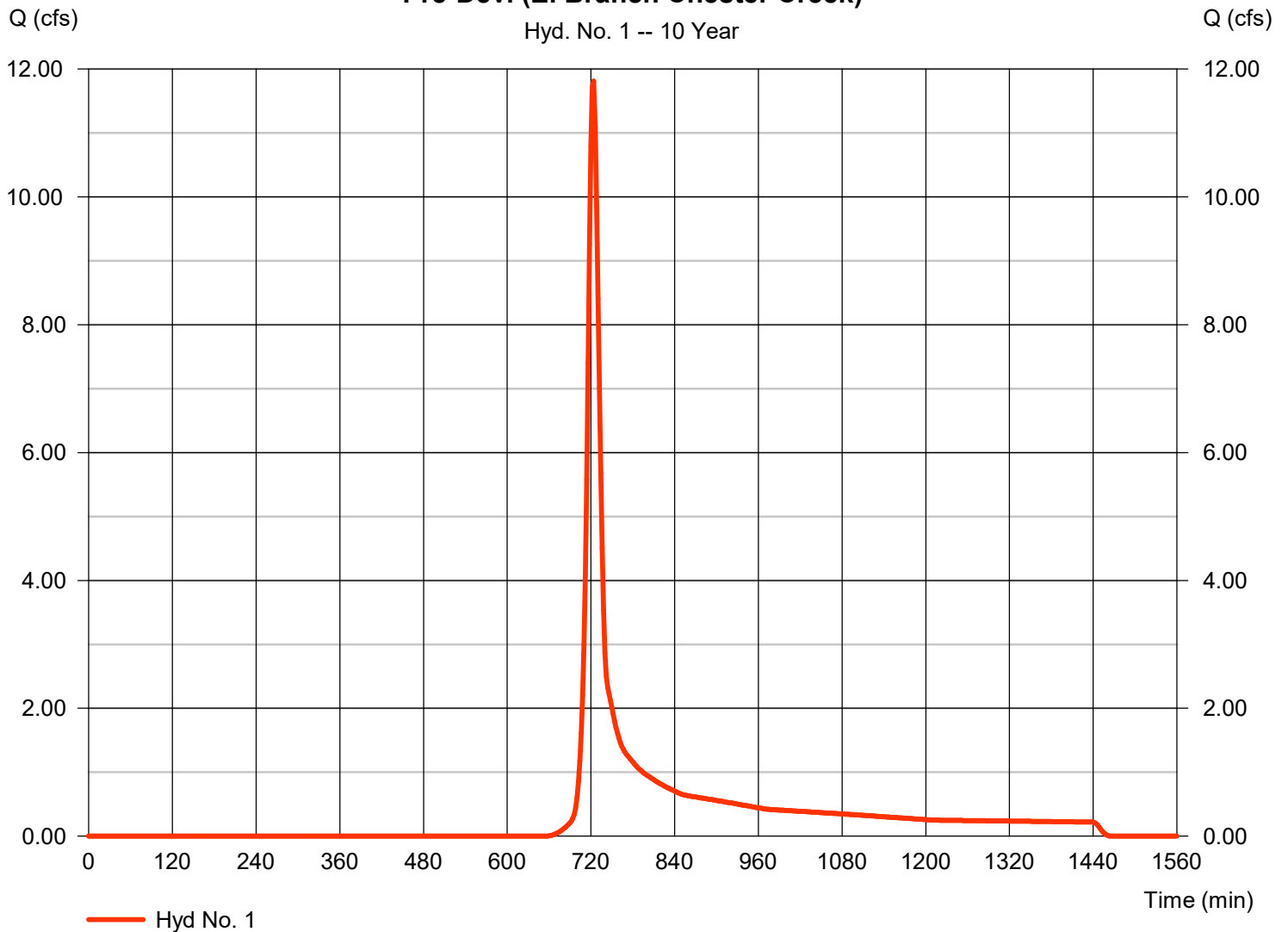
## Hyd. No. 1

Pre-Dev. (E. Branch Chester Creek)

Hydrograph type	= SCS Runoff	Peak discharge	= 11.81 cfs
Storm frequency	= 10 yrs	Time to peak	= 724 min
Time interval	= 2 min	Hyd. volume	= 34,689 cuft
Drainage area	= 6.440 ac	Curve number	= 65
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 15.00 min
Total precip.	= 4.80 in	Distribution	= Type II
Storm duration	= 24 hrs	Shape factor	= 484

### Pre-Dev. (E. Branch Chester Creek)

Hyd. No. 1 -- 10 Year



# Hydrograph Report

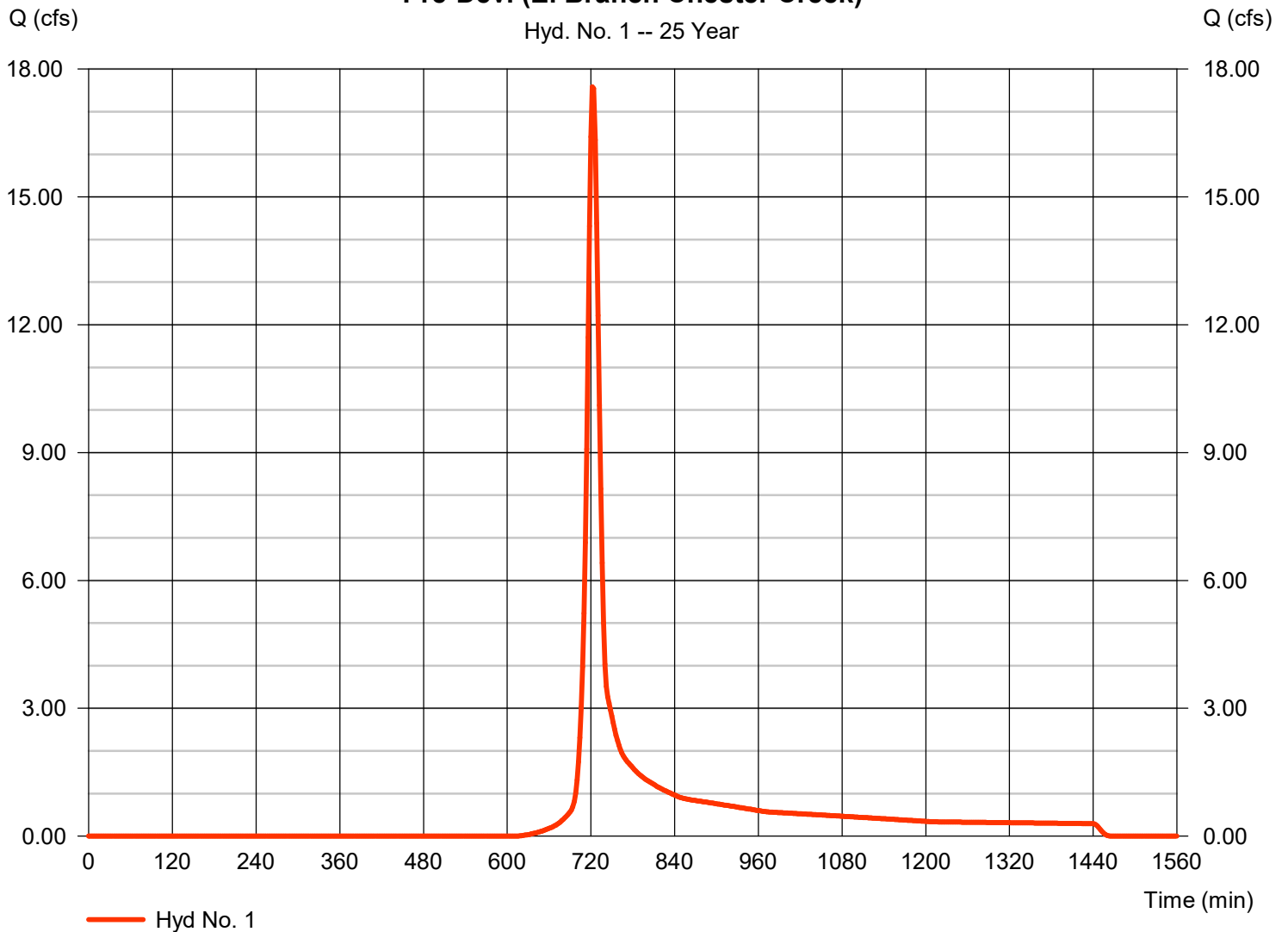
## Hyd. No. 1

Pre-Dev. (E. Branch Chester Creek)

Hydrograph type	= SCS Runoff	Peak discharge	= 17.58 cfs
Storm frequency	= 25 yrs	Time to peak	= 722 min
Time interval	= 2 min	Hyd. volume	= 50,466 cuft
Drainage area	= 6.440 ac	Curve number	= 65
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 15.00 min
Total precip.	= 5.81 in	Distribution	= Type II
Storm duration	= 24 hrs	Shape factor	= 484

### Pre-Dev. (E. Branch Chester Creek)

Hyd. No. 1 -- 25 Year

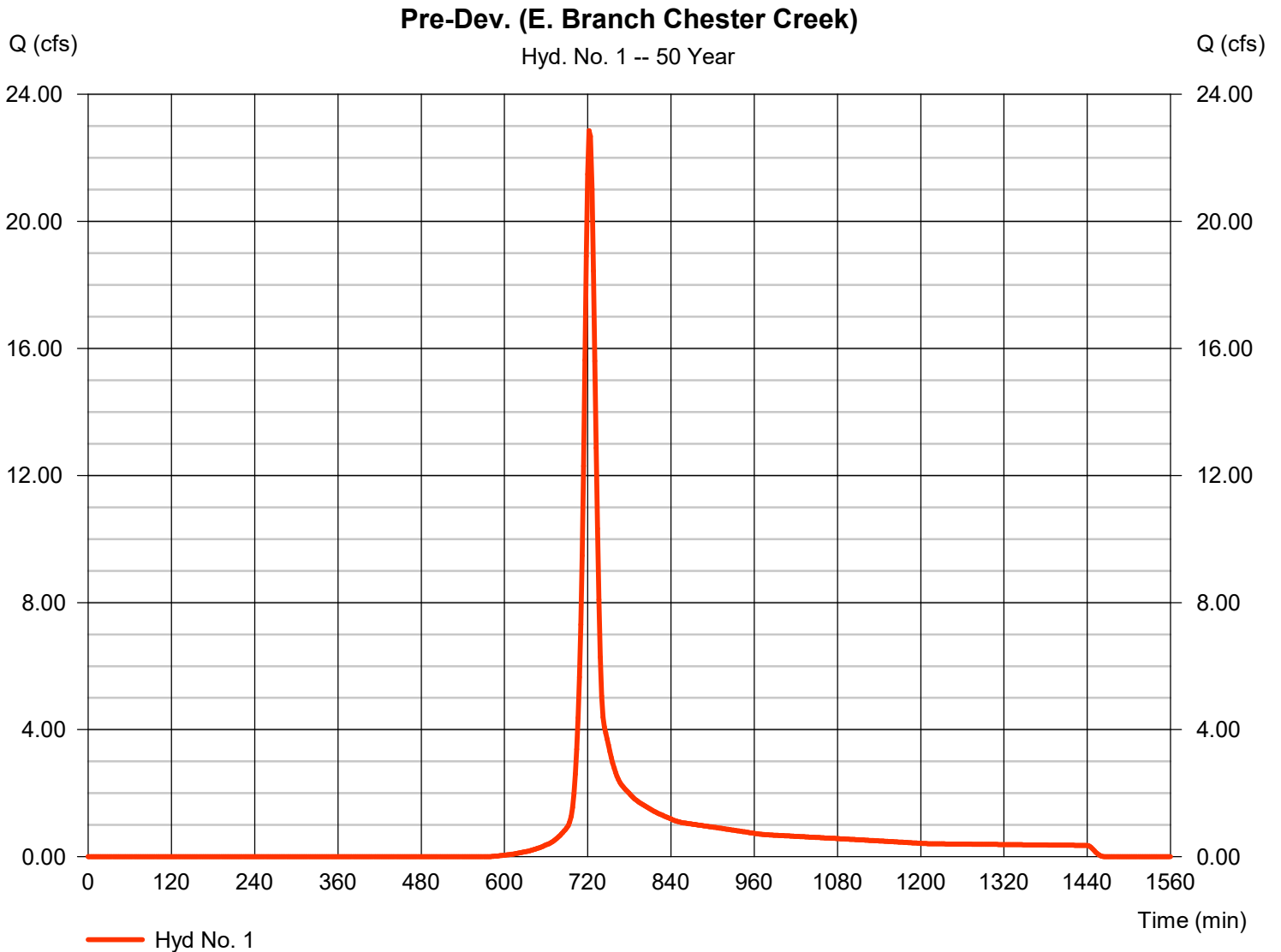


# Hydrograph Report

## Hyd. No. 1

Pre-Dev. (E. Branch Chester Creek)

Hydrograph type	= SCS Runoff	Peak discharge	= 22.86 cfs
Storm frequency	= 50 yrs	Time to peak	= 722 min
Time interval	= 2 min	Hyd. volume	= 64,778 cuft
Drainage area	= 6.440 ac	Curve number	= 65
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 15.00 min
Total precip.	= 6.66 in	Distribution	= Type II
Storm duration	= 24 hrs	Shape factor	= 484

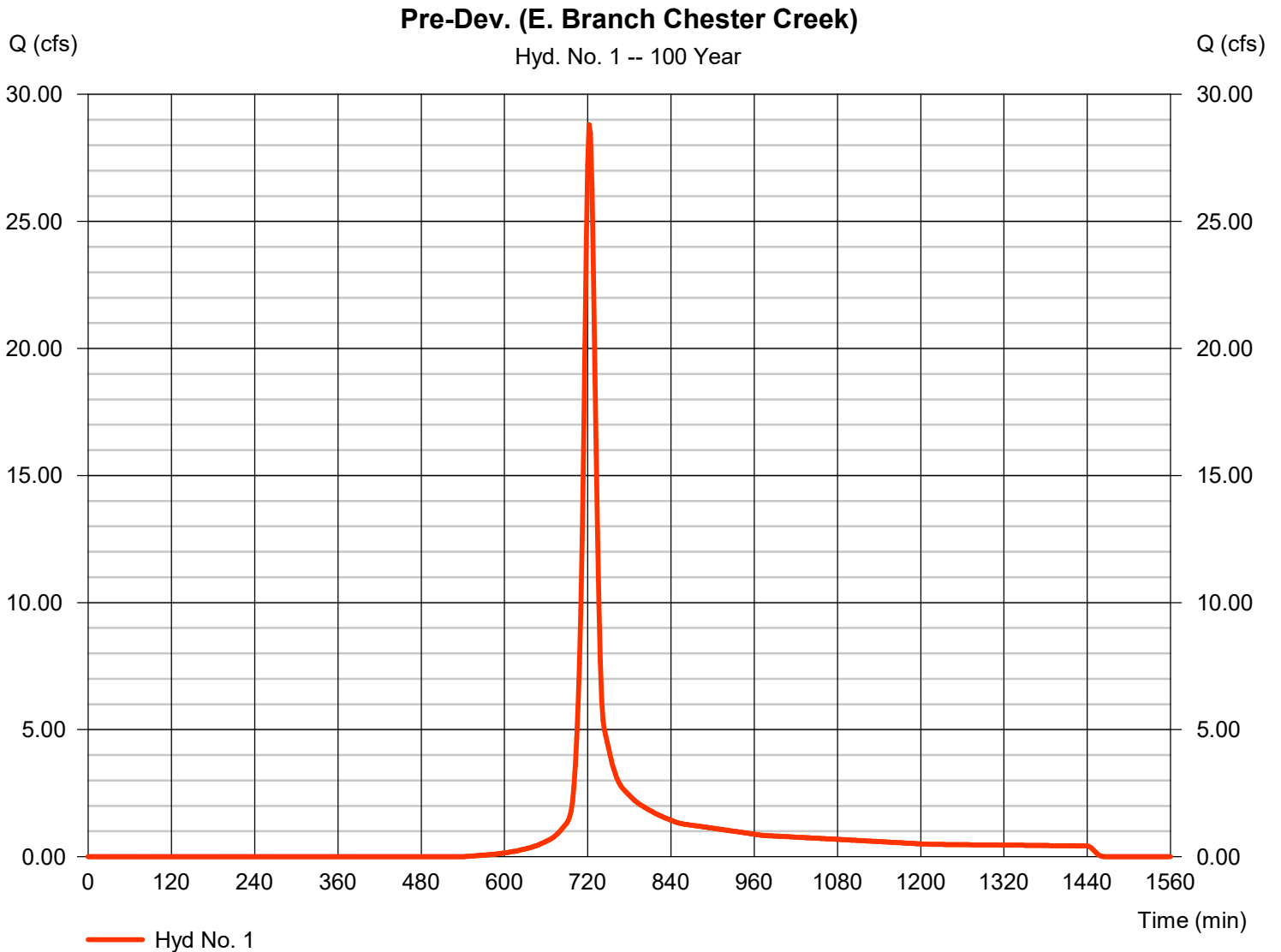


# Hydrograph Report

## Hyd. No. 1

Pre-Dev. (E. Branch Chester Creek)

Hydrograph type	= SCS Runoff	Peak discharge	= 28.81 cfs
Storm frequency	= 100 yrs	Time to peak	= 722 min
Time interval	= 2 min	Hyd. volume	= 81,084 cuft
Drainage area	= 6.440 ac	Curve number	= 65
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 15.00 min
Total precip.	= 7.58 in	Distribution	= Type II
Storm duration	= 24 hrs	Shape factor	= 484

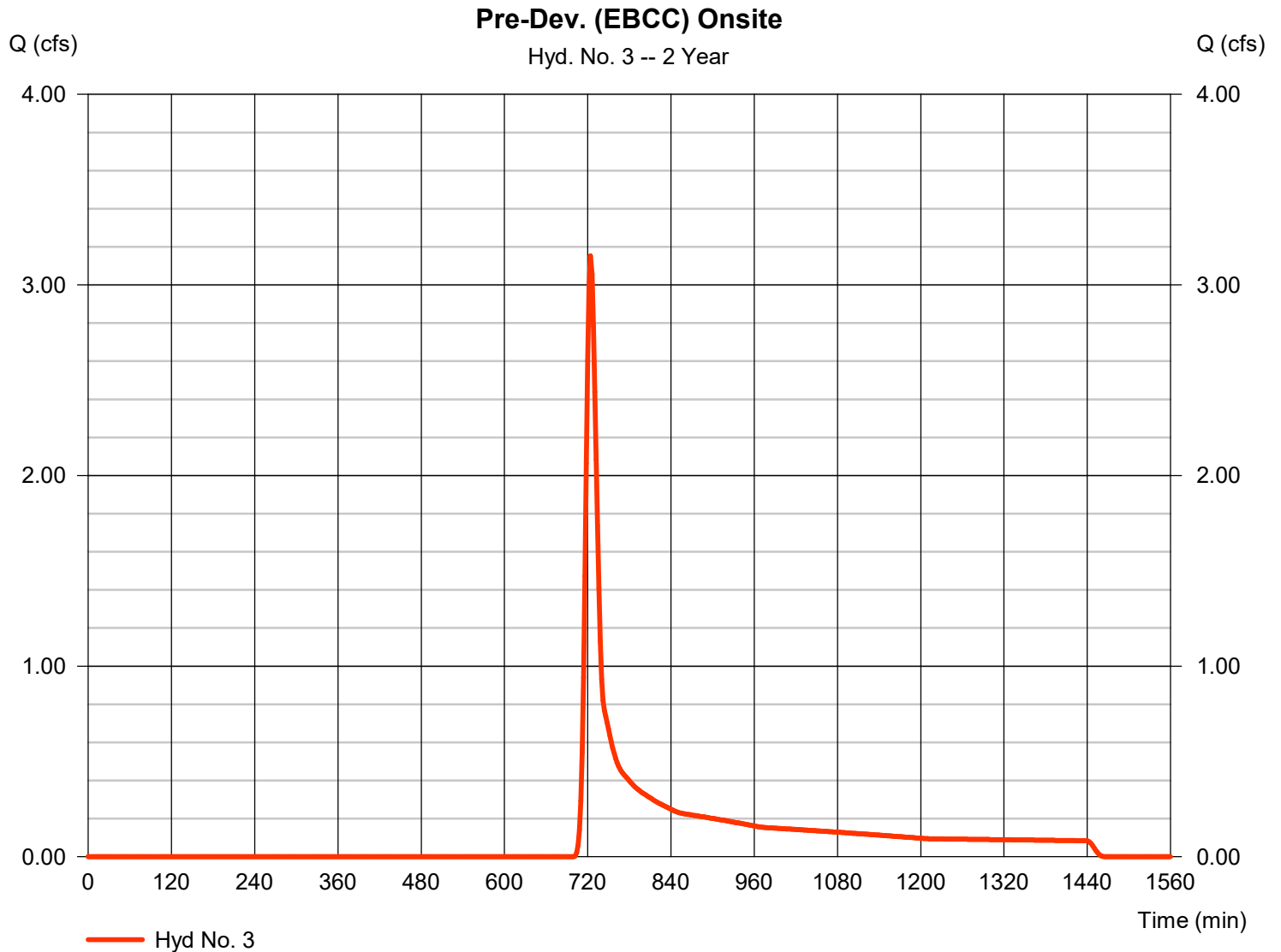


# Hydrograph Report

## Hyd. No. 3

Pre-Dev. (EBCC) Onsite

Hydrograph type	= SCS Runoff	Peak discharge	= 3.153 cfs
Storm frequency	= 2 yrs	Time to peak	= 724 min
Time interval	= 2 min	Hyd. volume	= 10,631 cuft
Drainage area	= 4.770 ac	Curve number	= 65
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 15.00 min
Total precip.	= 3.26 in	Distribution	= Type II
Storm duration	= 24 hrs	Shape factor	= 484

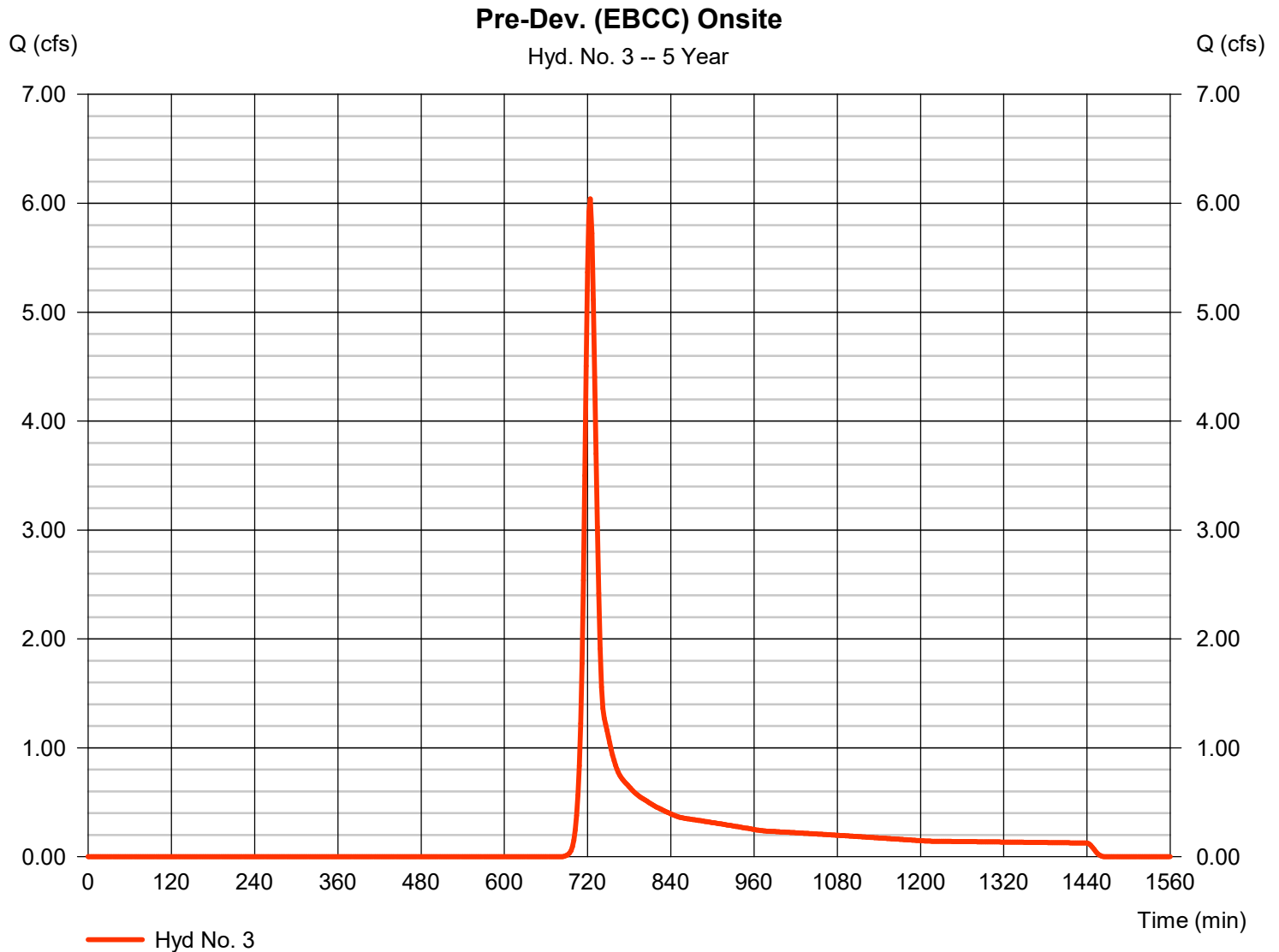


# Hydrograph Report

## Hyd. No. 3

Pre-Dev. (EBCC) Onsite

Hydrograph type	= SCS Runoff	Peak discharge	= 6.041 cfs
Storm frequency	= 5 yrs	Time to peak	= 724 min
Time interval	= 2 min	Hyd. volume	= 18,350 cuft
Drainage area	= 4.770 ac	Curve number	= 65
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 15.00 min
Total precip.	= 4.10 in	Distribution	= Type II
Storm duration	= 24 hrs	Shape factor	= 484

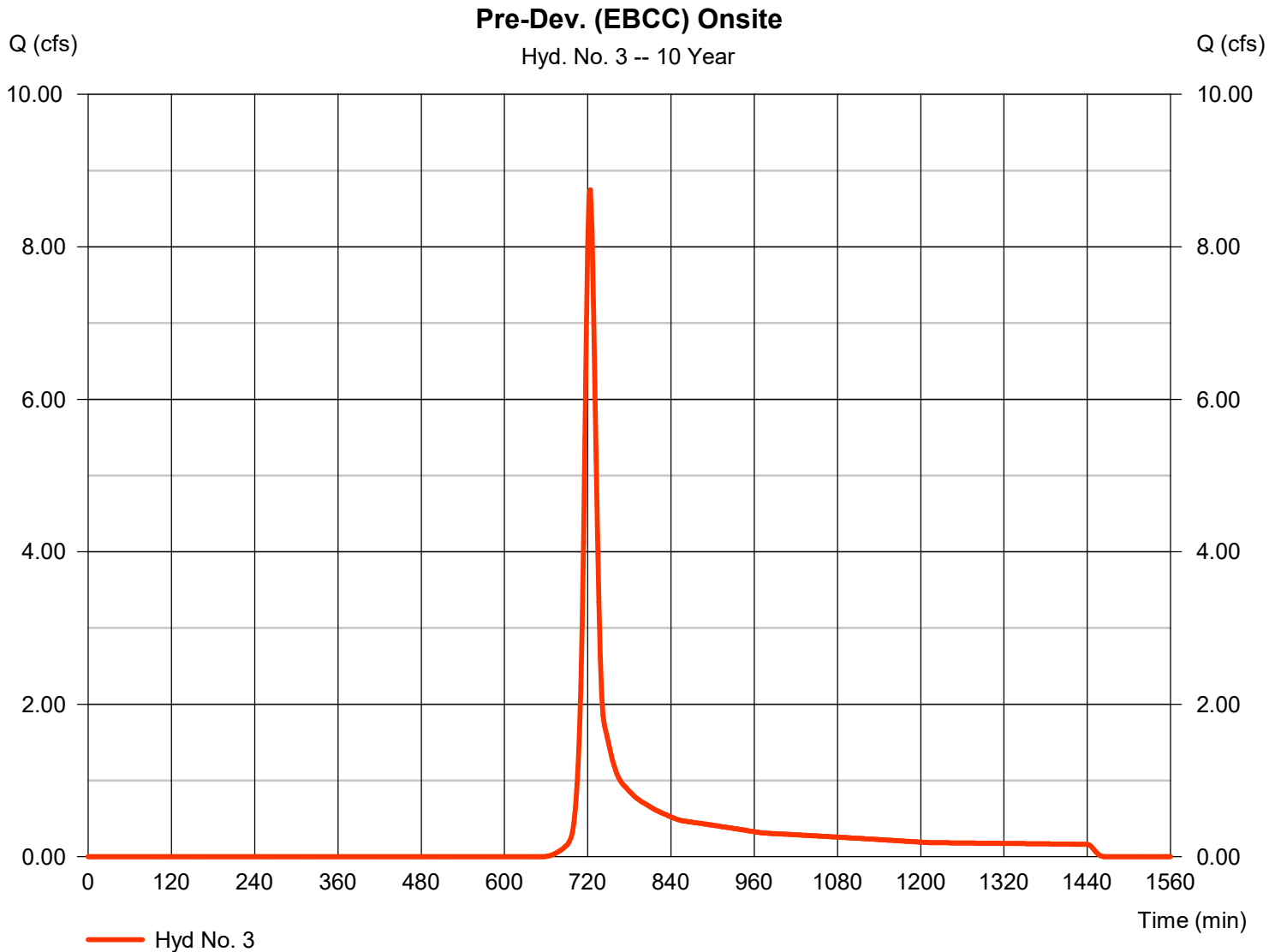


# Hydrograph Report

## Hyd. No. 3

Pre-Dev. (EBCC) Onsite

Hydrograph type	= SCS Runoff	Peak discharge	= 8.748 cfs
Storm frequency	= 10 yrs	Time to peak	= 724 min
Time interval	= 2 min	Hyd. volume	= 25,694 cuft
Drainage area	= 4.770 ac	Curve number	= 65
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 15.00 min
Total precip.	= 4.80 in	Distribution	= Type II
Storm duration	= 24 hrs	Shape factor	= 484

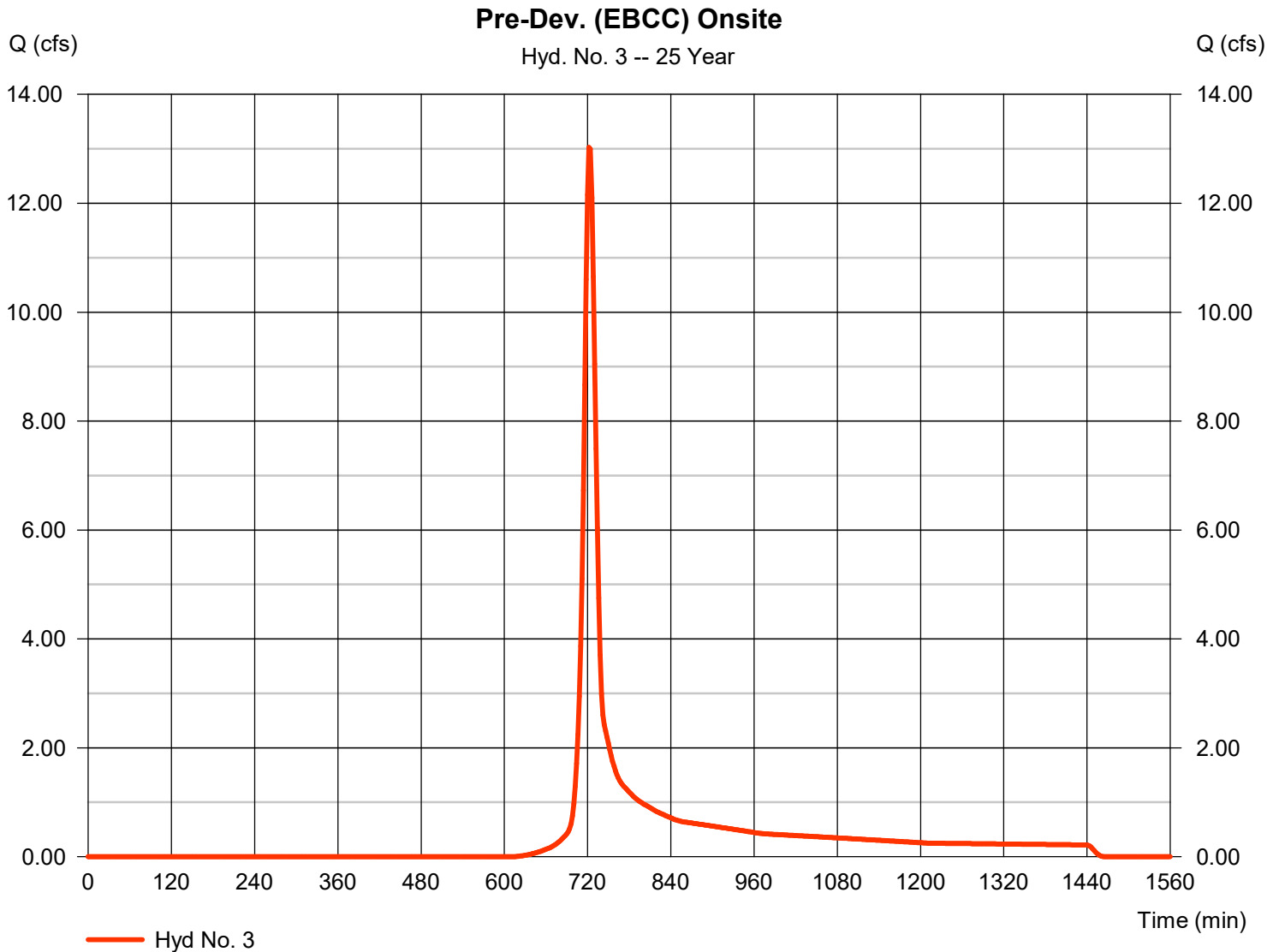


# Hydrograph Report

## Hyd. No. 3

Pre-Dev. (EBCC) Onsite

Hydrograph type	= SCS Runoff	Peak discharge	= 13.02 cfs
Storm frequency	= 25 yrs	Time to peak	= 722 min
Time interval	= 2 min	Hyd. volume	= 37,380 cuft
Drainage area	= 4.770 ac	Curve number	= 65
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 15.00 min
Total precip.	= 5.81 in	Distribution	= Type II
Storm duration	= 24 hrs	Shape factor	= 484



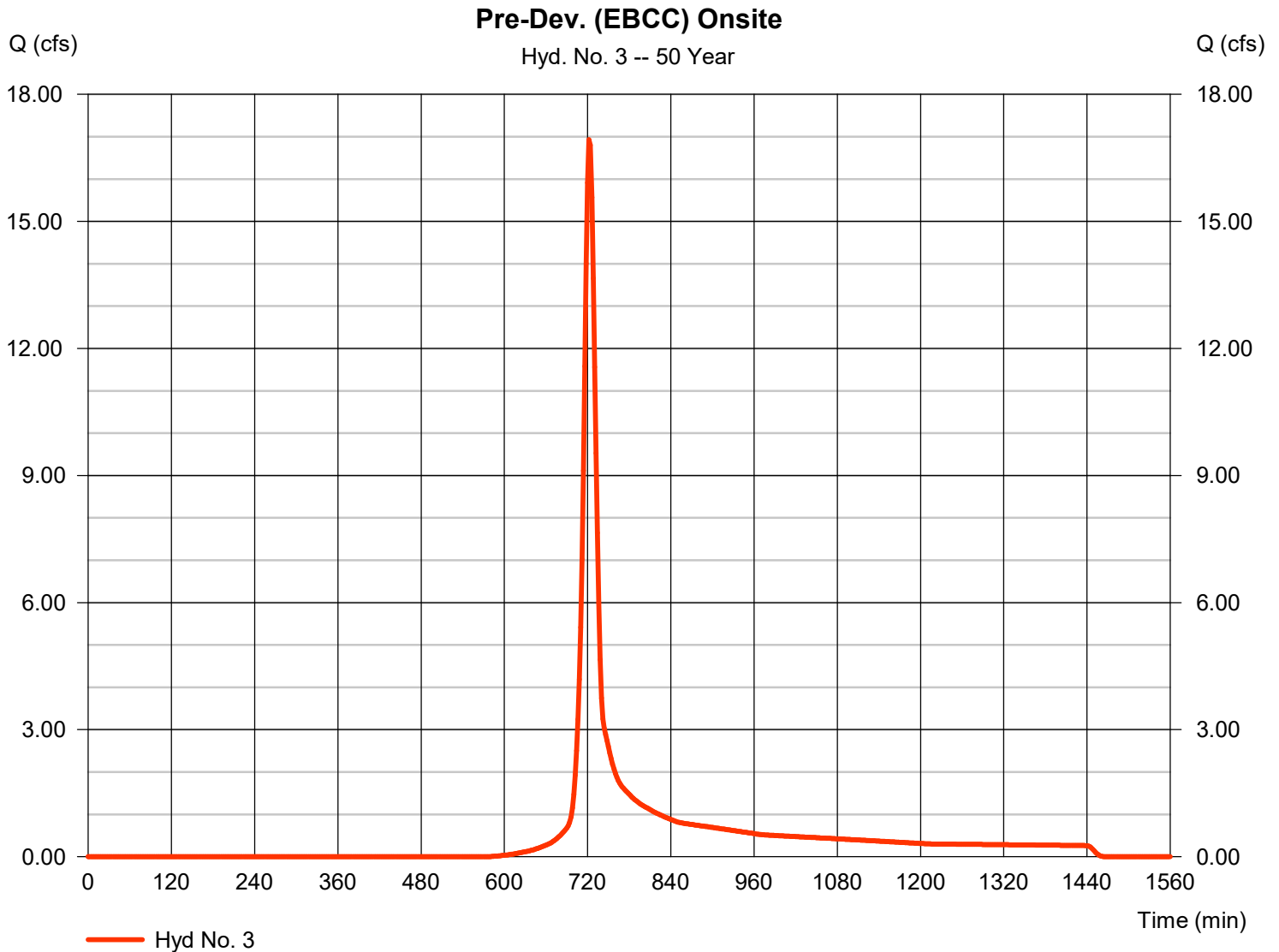


# Hydrograph Report

## Hyd. No. 3

Pre-Dev. (EBCC) Onsite

Hydrograph type	= SCS Runoff	Peak discharge	= 16.93 cfs
Storm frequency	= 50 yrs	Time to peak	= 722 min
Time interval	= 2 min	Hyd. volume	= 47,980 cuft
Drainage area	= 4.770 ac	Curve number	= 65
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 15.00 min
Total precip.	= 6.66 in	Distribution	= Type II
Storm duration	= 24 hrs	Shape factor	= 484

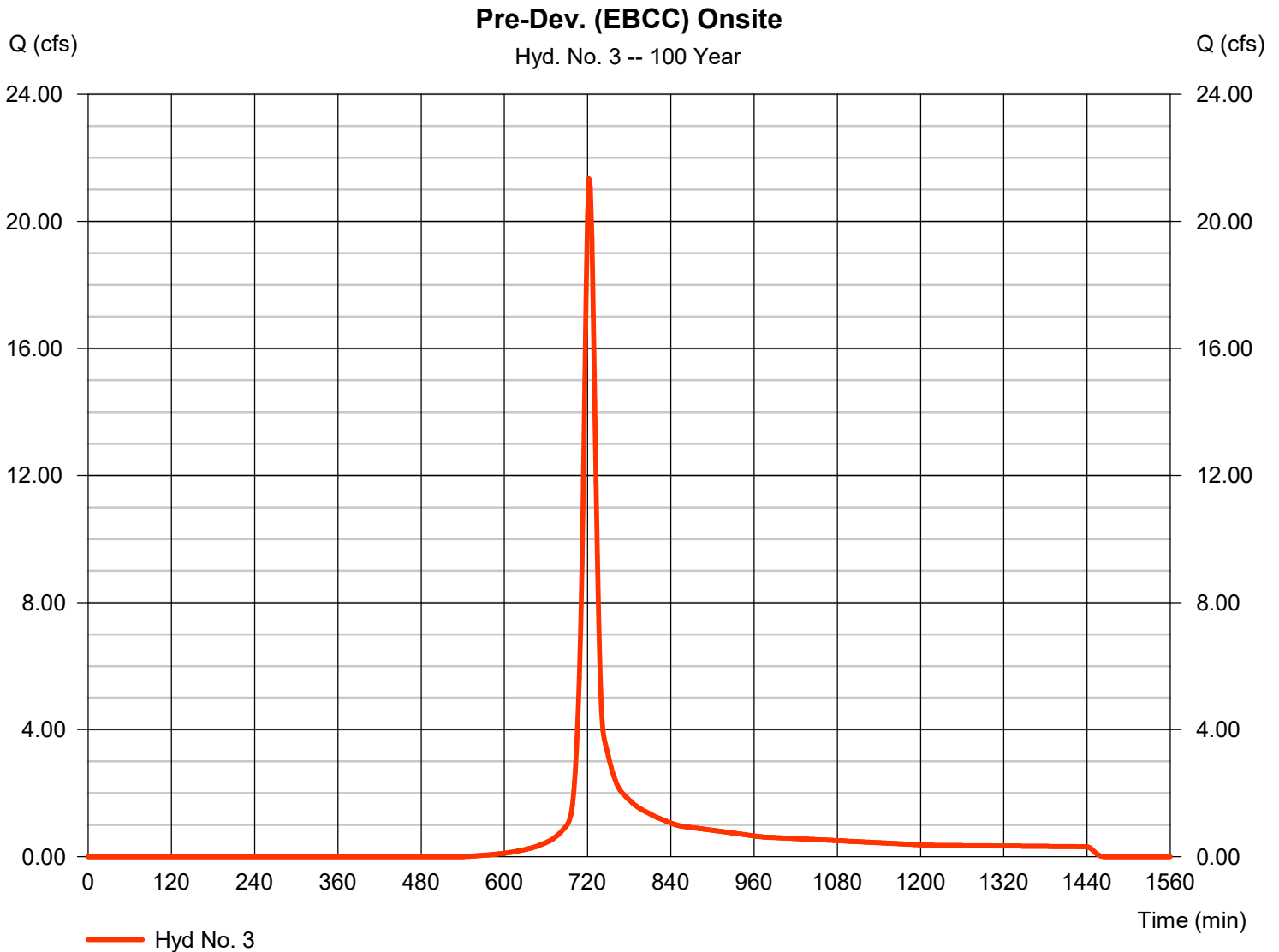


# Hydrograph Report

## Hyd. No. 3

Pre-Dev. (EBCC) Onsite

Hydrograph type	= SCS Runoff	Peak discharge	= 21.34 cfs
Storm frequency	= 100 yrs	Time to peak	= 722 min
Time interval	= 2 min	Hyd. volume	= 60,058 cuft
Drainage area	= 4.770 ac	Curve number	= 65
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 15.00 min
Total precip.	= 7.58 in	Distribution	= Type II
Storm duration	= 24 hrs	Shape factor	= 484



## **UNT. TO EAST BRANCH CHESTER CREEK**



**ELA SPORT**  
 ATHLETIC FACILITIES DESIGN  
 & CONSULTING

737 S. BROAD STREET  
 LITITZ, PA 17543  
 (717) 626-72713

**NRCS (SCS) TR-55- WATERSHED WEIGHTED  
 CURVE NUMBER  
 PRE-DEVELOPMENT SUMMARY**

PROJECT: The Westtown School - Oak Lane Project  
 LOCATION: Westtown Township  
 COUNTY: Chester

LAND USE	HSG	Area (ac)				Total Area (ac.)	Composite 'CN' Value	Tc Min.	
		Parking, Other Impervious	Row Crops (C+CR)	Open Space	Woods/Forest				
"CN" Value	B	98	74	61	80	77			
	D		85						
WATERSHED									
Unt. to East Branch Chester Creek		0.01	0.00	14.50	2.09	0.00	16.60	63	22
Unt. to EBCC Onsite (Reduction Factor)		0.01	0.00	12.57	1.53	0.00	14.10	63	22

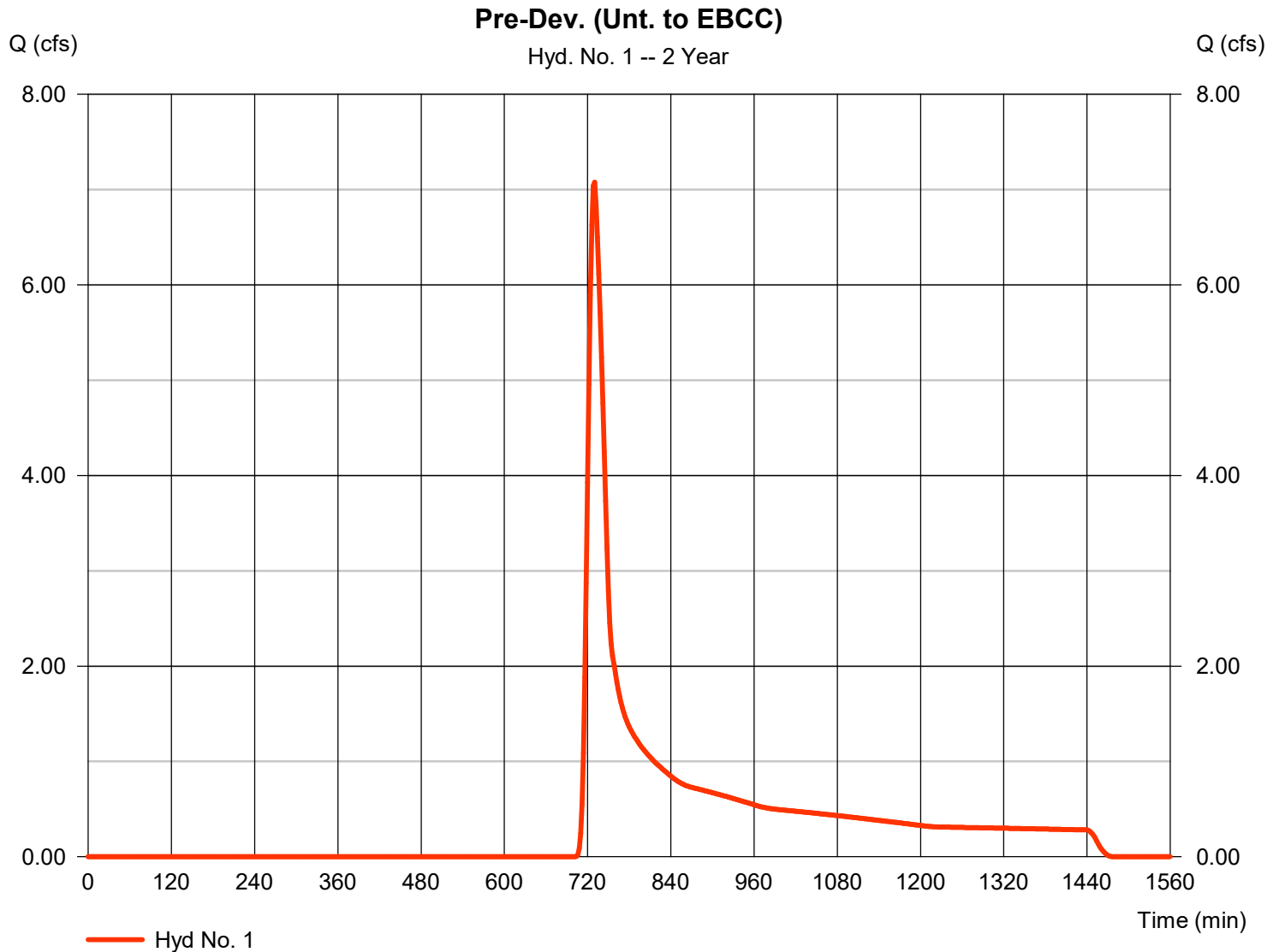


# Hydrograph Report

## Hyd. No. 1

Pre-Dev. (Unt. to EBCC)

Hydrograph type	= SCS Runoff	Peak discharge	= 7.080 cfs
Storm frequency	= 2 yrs	Time to peak	= 730 min
Time interval	= 2 min	Hyd. volume	= 33,512 cuft
Drainage area	= 16.600 ac	Curve number	= 63
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 22.00 min
Total precip.	= 3.26 in	Distribution	= Type II
Storm duration	= 24 hrs	Shape factor	= 484

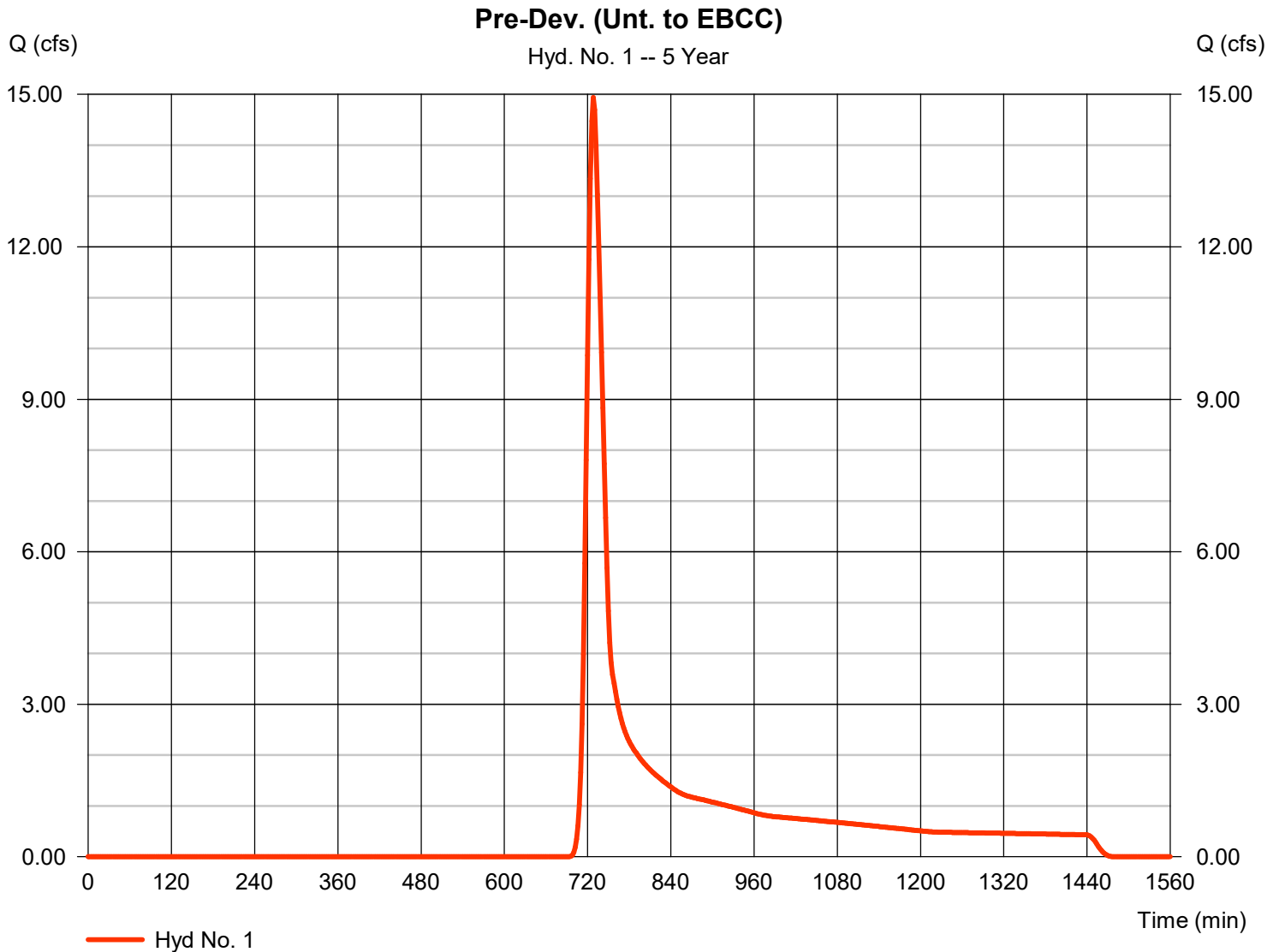


# Hydrograph Report

## Hyd. No. 1

Pre-Dev. (Unt. to EBCC)

Hydrograph type	= SCS Runoff	Peak discharge	= 14.94 cfs
Storm frequency	= 5 yrs	Time to peak	= 728 min
Time interval	= 2 min	Hyd. volume	= 59,657 cuft
Drainage area	= 16.600 ac	Curve number	= 63
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 22.00 min
Total precip.	= 4.10 in	Distribution	= Type II
Storm duration	= 24 hrs	Shape factor	= 484

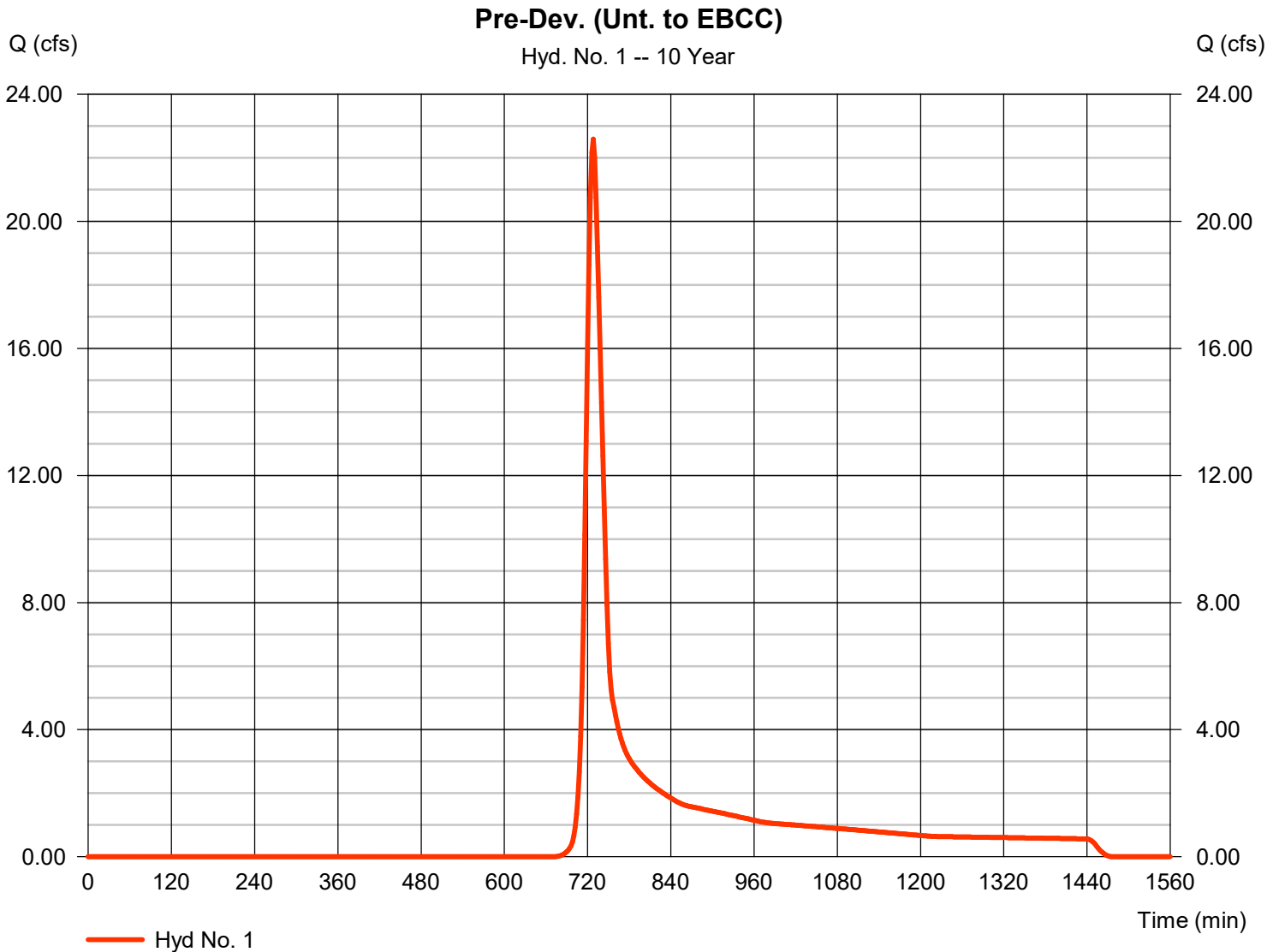


# Hydrograph Report

## Hyd. No. 1

Pre-Dev. (Unt. to EBCC)

Hydrograph type	= SCS Runoff	Peak discharge	= 22.59 cfs
Storm frequency	= 10 yrs	Time to peak	= 728 min
Time interval	= 2 min	Hyd. volume	= 84,871 cuft
Drainage area	= 16.600 ac	Curve number	= 63
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 22.00 min
Total precip.	= 4.80 in	Distribution	= Type II
Storm duration	= 24 hrs	Shape factor	= 484



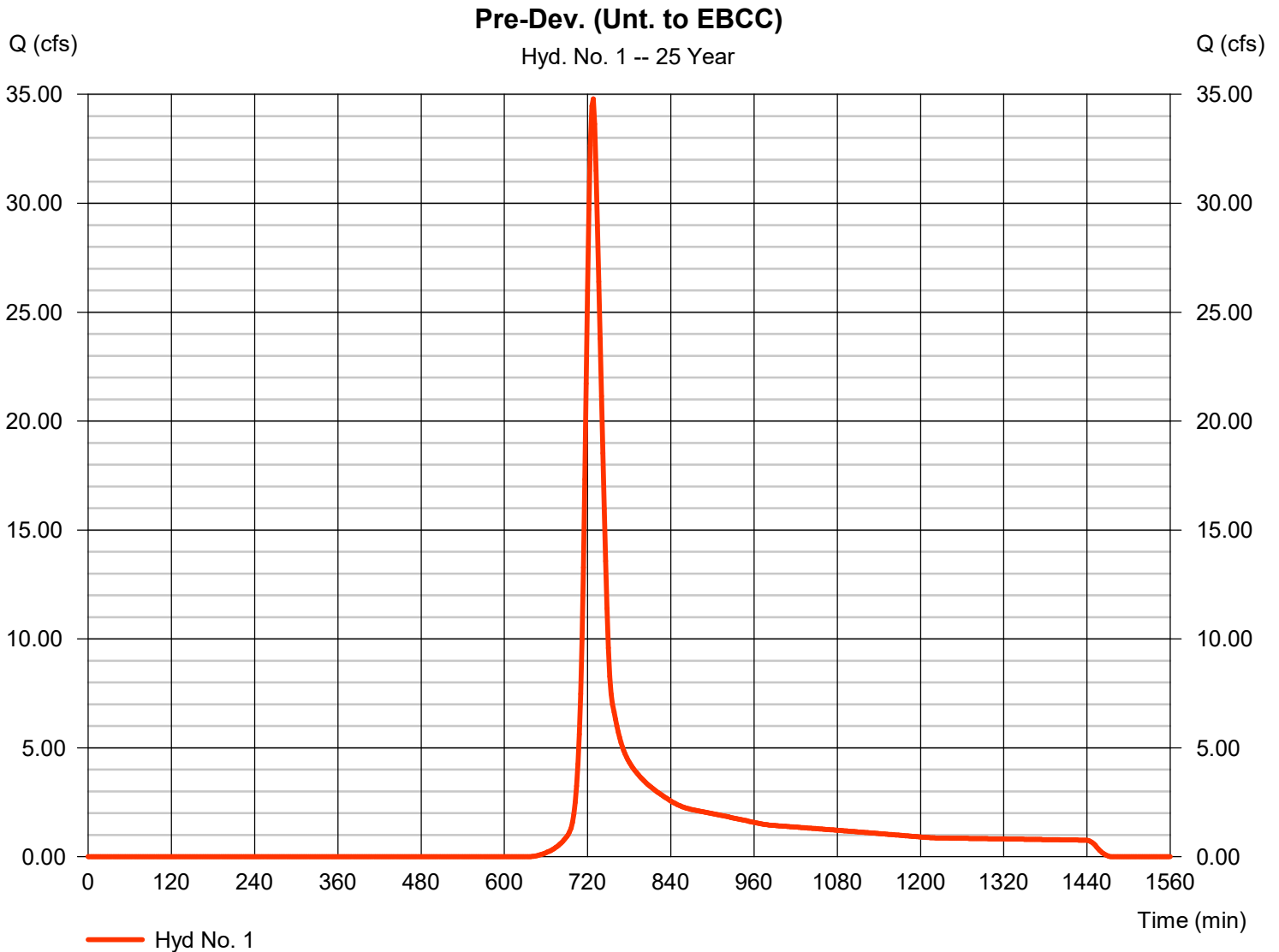


# Hydrograph Report

## Hyd. No. 1

Pre-Dev. (Unt. to EBCC)

Hydrograph type	= SCS Runoff	Peak discharge	= 34.79 cfs
Storm frequency	= 25 yrs	Time to peak	= 728 min
Time interval	= 2 min	Hyd. volume	= 125,412 cuft
Drainage area	= 16.600 ac	Curve number	= 63
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 22.00 min
Total precip.	= 5.81 in	Distribution	= Type II
Storm duration	= 24 hrs	Shape factor	= 484

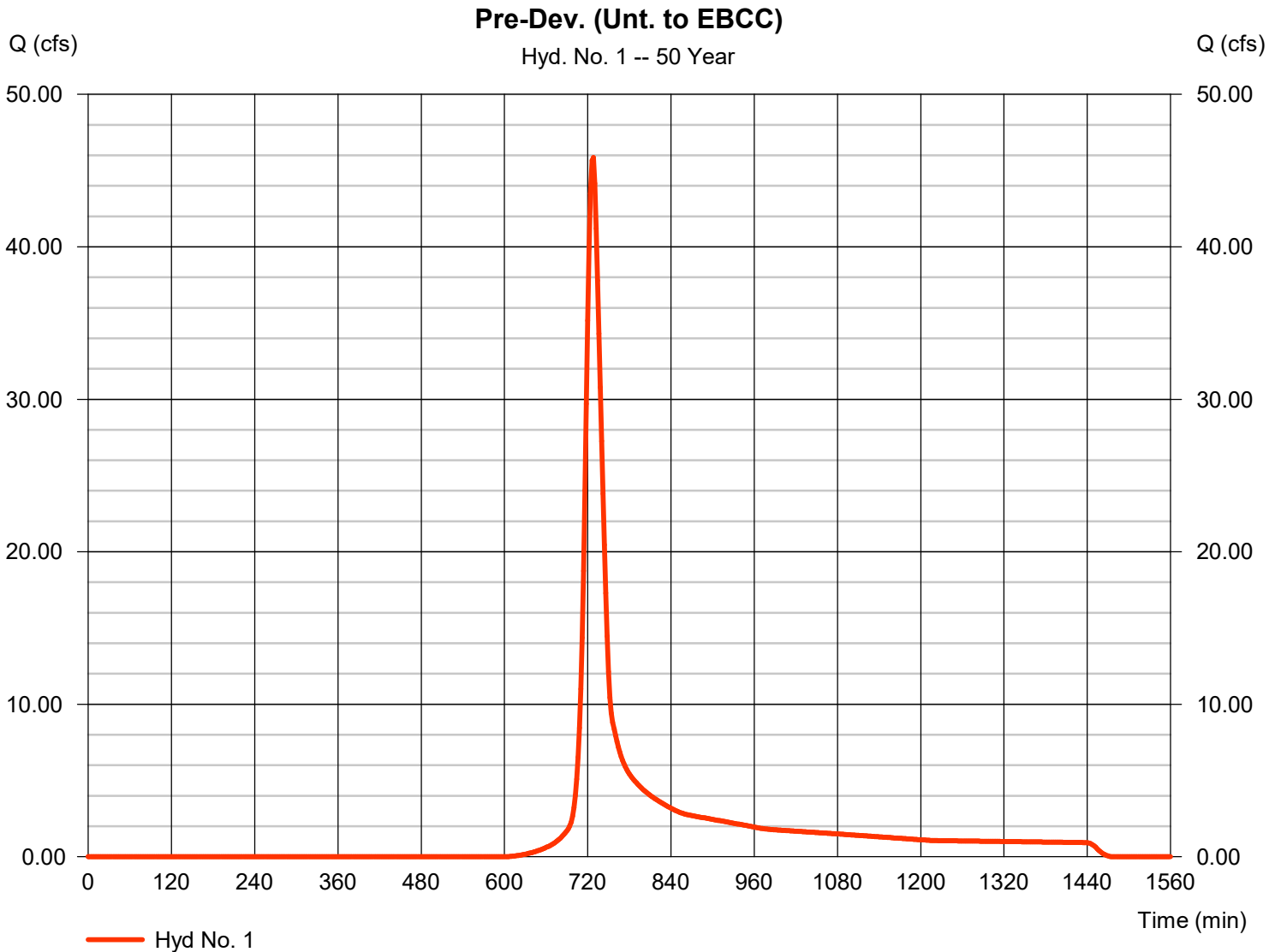


# Hydrograph Report

## Hyd. No. 1

Pre-Dev. (Unt. to EBCC)

Hydrograph type	= SCS Runoff	Peak discharge	= 45.85 cfs
Storm frequency	= 50 yrs	Time to peak	= 728 min
Time interval	= 2 min	Hyd. volume	= 162,480 cuft
Drainage area	= 16.600 ac	Curve number	= 63
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 22.00 min
Total precip.	= 6.66 in	Distribution	= Type II
Storm duration	= 24 hrs	Shape factor	= 484



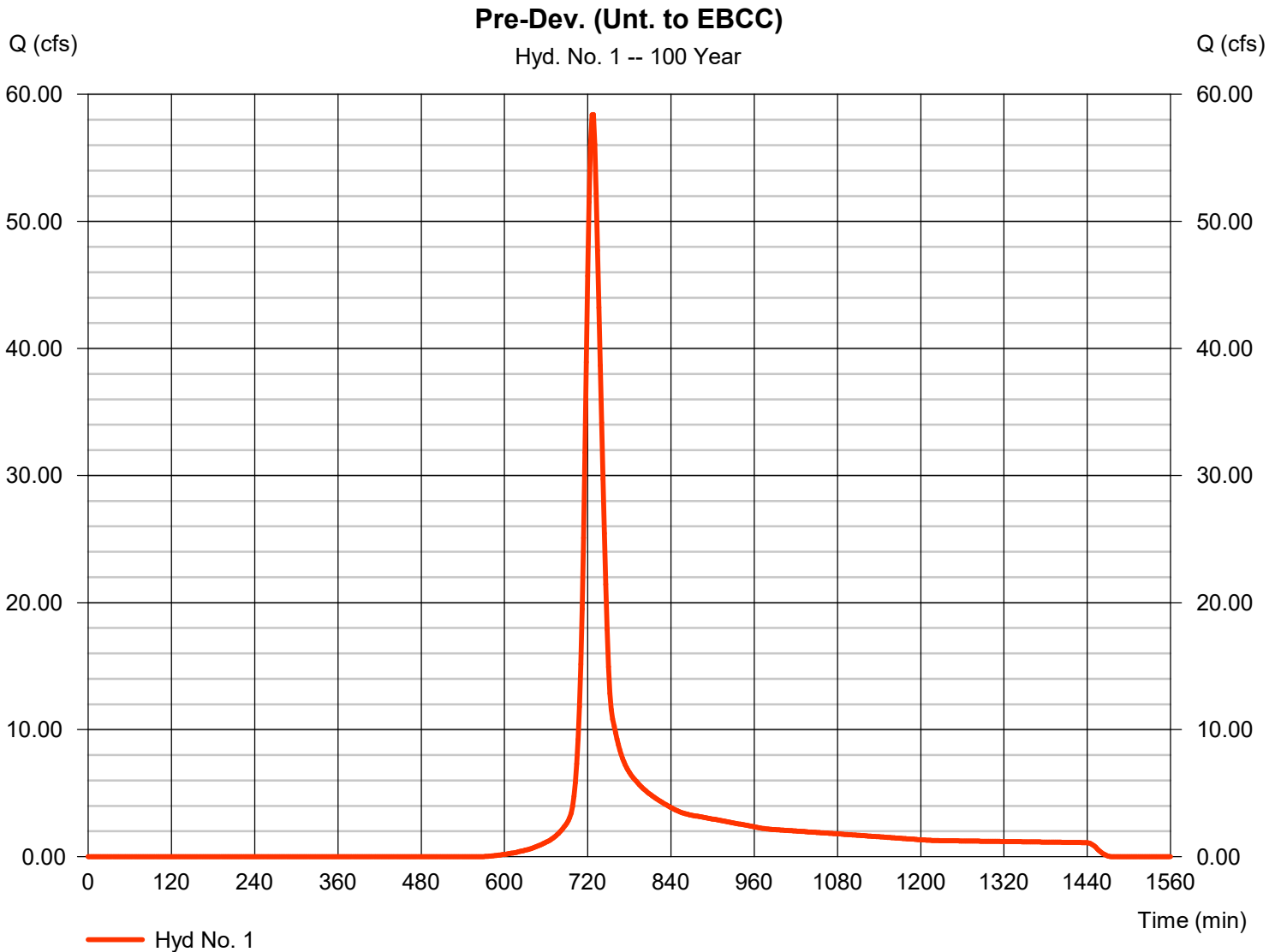
# Hydrograph Report

## Hyd. No. 1

Pre-Dev. (Unt. to EBCC)

Hydrograph type = SCS Runoff  
Storm frequency = 100 yrs  
Time interval = 2 min  
Drainage area = 16.600 ac  
Basin Slope = 0.0 %  
Tc method = User  
Total precip. = 7.58 in  
Storm duration = 24 hrs

Peak discharge = 58.42 cfs  
Time to peak = 728 min  
Hyd. volume = 204,952 cuft  
Curve number = 63  
Hydraulic length = 0 ft  
Time of conc. (Tc) = 22.00 min  
Distribution = Type II  
Shape factor = 484



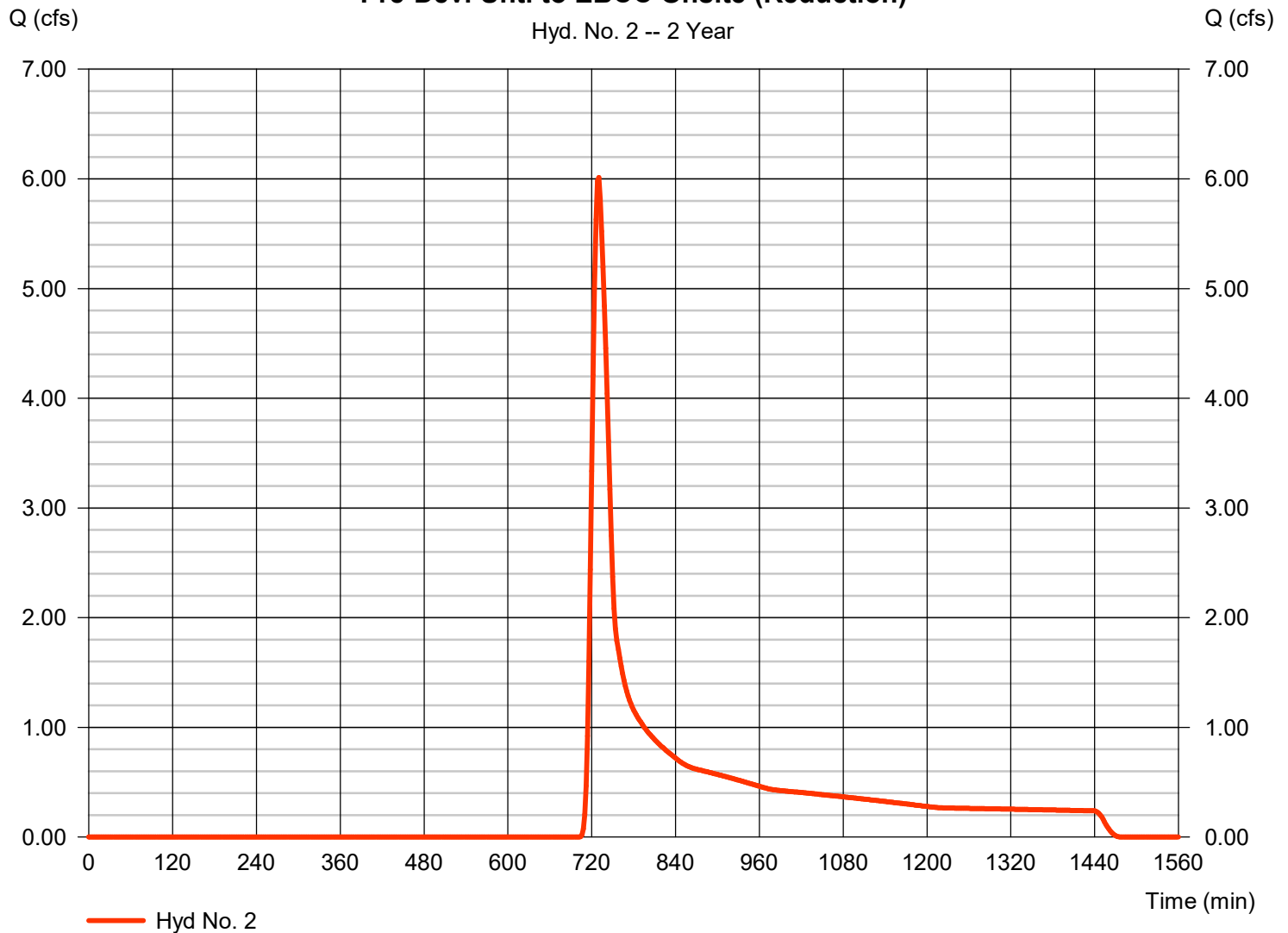
# Hydrograph Report

## Hyd. No. 2

Pre-Dev. Unt. to EBCC Onsite (Reduction)

Hydrograph type	= SCS Runoff	Peak discharge	= 6.014 cfs
Storm frequency	= 2 yrs	Time to peak	= 730 min
Time interval	= 2 min	Hyd. volume	= 28,465 cuft
Drainage area	= 14.100 ac	Curve number	= 63
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 22.00 min
Total precip.	= 3.26 in	Distribution	= Type II
Storm duration	= 24 hrs	Shape factor	= 484

Pre-Dev. Unt. to EBCC Onsite (Reduction)



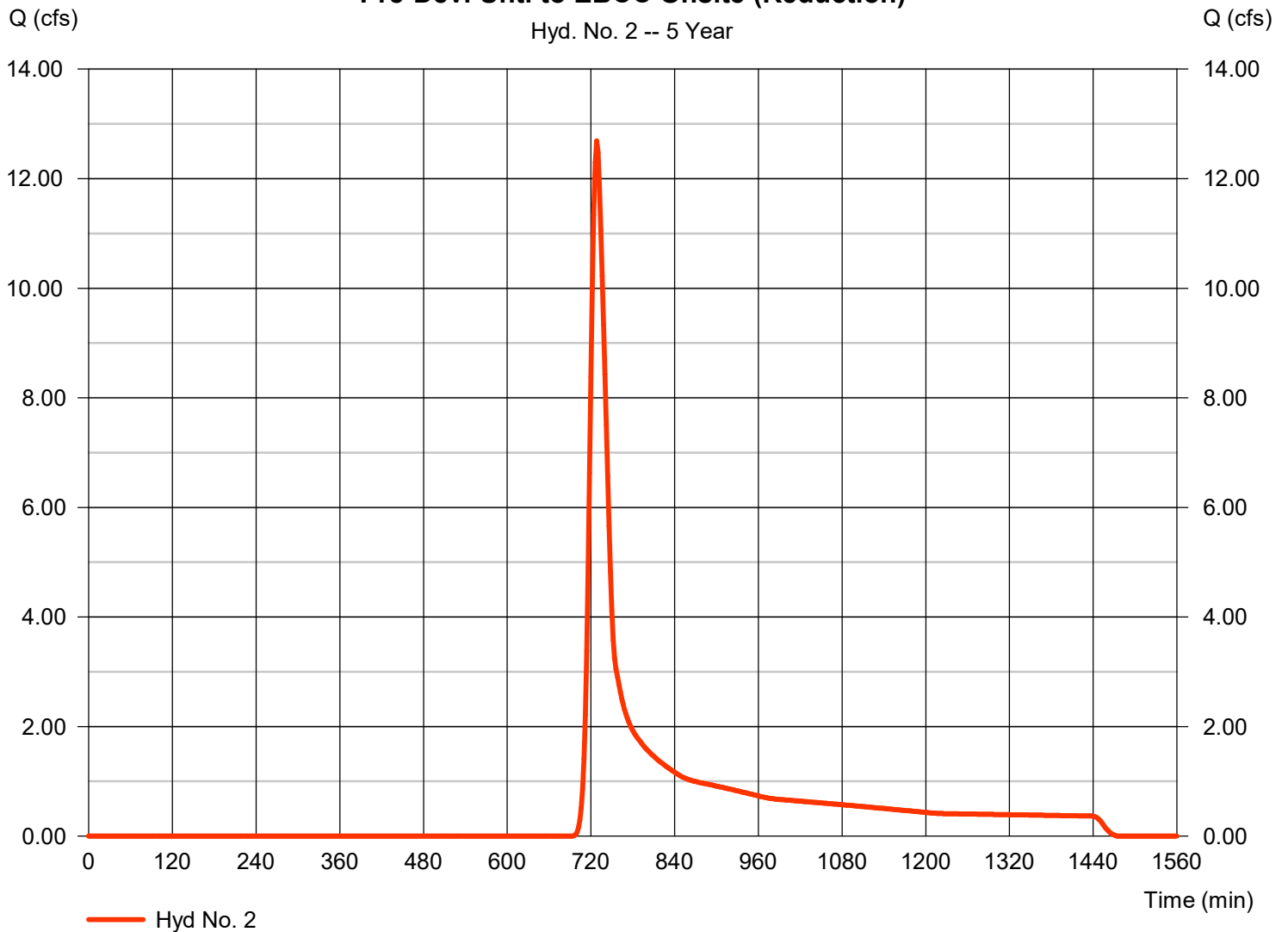
# Hydrograph Report

## Hyd. No. 2

Pre-Dev. Unt. to EBCC Onsite (Reduction)

Hydrograph type	= SCS Runoff	Peak discharge	= 12.69 cfs
Storm frequency	= 5 yrs	Time to peak	= 728 min
Time interval	= 2 min	Hyd. volume	= 50,673 cuft
Drainage area	= 14.100 ac	Curve number	= 63
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 22.00 min
Total precip.	= 4.10 in	Distribution	= Type II
Storm duration	= 24 hrs	Shape factor	= 484

Pre-Dev. Unt. to EBCC Onsite (Reduction)

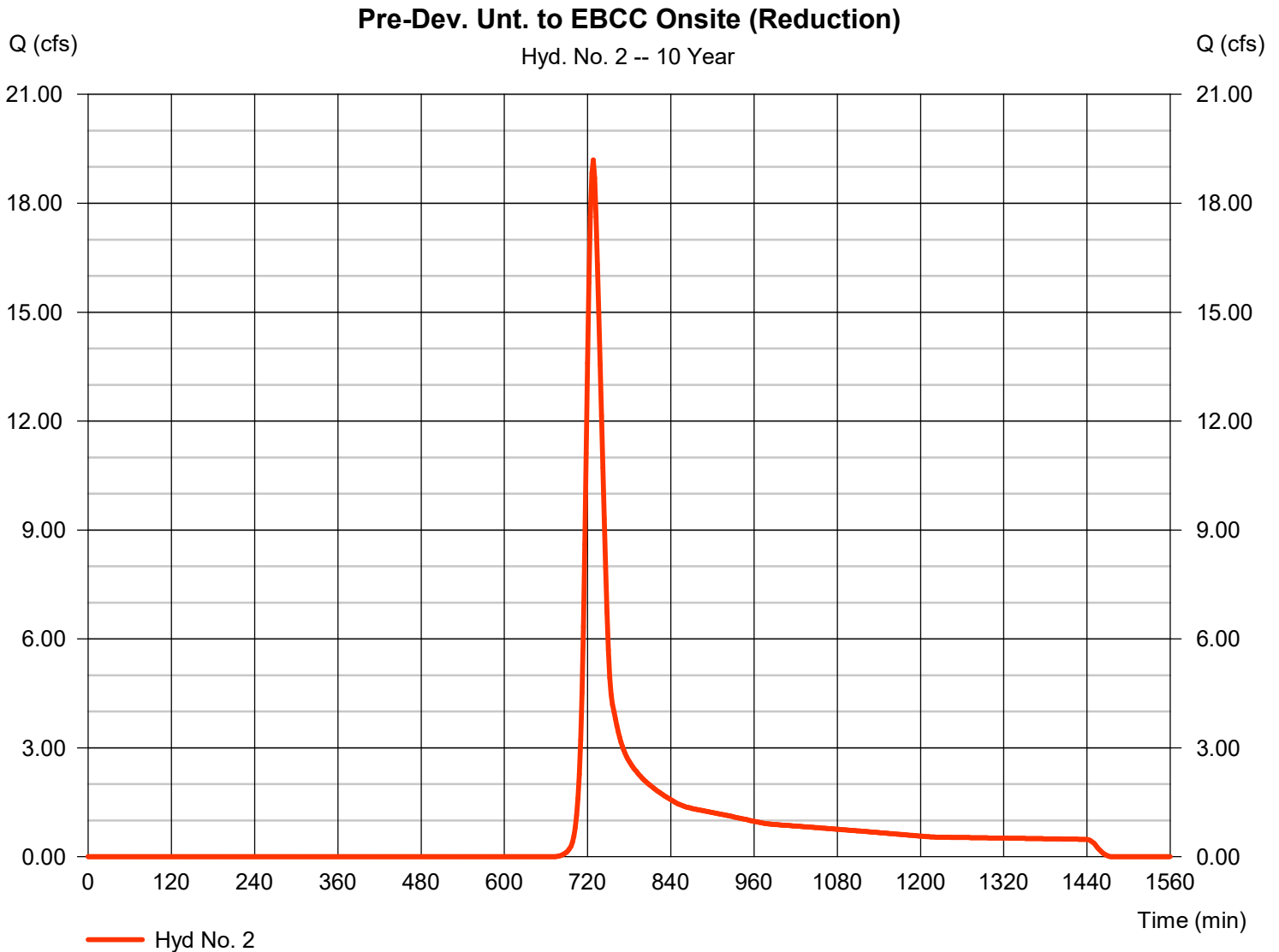


# Hydrograph Report

## Hyd. No. 2

Pre-Dev. Unt. to EBCC Onsite (Reduction)

Hydrograph type	= SCS Runoff	Peak discharge	= 19.19 cfs
Storm frequency	= 10 yrs	Time to peak	= 728 min
Time interval	= 2 min	Hyd. volume	= 72,090 cuft
Drainage area	= 14.100 ac	Curve number	= 63
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 22.00 min
Total precip.	= 4.80 in	Distribution	= Type II
Storm duration	= 24 hrs	Shape factor	= 484



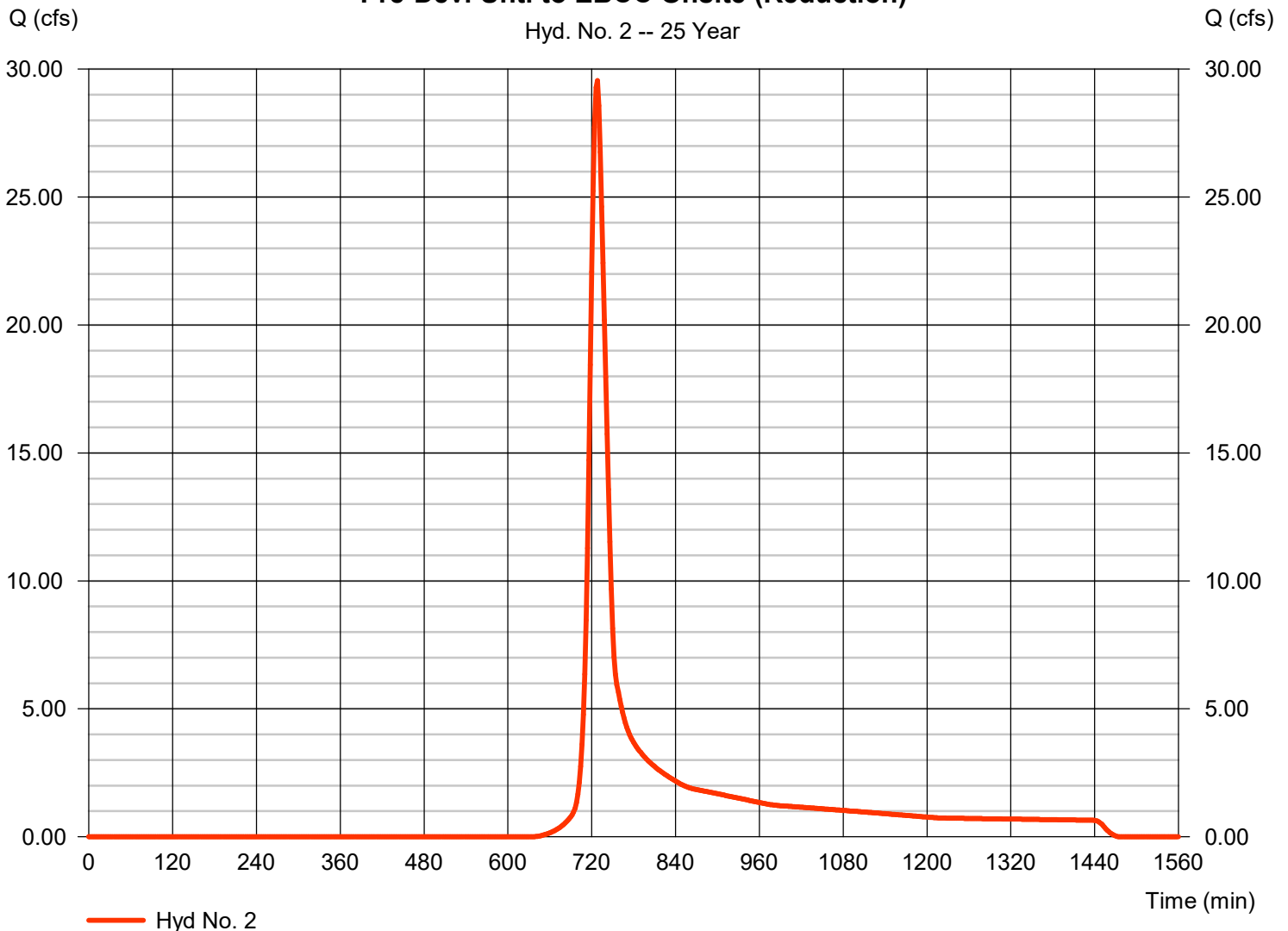
# Hydrograph Report

## Hyd. No. 2

Pre-Dev. Unt. to EBCC Onsite (Reduction)

Hydrograph type	= SCS Runoff	Peak discharge	= 29.55 cfs
Storm frequency	= 25 yrs	Time to peak	= 728 min
Time interval	= 2 min	Hyd. volume	= 106,524 cuft
Drainage area	= 14.100 ac	Curve number	= 63
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 22.00 min
Total precip.	= 5.81 in	Distribution	= Type II
Storm duration	= 24 hrs	Shape factor	= 484

Pre-Dev. Unt. to EBCC Onsite (Reduction)

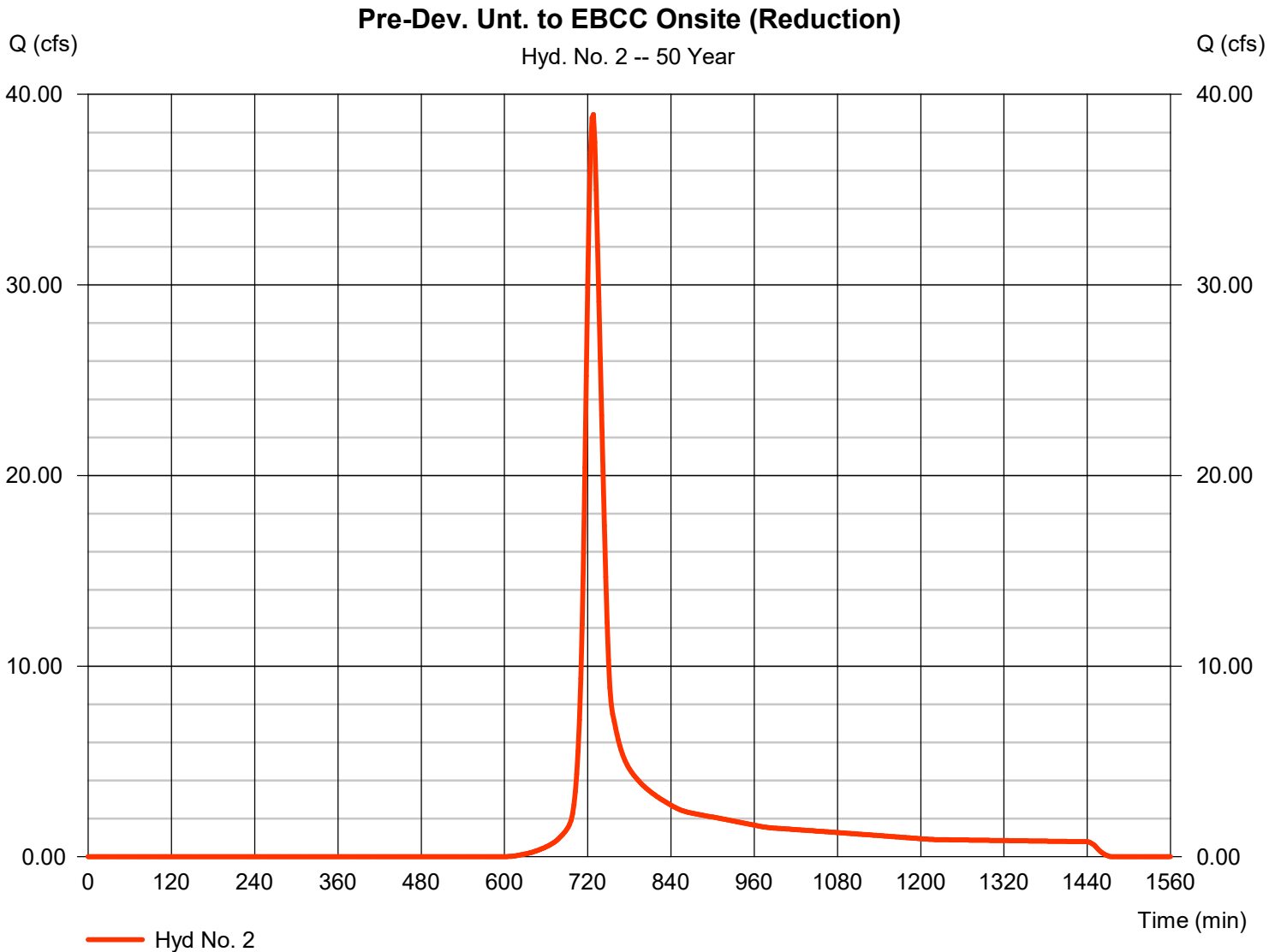


# Hydrograph Report

## Hyd. No. 2

Pre-Dev. Unt. to EBCC Onsite (Reduction)

Hydrograph type	= SCS Runoff	Peak discharge	= 38.95 cfs
Storm frequency	= 50 yrs	Time to peak	= 728 min
Time interval	= 2 min	Hyd. volume	= 138,010 cuft
Drainage area	= 14.100 ac	Curve number	= 63
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 22.00 min
Total precip.	= 6.66 in	Distribution	= Type II
Storm duration	= 24 hrs	Shape factor	= 484



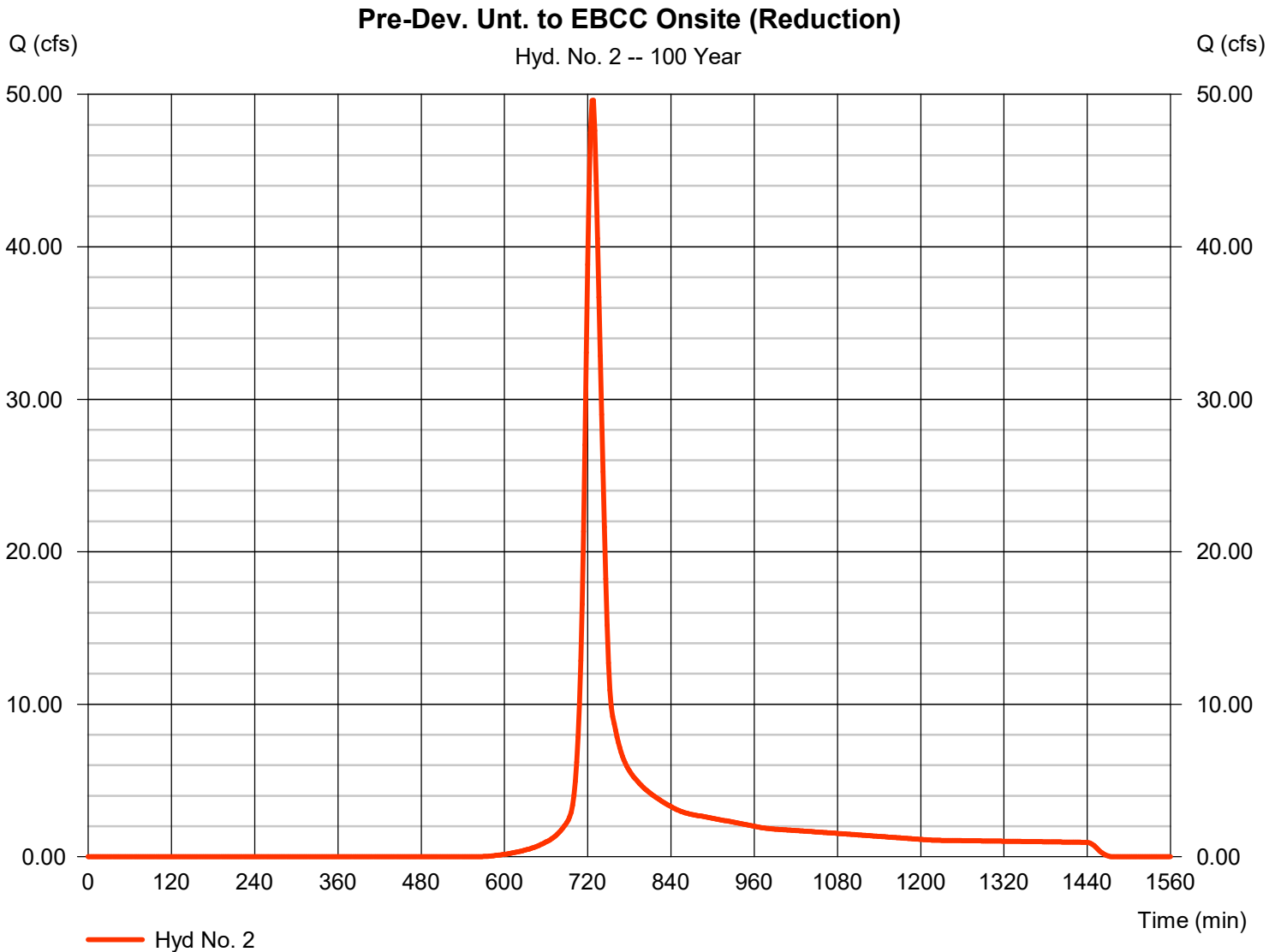


# Hydrograph Report

## Hyd. No. 2

Pre-Dev. Unt. to EBCC Onsite (Reduction)

Hydrograph type	= SCS Runoff	Peak discharge	= 49.62 cfs
Storm frequency	= 100 yrs	Time to peak	= 728 min
Time interval	= 2 min	Hyd. volume	= 174,085 cuft
Drainage area	= 14.100 ac	Curve number	= 63
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 22.00 min
Total precip.	= 7.58 in	Distribution	= Type II
Storm duration	= 24 hrs	Shape factor	= 484



## **POST-DEVELOPMENT HYDROLOGY (EAST BRANCH CHESTER CREEK)**

# ELA SPORT

ATHLETIC FACILITIES DESIGN & CONSULTING

737 S. BROAD STREET  
LITITZ, PA 17543  
(717) 626-72713

# NRCS (SCS) TR-55- WATERSHED WEIGHTED

CURVE NUMBER

## POST-DEVELOPMENT SUMMARY

PROJECT: The Westtown School - Oak Lane Project  
LOCATION: Westtown Township  
COUNTY: Chester



WATERSHED	LAND USE	Area (ac)				Total Area (ac.)	Composite 'CN' Value	Tc Min.					
		Parking, Other Impervious (Disturbed Area)	Parking, Other Impervious (Undisturbed Area)	Open Space (Disturbed Area)	Open Space (Undisturbed Area)								
East Branch Chester Creek Undetained	HSG	B	B	B	B	0.11	0.03	0.98	0.00	0.00	1.13	66	5
	"CN" Value	98	98	61	61								
BMP 1													
		1.07	0.16	2.28	1.47	4.98	70	13					



**ELA SPORT**  
**ATHLETIC FACILITIES**  
**DESIGN & CONSULTING**

737 S. BROAD STREET  
 LITITZ, PA 17543  
 (717) 626-72713

**SUMMARY - SUBAREAS TIME OF CONCENTRATION PRE-DEVELOPMENT CONDITIONS**

**PROJECT:** The Westtown School - Oak Lane Project  
**LOCATION:** Westtown Township  
**COUNTY:** Chester

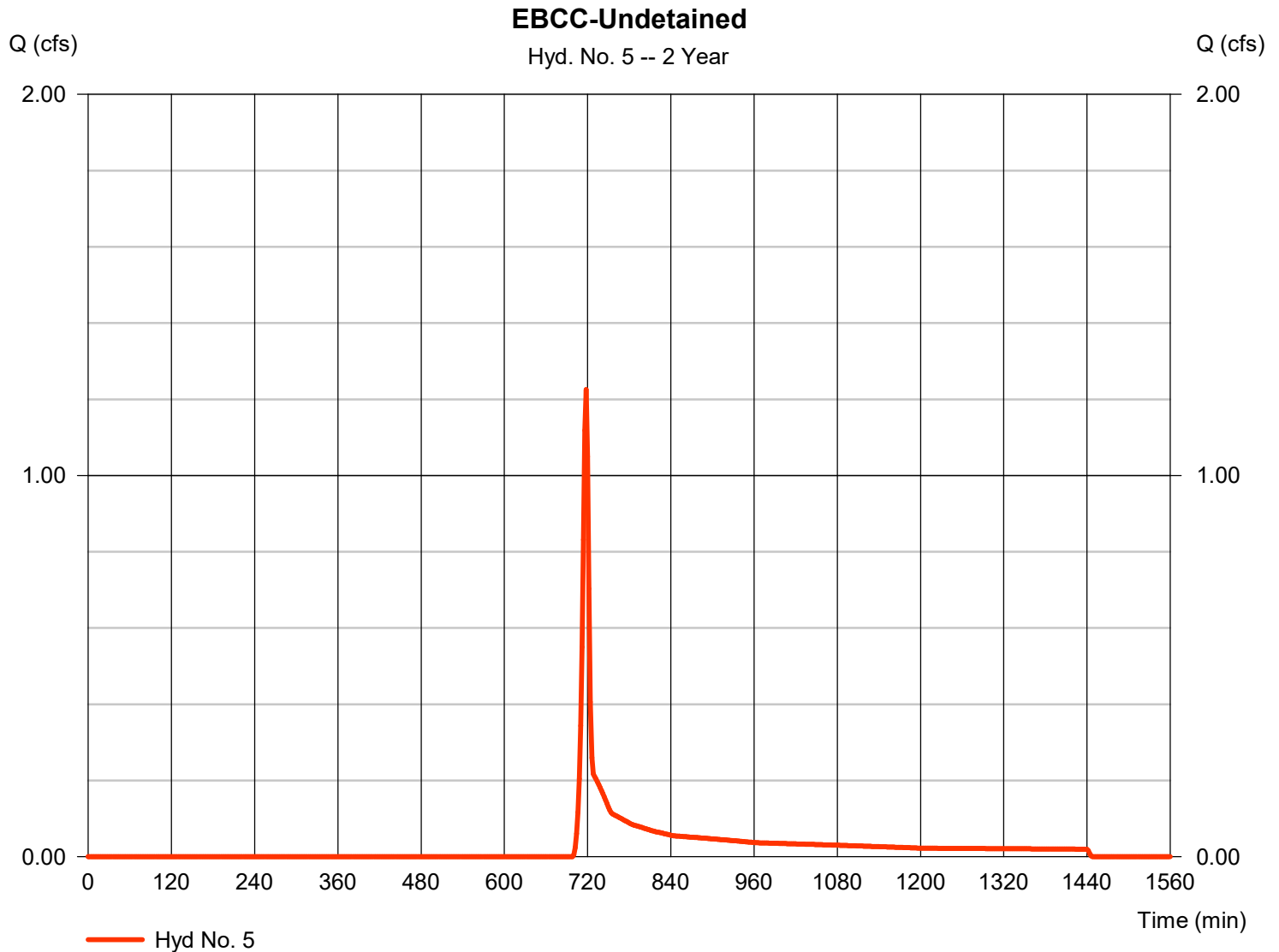
Time of concentration (Tc) or travel time (Tt)																					
NRCS Velocity(Segmental) Method																					
Sub area	overland						Shallow Concentrated						Channel or Pipe						Total		
	Length L <sub>1</sub> 100 ft. max.	Slope S <sub>1</sub> ft./ft.	Manning's n	2 yr rainfall in.	Tc Min.	Flow Path Cover	Length L <sub>2</sub> ft.	Slope S <sub>2</sub> ft./ft.	Average Velocity ft./s	Min.	Tt	Channel or Pipe	C/P	Flow Area sq.ft.	Wetted Perimeter ft.	Pipe Diameter in.	Slope S <sub>3</sub> ft./ft.	Manning's n	Length L <sub>3</sub> ft.	Tt Min.	Hrs.
BMP 1	100	0.040	0.24	3.26	11	U/P		0	0.0	0	0.0		0.00	0.00						0	
				3.26	0	U	180	4	0.8	0	0.060		0.00	0.00						0	
				3.26	0	P	153	2.3	1.1	0	0.013		0.00	0.00						0	
					0	U	40	6.8	0.1	0	0.180		0.00	0.00						0	
					0	U	65	2	0.5	0	0.015		0.00	0.00						0.0	
					10.7				2.5											0.0	0.22

# Hydrograph Report

## Hyd. No. 5

EBCC-Undetained

Hydrograph type	= SCS Runoff	Peak discharge	= 1.225 cfs
Storm frequency	= 2 yrs	Time to peak	= 718 min
Time interval	= 2 min	Hyd. volume	= 2,590 cuft
Drainage area	= 1.130 ac	Curve number	= 66
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 5.00 min
Total precip.	= 3.26 in	Distribution	= Type II
Storm duration	= 24 hrs	Shape factor	= 484

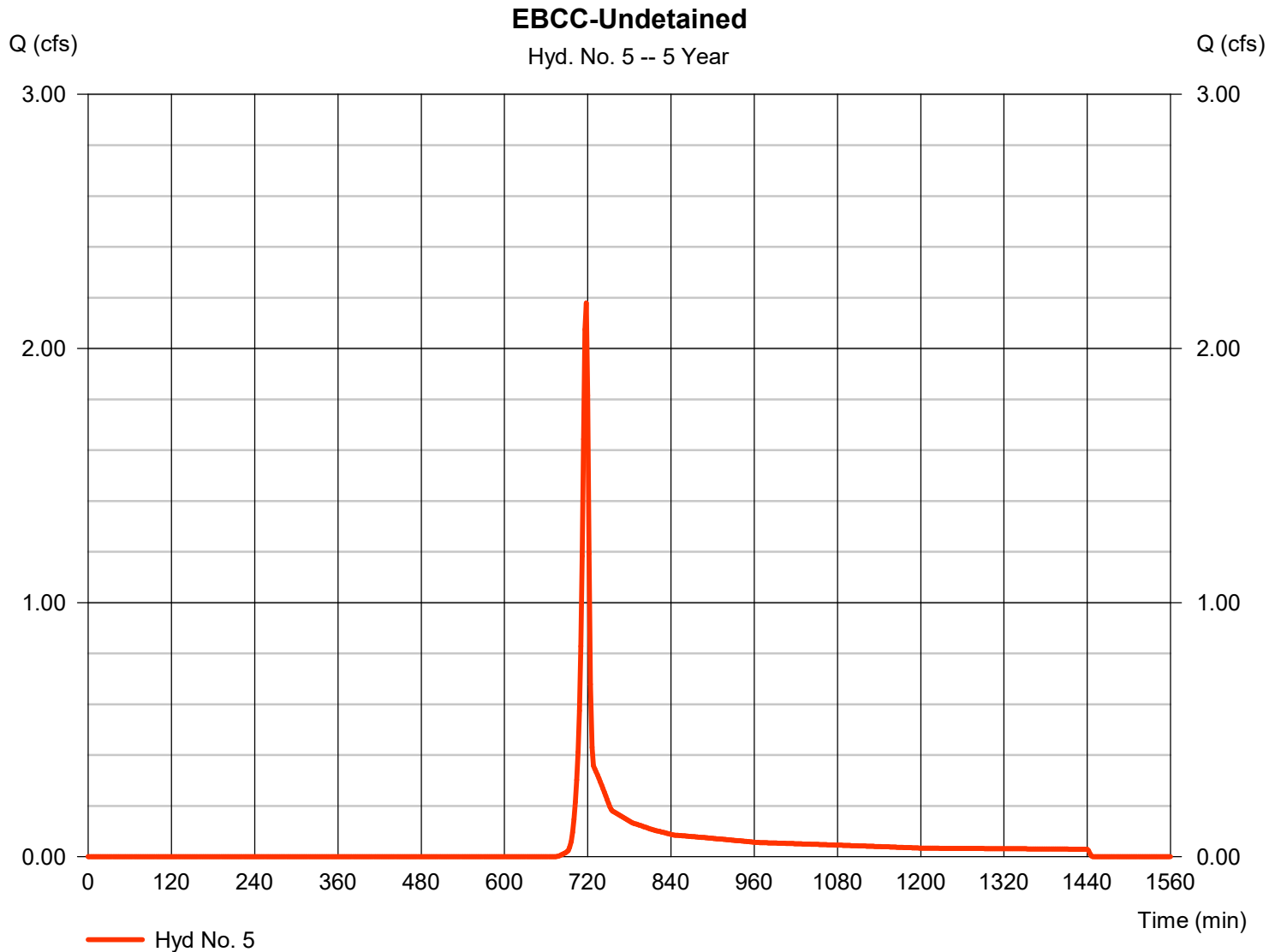


# Hydrograph Report

## Hyd. No. 5

EBCC-Undetained

Hydrograph type	= SCS Runoff	Peak discharge	= 2.179 cfs
Storm frequency	= 5 yrs	Time to peak	= 718 min
Time interval	= 2 min	Hyd. volume	= 4,408 cuft
Drainage area	= 1.130 ac	Curve number	= 66
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 5.00 min
Total precip.	= 4.10 in	Distribution	= Type II
Storm duration	= 24 hrs	Shape factor	= 484

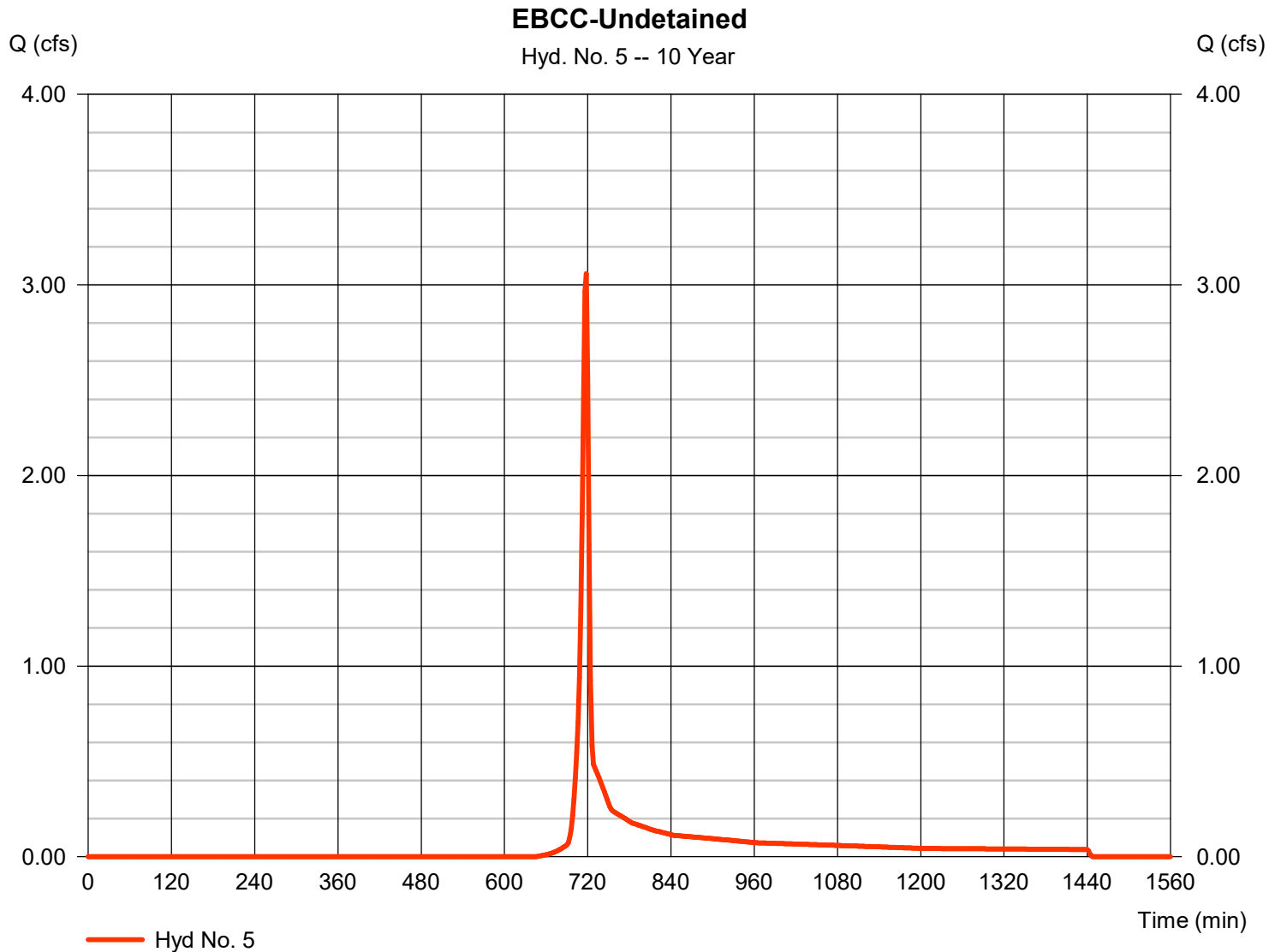


# Hydrograph Report

## Hyd. No. 5

EBCC-Undetained

Hydrograph type	= SCS Runoff	Peak discharge	= 3.059 cfs
Storm frequency	= 10 yrs	Time to peak	= 718 min
Time interval	= 2 min	Hyd. volume	= 6,126 cuft
Drainage area	= 1.130 ac	Curve number	= 66
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 5.00 min
Total precip.	= 4.80 in	Distribution	= Type II
Storm duration	= 24 hrs	Shape factor	= 484

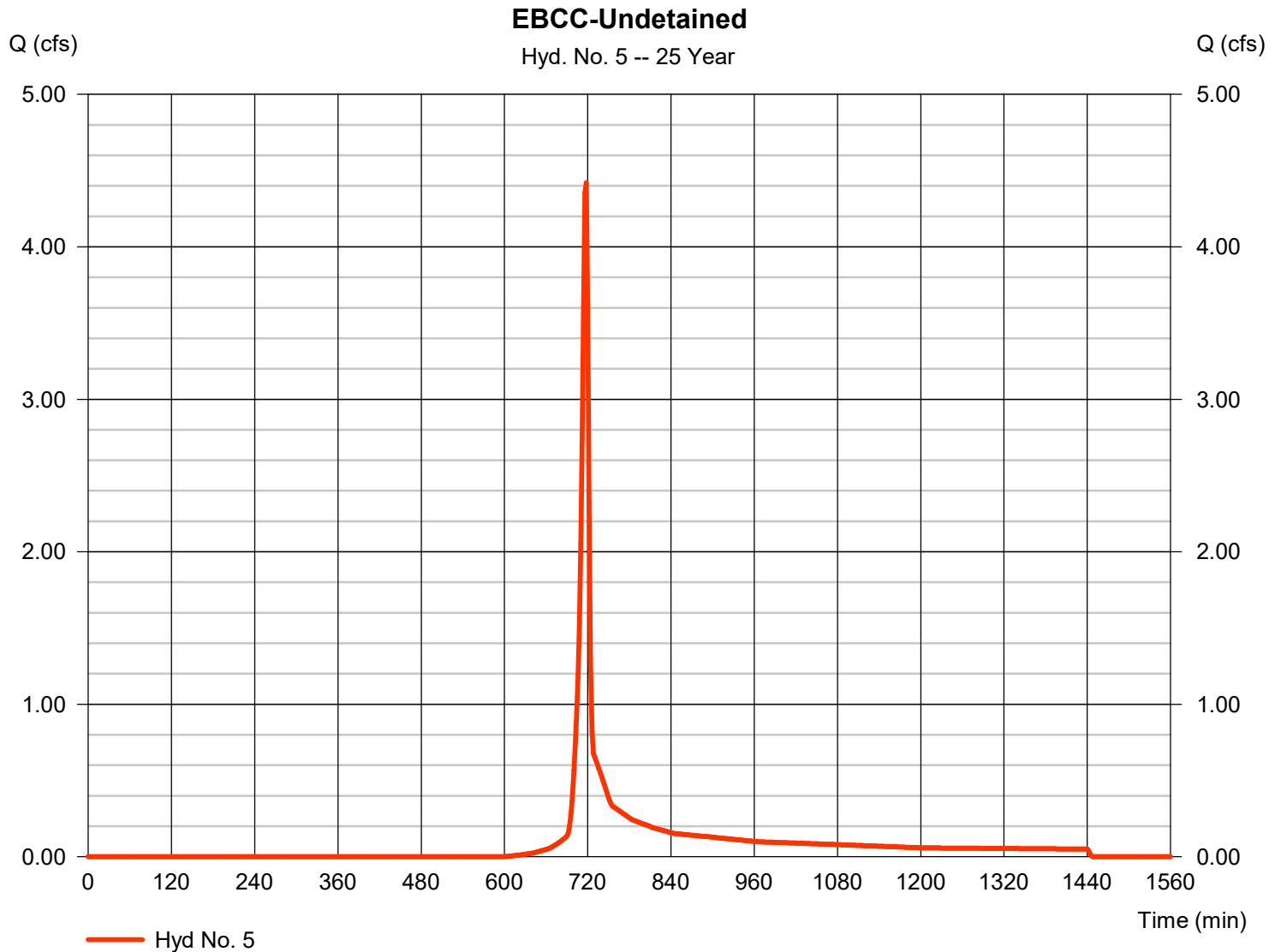


# Hydrograph Report

## Hyd. No. 5

EBCC-Undetained

Hydrograph type	= SCS Runoff	Peak discharge	= 4.420 cfs
Storm frequency	= 25 yrs	Time to peak	= 718 min
Time interval	= 2 min	Hyd. volume	= 8,846 cuft
Drainage area	= 1.130 ac	Curve number	= 66
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 5.00 min
Total precip.	= 5.81 in	Distribution	= Type II
Storm duration	= 24 hrs	Shape factor	= 484



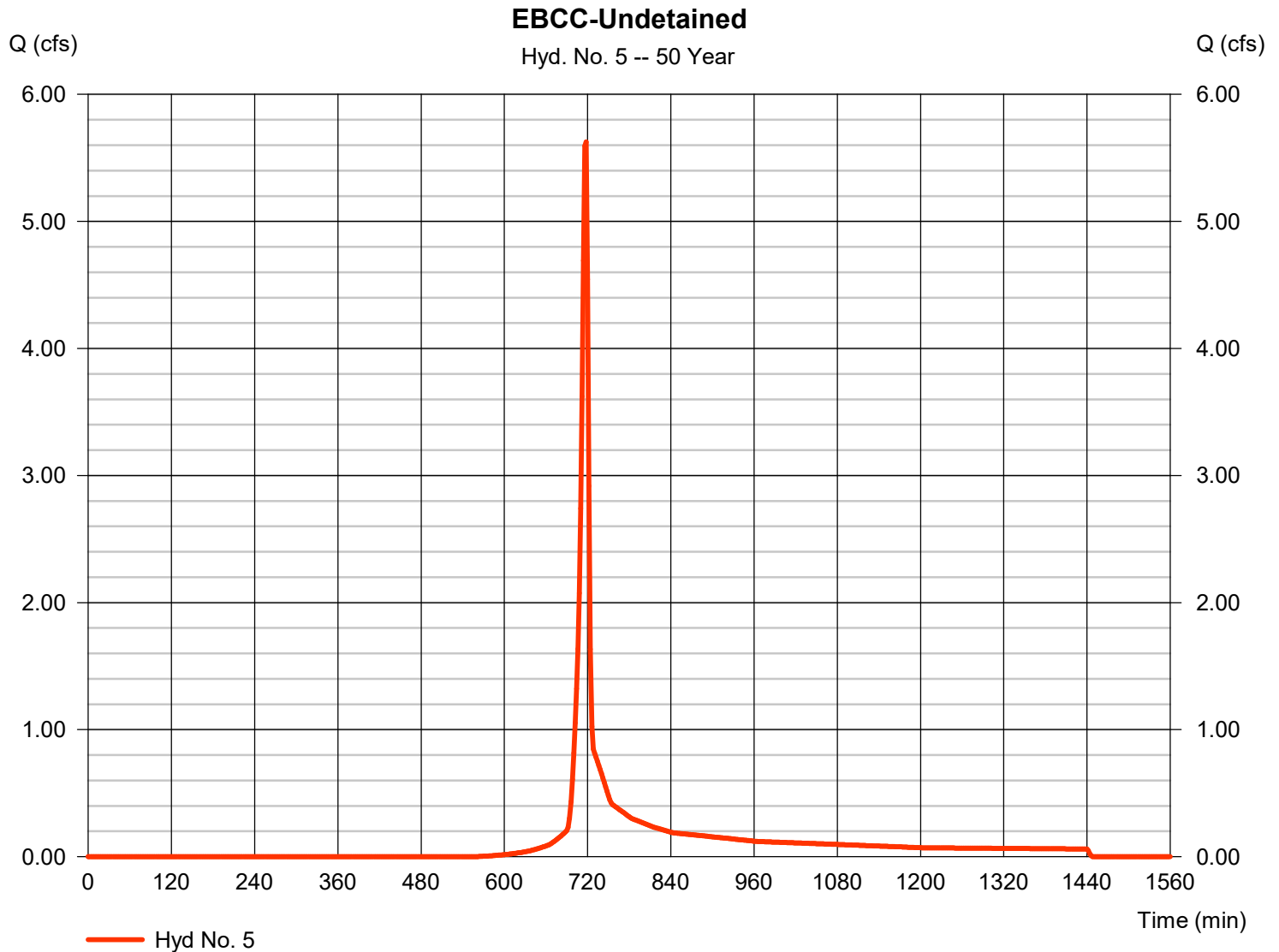


# Hydrograph Report

## Hyd. No. 5

EBCC-Undetained

Hydrograph type	= SCS Runoff	Peak discharge	= 5.626 cfs
Storm frequency	= 50 yrs	Time to peak	= 718 min
Time interval	= 2 min	Hyd. volume	= 11,305 cuft
Drainage area	= 1.130 ac	Curve number	= 66
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 5.00 min
Total precip.	= 6.66 in	Distribution	= Type II
Storm duration	= 24 hrs	Shape factor	= 484

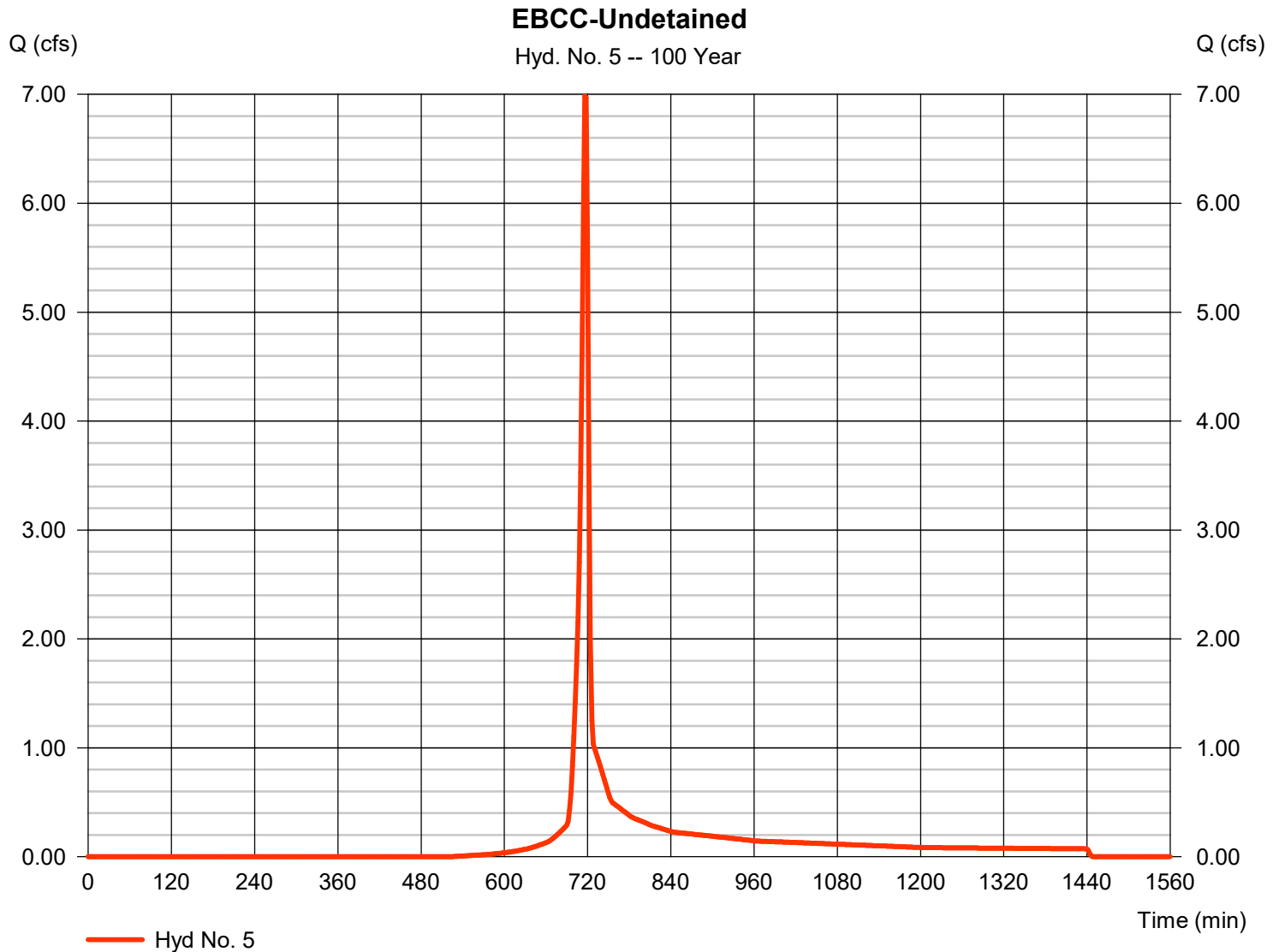


# Hydrograph Report

## Hyd. No. 5

EBCC-Undetained

Hydrograph type	= SCS Runoff	Peak discharge	= 6.983 cfs
Storm frequency	= 100 yrs	Time to peak	= 716 min
Time interval	= 2 min	Hyd. volume	= 14,098 cuft
Drainage area	= 1.130 ac	Curve number	= 66
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 5.00 min
Total precip.	= 7.58 in	Distribution	= Type II
Storm duration	= 24 hrs	Shape factor	= 484

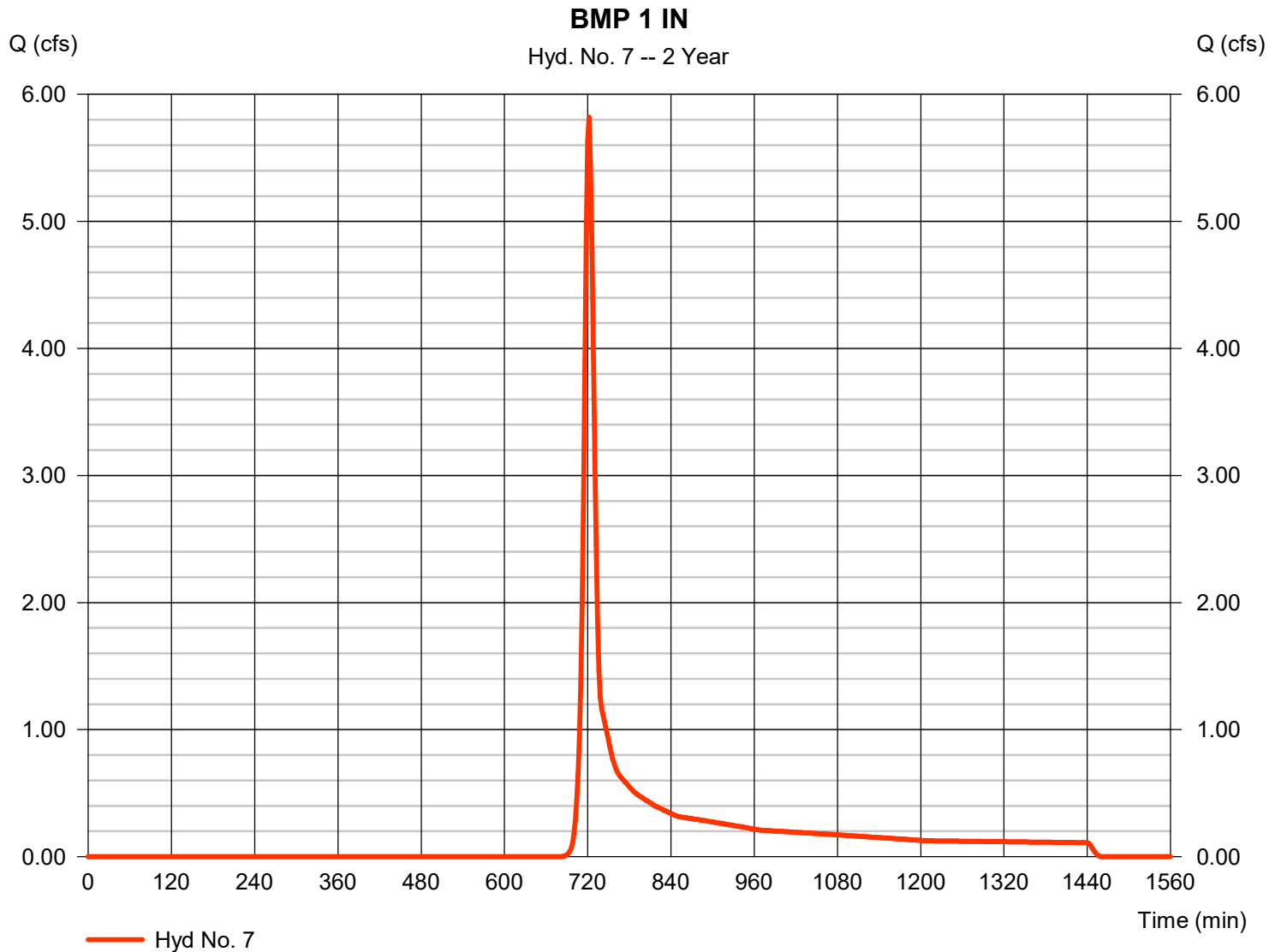


# Hydrograph Report

## Hyd. No. 7

BMP 1 IN

Hydrograph type	= SCS Runoff	Peak discharge	= 5.820 cfs
Storm frequency	= 2 yrs	Time to peak	= 722 min
Time interval	= 2 min	Hyd. volume	= 16,092 cuft
Drainage area	= 4.980 ac	Curve number	= 70
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 13.00 min
Total precip.	= 3.26 in	Distribution	= Type II
Storm duration	= 24 hrs	Shape factor	= 484



# Hydrograph Report

Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2022

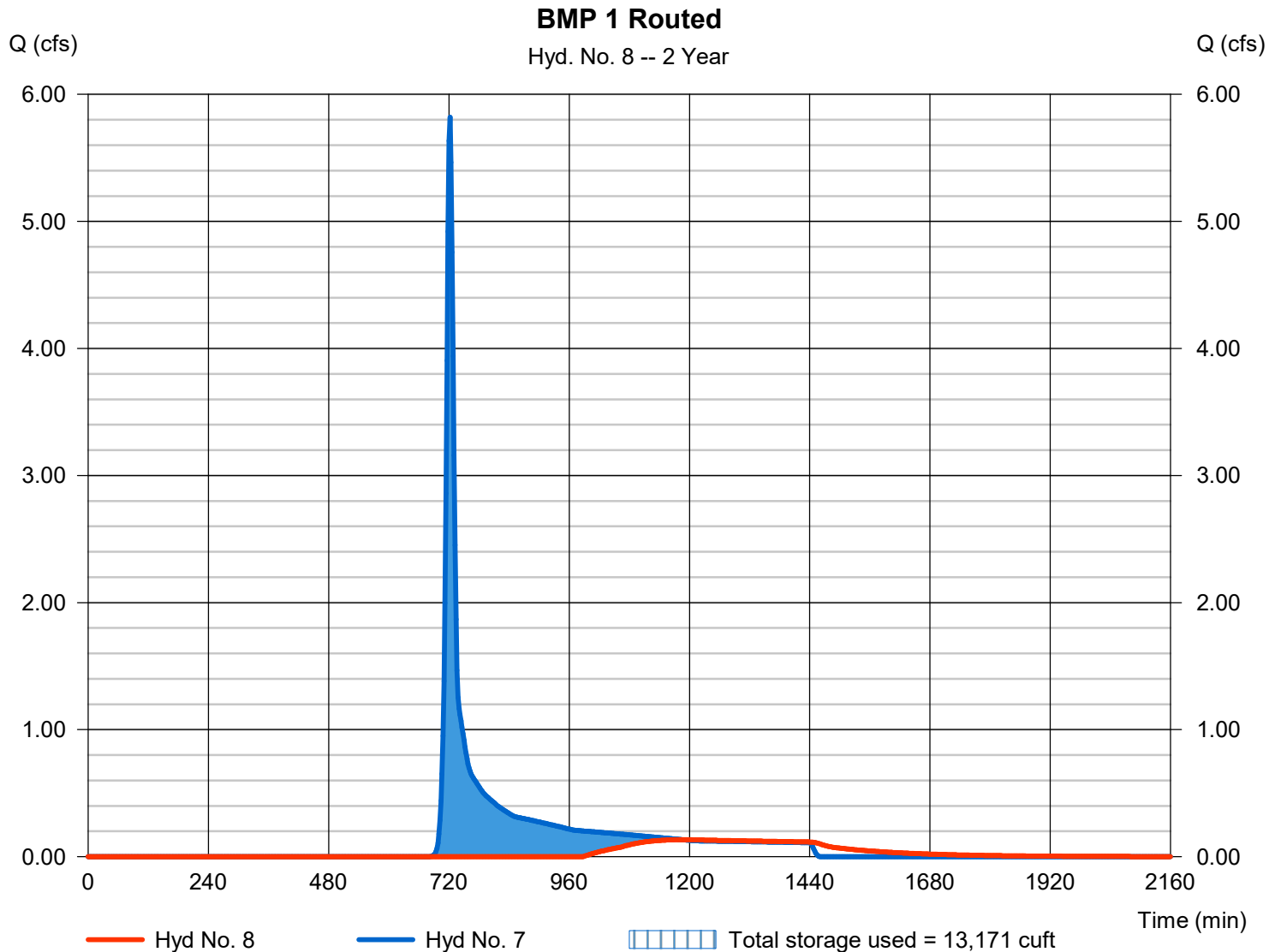
Monday, 01 / 16 / 2023

## Hyd. No. 8

BMP 1 Routed

Hydrograph type	= Reservoir	Peak discharge	= 0.134 cfs
Storm frequency	= 2 yrs	Time to peak	= 1186 min
Time interval	= 2 min	Hyd. volume	= 3,882 cuft
Inflow hyd. No.	= 7 - BMP 1 IN	Max. Elevation	= 290.57 ft
Reservoir name	= BMP 1	Max. Storage	= 13,171 cuft

Storage Indication method used.



# Pond Report

## Pond No. 7 - BMP 1

### Pond Data

Contours -User-defined contour areas. Conic method used for volume calculation. Begining Elevation = 289.50 ft

### Stage / Storage Table

Stage (ft)	Elevation (ft)	Contour area (sqft)	Incr. Storage (cuft)	Total storage (cuft)
0.00	289.50	11,329	0	0
0.50	290.00	12,199	5,880	5,880
1.00	290.50	13,093	6,321	12,201
1.50	291.00	13,943	6,757	18,958
2.50	292.00	15,850	14,885	33,843
3.50	293.00	17,790	16,809	50,652

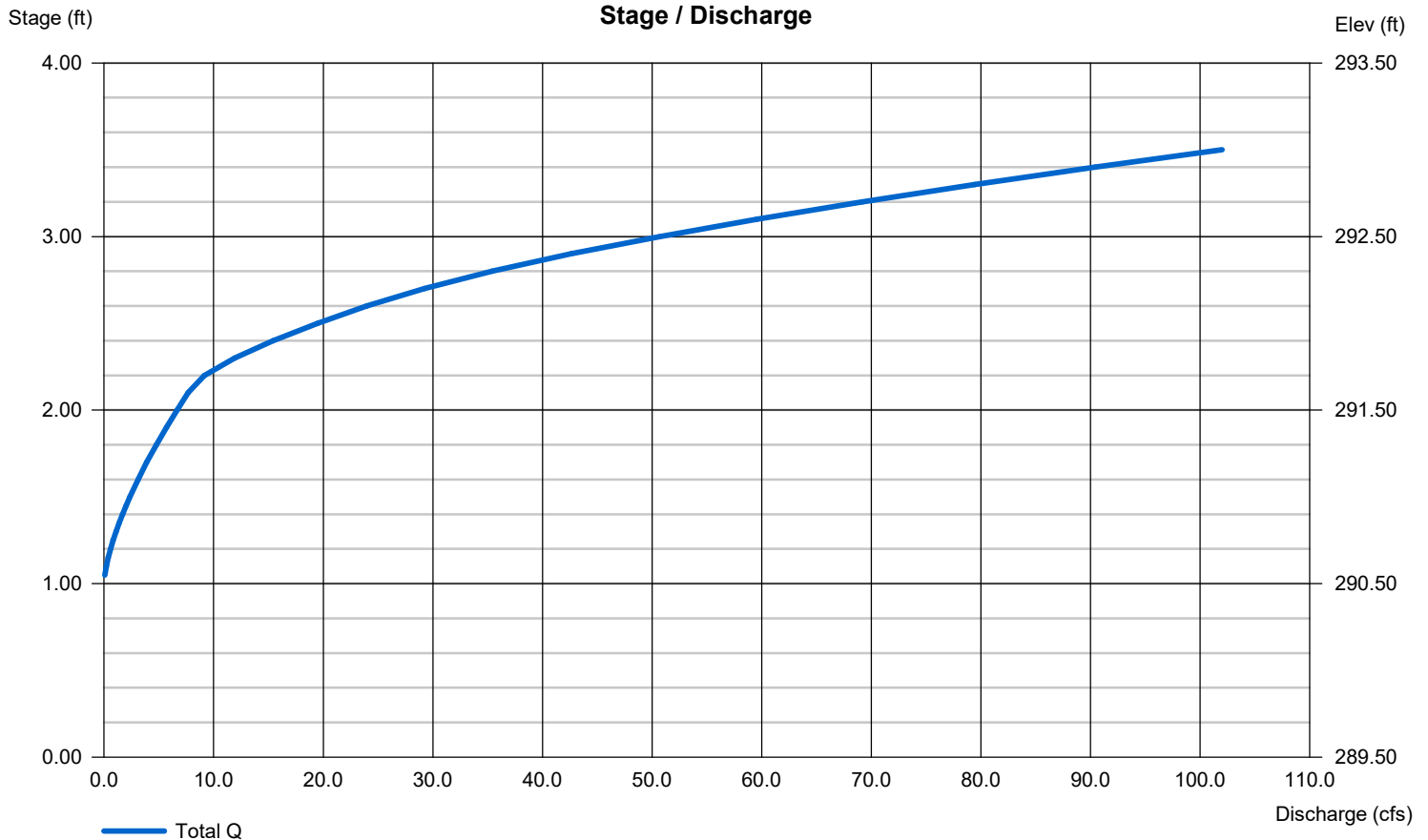
### Culvert / Orifice Structures

	[A]	[B]	[C]	[PrfRsr]
Rise (in)	= 18.00	Inactive	0.00	0.00
Span (in)	= 18.00	0.00	0.00	0.00
No. Barrels	= 1	1	0	0
Invert El. (ft)	= 284.25	0.00	0.00	0.00
Length (ft)	= 28.47	0.10	0.00	0.00
Slope (%)	= 0.53	0.00	0.00	n/a
N-Value	= .013	.013	.013	n/a
Orifice Coeff.	= 0.60	0.60	0.60	0.60
Multi-Stage	= n/a	Yes	No	No

### Weir Structures

	[A]	[B]	[C]	[D]
Crest Len (ft)	= 10.50	2.00	30.00	0.00
Crest El. (ft)	= 291.65	290.50	292.00	0.00
Weir Coeff.	= 3.33	3.33	2.60	3.33
Weir Type	= 1	Rect	Broad	---
Multi-Stage	= Yes	Yes	No	No
Exfil.(in/hr)	= 0.000 (by Wet area)			
TW Elev. (ft)	= 0.00			

Note: Culvert/Orifice outflows are analyzed under inlet (ic) and outlet (oc) control. Weir risers checked for orifice conditions (ic) and submergence (s).

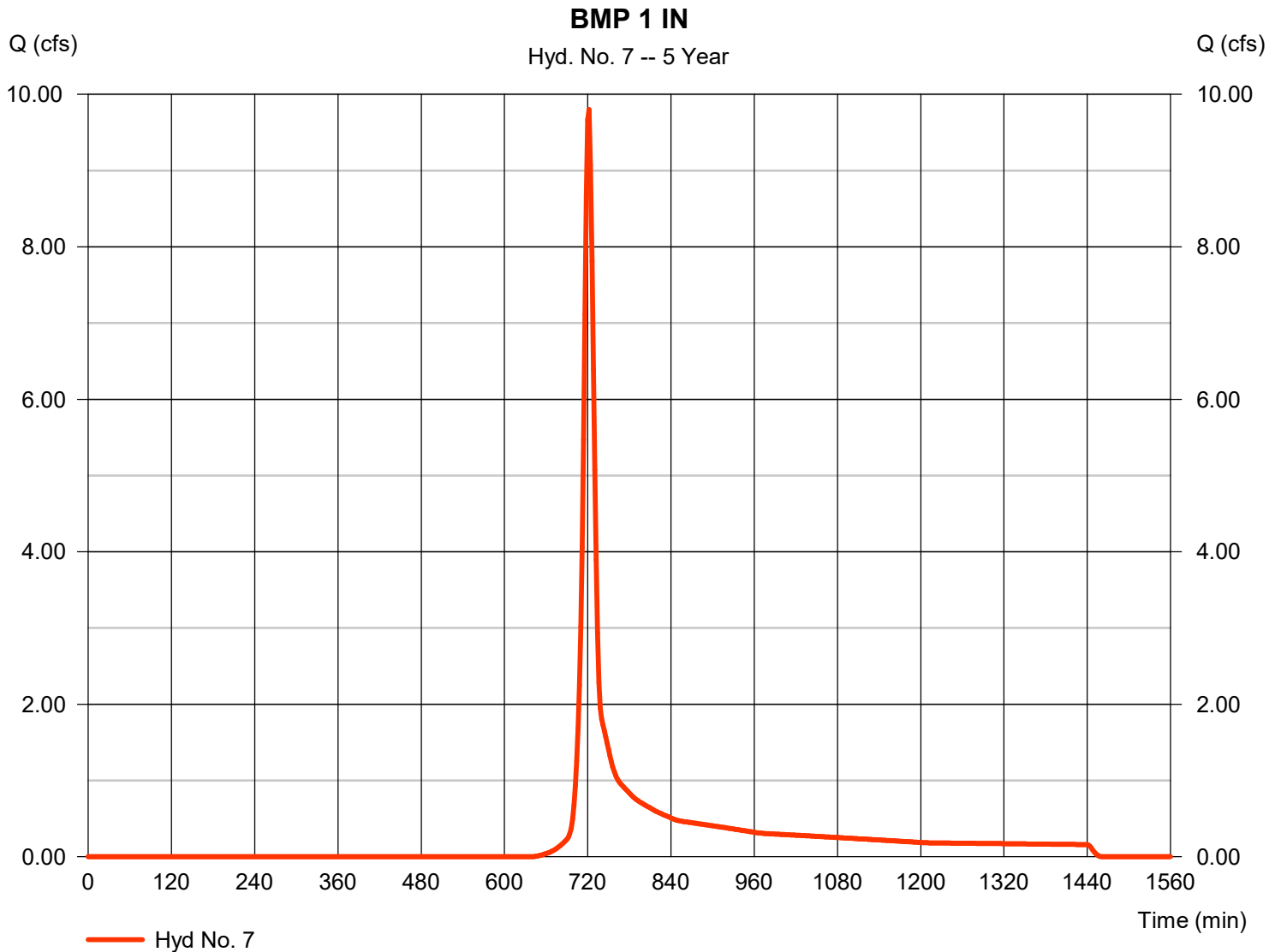


# Hydrograph Report

## Hyd. No. 7

BMP 1 IN

Hydrograph type	= SCS Runoff	Peak discharge	= 9.799 cfs
Storm frequency	= 5 yrs	Time to peak	= 722 min
Time interval	= 2 min	Hyd. volume	= 26,040 cuft
Drainage area	= 4.980 ac	Curve number	= 70
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 13.00 min
Total precip.	= 4.10 in	Distribution	= Type II
Storm duration	= 24 hrs	Shape factor	= 484



# Hydrograph Report

Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2022

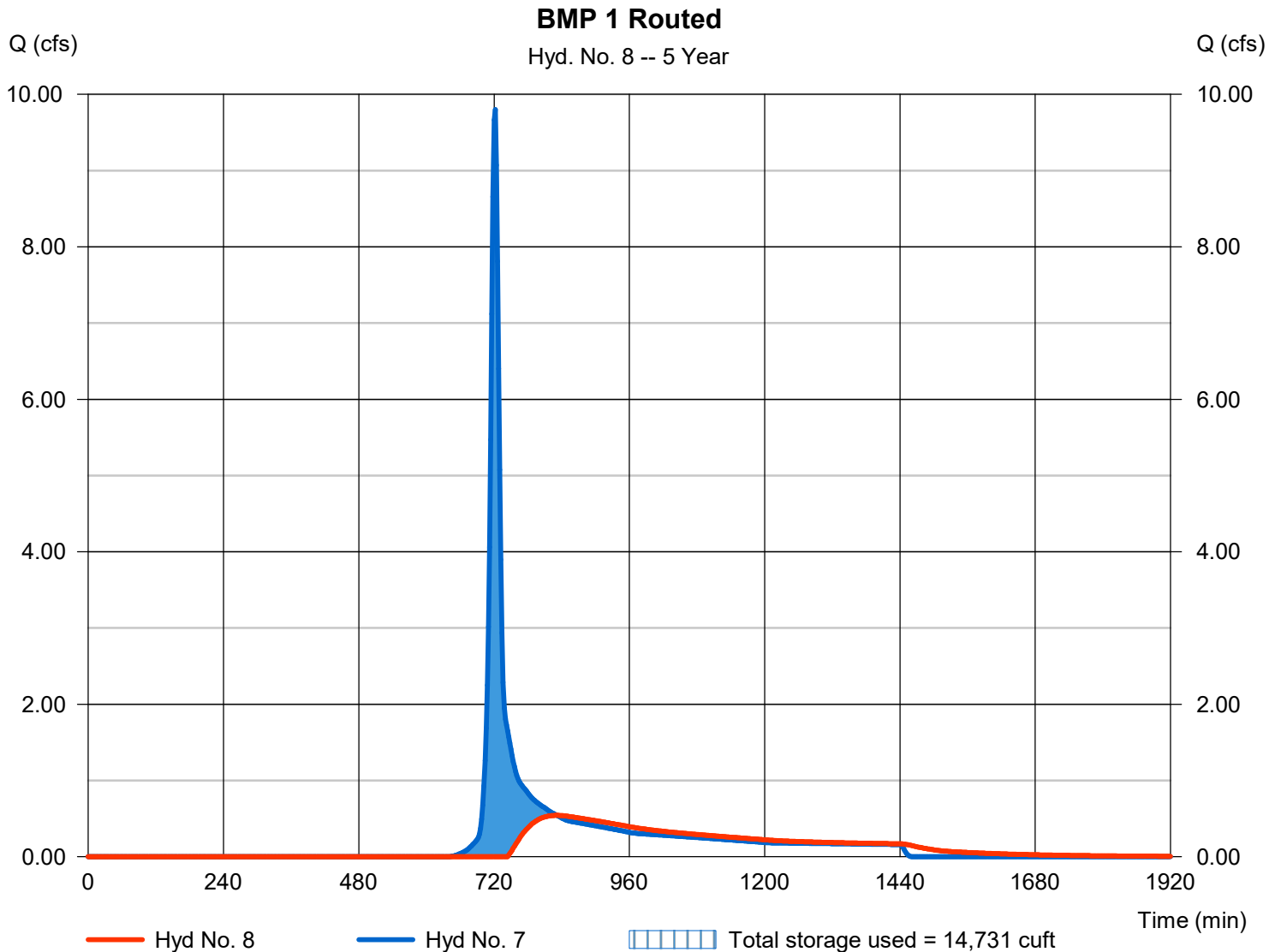
Monday, 01 / 16 / 2023

## Hyd. No. 8

BMP 1 Routed

Hydrograph type	= Reservoir	Peak discharge	= 0.542 cfs
Storm frequency	= 5 yrs	Time to peak	= 832 min
Time interval	= 2 min	Hyd. volume	= 13,830 cuft
Inflow hyd. No.	= 7 - BMP 1 IN	Max. Elevation	= 290.69 ft
Reservoir name	= BMP 1	Max. Storage	= 14,731 cuft

Storage Indication method used.

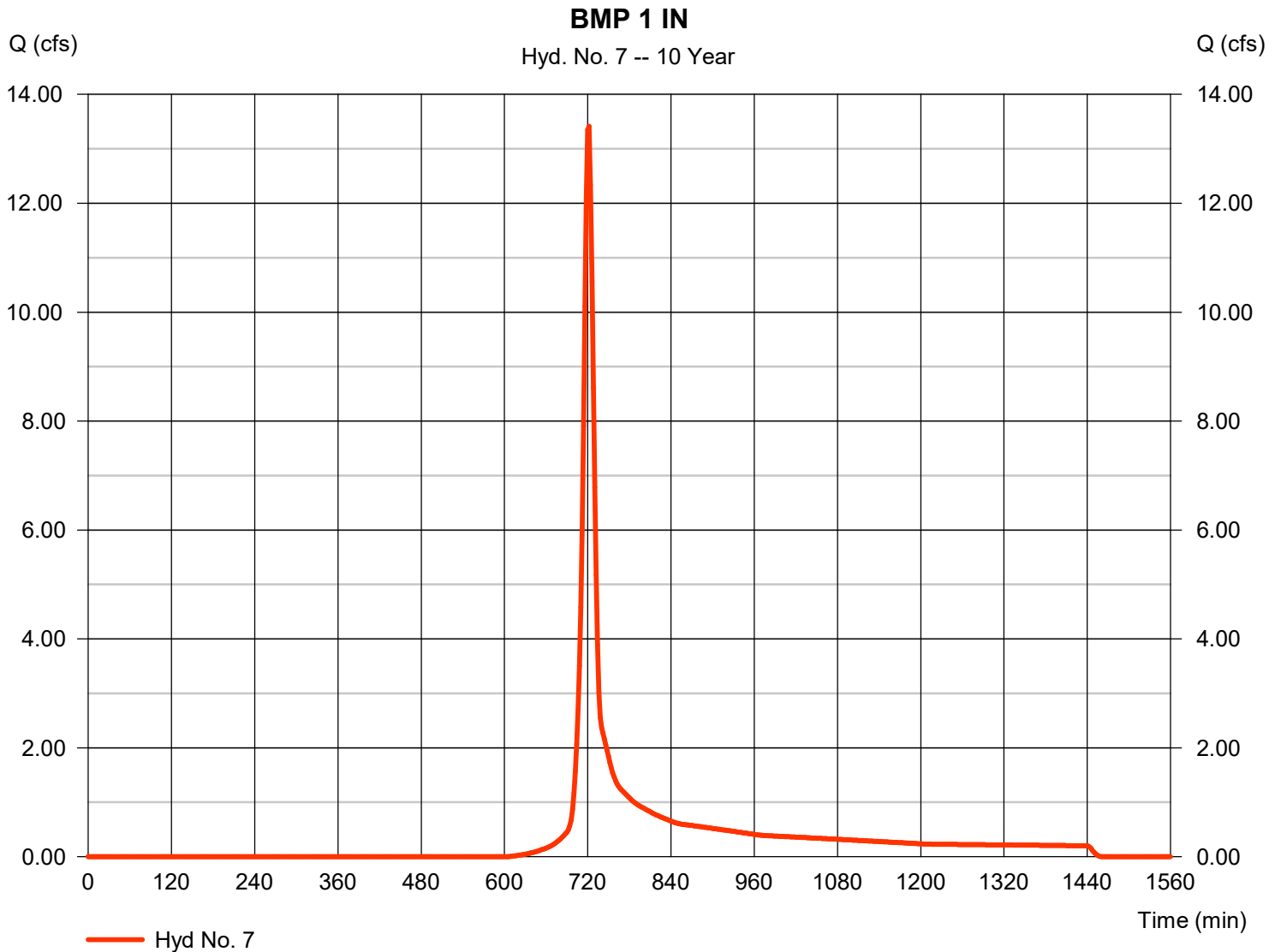


# Hydrograph Report

## Hyd. No. 7

BMP 1 IN

Hydrograph type	= SCS Runoff	Peak discharge	= 13.41 cfs
Storm frequency	= 10 yrs	Time to peak	= 722 min
Time interval	= 2 min	Hyd. volume	= 35,221 cuft
Drainage area	= 4.980 ac	Curve number	= 70
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 13.00 min
Total precip.	= 4.80 in	Distribution	= Type II
Storm duration	= 24 hrs	Shape factor	= 484





# Hydrograph Report

Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2022

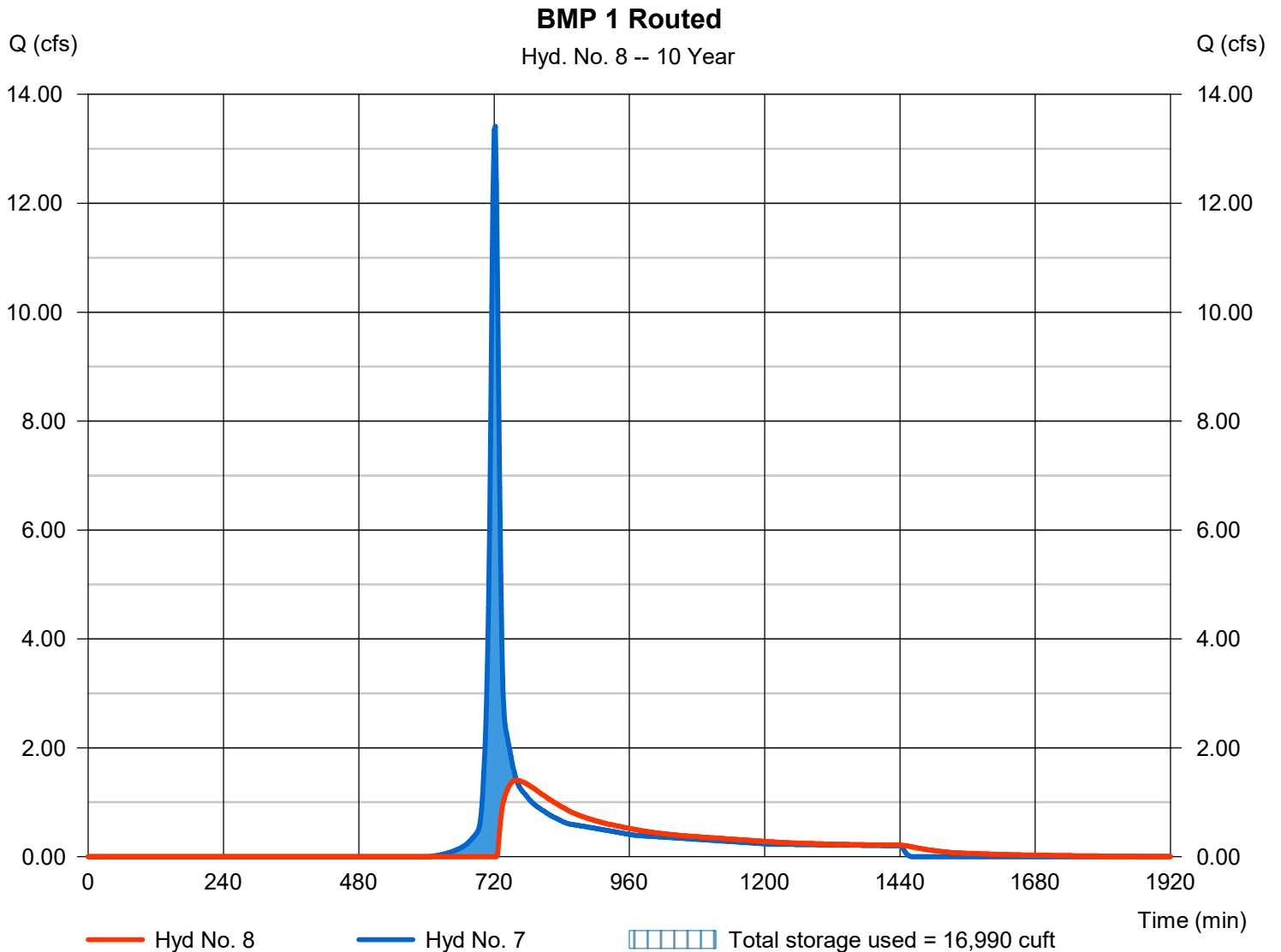
Monday, 01 / 16 / 2023

## Hyd. No. 8

BMP 1 Routed

Hydrograph type	= Reservoir	Peak discharge	= 1.405 cfs
Storm frequency	= 10 yrs	Time to peak	= 760 min
Time interval	= 2 min	Hyd. volume	= 23,010 cuft
Inflow hyd. No.	= 7 - BMP 1 IN	Max. Elevation	= 290.85 ft
Reservoir name	= BMP 1	Max. Storage	= 16,990 cuft

Storage Indication method used.

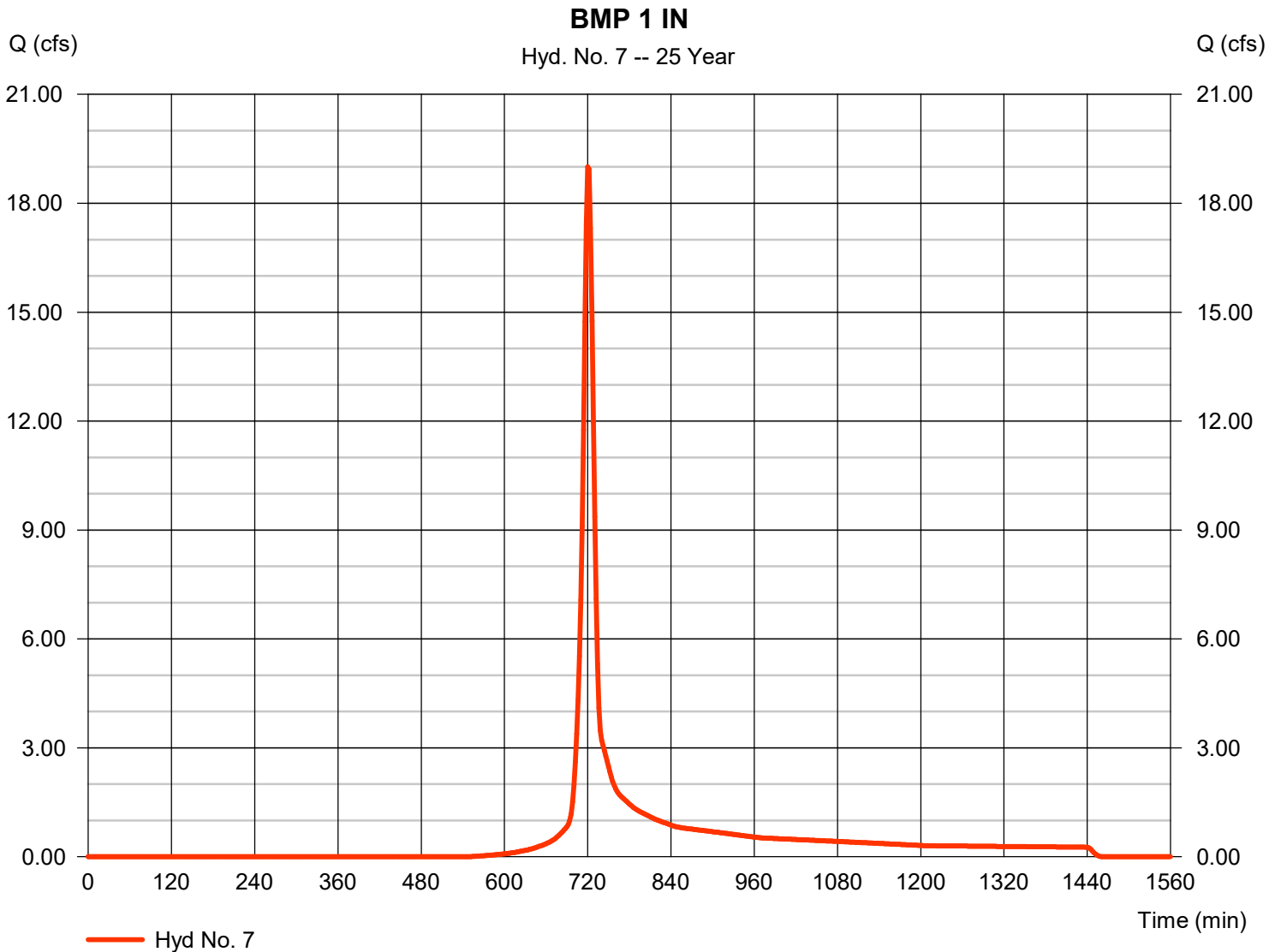


# Hydrograph Report

## Hyd. No. 7

BMP 1 IN

Hydrograph type	= SCS Runoff	Peak discharge	= 19.00 cfs
Storm frequency	= 25 yrs	Time to peak	= 720 min
Time interval	= 2 min	Hyd. volume	= 49,500 cuft
Drainage area	= 4.980 ac	Curve number	= 70
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 13.00 min
Total precip.	= 5.81 in	Distribution	= Type II
Storm duration	= 24 hrs	Shape factor	= 484



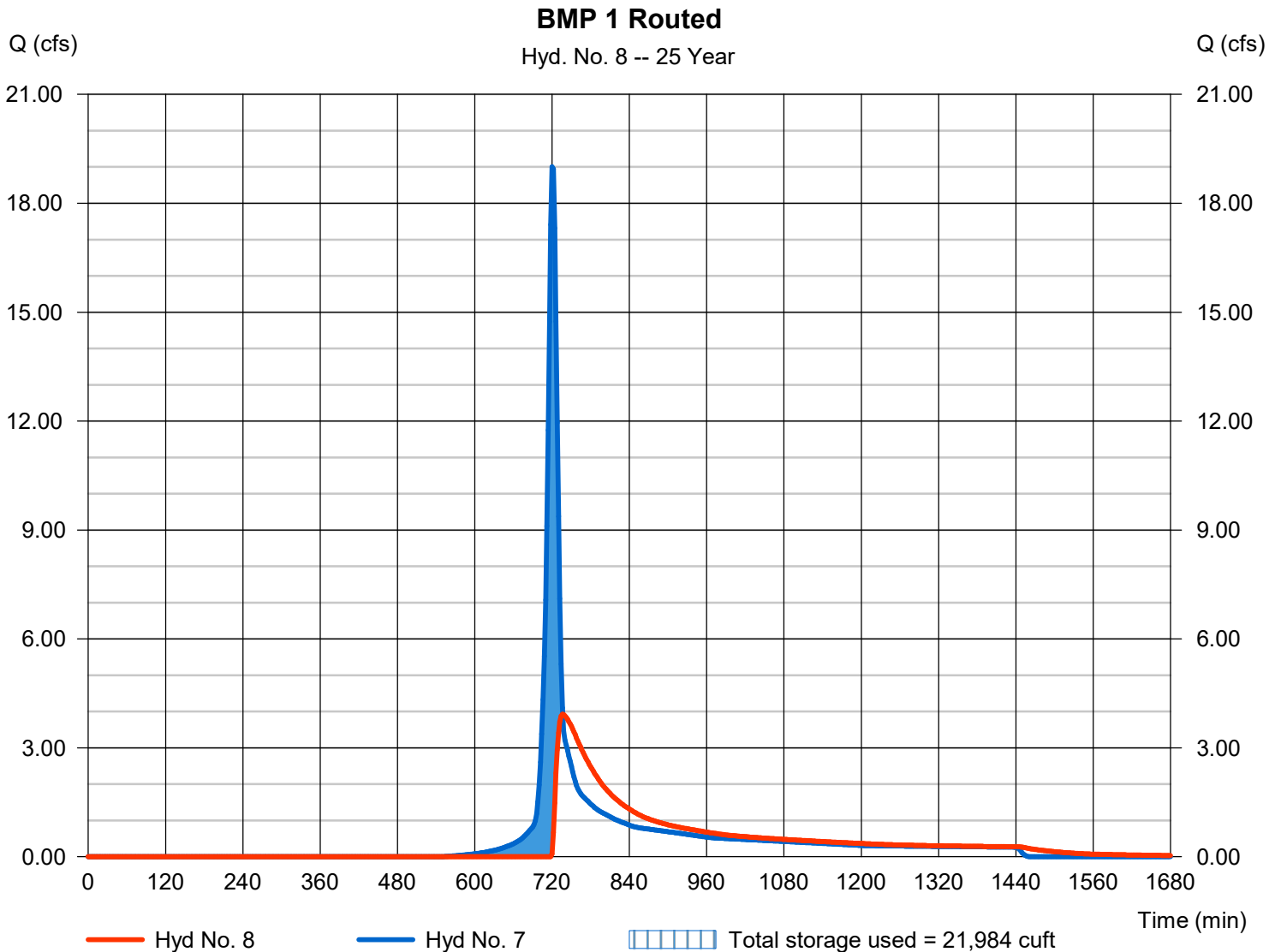
# Hydrograph Report

## Hyd. No. 8

BMP 1 Routed

Hydrograph type	= Reservoir	Peak discharge	= 3.929 cfs
Storm frequency	= 25 yrs	Time to peak	= 736 min
Time interval	= 2 min	Hyd. volume	= 37,290 cuft
Inflow hyd. No.	= 7 - BMP 1 IN	Max. Elevation	= 291.20 ft
Reservoir name	= BMP 1	Max. Storage	= 21,984 cuft

Storage Indication method used.

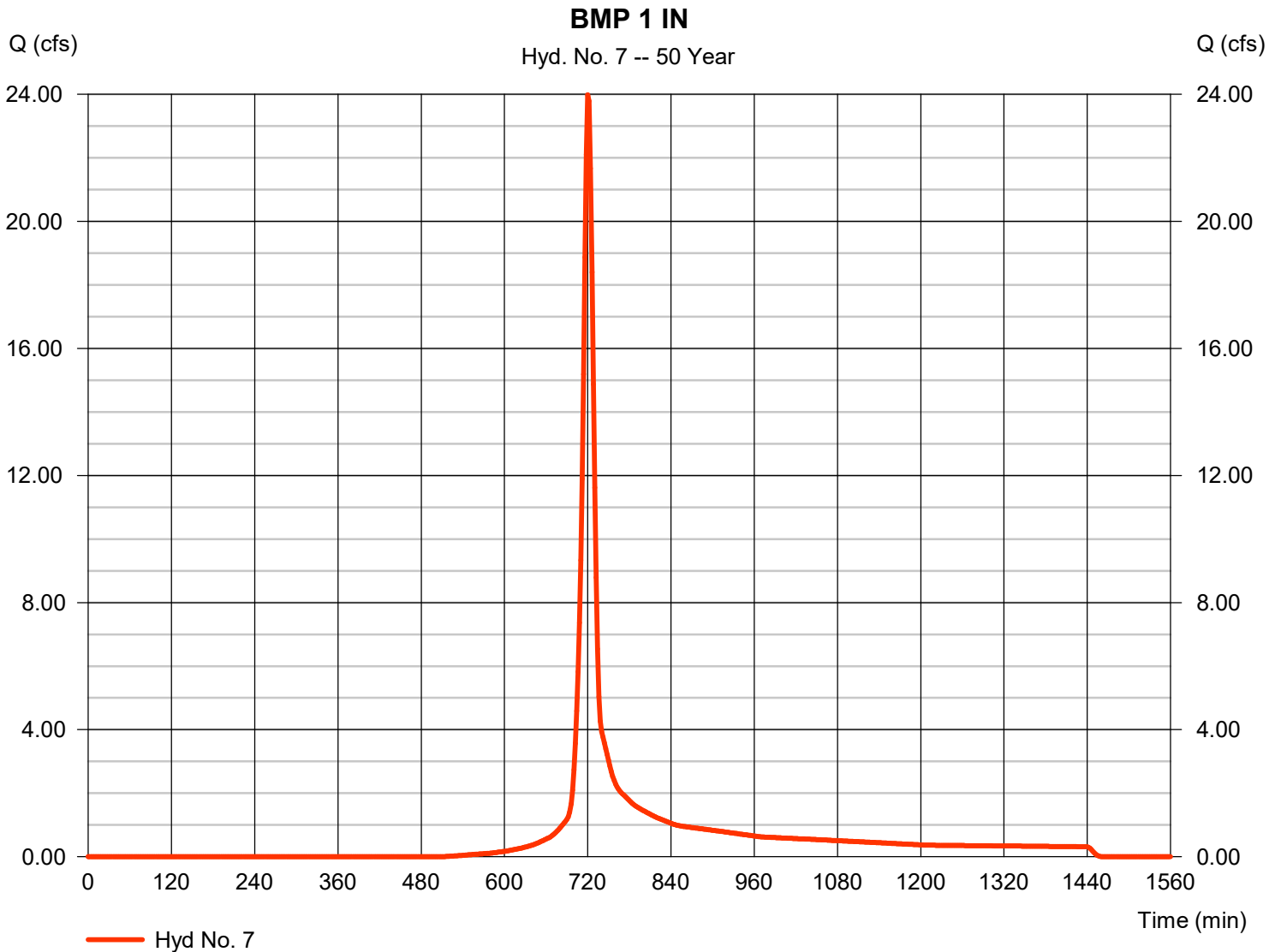


# Hydrograph Report

## Hyd. No. 7

BMP 1 IN

Hydrograph type	= SCS Runoff	Peak discharge	= 23.98 cfs
Storm frequency	= 50 yrs	Time to peak	= 720 min
Time interval	= 2 min	Hyd. volume	= 62,223 cuft
Drainage area	= 4.980 ac	Curve number	= 70
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 13.00 min
Total precip.	= 6.66 in	Distribution	= Type II
Storm duration	= 24 hrs	Shape factor	= 484



# Hydrograph Report

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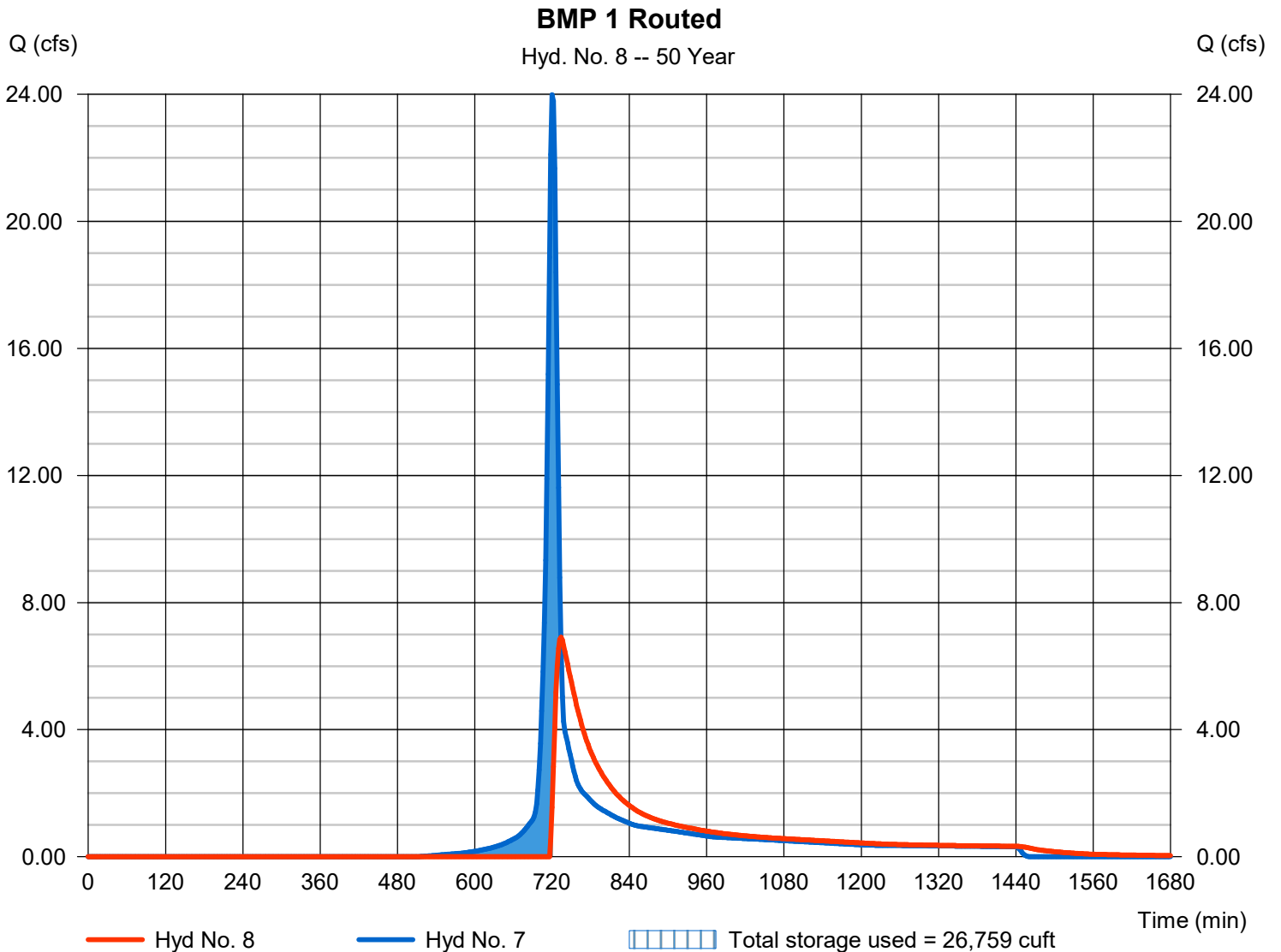
Monday, 01 / 16 / 2023

## Hyd. No. 8

BMP 1 Routed

Hydrograph type	= Reservoir	Peak discharge	= 6.906 cfs
Storm frequency	= 50 yrs	Time to peak	= 734 min
Time interval	= 2 min	Hyd. volume	= 50,013 cuft
Inflow hyd. No.	= 7 - BMP 1 IN	Max. Elevation	= 291.52 ft
Reservoir name	= BMP 1	Max. Storage	= 26,759 cuft

Storage Indication method used.

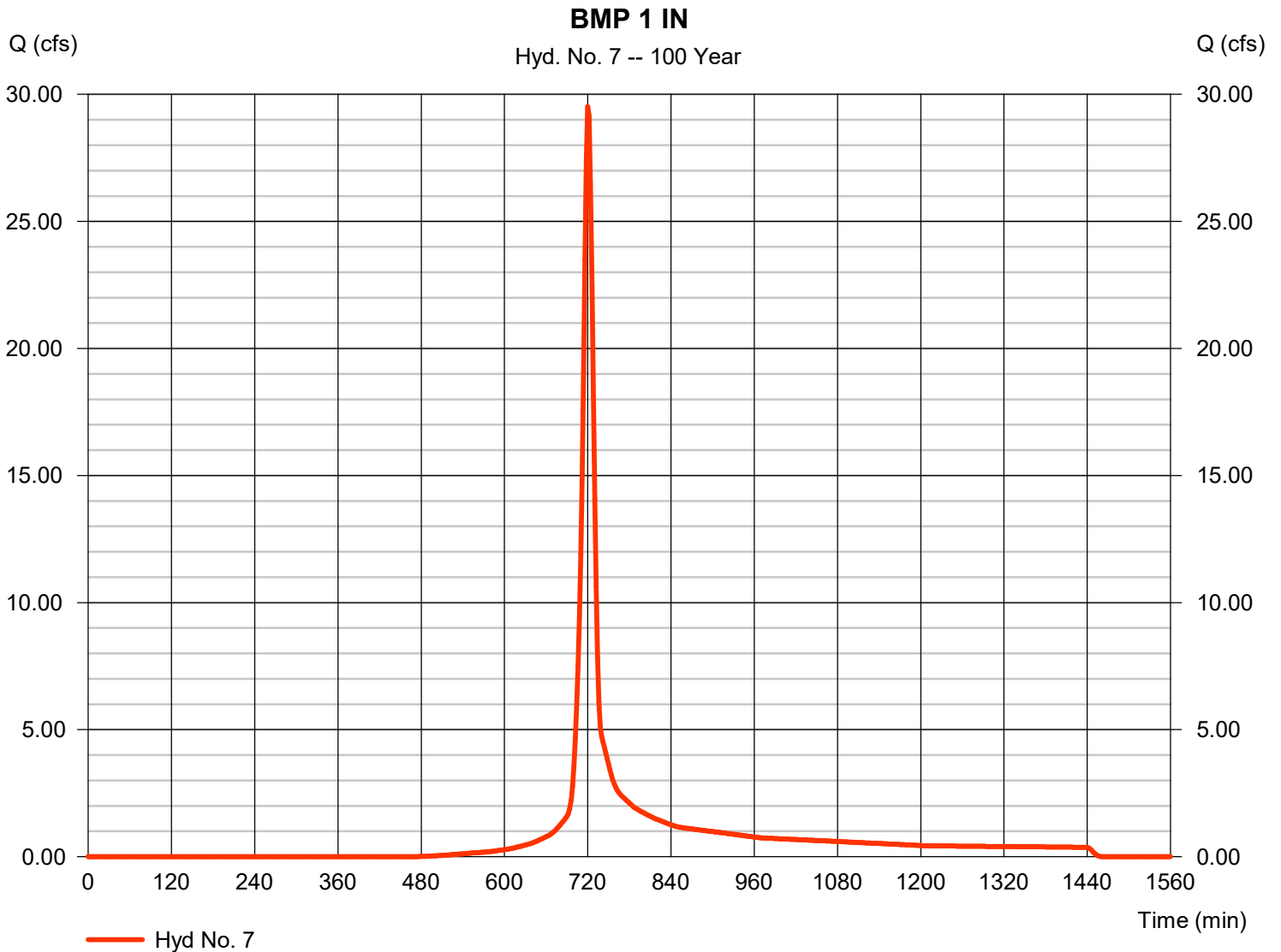


# Hydrograph Report

## Hyd. No. 7

BMP 1 IN

Hydrograph type	= SCS Runoff	Peak discharge	= 29.52 cfs
Storm frequency	= 100 yrs	Time to peak	= 720 min
Time interval	= 2 min	Hyd. volume	= 76,538 cuft
Drainage area	= 4.980 ac	Curve number	= 70
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 13.00 min
Total precip.	= 7.58 in	Distribution	= Type II
Storm duration	= 24 hrs	Shape factor	= 484



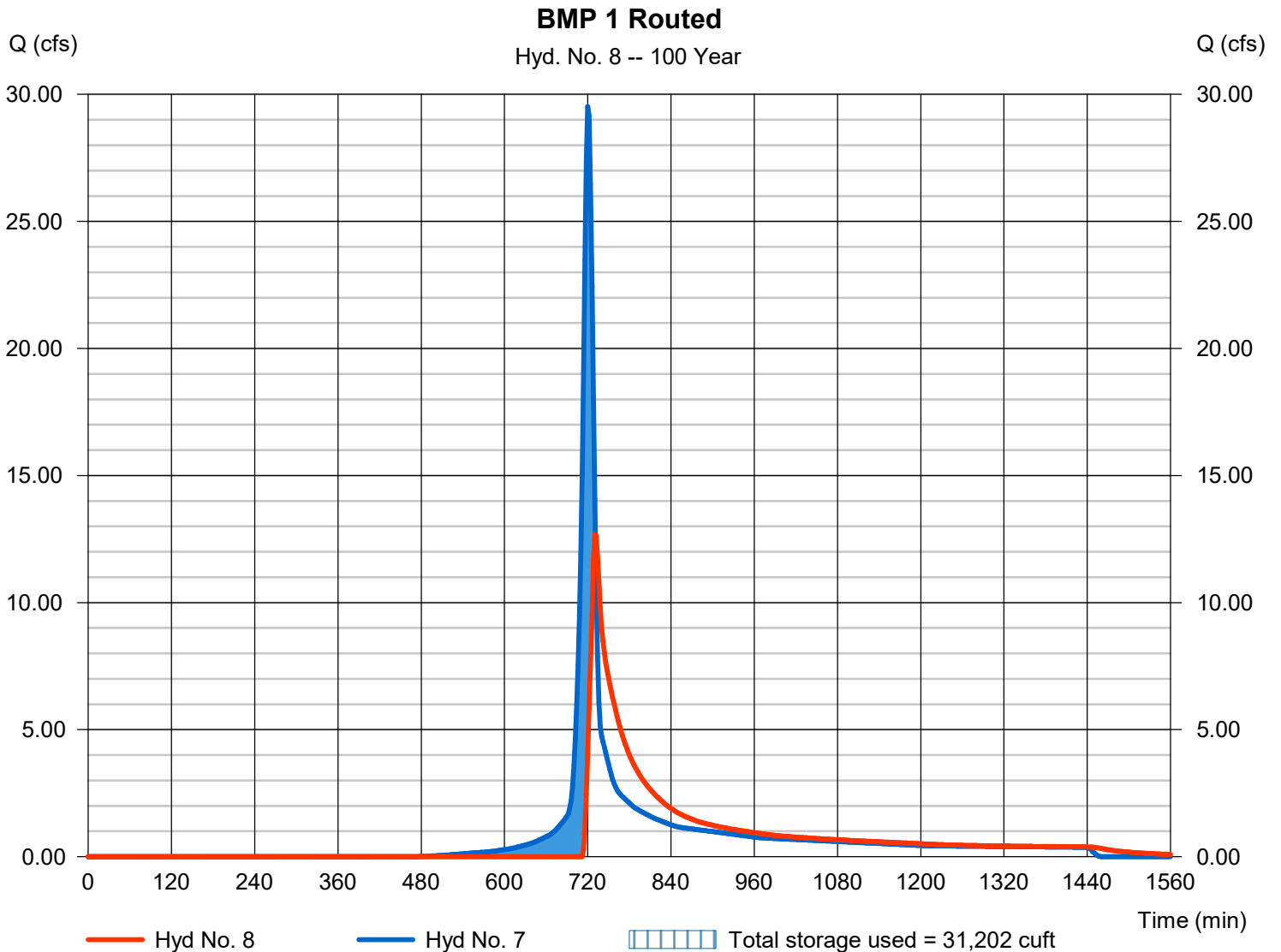
# Hydrograph Report

## Hyd. No. 8

BMP 1 Routed

Hydrograph type	= Reservoir	Peak discharge	= 12.69 cfs
Storm frequency	= 100 yrs	Time to peak	= 730 min
Time interval	= 2 min	Hyd. volume	= 64,328 cuft
Inflow hyd. No.	= 7 - BMP 1 IN	Max. Elevation	= 291.82 ft
Reservoir name	= BMP 1	Max. Storage	= 31,202 cuft

Storage Indication method used.

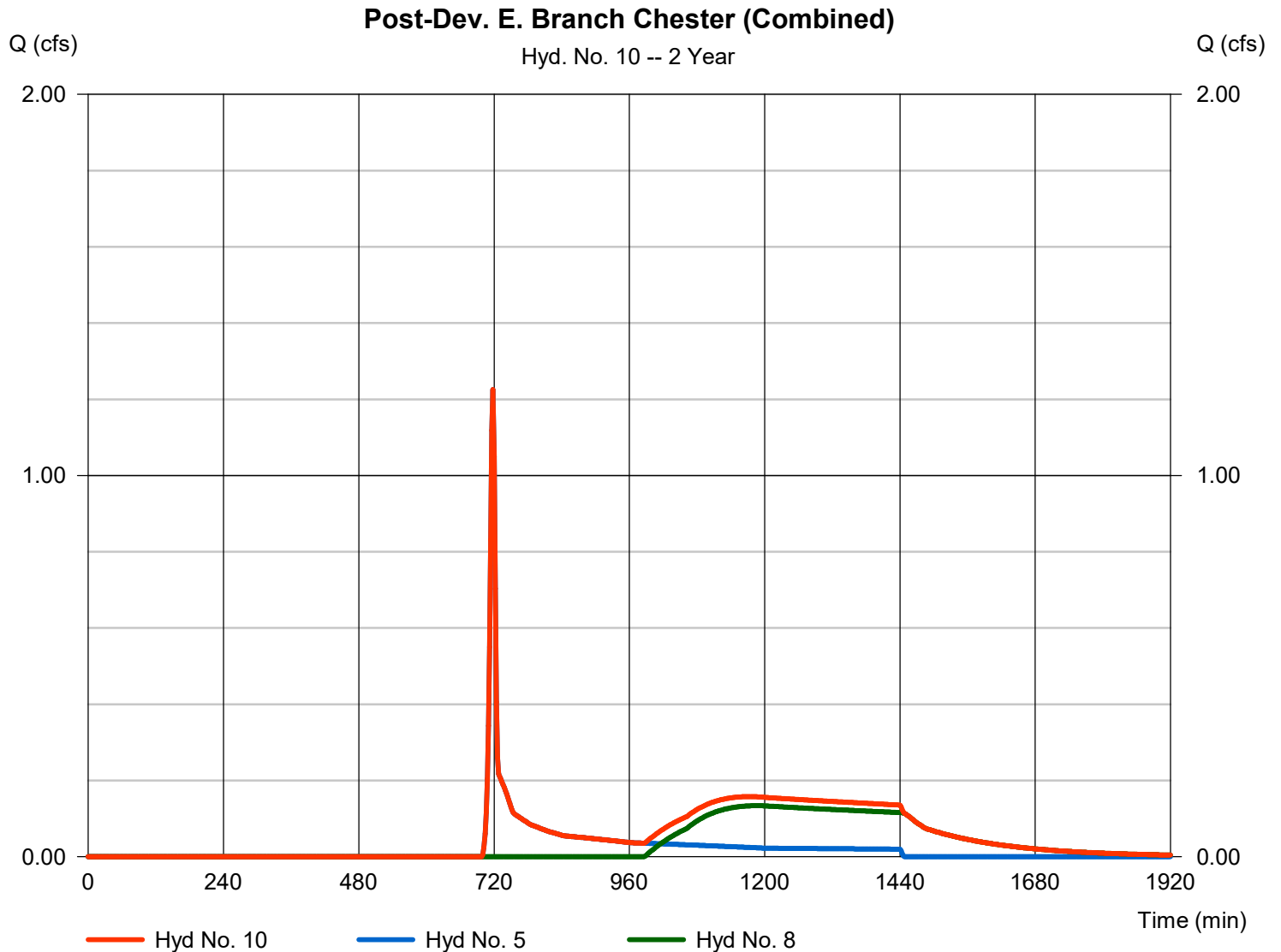


# Hydrograph Report

## Hyd. No. 10

Post-Dev. E. Branch Chester (Combined)

Hydrograph type	= Combine	Peak discharge	= 1.225 cfs
Storm frequency	= 2 yrs	Time to peak	= 718 min
Time interval	= 2 min	Hyd. volume	= 6,472 cuft
Inflow hyds.	= 5, 8	Contrib. drain. area	= 1.130 ac





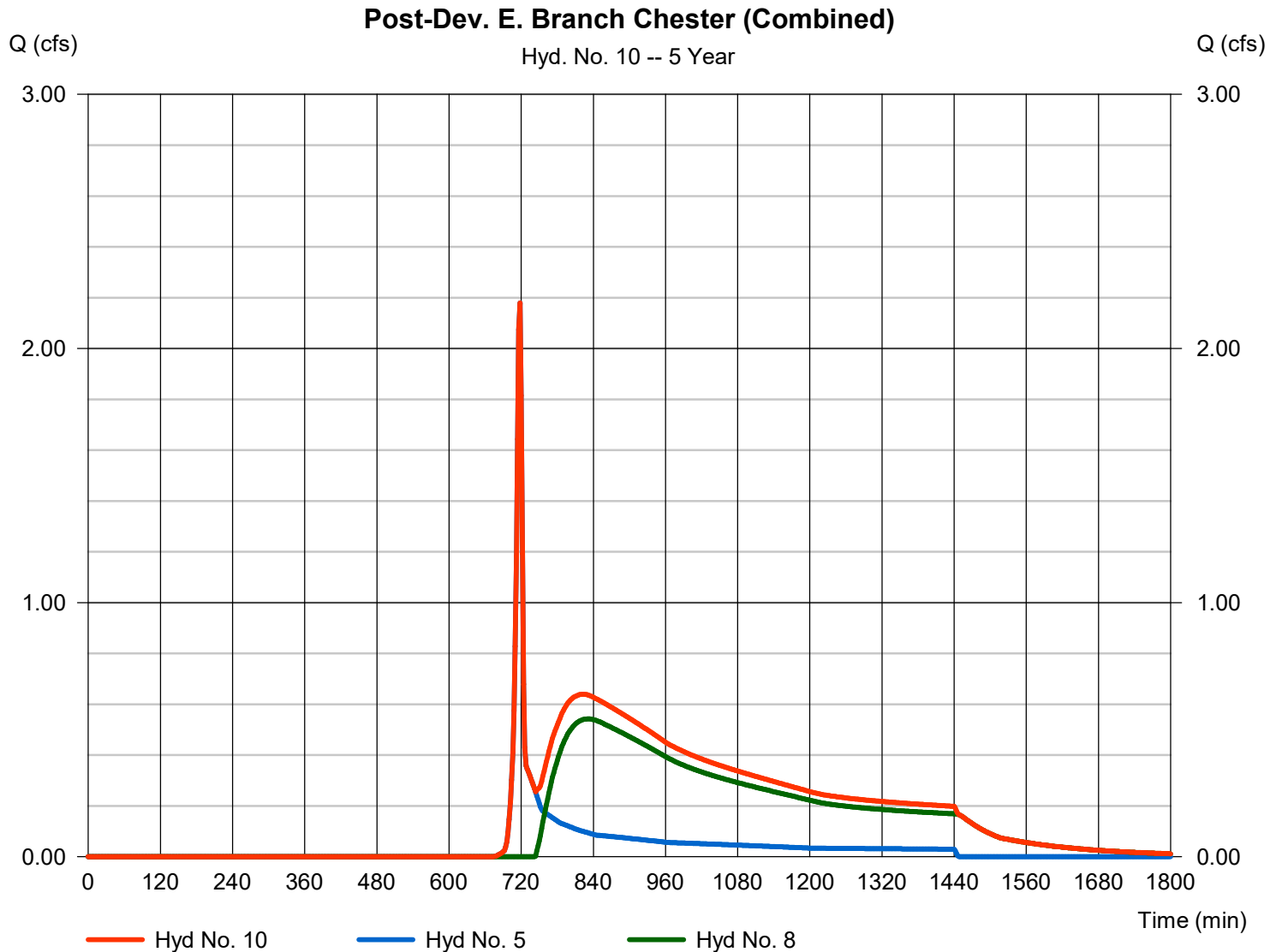
# Hydrograph Report

## Hyd. No. 10

Post-Dev. E. Branch Chester (Combined)

Hydrograph type = Combine  
Storm frequency = 5 yrs  
Time interval = 2 min  
Inflow hyds. = 5, 8

Peak discharge = 2.179 cfs  
Time to peak = 718 min  
Hyd. volume = 18,238 cuft  
Contrib. drain. area = 1.130 ac



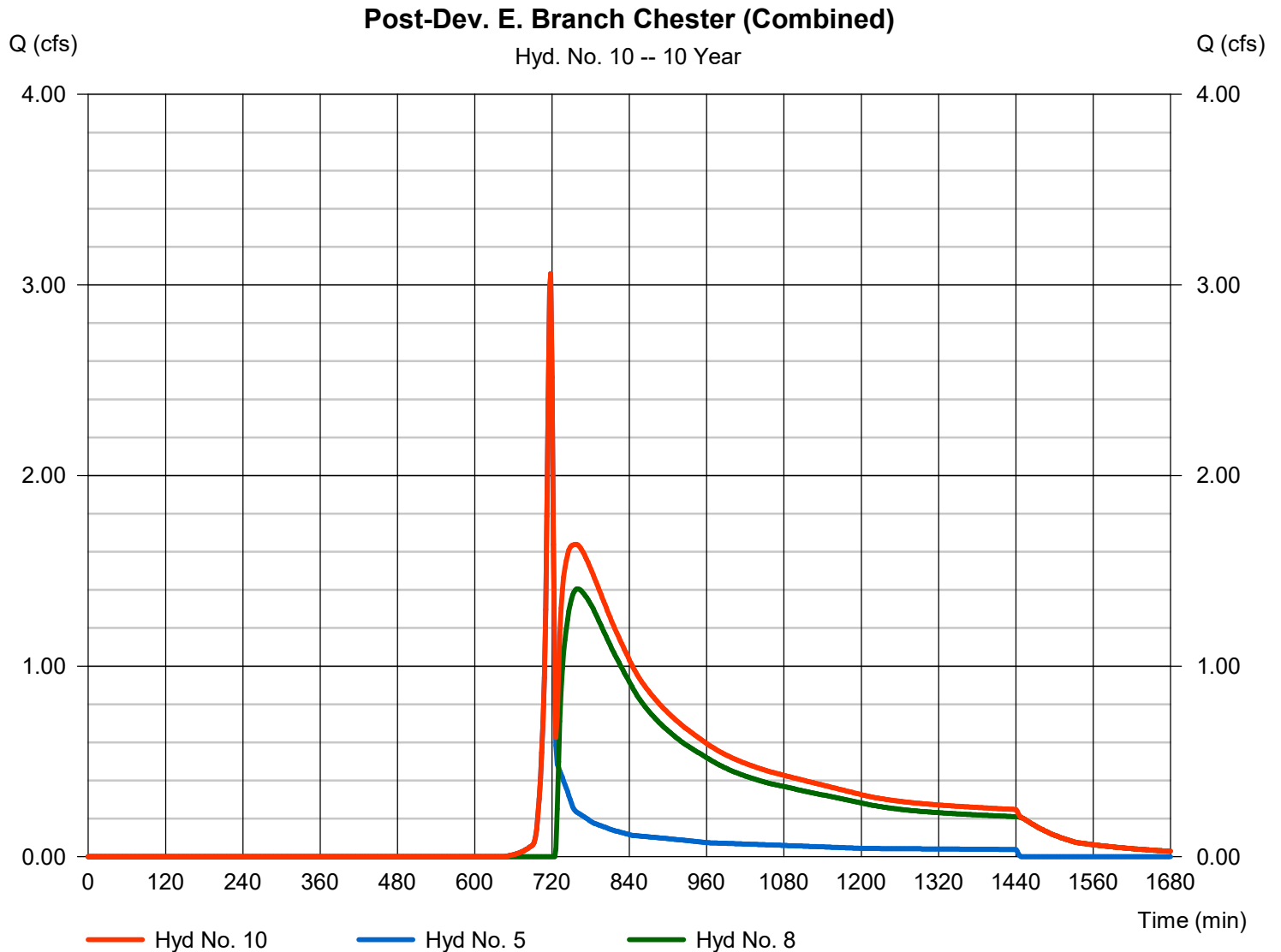
# Hydrograph Report

## Hyd. No. 10

Post-Dev. E. Branch Chester (Combined)

Hydrograph type = Combine  
Storm frequency = 10 yrs  
Time interval = 2 min  
Inflow hyds. = 5, 8

Peak discharge = 3.059 cfs  
Time to peak = 718 min  
Hyd. volume = 29,136 cuft  
Contrib. drain. area = 1.130 ac

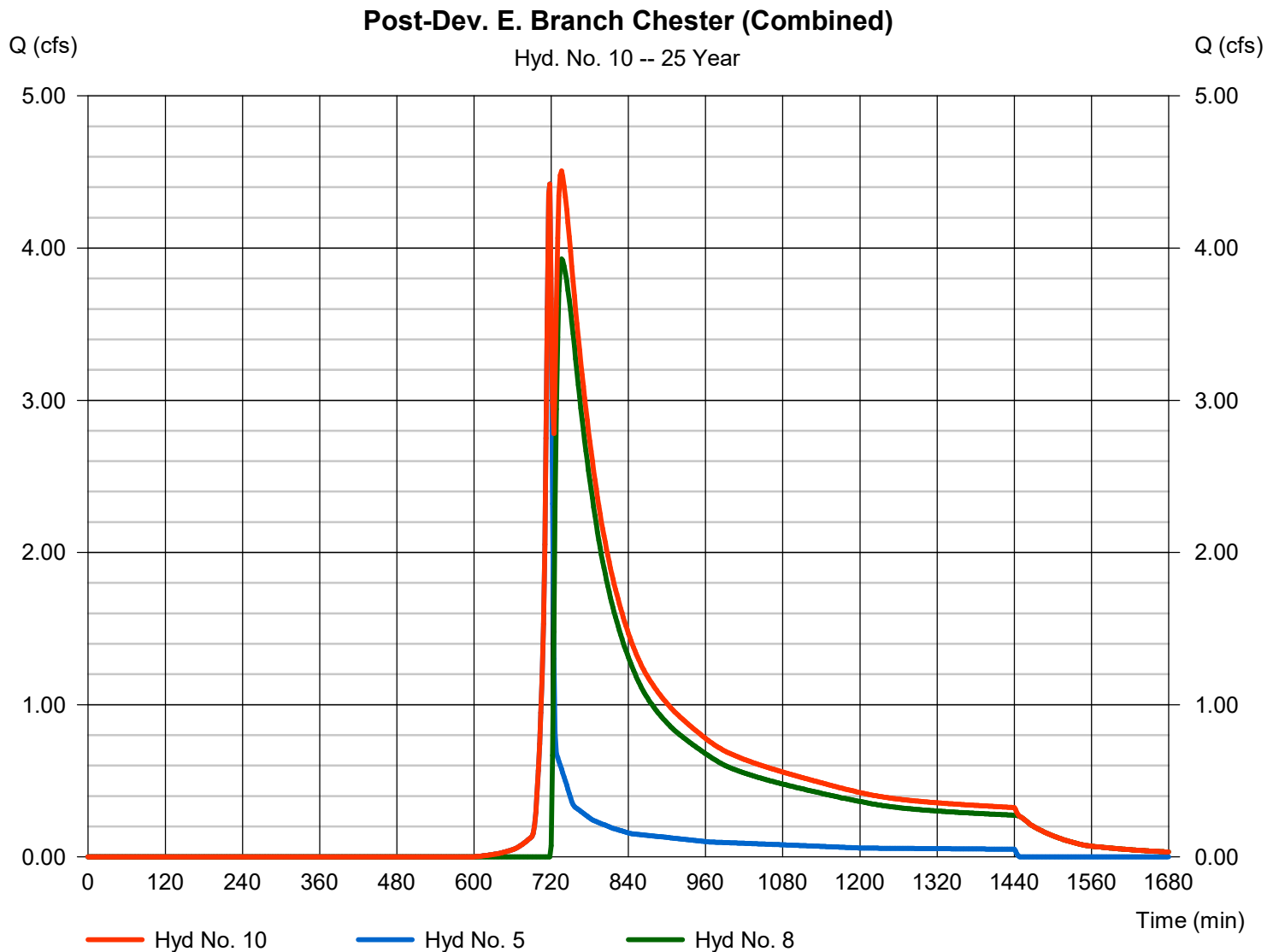


# Hydrograph Report

## Hyd. No. 10

Post-Dev. E. Branch Chester (Combined)

Hydrograph type	= Combine	Peak discharge	= 4.506 cfs
Storm frequency	= 25 yrs	Time to peak	= 736 min
Time interval	= 2 min	Hyd. volume	= 46,136 cuft
Inflow hyds.	= 5, 8	Contrib. drain. area	= 1.130 ac



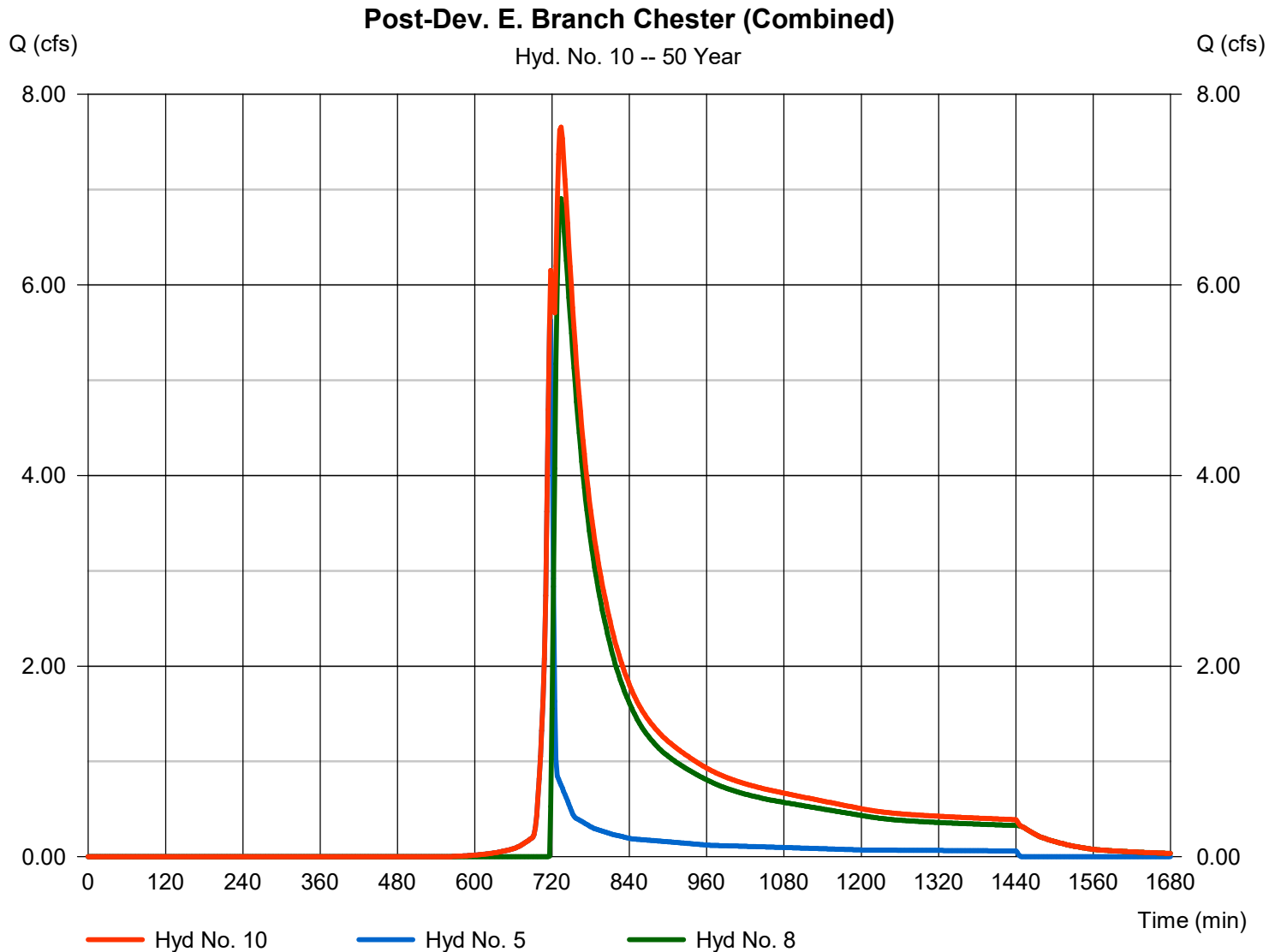
# Hydrograph Report

## Hyd. No. 10

Post-Dev. E. Branch Chester (Combined)

Hydrograph type = Combine  
Storm frequency = 50 yrs  
Time interval = 2 min  
Inflow hyds. = 5, 8

Peak discharge = 7.657 cfs  
Time to peak = 734 min  
Hyd. volume = 61,318 cuft  
Contrib. drain. area = 1.130 ac



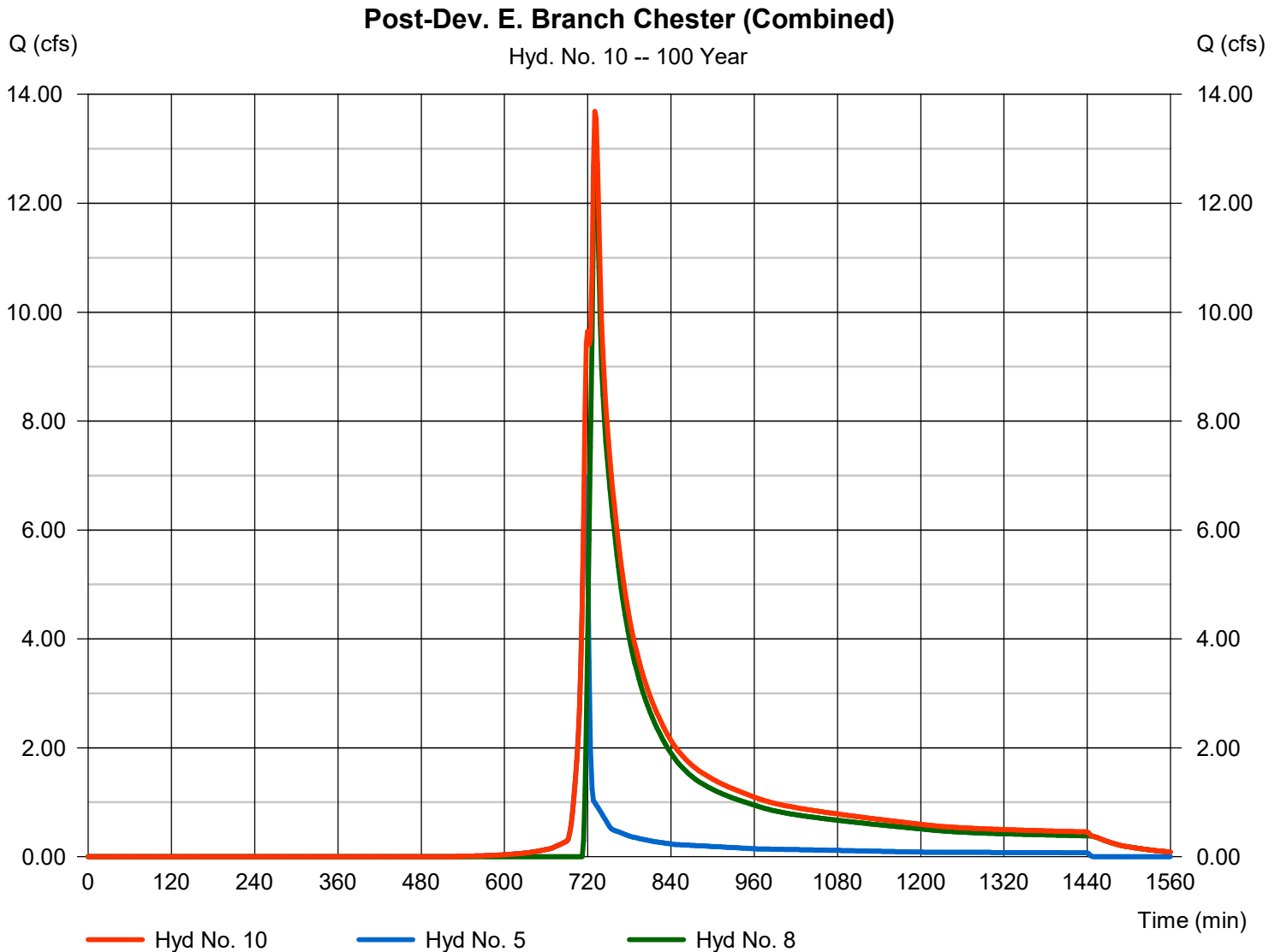
# Hydrograph Report

## Hyd. No. 10

Post-Dev. E. Branch Chester (Combined)

Hydrograph type = Combine  
Storm frequency = 100 yrs  
Time interval = 2 min  
Inflow hyds. = 5, 8

Peak discharge = 13.69 cfs  
Time to peak = 730 min  
Hyd. volume = 78,426 cuft  
Contrib. drain. area = 1.130 ac



## **UNT. TO EAST BRANCH CHESTER CREEK**

# ELA SPORT

ATHLETIC FACILITIES  
DESIGN & CONSULTING

737 S. BROAD STREET  
LITITZ, PA 17543  
(717) 626-72713

# NRCS (SCS) TR-55- WATERSHED WEIGHTED CURVE NUMBER POST-DEVELOPMENT SUMMARY

PROJECT: The Westtown School - Oak Lane Project  
LOCATION: Westtown Township  
COUNTY: Chester



LAND USE	Area (ac)						Total Area (ac.)	Composite 'CN' Value	Tc Min.
	Parking, Other Impervious (Disturbed Area)	Parking, Other Impervious (Undisturbed Area)	Open Space (Disturbed Area)	Open Space (Undisturbed Area)	Open Space (Disturbed Area)	Open Space (Undisturbed Area)			
HSG	B	B	B	B	D	D			
"CN" Value	98	98	61	61	80	80			
<b>WATERSHED</b>									
Infiltration Basin - BMP 4	0.36	0.00	6.01	1.94	0.87	0.56	9.74	65	22
Infiltration Bed - BMP 2	2.22	0.00	0.00	0.00	0.00	0.00	2.22	98	5
Infiltration Bed - BMP 3	2.22	0.00	0.00	0.00	0.00	0.00	2.22	98	5
Undetained	0.01	0.00	2.07	0.00	0.66	0.00	2.74	66	12



**ELA SPORT**  
**ATHLETIC FACILITIES**  
**DESIGN & CONSULTING**

737 S. BROAD STREET  
 LITITZ, PA 17543  
 (717) 626-72713

**SUMMARY - SUBAREAS TIME OF CONCENTRATION PRE-DEVELOPMENT CONDITIONS**

PROJECT: The Westtown School - Oak Lane Project  
 LOCATION: Westtown Township  
 COUNTY: Chester

**Time of concentration (Tc) or travel time (Tt)**  
**NRCS Velocity(Segmental) Method**

Sub area	overland						Shallow Concentrated							Channel or Pipe							Total	
	Length L <sub>1</sub> 100 ft. max.	Slope S <sub>1</sub>	Manning's n	2 yr rainfall in.	Tc Min.	Flow Path Cover	Length L <sub>2</sub> ft.	Slope S <sub>2</sub> ft./ft.	Average Velocity ft./s	Tt Min.	Channel or Pipe C/P	Flow Area sq.ft.	Wetted Perimeter ft.	Pipe Diameter in.	Slope S <sub>3</sub> ft./ft.	Manning's n	Length L <sub>3</sub> ft.	Tt Min.	Tc Hrs.	Tt Min.	Tt Hrs.	
BMP 1	100	0.011	0.24	3.26	18			0	0.0	0.0	0.00	0.00						0				
				3.26	0	U	350	0.011	1.7	3.4	0.00	0.00						0				
				3.26	0	U	62	0.167	6.6	0.2	0.00	0.00						0				
					0				0	0	0.00	0.00						0				
					0				0	0	0.00	0.00						0.0				
					18					3.6								0.0			0.37	
Unt. to EBCC	100	0.040	0.24	3.26	10.7			0	0	0.0	0.00	0.00						0.0				
Undetained						U	313	0.048	3.5	1.5	0.00	0.00						0.0				
					0				0	0	0.00	0.00						0.0				
					0				0	0	0.00	0.00						0.0				
					0				0	0	0.00	0.00						0.0				
					0				0	0	0.00	0.00						0.0				
					0				0	0	0.00	0.00						0.0				
					0				0	0	0.00	0.00						0.0				
					10.7				0	1.5	0.00	0.00						0.0			0.20	
																		0			12	
																					0.20	

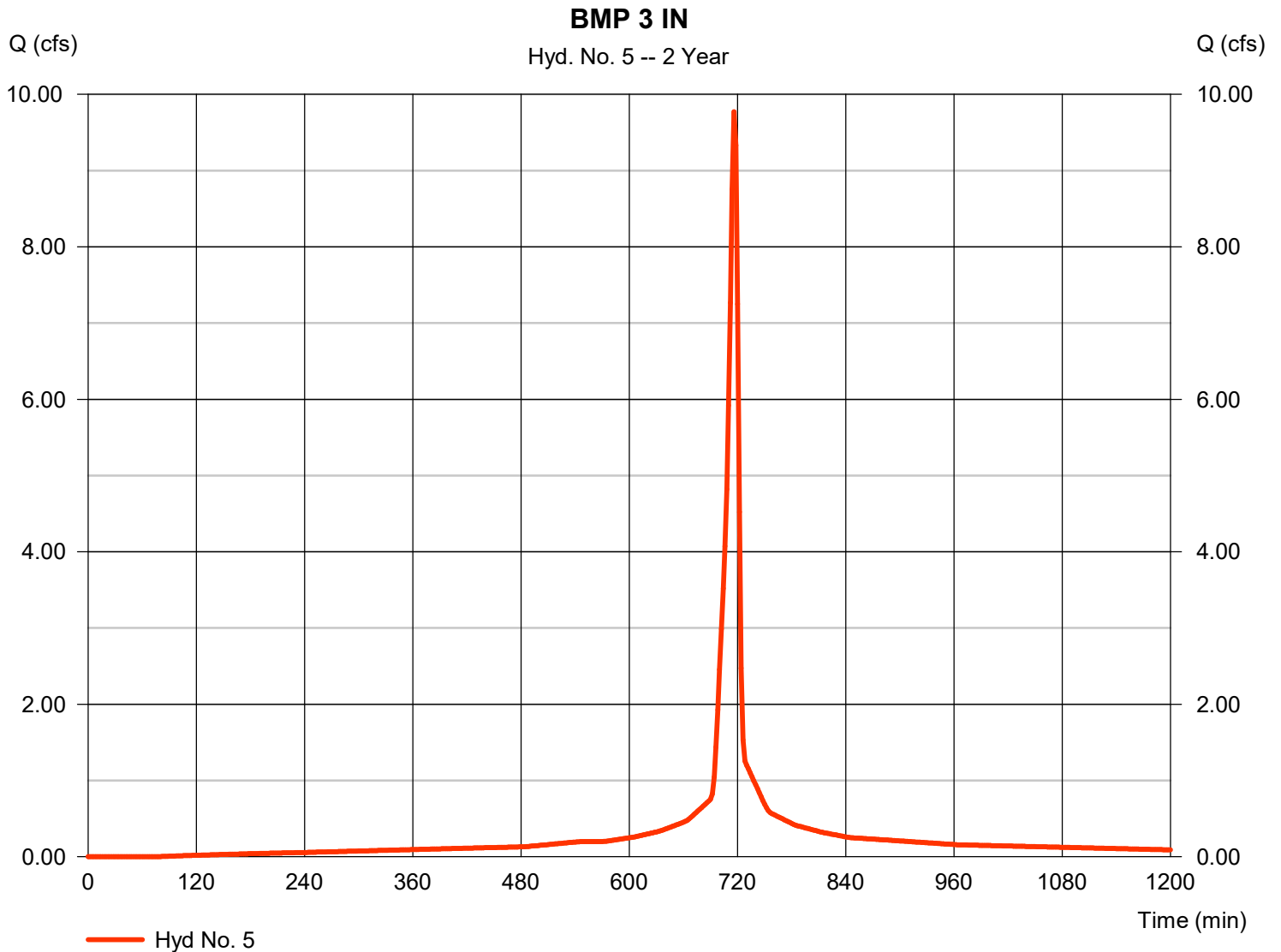


# Hydrograph Report

## Hyd. No. 5

BMP 3 IN

Hydrograph type	= SCS Runoff	Peak discharge	= 9.771 cfs
Storm frequency	= 2 yrs	Time to peak	= 716 min
Time interval	= 2 min	Hyd. volume	= 22,871 cuft
Drainage area	= 2.220 ac	Curve number	= 98
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 5.00 min
Total precip.	= 3.26 in	Distribution	= Type II
Storm duration	= 24 hrs	Shape factor	= 484



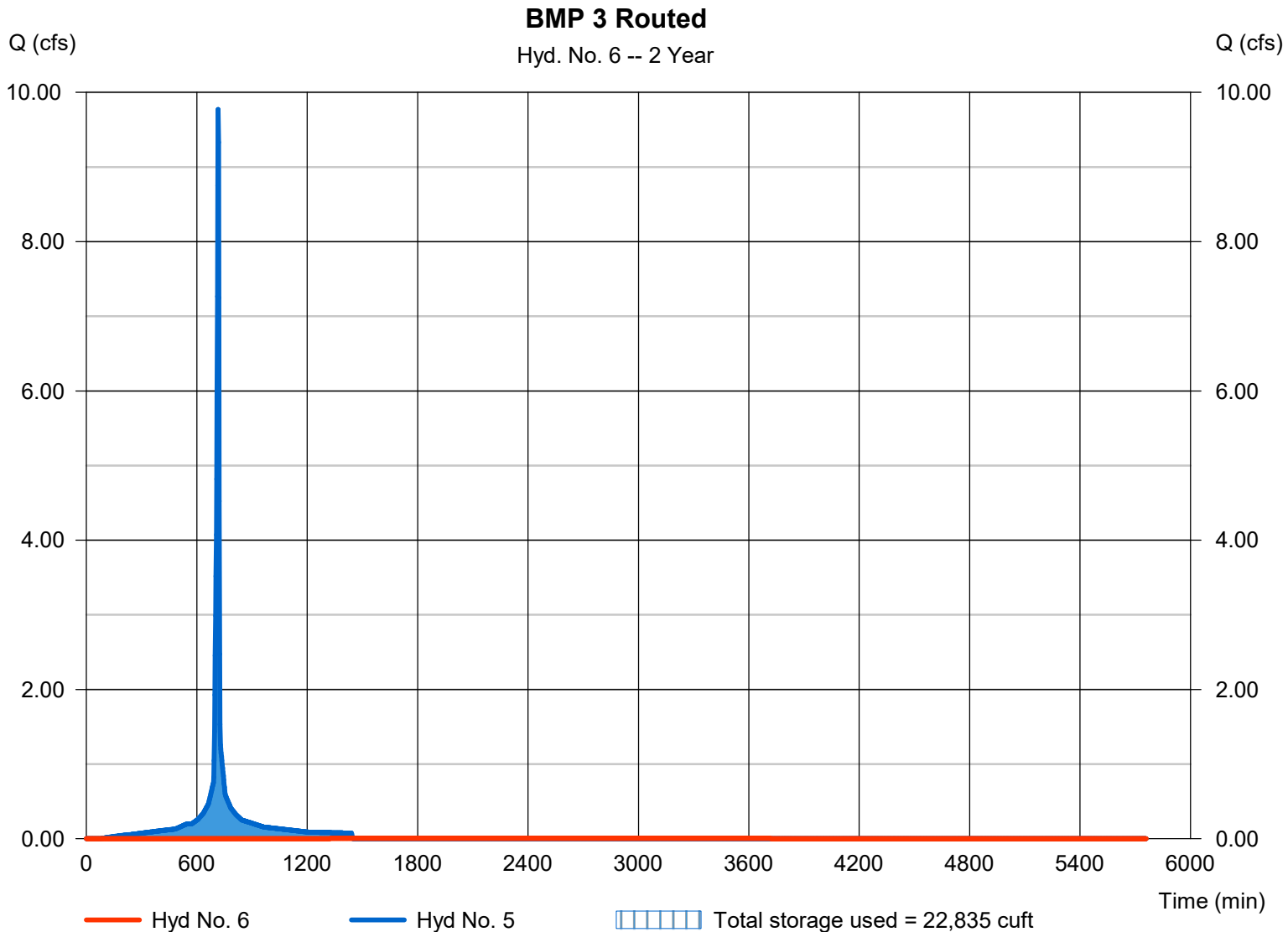
# Hydrograph Report

## Hyd. No. 6

BMP 3 Routed

Hydrograph type	= Reservoir	Peak discharge	= 0.006 cfs
Storm frequency	= 2 yrs	Time to peak	= 1446 min
Time interval	= 2 min	Hyd. volume	= 772 cuft
Inflow hyd. No.	= 5 - BMP 3 IN	Max. Elevation	= 321.04 ft
Reservoir name	= BMP 3	Max. Storage	= 22,835 cuft

Storage Indication method used.



# Pond Report

## Pond No. 7 - BMP 3

### Pond Data

Pond storage is based on user-defined values.

### Stage / Storage Table

Stage (ft)	Elevation (ft)	Contour area (sqft)	Incr. Storage (cuft)	Total storage (cuft)
0.00	319.00	n/a	0	0
1.00	320.00	n/a	10,878	10,878
2.00	321.00	n/a	11,038	21,916
2.65	321.65	n/a	14,567	36,483
2.75	321.75	n/a	3,600	40,083
3.50	322.50	n/a	28,665	68,748

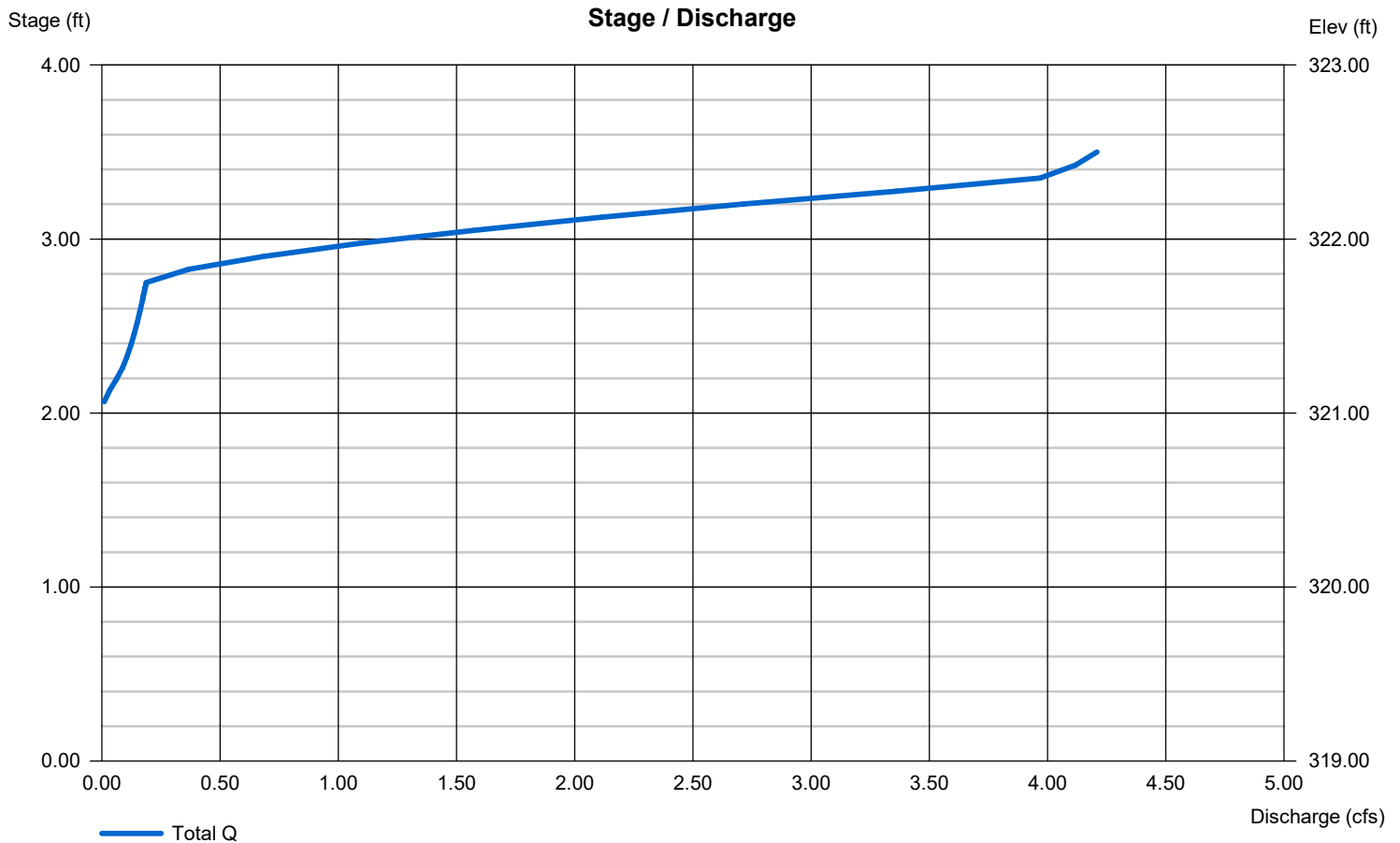
### Culvert / Orifice Structures

	[A]	[B]	[C]	[PrfRsr]
Rise (in)	= 12.00	3.00	0.00	0.00
Span (in)	= 12.00	3.00	0.00	0.00
No. Barrels	= 1	1	0	0
Invert El. (ft)	= 319.00	321.00	0.00	0.00
Length (ft)	= 245.00	0.10	0.00	0.00
Slope (%)	= 0.75	0.00	0.00	n/a
N-Value	= .013	.013	.013	n/a
Orifice Coeff.	= 0.60	0.60	0.60	0.60
Multi-Stage	= n/a	Yes	No	No

### Weir Structures

	[A]	[B]	[C]	[D]
Crest Len (ft)	= 3.14	0.00	0.00	0.00
Crest El. (ft)	= 321.75	0.00	0.00	0.00
Weir Coeff.	= 2.60	3.33	3.33	3.33
Weir Type	= Broad	---	---	---
Multi-Stage	= Yes	No	No	No
Exfil. (in/hr)	= 0.000 (by Wet area)			
TW Elev. (ft)	= 0.00			

Note: Culvert/Orifice outflows are analyzed under inlet (ic) and outlet (oc) control. Weir risers checked for orifice conditions (ic) and submergence (s).

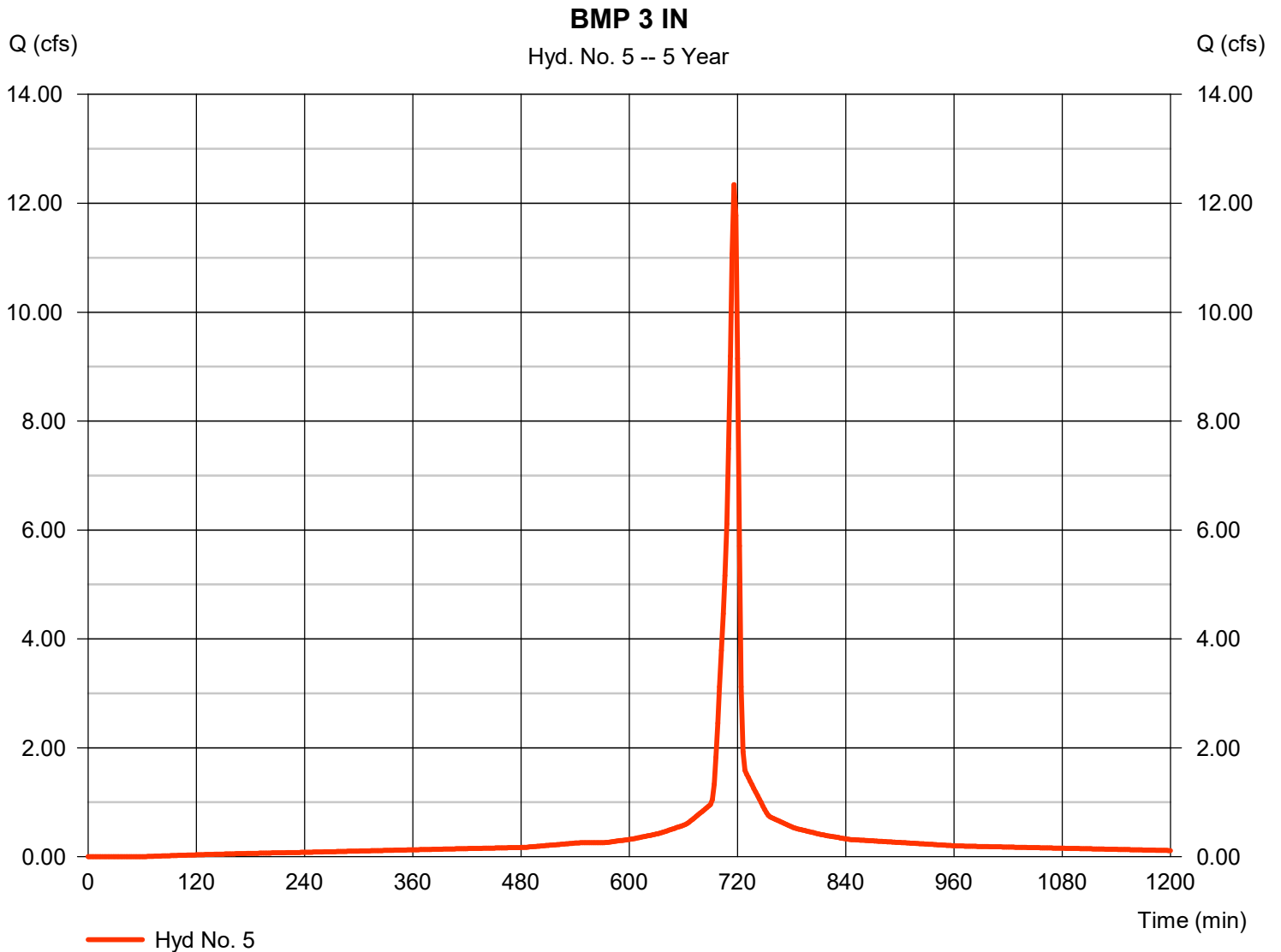


# Hydrograph Report

## Hyd. No. 5

BMP 3 IN

Hydrograph type	= SCS Runoff	Peak discharge	= 12.34 cfs
Storm frequency	= 5 yrs	Time to peak	= 716 min
Time interval	= 2 min	Hyd. volume	= 29,199 cuft
Drainage area	= 2.220 ac	Curve number	= 98
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 5.00 min
Total precip.	= 4.10 in	Distribution	= Type II
Storm duration	= 24 hrs	Shape factor	= 484



# Hydrograph Report

Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2022

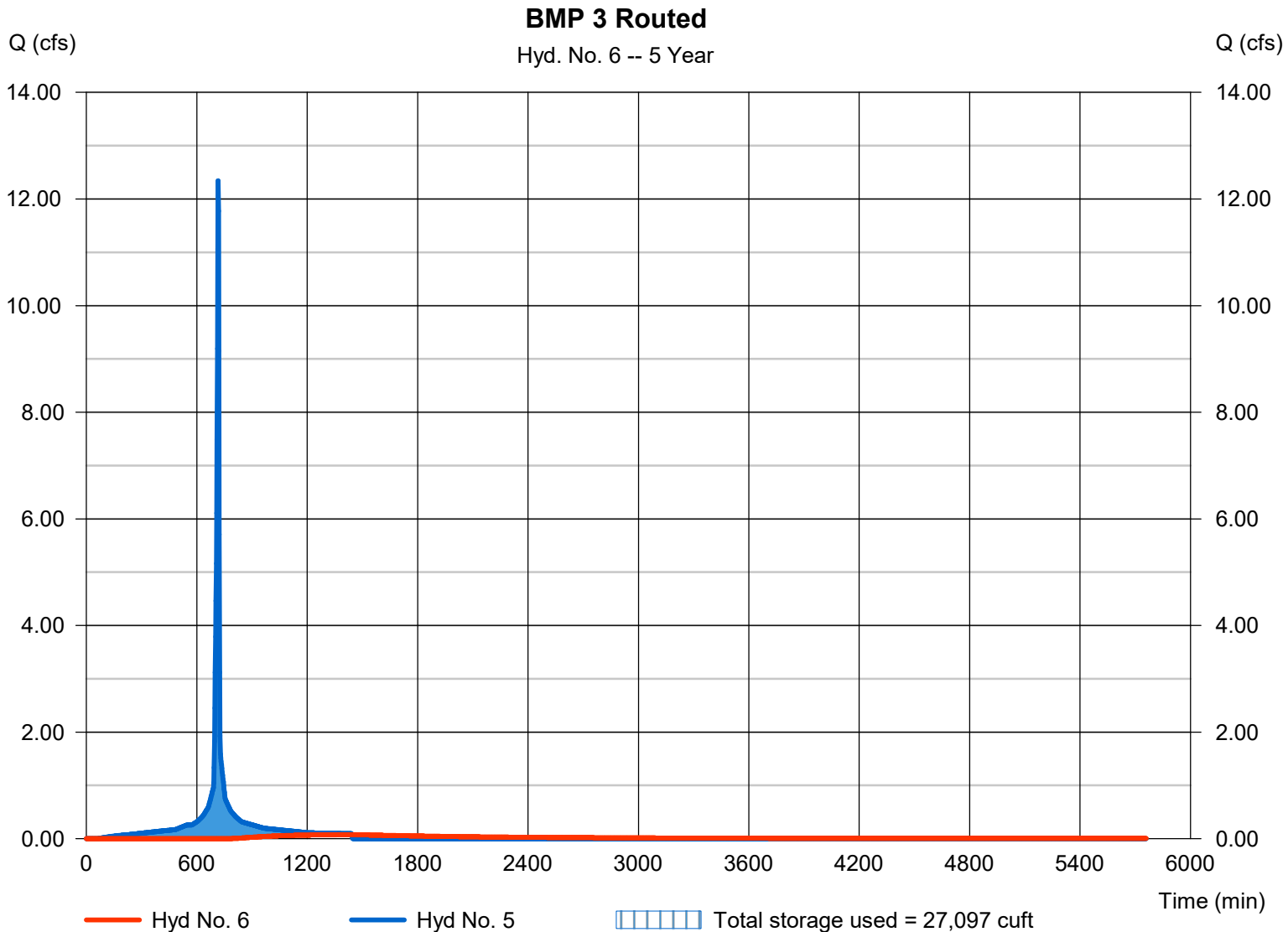
Monday, 01 / 16 / 2023

## Hyd. No. 6

BMP 3 Routed

Hydrograph type	= Reservoir	Peak discharge	= 0.076 cfs
Storm frequency	= 5 yrs	Time to peak	= 1442 min
Time interval	= 2 min	Hyd. volume	= 6,655 cuft
Inflow hyd. No.	= 5 - BMP 3 IN	Max. Elevation	= 321.23 ft
Reservoir name	= BMP 3	Max. Storage	= 27,097 cuft

Storage Indication method used.

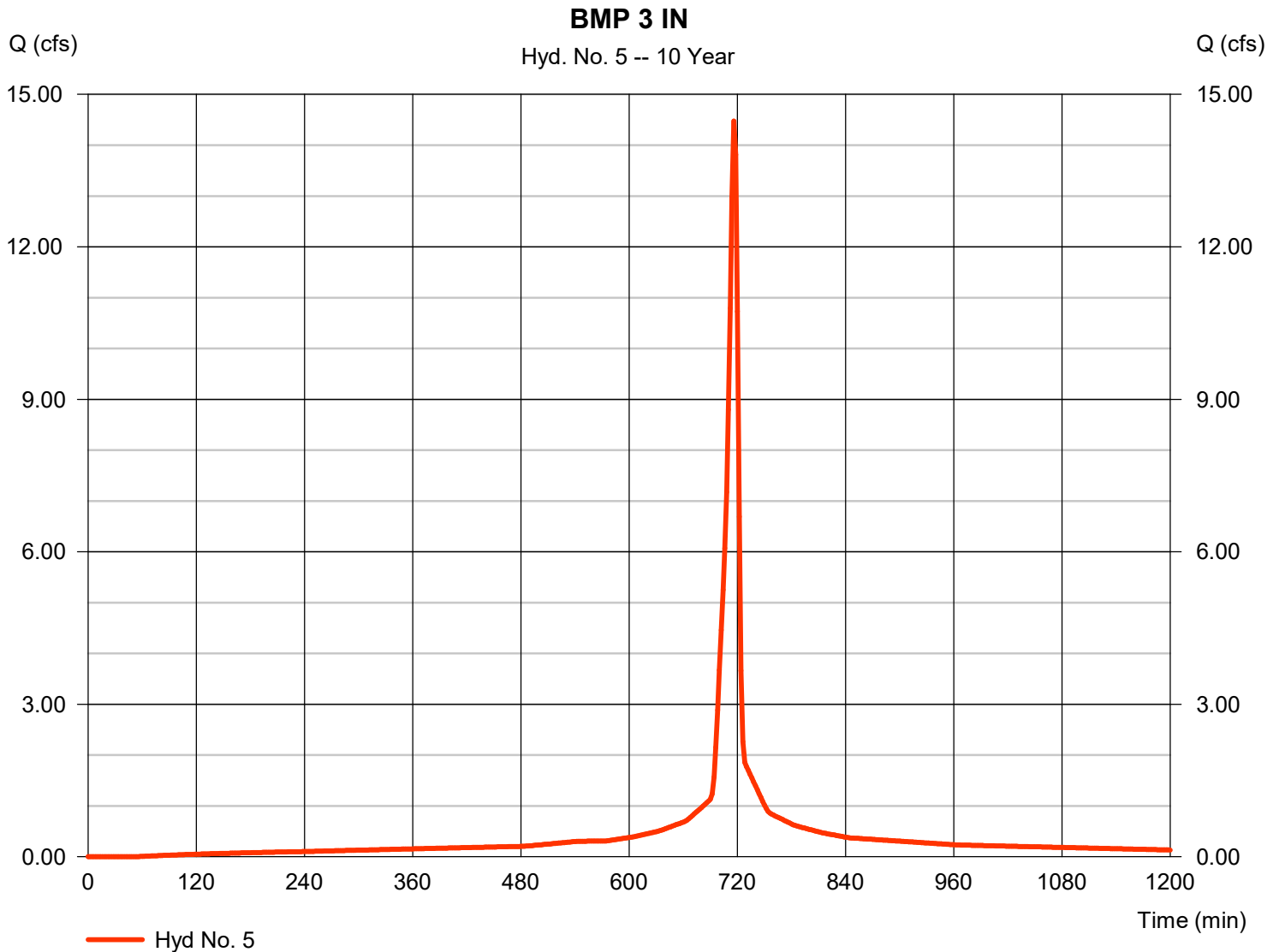


# Hydrograph Report

## Hyd. No. 5

BMP 3 IN

Hydrograph type	= SCS Runoff	Peak discharge	= 14.48 cfs
Storm frequency	= 10 yrs	Time to peak	= 716 min
Time interval	= 2 min	Hyd. volume	= 34,477 cuft
Drainage area	= 2.220 ac	Curve number	= 98
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 5.00 min
Total precip.	= 4.80 in	Distribution	= Type II
Storm duration	= 24 hrs	Shape factor	= 484



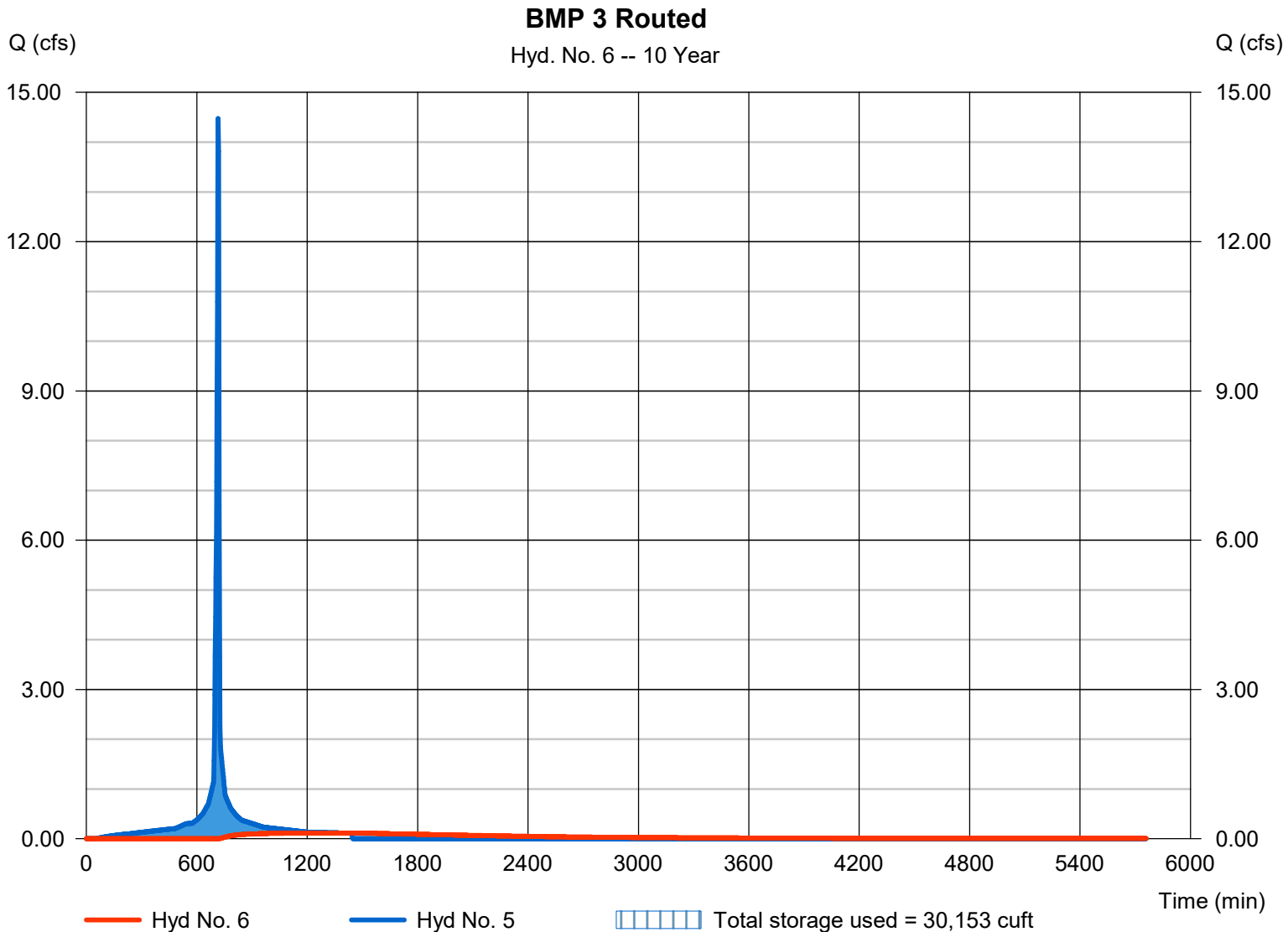
# Hydrograph Report

## Hyd. No. 6

BMP 3 Routed

Hydrograph type	= Reservoir	Peak discharge	= 0.116 cfs
Storm frequency	= 10 yrs	Time to peak	= 1378 min
Time interval	= 2 min	Hyd. volume	= 11,796 cuft
Inflow hyd. No.	= 5 - BMP 3 IN	Max. Elevation	= 321.37 ft
Reservoir name	= BMP 3	Max. Storage	= 30,153 cuft

Storage Indication method used.

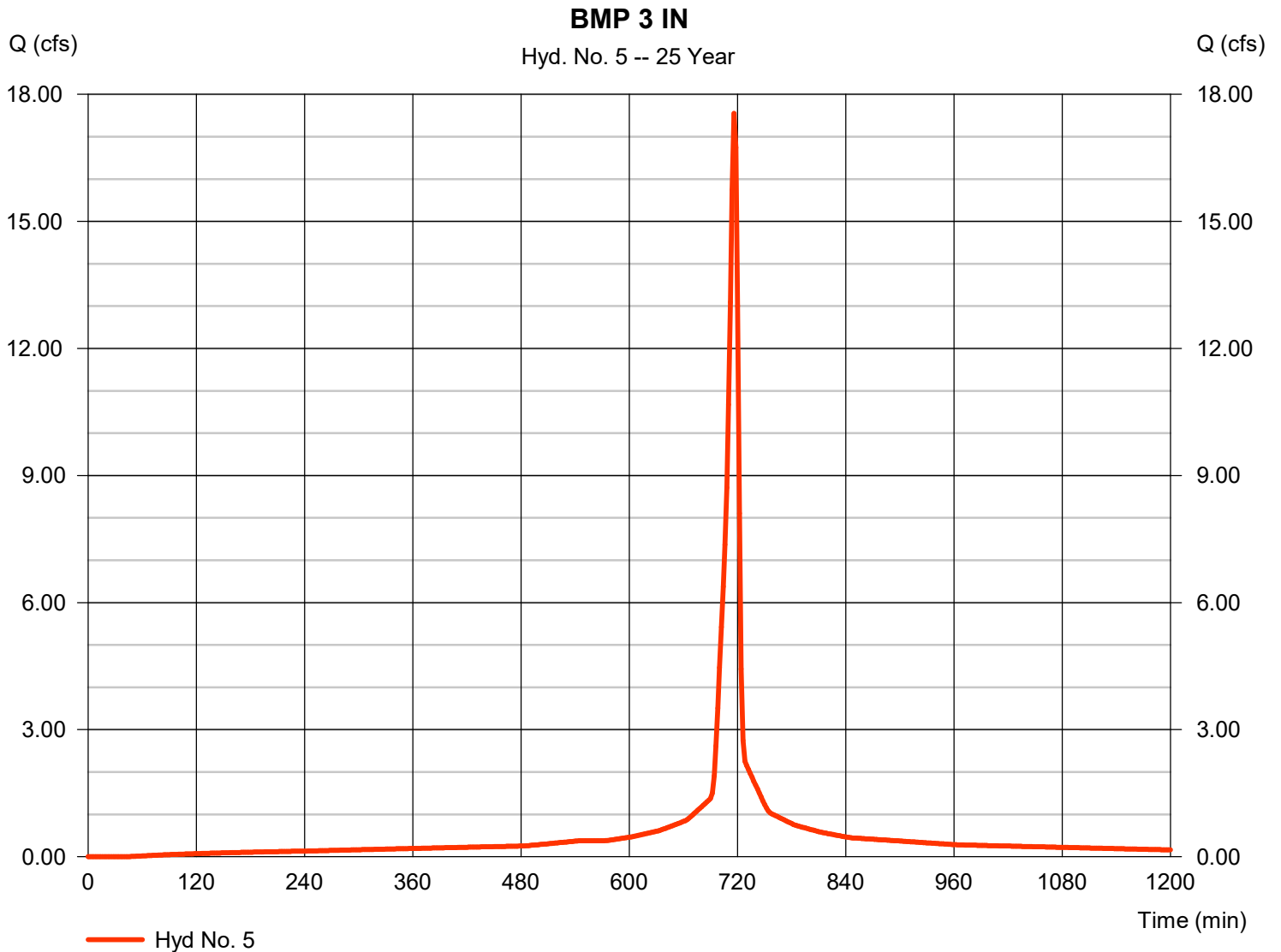


# Hydrograph Report

## Hyd. No. 5

BMP 3 IN

Hydrograph type	= SCS Runoff	Peak discharge	= 17.55 cfs
Storm frequency	= 25 yrs	Time to peak	= 716 min
Time interval	= 2 min	Hyd. volume	= 42,097 cuft
Drainage area	= 2.220 ac	Curve number	= 98
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 5.00 min
Total precip.	= 5.81 in	Distribution	= Type II
Storm duration	= 24 hrs	Shape factor	= 484





# Hydrograph Report

Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2022

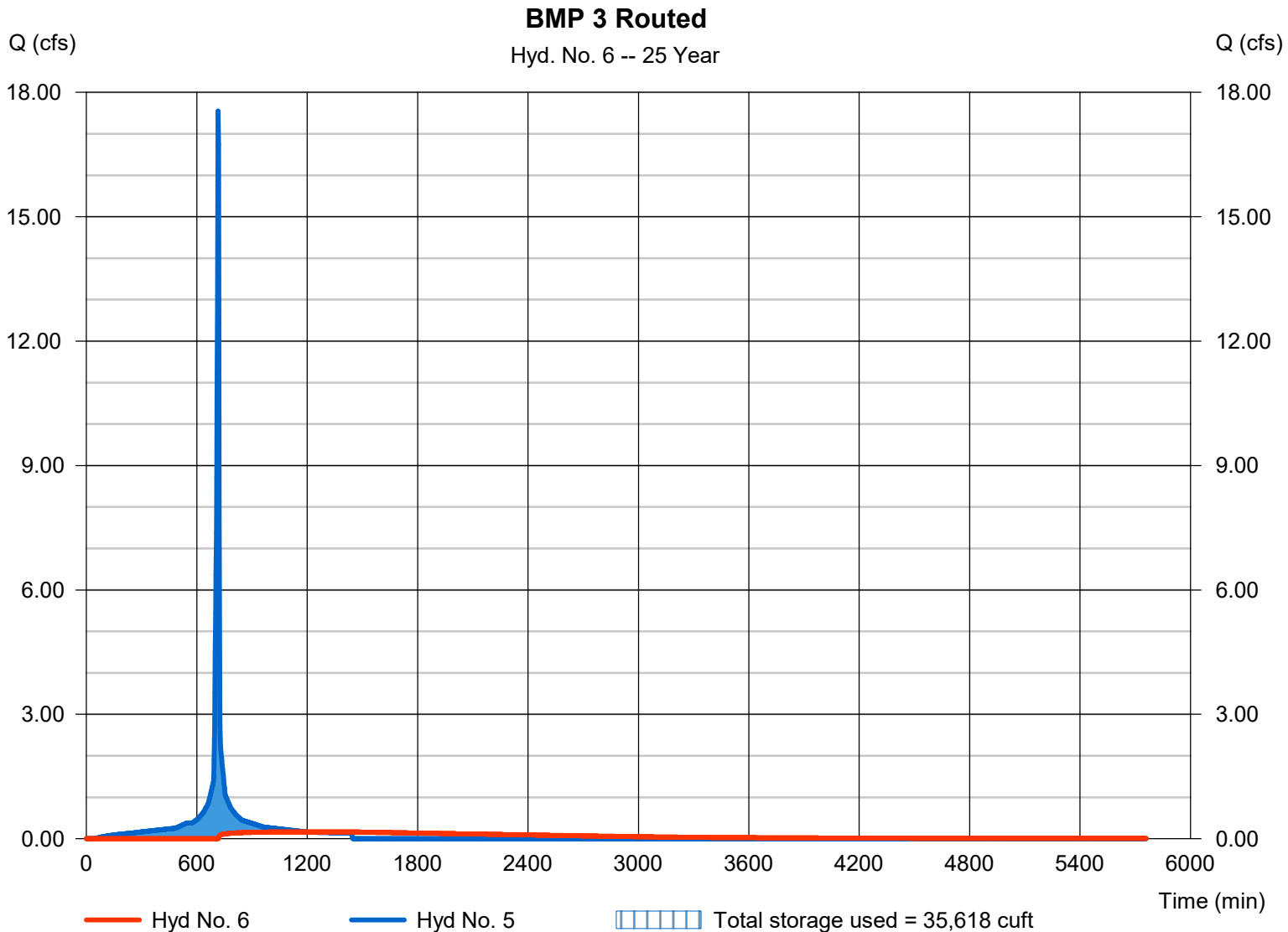
Monday, 01 / 16 / 2023

## Hyd. No. 6

BMP 3 Routed

Hydrograph type	= Reservoir	Peak discharge	= 0.165 cfs
Storm frequency	= 25 yrs	Time to peak	= 1190 min
Time interval	= 2 min	Hyd. volume	= 19,215 cuft
Inflow hyd. No.	= 5 - BMP 3 IN	Max. Elevation	= 321.61 ft
Reservoir name	= BMP 3	Max. Storage	= 35,618 cuft

Storage Indication method used.

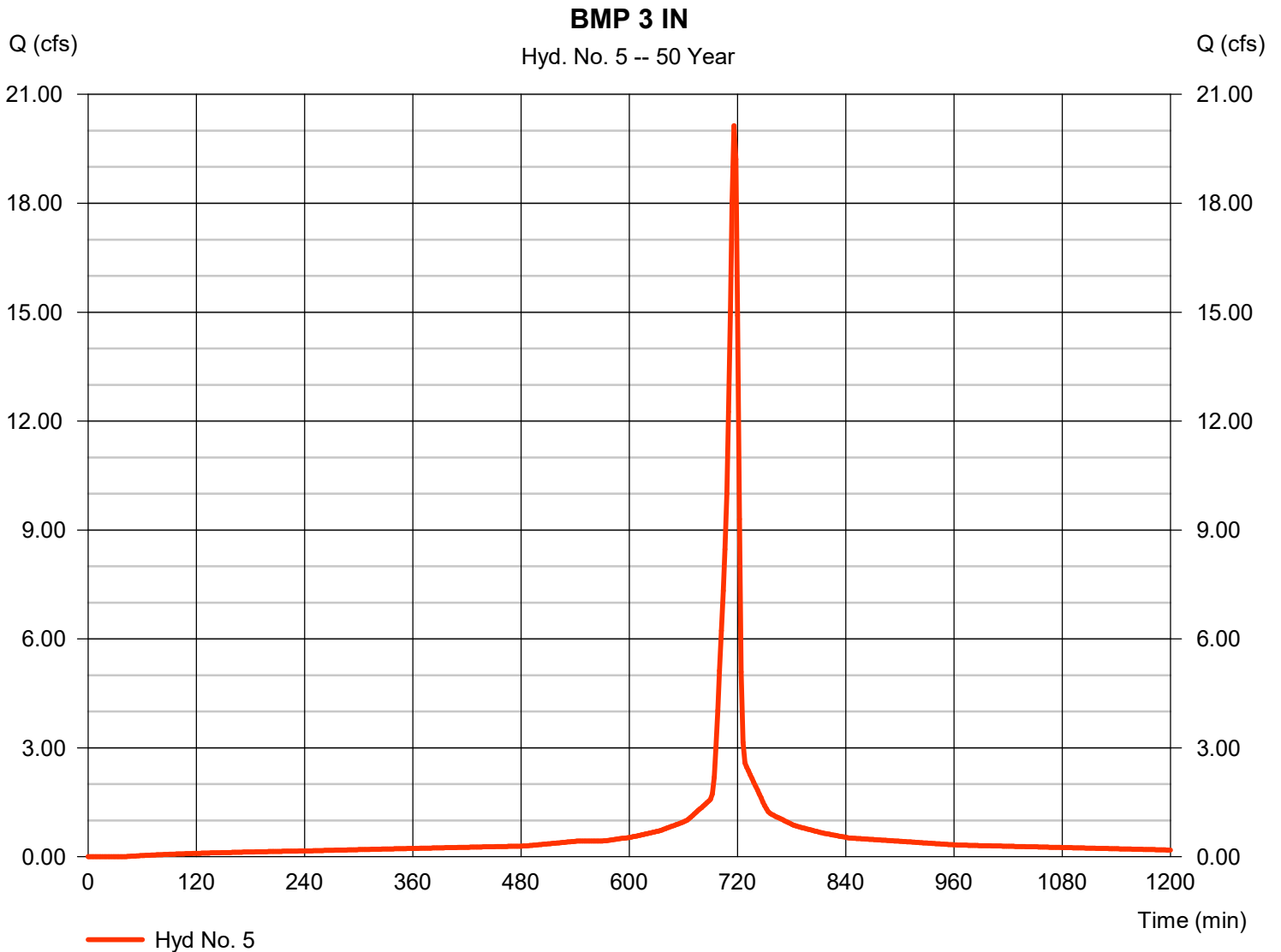


# Hydrograph Report

## Hyd. No. 5

BMP 3 IN

Hydrograph type	= SCS Runoff	Peak discharge	= 20.14 cfs
Storm frequency	= 50 yrs	Time to peak	= 716 min
Time interval	= 2 min	Hyd. volume	= 48,512 cuft
Drainage area	= 2.220 ac	Curve number	= 98
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 5.00 min
Total precip.	= 6.66 in	Distribution	= Type II
Storm duration	= 24 hrs	Shape factor	= 484



# Hydrograph Report

Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2022

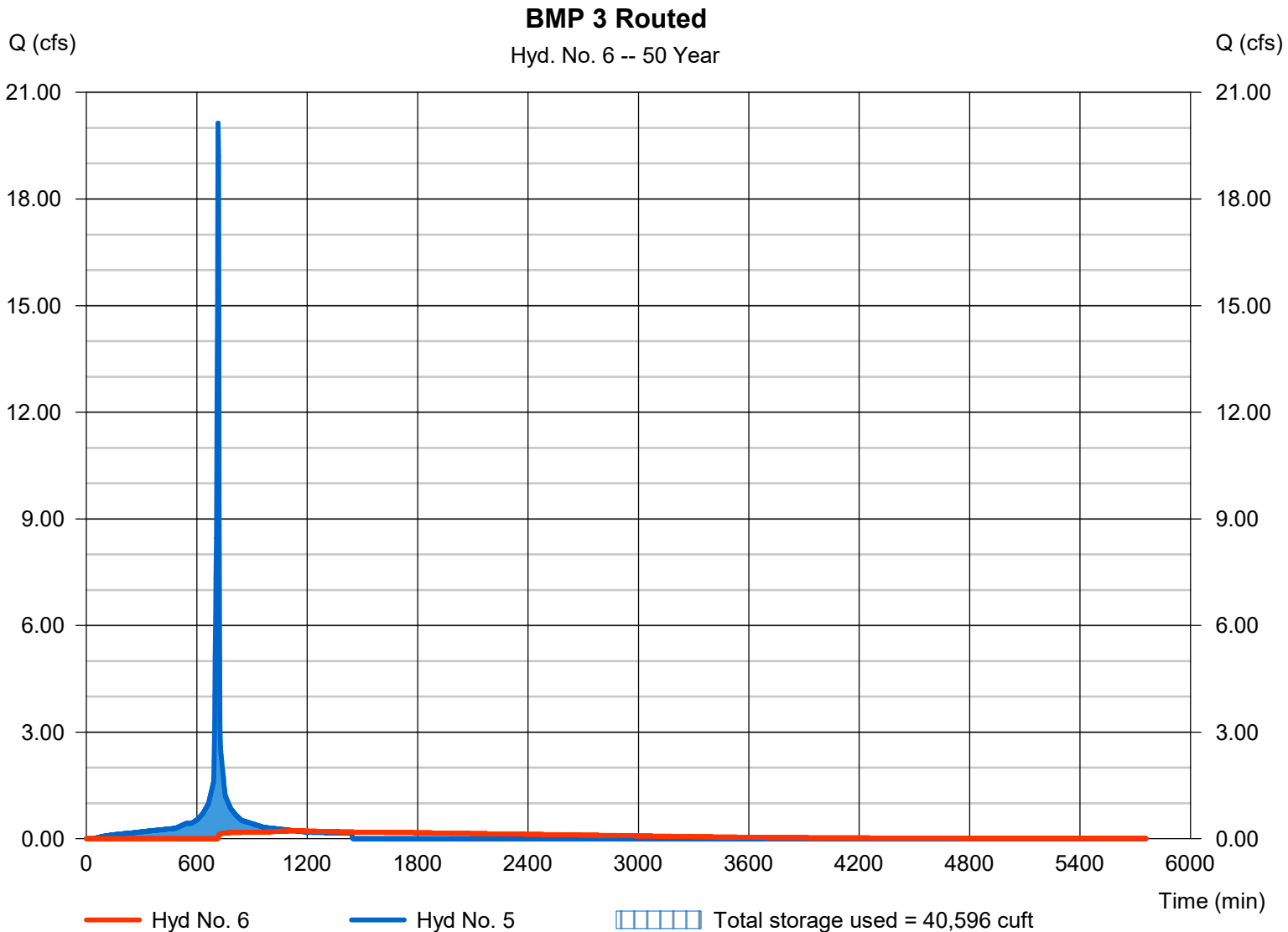
Monday, 01 / 16 / 2023

## Hyd. No. 6

BMP 3 Routed

Hydrograph type	= Reservoir	Peak discharge	= 0.219 cfs
Storm frequency	= 50 yrs	Time to peak	= 1140 min
Time interval	= 2 min	Hyd. volume	= 25,455 cuft
Inflow hyd. No.	= 5 - BMP 3 IN	Max. Elevation	= 321.76 ft
Reservoir name	= BMP 3	Max. Storage	= 40,596 cuft

Storage Indication method used.

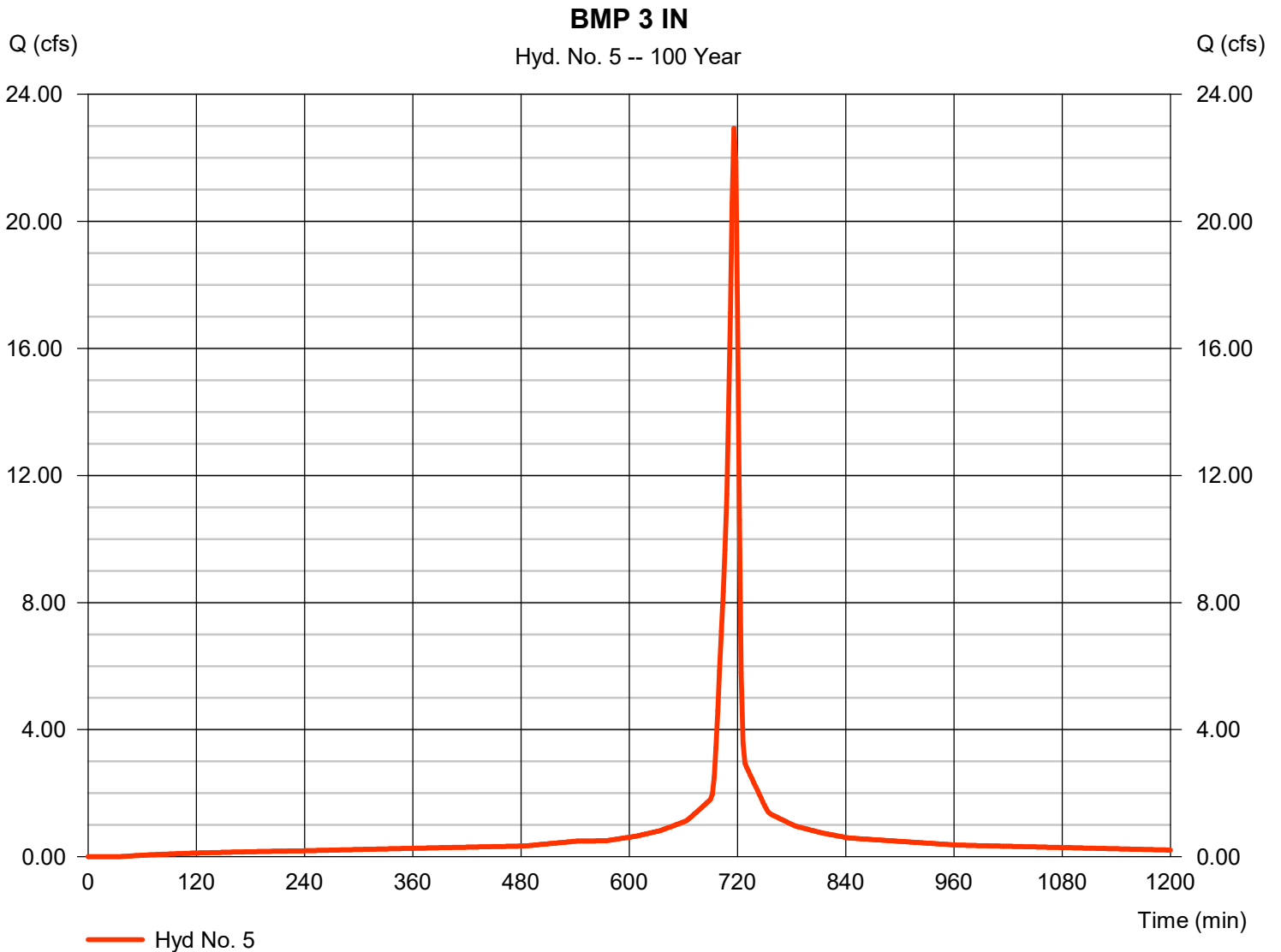


# Hydrograph Report

## Hyd. No. 5

BMP 3 IN

Hydrograph type	= SCS Runoff	Peak discharge	= 22.94 cfs
Storm frequency	= 100 yrs	Time to peak	= 716 min
Time interval	= 2 min	Hyd. volume	= 55,457 cuft
Drainage area	= 2.220 ac	Curve number	= 98
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 5.00 min
Total precip.	= 7.58 in	Distribution	= Type II
Storm duration	= 24 hrs	Shape factor	= 484



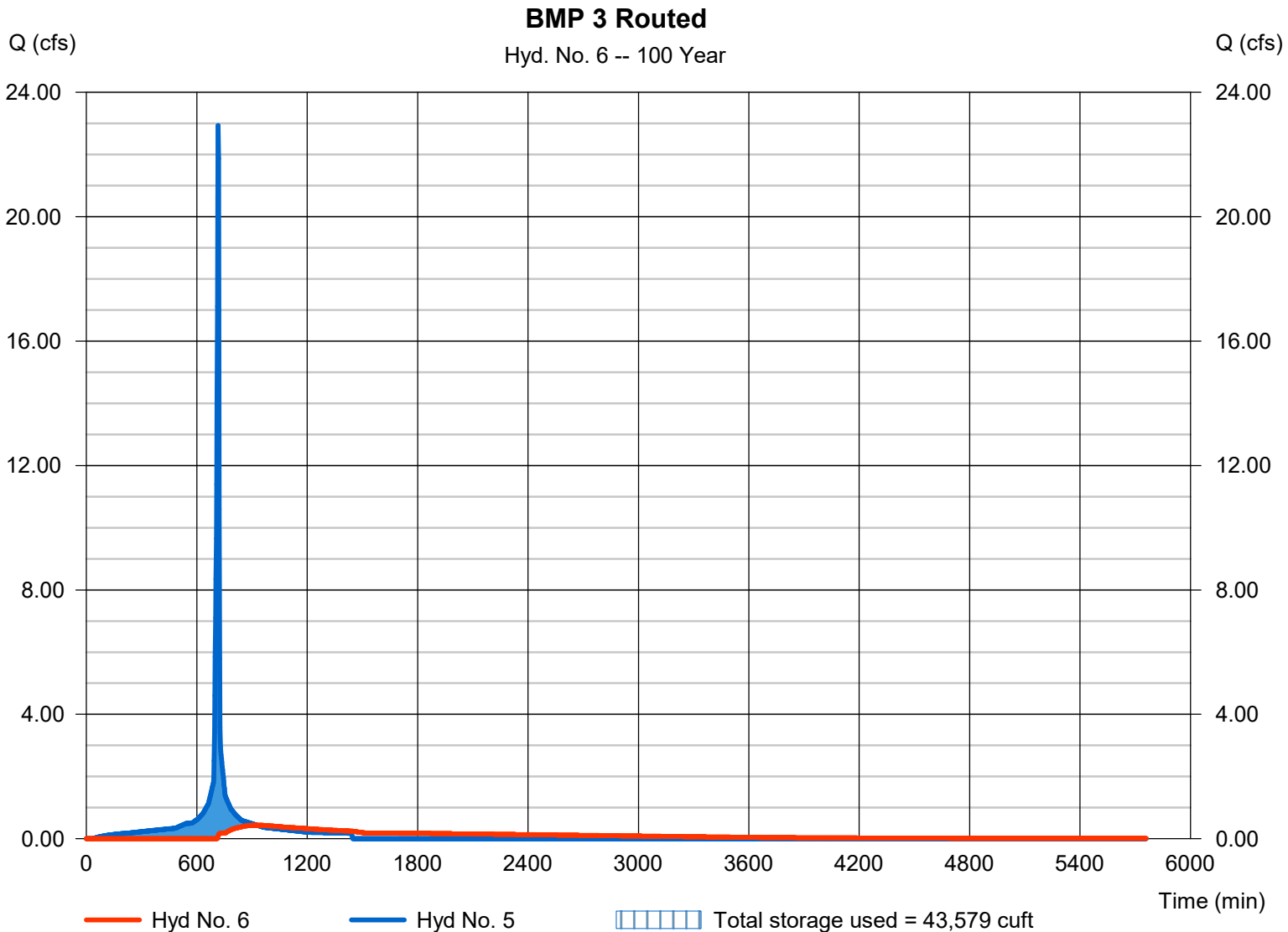
# Hydrograph Report

## Hyd. No. 6

BMP 3 Routed

Hydrograph type	= Reservoir	Peak discharge	= 0.435 cfs
Storm frequency	= 100 yrs	Time to peak	= 926 min
Time interval	= 2 min	Hyd. volume	= 32,369 cuft
Inflow hyd. No.	= 5 - BMP 3 IN	Max. Elevation	= 321.84 ft
Reservoir name	= BMP 3	Max. Storage	= 43,579 cuft

Storage Indication method used.



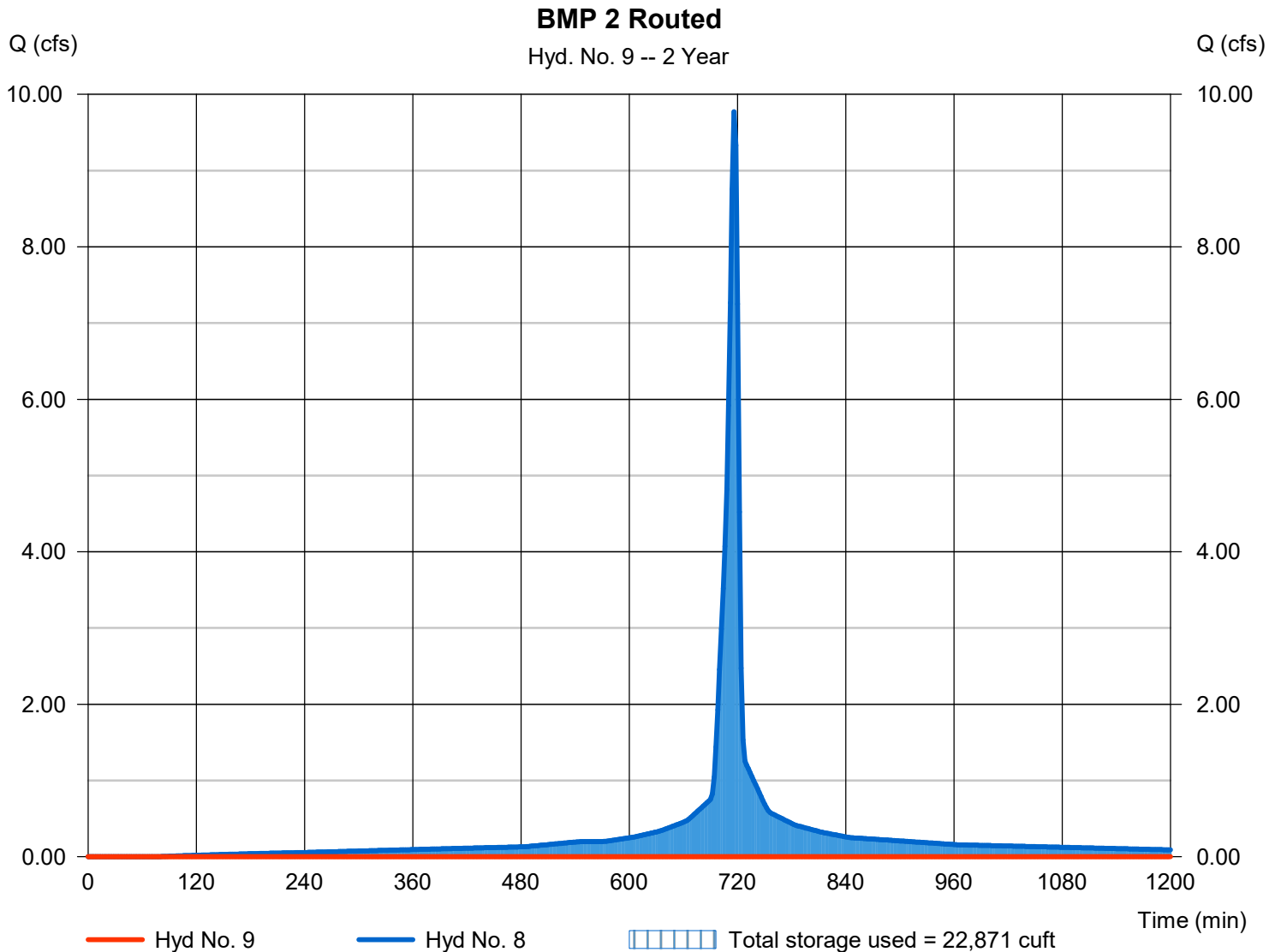
# Hydrograph Report

## Hyd. No. 9

BMP 2 Routed

Hydrograph type	= Reservoir	Peak discharge	= 0.000 cfs
Storm frequency	= 2 yrs	Time to peak	= n/a
Time interval	= 2 min	Hyd. volume	= 0 cuft
Inflow hyd. No.	= 8 - BMP 2 IN	Max. Elevation	= 316.75 ft
Reservoir name	= BMP 2	Max. Storage	= 22,871 cuft

Storage Indication method used.



# Pond Report

## Pond No. 6 - BMP 2

### Pond Data

Pond storage is based on user-defined values.

### Stage / Storage Table

Stage (ft)	Elevation (ft)	Contour area (sqft)	Incr. Storage (cuft)	Total storage (cuft)
0.00	316.00	n/a	0	0
0.67	316.67	n/a	20,294	20,294
0.75	316.75	n/a	2,741	23,035
1.50	317.50	n/a	28,665	51,700

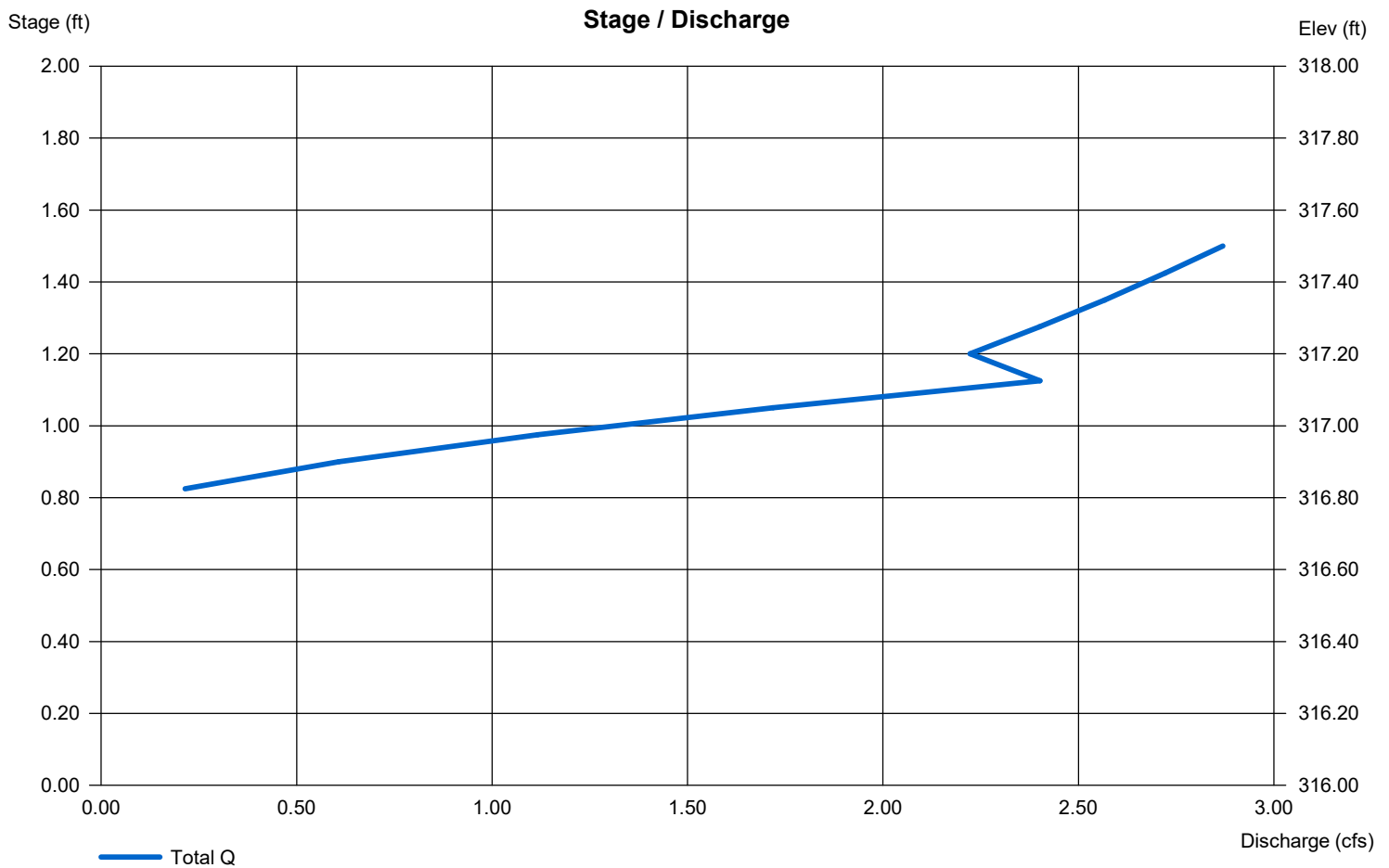
### Culvert / Orifice Structures

	[A]	[B]	[C]	[PrfRsr]
Rise (in)	= 15.00	0.00	0.00	0.00
Span (in)	= 15.00	0.00	0.00	0.00
No. Barrels	= 1	0	0	0
Invert El. (ft)	= 312.50	0.00	0.00	0.00
Length (ft)	= 84.00	0.00	0.00	0.00
Slope (%)	= 0.53	0.00	0.00	n/a
N-Value	= .013	.013	.013	n/a
Orifice Coeff.	= 0.60	0.60	0.60	0.60
Multi-Stage	= n/a	No	No	No

### Weir Structures

	[A]	[B]	[C]	[D]
Crest Len (ft)	= 3.14	0.00	0.00	0.00
Crest El. (ft)	= 316.75	0.00	0.00	0.00
Weir Coeff.	= 3.33	3.33	3.33	3.33
Weir Type	= 1	---	---	---
Multi-Stage	= Yes	No	No	No
Exfil.(in/hr)	= 0.000 (by Wet area)			
TW Elev. (ft)	= 0.00			

Note: Culvert/Orifice outflows are analyzed under inlet (ic) and outlet (oc) control. Weir risers checked for orifice conditions (ic) and submergence (s).



# Hydrograph Report

Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2022

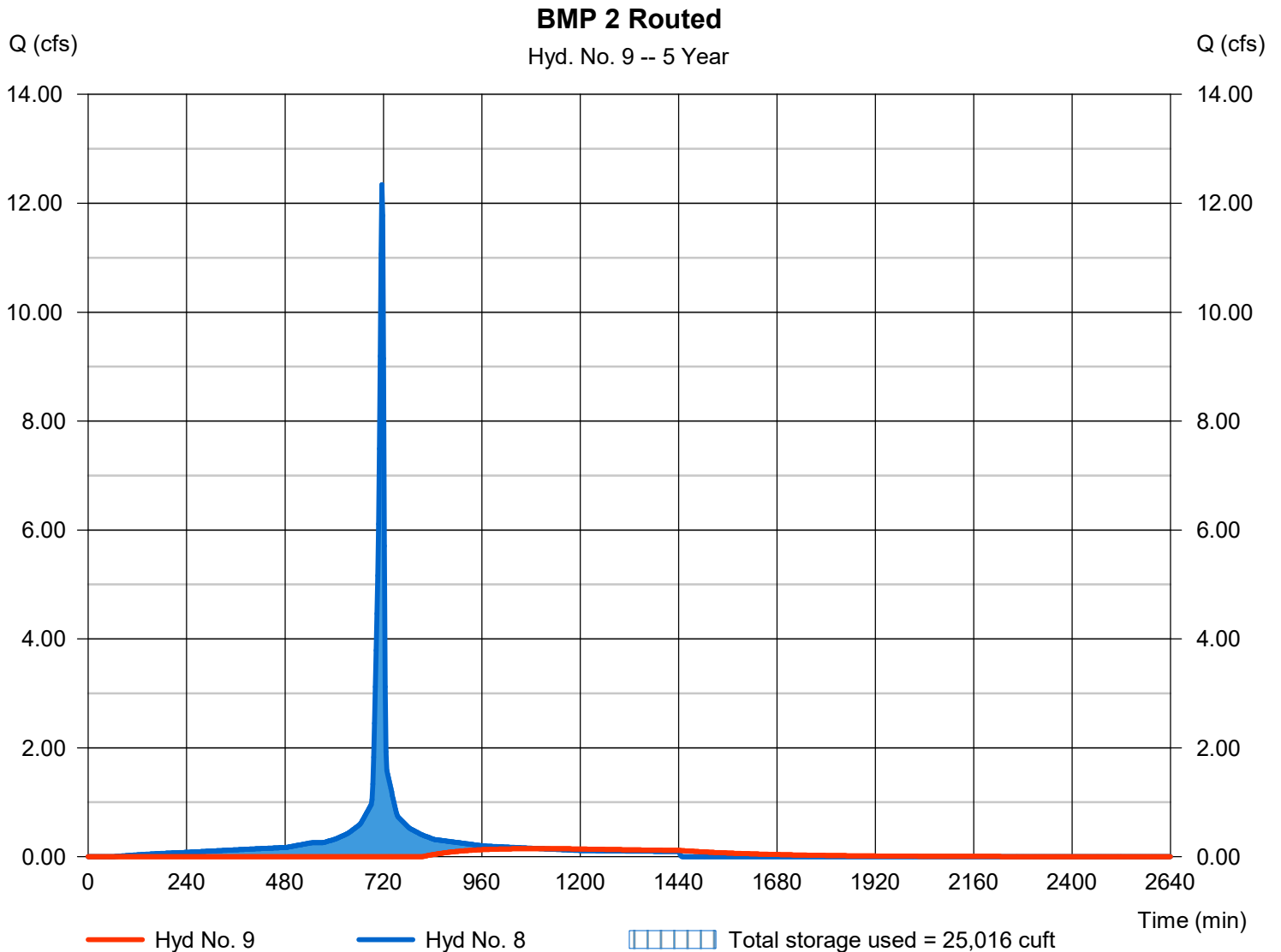
Monday, 01 / 16 / 2023

## Hyd. No. 9

BMP 2 Routed

Hydrograph type	= Reservoir	Peak discharge	= 0.148 cfs
Storm frequency	= 5 yrs	Time to peak	= 1100 min
Time interval	= 2 min	Hyd. volume	= 6,151 cuft
Inflow hyd. No.	= 8 - BMP 2 IN	Max. Elevation	= 316.80 ft
Reservoir name	= BMP 2	Max. Storage	= 25,016 cuft

Storage Indication method used.





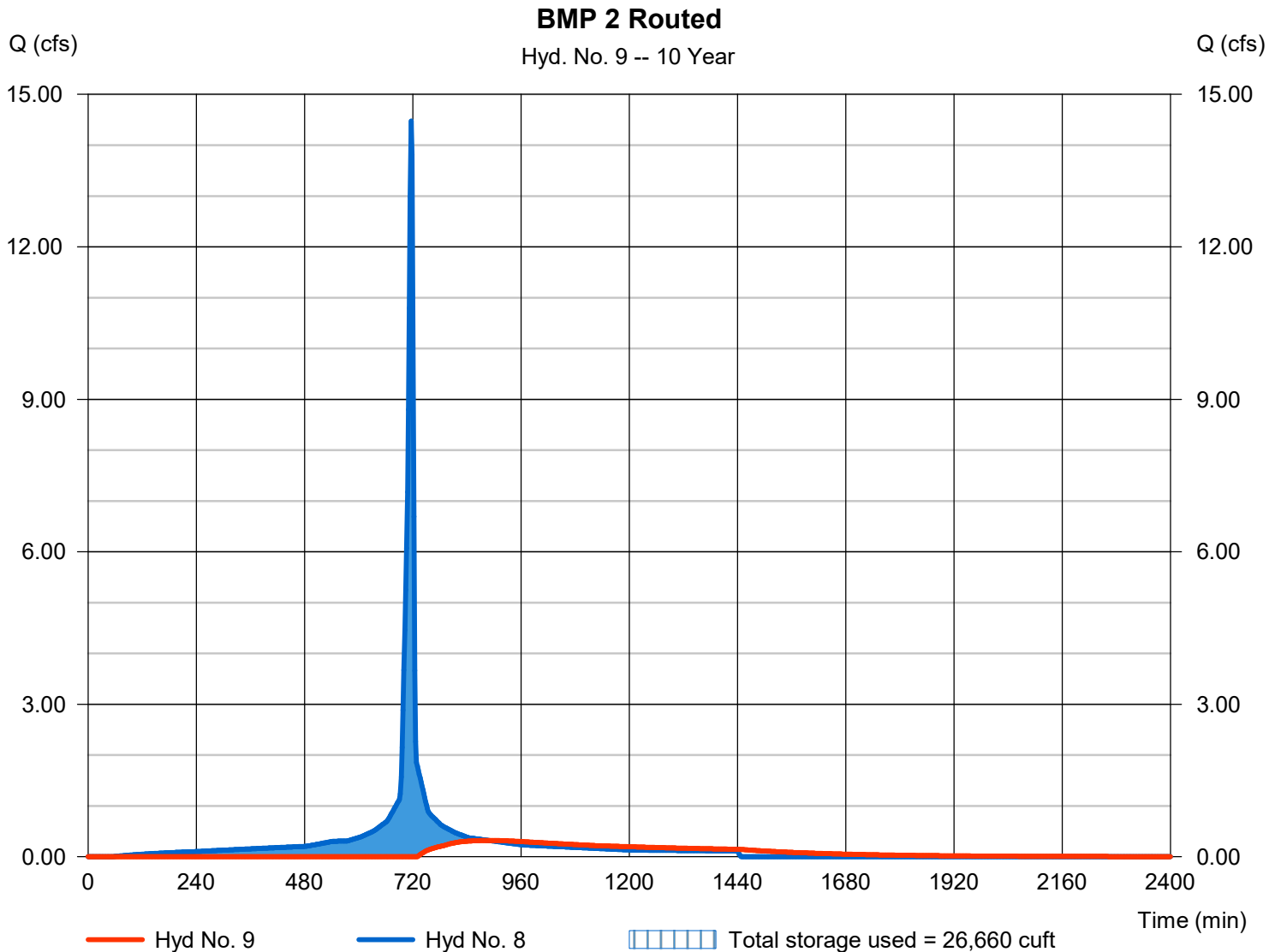
# Hydrograph Report

## Hyd. No. 9

### BMP 2 Routed

Hydrograph type	= Reservoir	Peak discharge	= 0.319 cfs
Storm frequency	= 10 yrs	Time to peak	= 888 min
Time interval	= 2 min	Hyd. volume	= 11,429 cuft
Inflow hyd. No.	= 8 - BMP 2 IN	Max. Elevation	= 316.84 ft
Reservoir name	= BMP 2	Max. Storage	= 26,660 cuft

Storage Indication method used.



# Hydrograph Report

Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2022

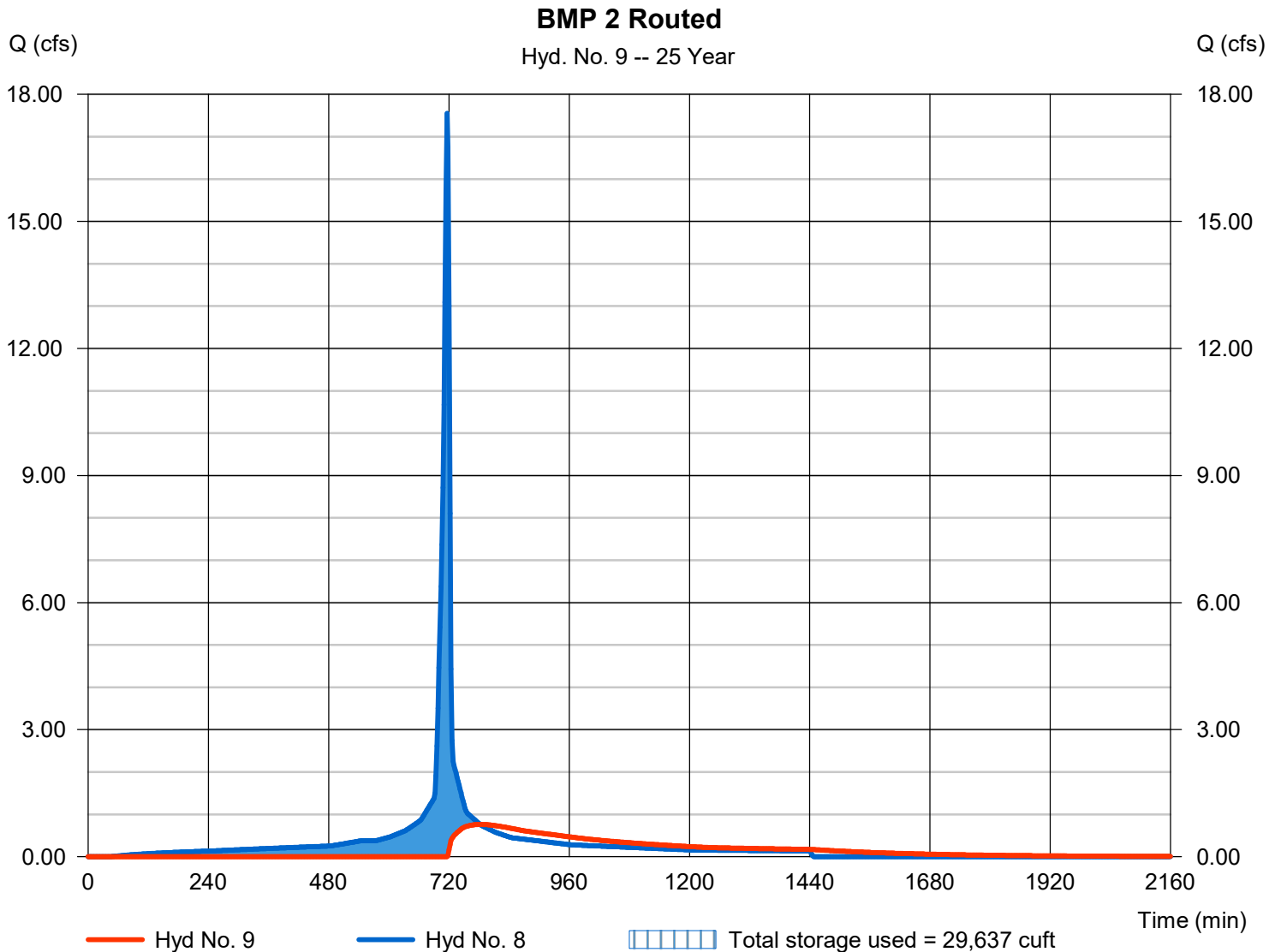
Monday, 01 / 16 / 2023

## Hyd. No. 9

BMP 2 Routed

Hydrograph type	= Reservoir	Peak discharge	= 0.762 cfs
Storm frequency	= 25 yrs	Time to peak	= 782 min
Time interval	= 2 min	Hyd. volume	= 19,048 cuft
Inflow hyd. No.	= 8 - BMP 2 IN	Max. Elevation	= 316.92 ft
Reservoir name	= BMP 2	Max. Storage	= 29,637 cuft

Storage Indication method used.



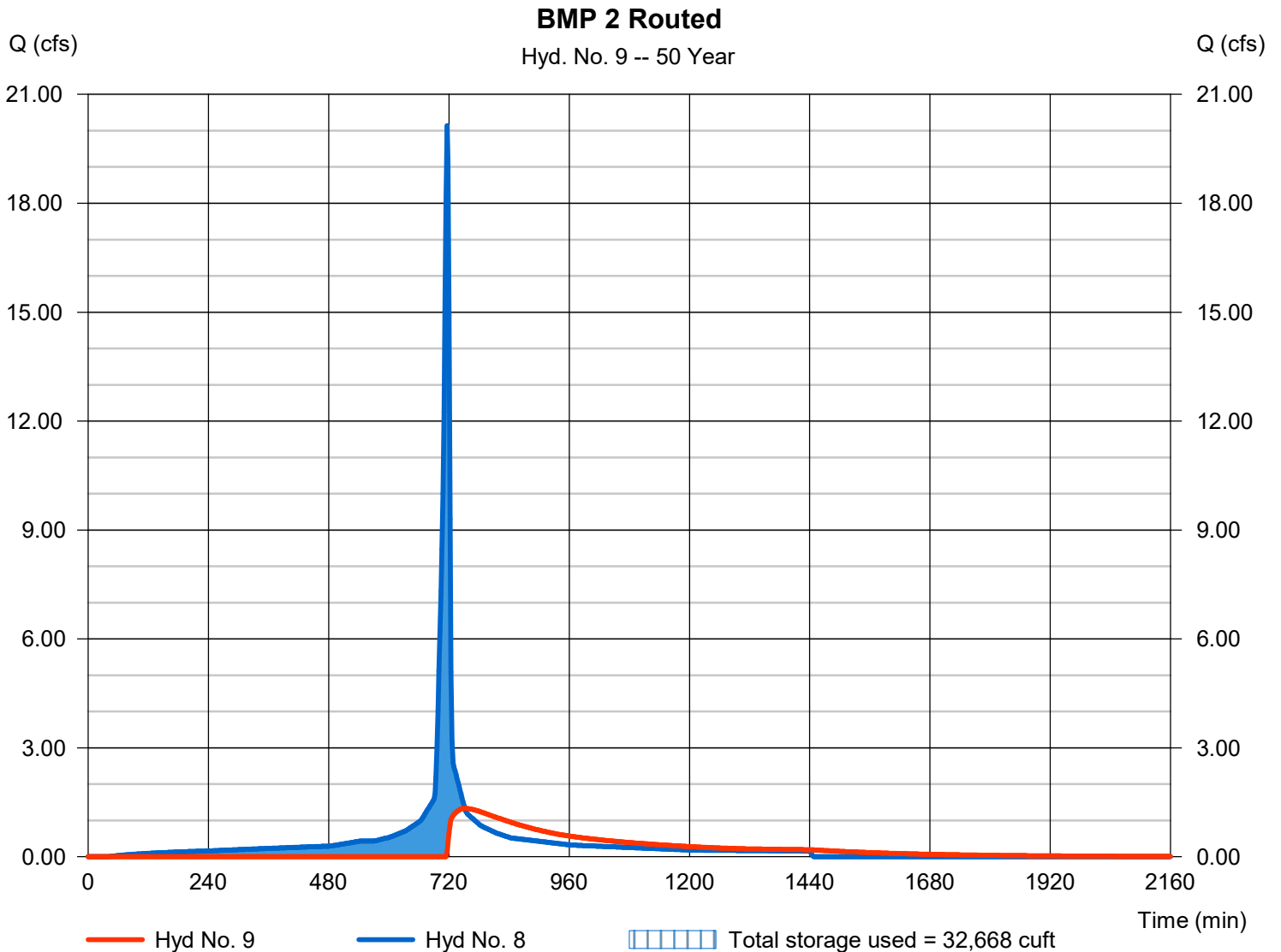
# Hydrograph Report

## Hyd. No. 9

### BMP 2 Routed

Hydrograph type	= Reservoir	Peak discharge	= 1.333 cfs
Storm frequency	= 50 yrs	Time to peak	= 752 min
Time interval	= 2 min	Hyd. volume	= 25,463 cuft
Inflow hyd. No.	= 8 - BMP 2 IN	Max. Elevation	= 317.00 ft
Reservoir name	= BMP 2	Max. Storage	= 32,668 cuft

Storage Indication method used.



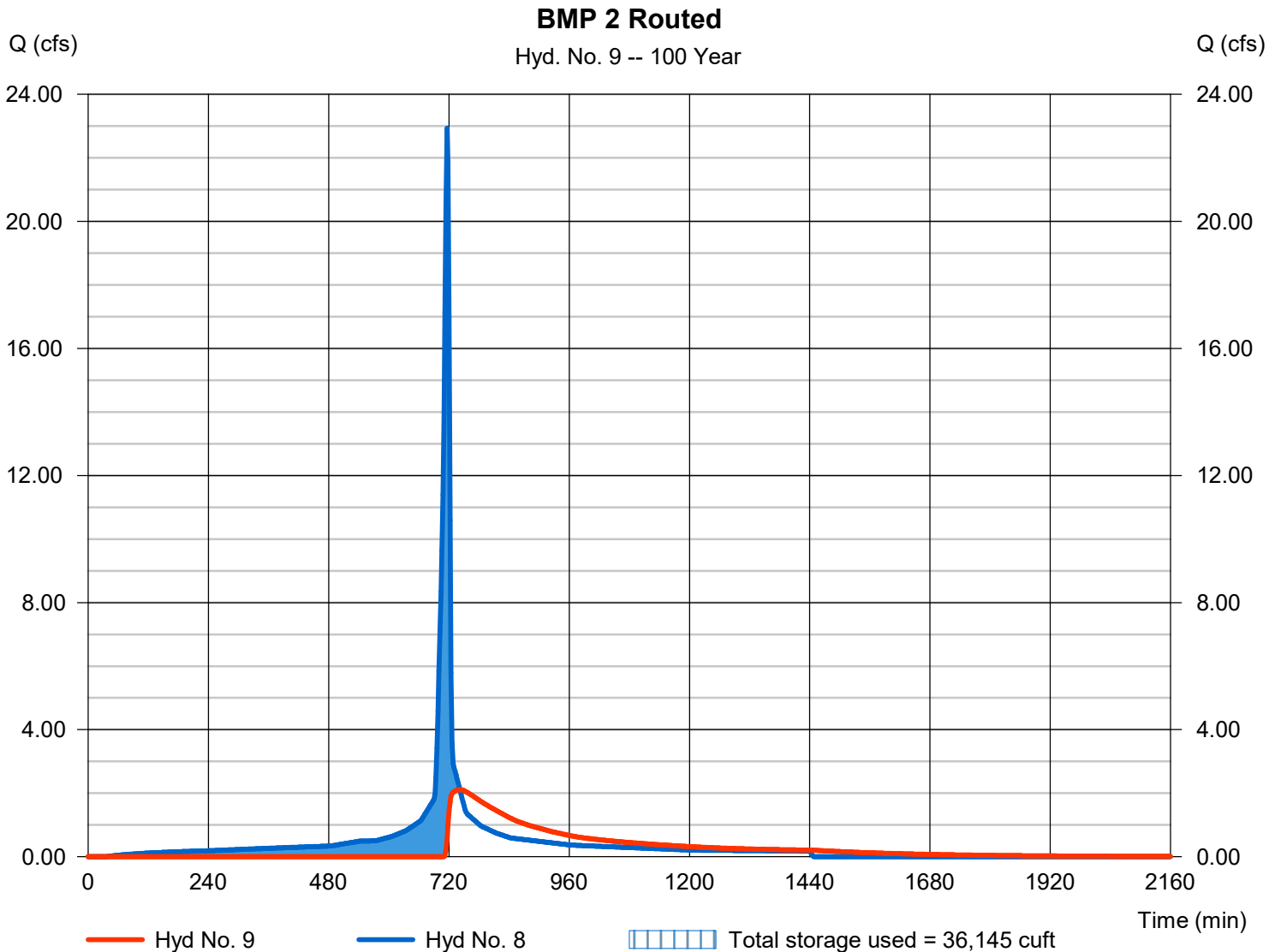
# Hydrograph Report

## Hyd. No. 9

### BMP 2 Routed

Hydrograph type	= Reservoir	Peak discharge	= 2.110 cfs
Storm frequency	= 100 yrs	Time to peak	= 742 min
Time interval	= 2 min	Hyd. volume	= 32,409 cuft
Inflow hyd. No.	= 8 - BMP 2 IN	Max. Elevation	= 317.09 ft
Reservoir name	= BMP 2	Max. Storage	= 36,145 cuft

Storage Indication method used.

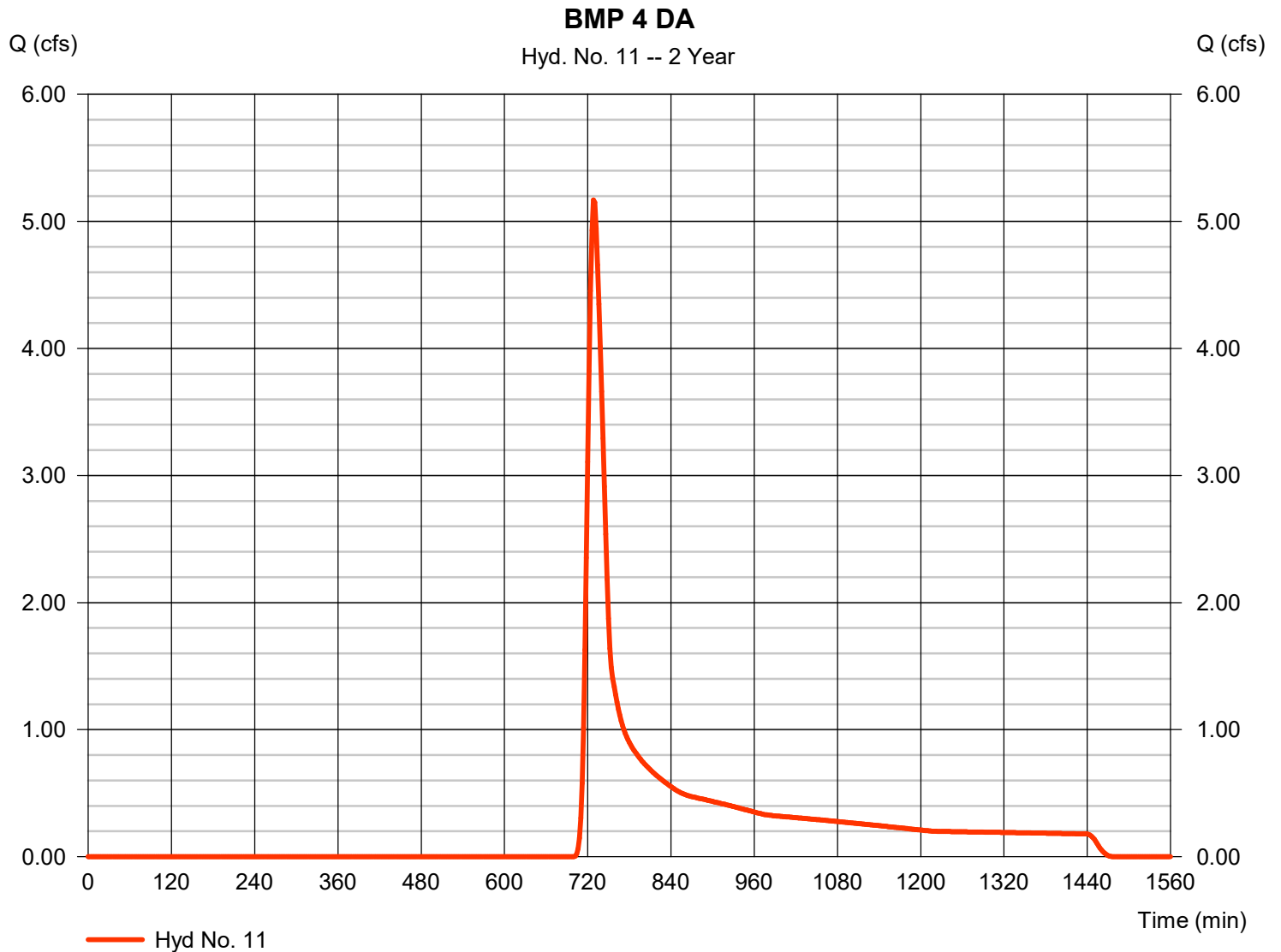


# Hydrograph Report

## Hyd. No. 11

BMP 4 DA

Hydrograph type	= SCS Runoff	Peak discharge	= 5.169 cfs
Storm frequency	= 2 yrs	Time to peak	= 728 min
Time interval	= 2 min	Hyd. volume	= 22,661 cuft
Drainage area	= 9.740 ac	Curve number	= 65
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 22.00 min
Total precip.	= 3.26 in	Distribution	= Type II
Storm duration	= 24 hrs	Shape factor	= 484



# Hydrograph Report

Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2022

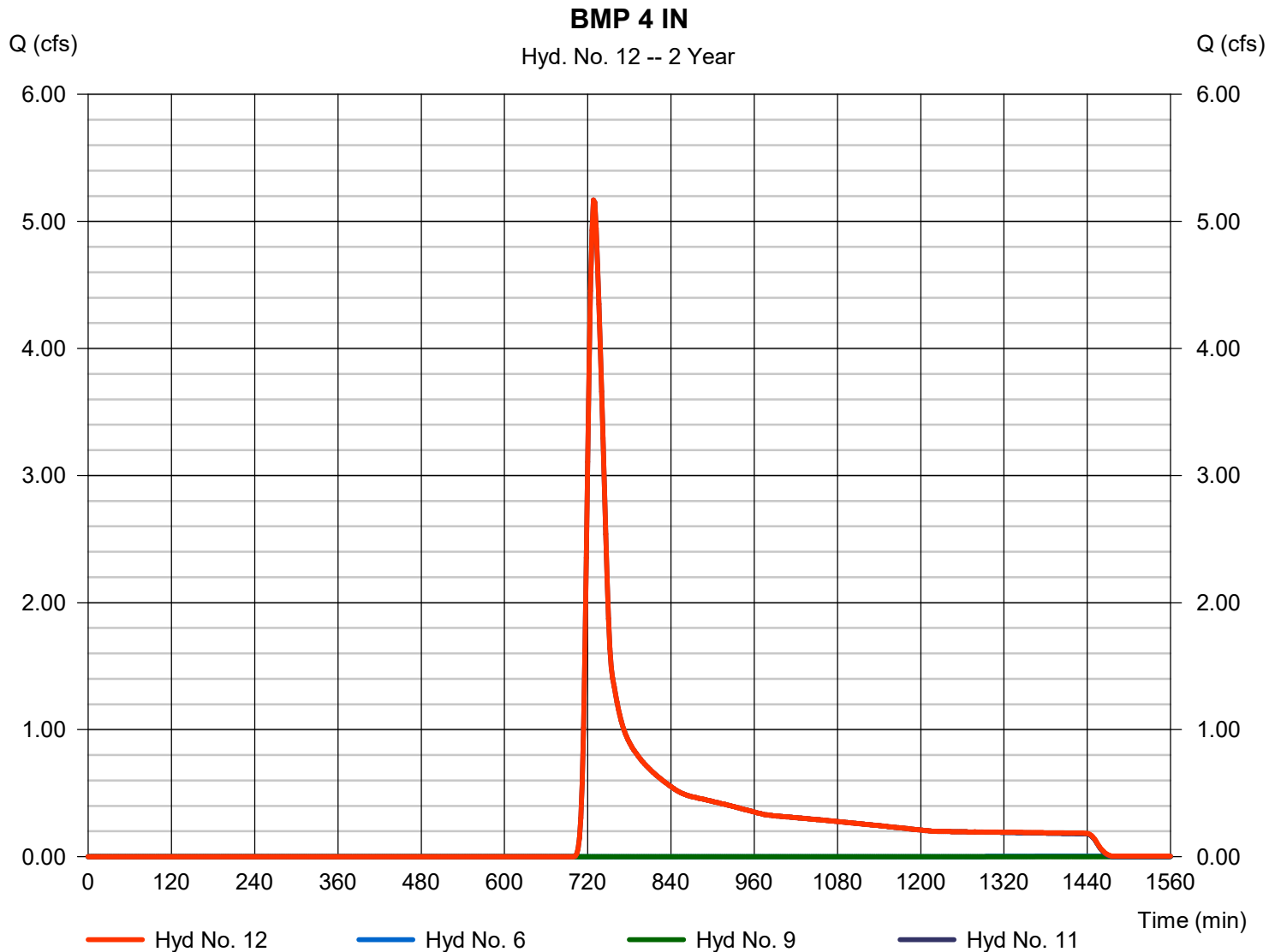
Monday, 01 / 16 / 2023

## Hyd. No. 12

BMP 4 IN

Hydrograph type = Combine  
Storm frequency = 2 yrs  
Time interval = 2 min  
Inflow hyds. = 6, 9, 11

Peak discharge = 5.169 cfs  
Time to peak = 728 min  
Hyd. volume = 23,433 cuft  
Contrib. drain. area = 9.740 ac



# Hydrograph Report

Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2022

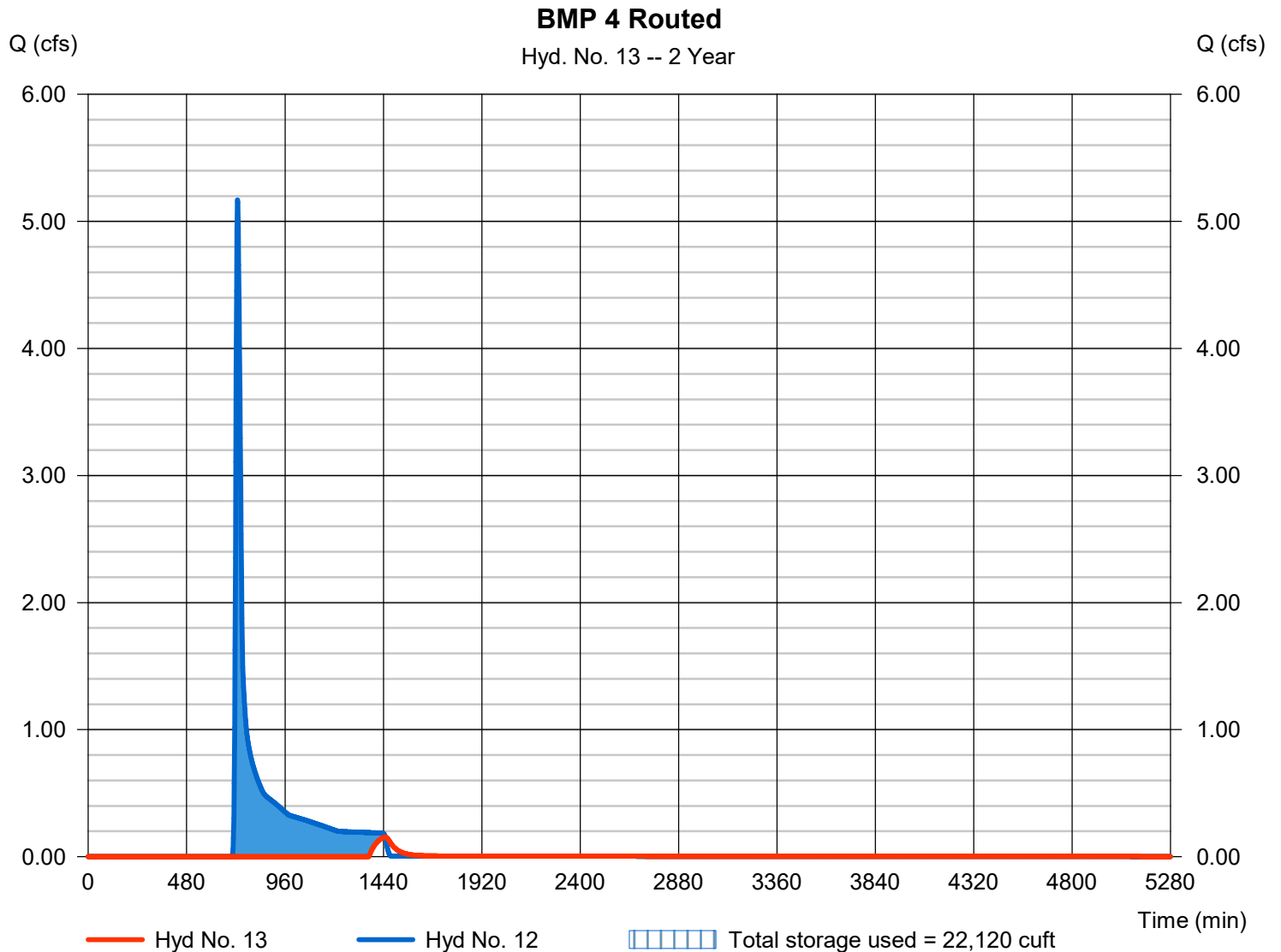
Monday, 01 / 16 / 2023

## Hyd. No. 13

BMP 4 Routed

Hydrograph type	= Reservoir	Peak discharge	= 0.155 cfs
Storm frequency	= 2 yrs	Time to peak	= 1448 min
Time interval	= 2 min	Hyd. volume	= 1,707 cuft
Inflow hyd. No.	= 12 - BMP 4 IN	Max. Elevation	= 311.01 ft
Reservoir name	= BMP 4	Max. Storage	= 22,120 cuft

Storage Indication method used.



# Pond Report

## Pond No. 5 - BMP 4

### Pond Data

Contours -User-defined contour areas. Conic method used for volume calculation. Begining Elevation = 310.00 ft

### Stage / Storage Table

Stage (ft)	Elevation (ft)	Contour area (sqft)	Incr. Storage (cuft)	Total storage (cuft)
0.00	310.00	18,641	0	0
1.00	311.00	24,964	21,724	21,724
2.00	312.00	31,828	28,324	50,047
3.00	313.00	39,079	35,388	85,435
4.00	314.00	46,489	42,726	128,162
4.50	314.50	48,534	23,752	151,913

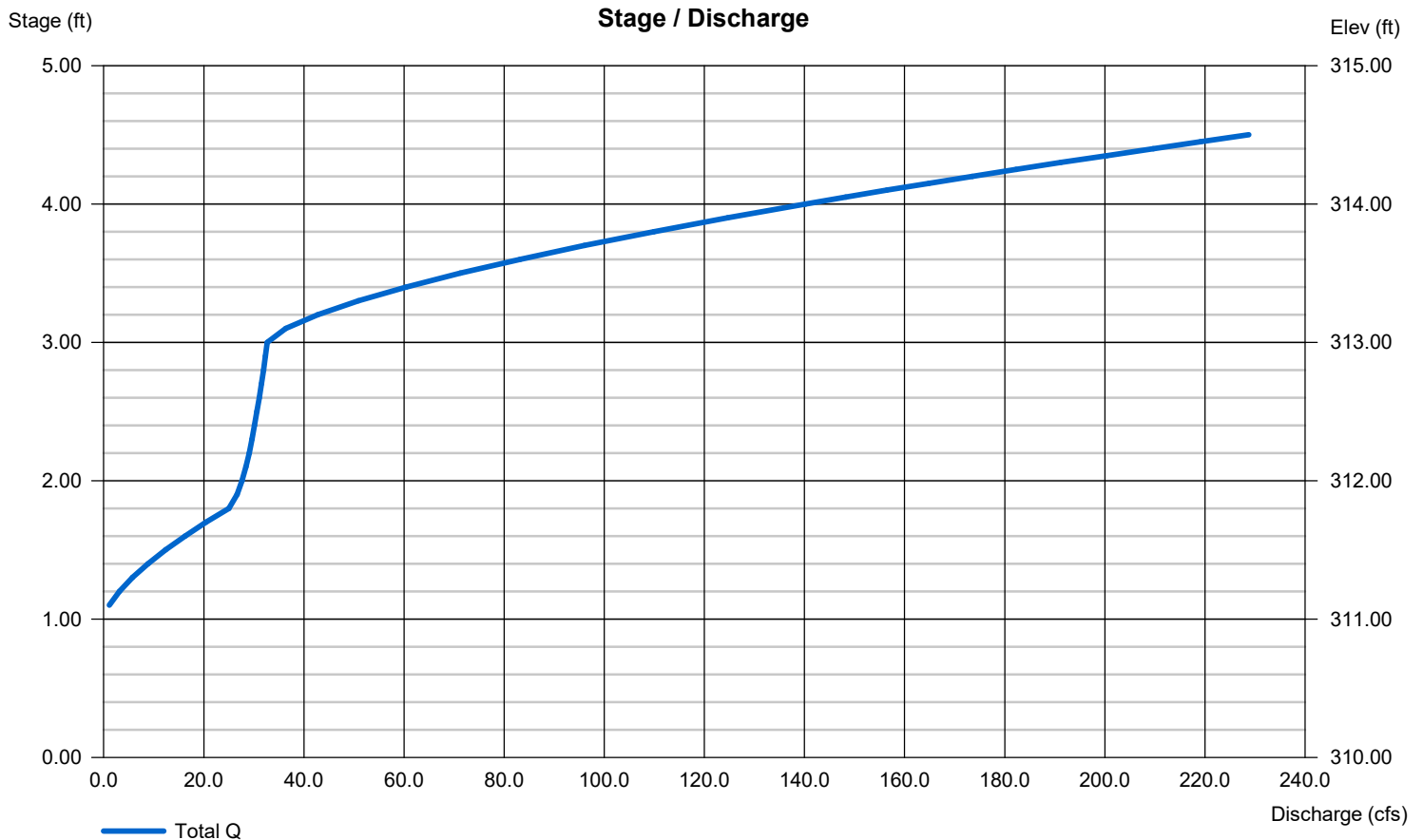
### Culvert / Orifice Structures

	[A]	[B]	[C]	[PrfRsr]
Rise (in)	= 24.00	0.00	0.00	0.00
Span (in)	= 24.00	0.00	0.00	0.00
No. Barrels	= 1	0	0	0
Invert El. (ft)	= 307.25	0.00	0.00	0.00
Length (ft)	= 36.00	0.00	0.00	0.00
Slope (%)	= 0.69	0.00	0.00	n/a
N-Value	= .013	.013	.013	n/a
Orifice Coeff.	= 0.60	0.60	0.60	0.60
Multi-Stage	= n/a	No	No	No

### Weir Structures

	[A]	[B]	[C]	[D]
Crest Len (ft)	= 10.50	Inactive	40.00	0.00
Crest El. (ft)	= 311.00	311.00	313.00	0.00
Weir Coeff.	= 3.33	3.33	2.60	3.33
Weir Type	= 1	Rect	Broad	---
Multi-Stage	= Yes	Yes	No	No
Exfil.(in/hr)	= 0.000 (by Contour)			
TW Elev. (ft)	= 0.00			

Note: Culvert/Orifice outflows are analyzed under inlet (ic) and outlet (oc) control. Weir risers checked for orifice conditions (ic) and submergence (s).



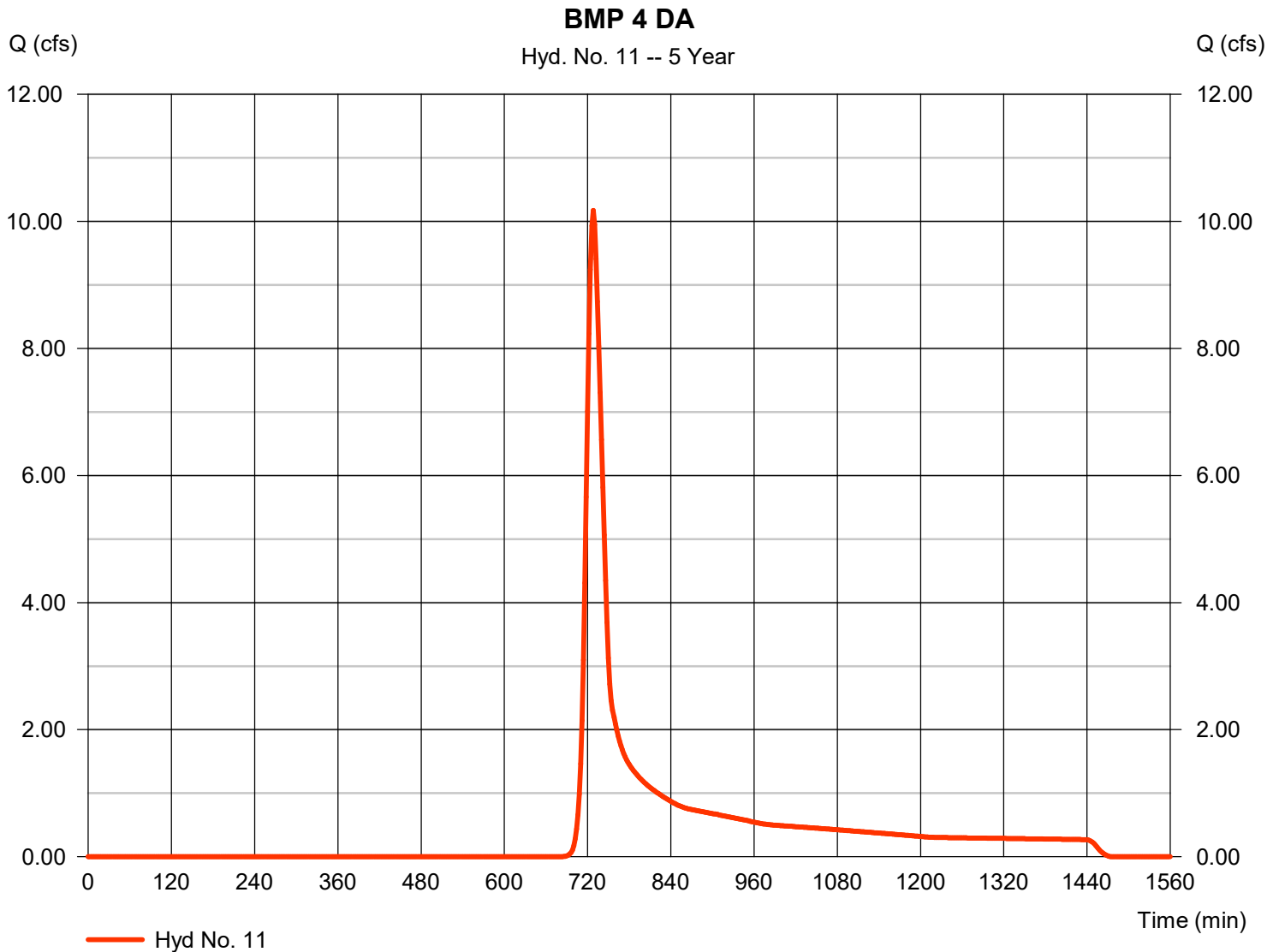


# Hydrograph Report

## Hyd. No. 11

BMP 4 DA

Hydrograph type	= SCS Runoff	Peak discharge	= 10.17 cfs
Storm frequency	= 5 yrs	Time to peak	= 728 min
Time interval	= 2 min	Hyd. volume	= 39,117 cuft
Drainage area	= 9.740 ac	Curve number	= 65
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 22.00 min
Total precip.	= 4.10 in	Distribution	= Type II
Storm duration	= 24 hrs	Shape factor	= 484



# Hydrograph Report

Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2022

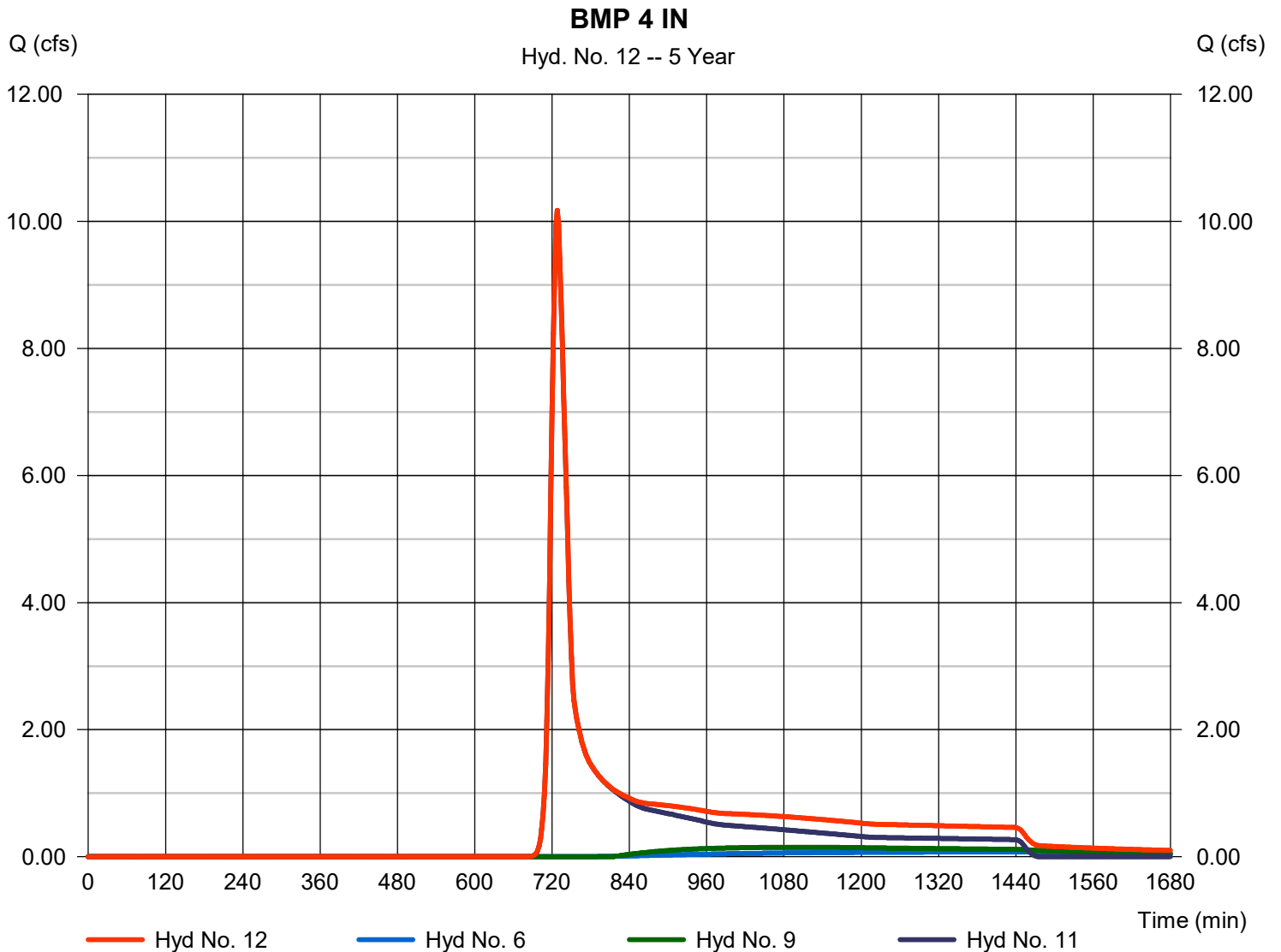
Monday, 01 / 16 / 2023

## Hyd. No. 12

BMP 4 IN

Hydrograph type = Combine  
Storm frequency = 5 yrs  
Time interval = 2 min  
Inflow hyds. = 6, 9, 11

Peak discharge = 10.17 cfs  
Time to peak = 728 min  
Hyd. volume = 51,923 cuft  
Contrib. drain. area = 9.740 ac



# Hydrograph Report

Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2022

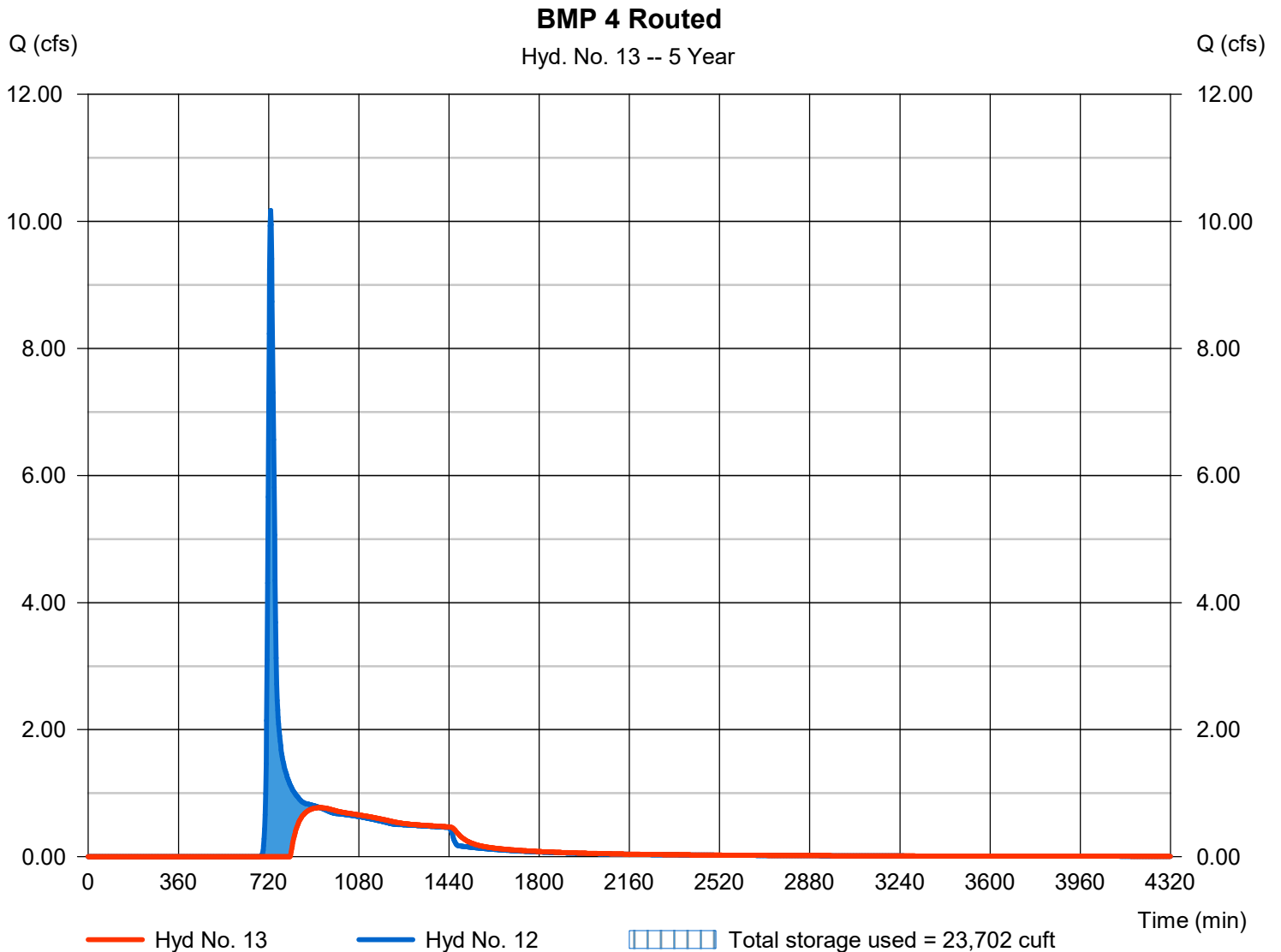
Monday, 01 / 16 / 2023

## Hyd. No. 13

BMP 4 Routed

Hydrograph type	= Reservoir	Peak discharge	= 0.772 cfs
Storm frequency	= 5 yrs	Time to peak	= 924 min
Time interval	= 2 min	Hyd. volume	= 30,189 cuft
Inflow hyd. No.	= 12 - BMP 4 IN	Max. Elevation	= 311.07 ft
Reservoir name	= BMP 4	Max. Storage	= 23,702 cuft

Storage Indication method used.

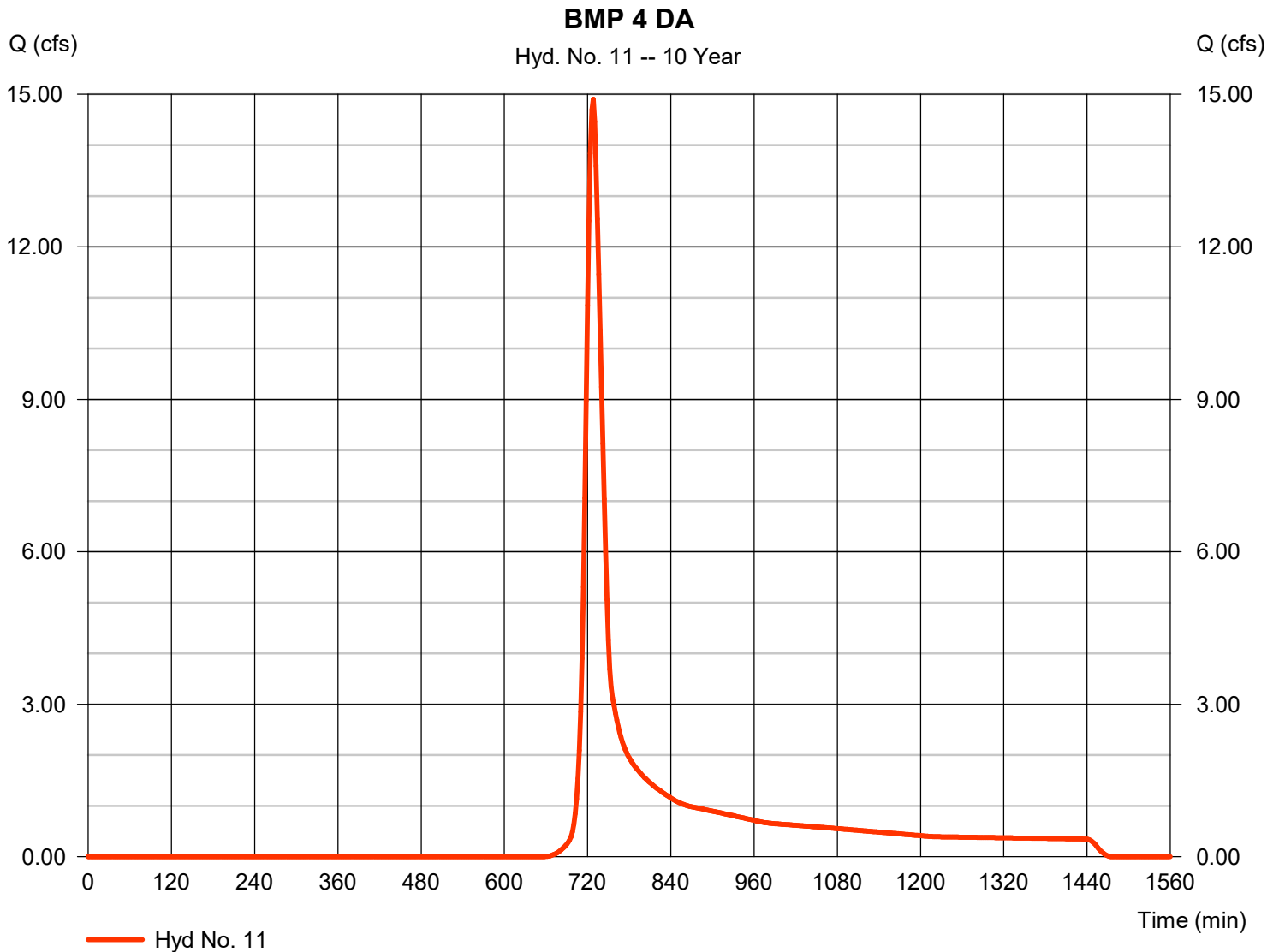


# Hydrograph Report

## Hyd. No. 11

BMP 4 DA

Hydrograph type	= SCS Runoff	Peak discharge	= 14.91 cfs
Storm frequency	= 10 yrs	Time to peak	= 728 min
Time interval	= 2 min	Hyd. volume	= 54,771 cuft
Drainage area	= 9.740 ac	Curve number	= 65
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 22.00 min
Total precip.	= 4.80 in	Distribution	= Type II
Storm duration	= 24 hrs	Shape factor	= 484



# Hydrograph Report

Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2022

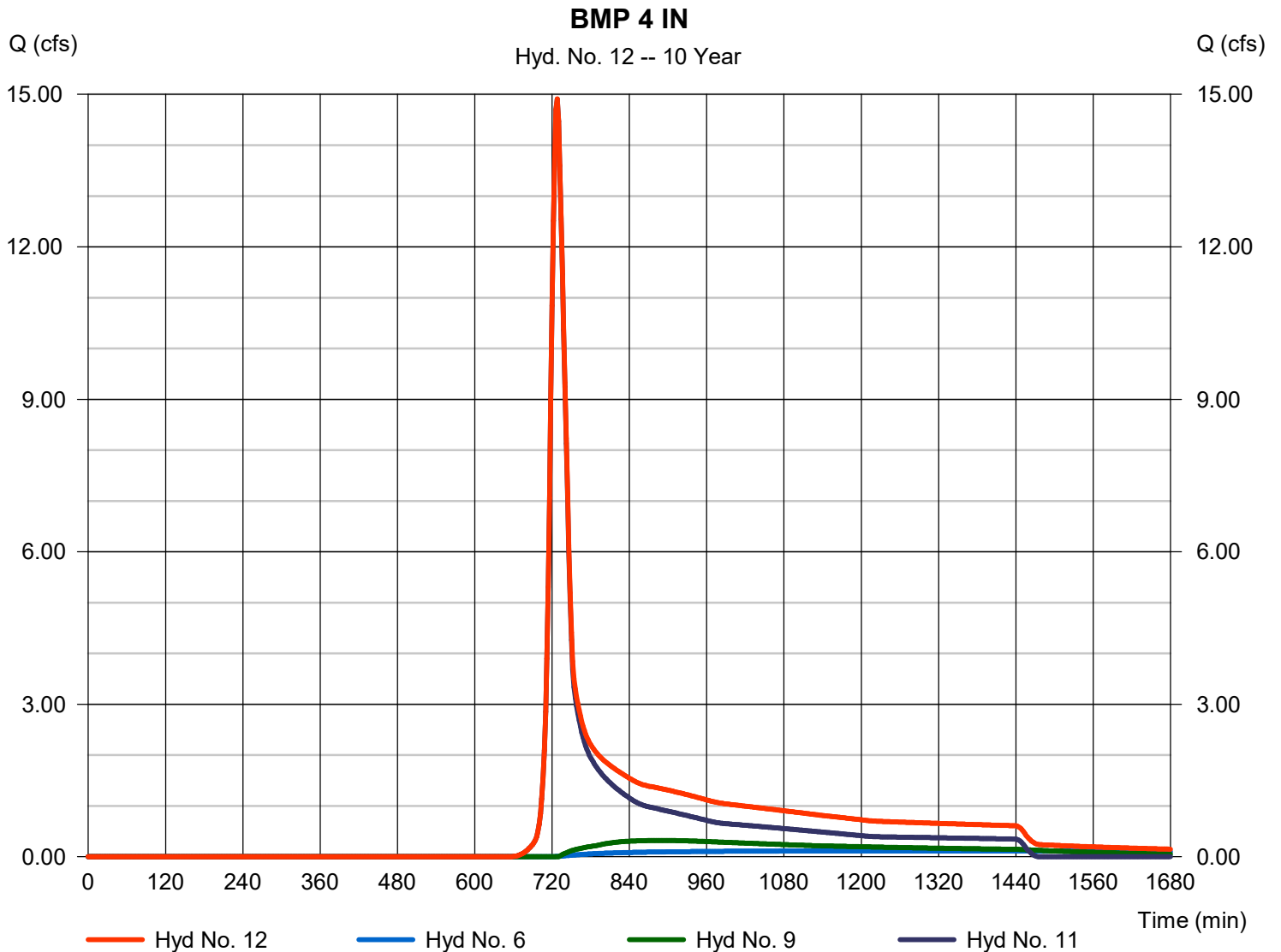
Monday, 01 / 16 / 2023

## Hyd. No. 12

BMP 4 IN

Hydrograph type = Combine  
Storm frequency = 10 yrs  
Time interval = 2 min  
Inflow hyds. = 6, 9, 11

Peak discharge = 14.91 cfs  
Time to peak = 728 min  
Hyd. volume = 77,995 cuft  
Contrib. drain. area = 9.740 ac



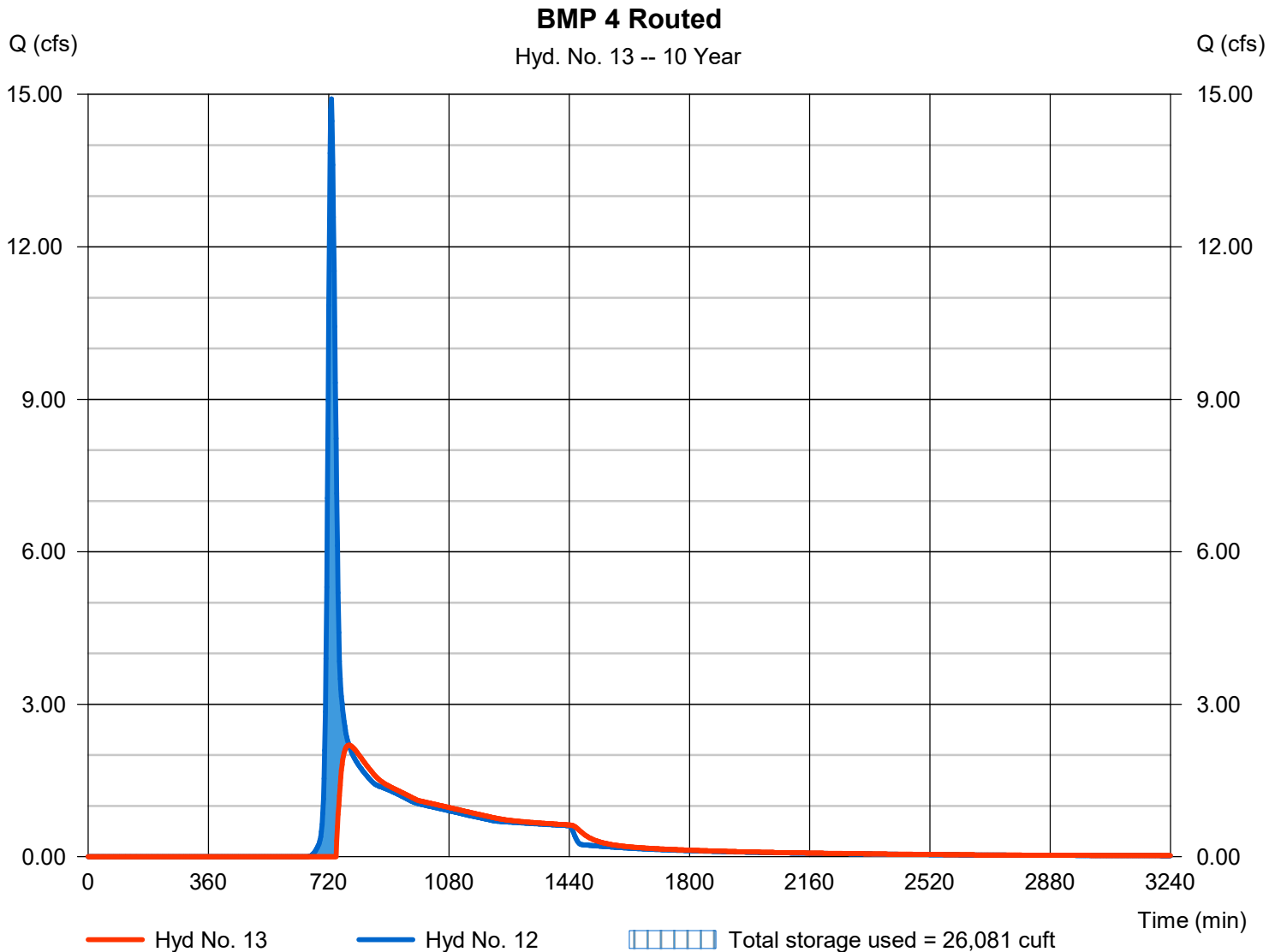
# Hydrograph Report

## Hyd. No. 13

BMP 4 Routed

Hydrograph type	= Reservoir	Peak discharge	= 2.194 cfs
Storm frequency	= 10 yrs	Time to peak	= 780 min
Time interval	= 2 min	Hyd. volume	= 56,259 cuft
Inflow hyd. No.	= 12 - BMP 4 IN	Max. Elevation	= 311.15 ft
Reservoir name	= BMP 4	Max. Storage	= 26,081 cuft

Storage Indication method used.

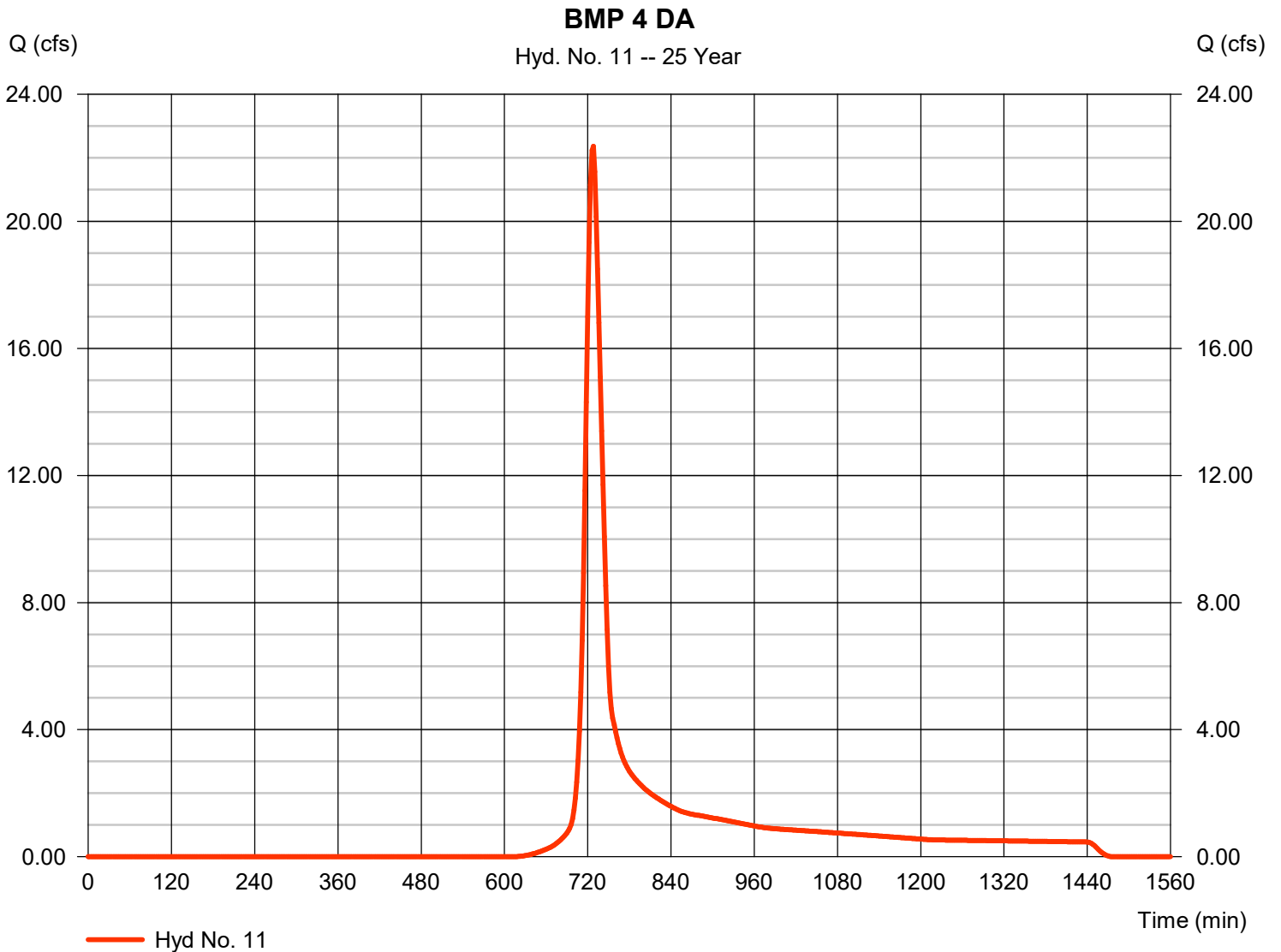


# Hydrograph Report

## Hyd. No. 11

BMP 4 DA

Hydrograph type	= SCS Runoff	Peak discharge	= 22.37 cfs
Storm frequency	= 25 yrs	Time to peak	= 728 min
Time interval	= 2 min	Hyd. volume	= 79,682 cuft
Drainage area	= 9.740 ac	Curve number	= 65
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 22.00 min
Total precip.	= 5.81 in	Distribution	= Type II
Storm duration	= 24 hrs	Shape factor	= 484



# Hydrograph Report

Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2022

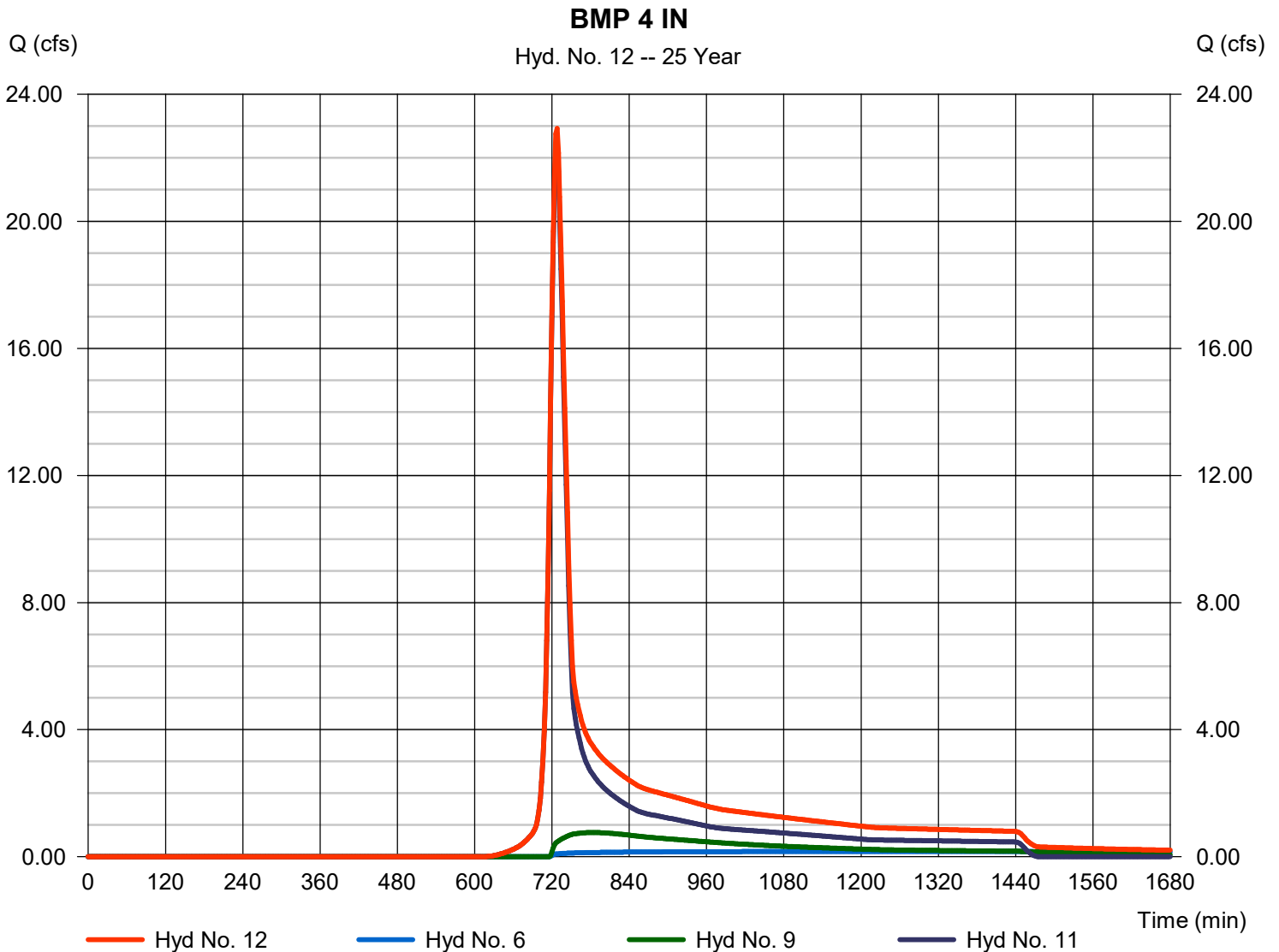
Monday, 01 / 16 / 2023

## Hyd. No. 12

BMP 4 IN

Hydrograph type = Combine  
Storm frequency = 25 yrs  
Time interval = 2 min  
Inflow hyds. = 6, 9, 11

Peak discharge = 22.92 cfs  
Time to peak = 728 min  
Hyd. volume = 117,945 cuft  
Contrib. drain. area = 9.740 ac





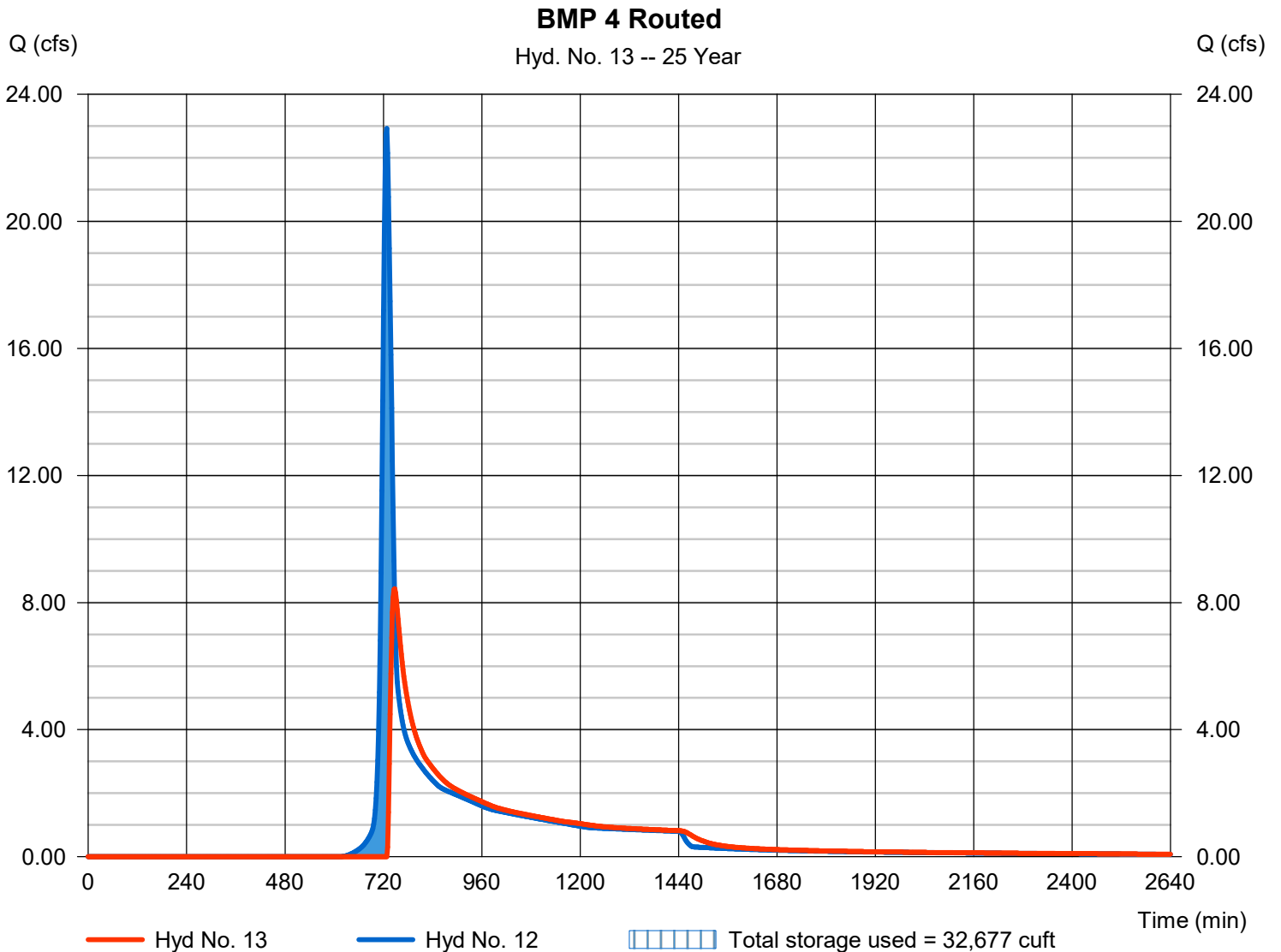
# Hydrograph Report

## Hyd. No. 13

BMP 4 Routed

Hydrograph type	= Reservoir	Peak discharge	= 8.434 cfs
Storm frequency	= 25 yrs	Time to peak	= 748 min
Time interval	= 2 min	Hyd. volume	= 96,206 cuft
Inflow hyd. No.	= 12 - BMP 4 IN	Max. Elevation	= 311.39 ft
Reservoir name	= BMP 4	Max. Storage	= 32,677 cuft

Storage Indication method used.

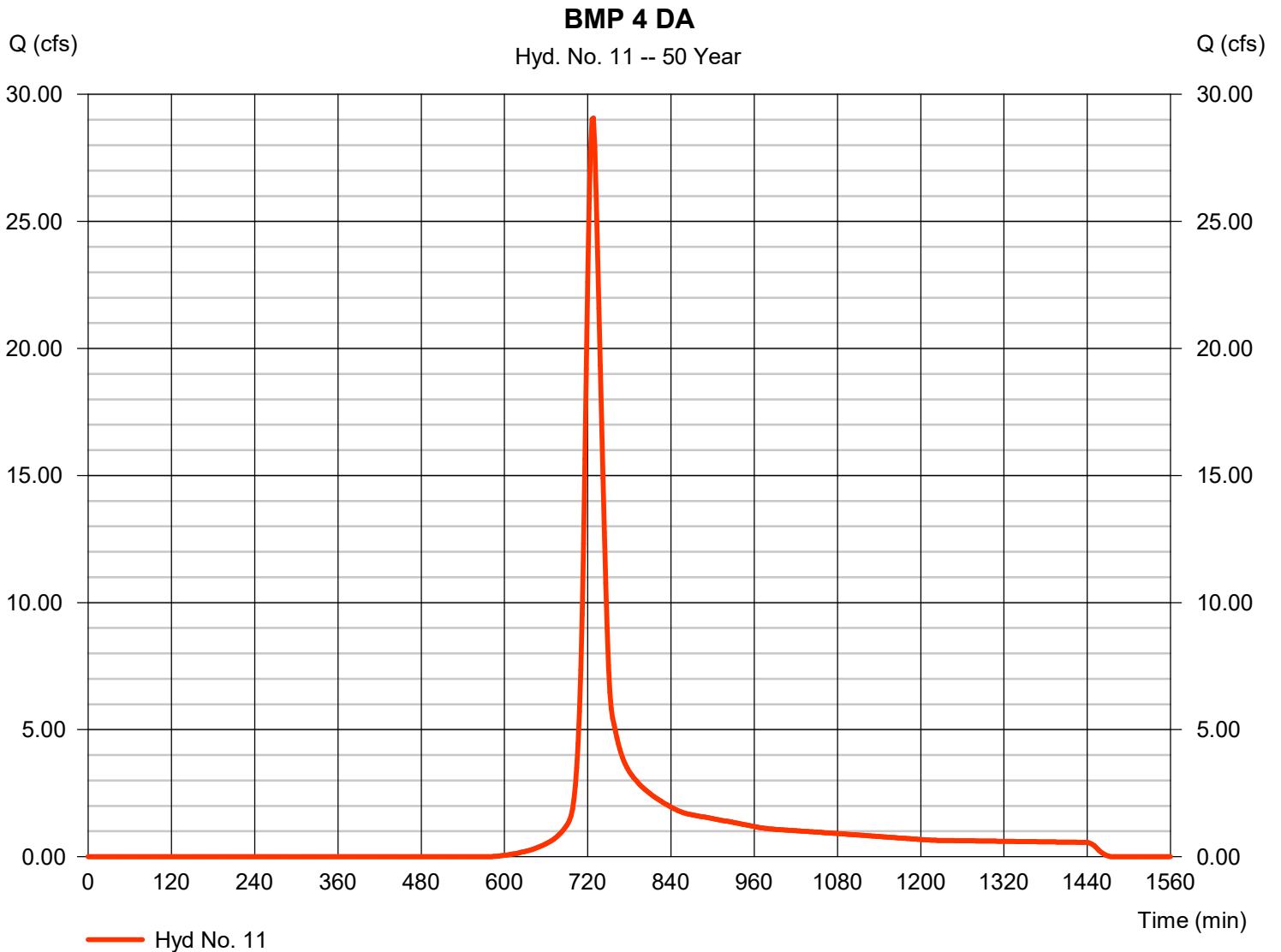


# Hydrograph Report

## Hyd. No. 11

BMP 4 DA

Hydrograph type	= SCS Runoff	Peak discharge	= 29.07 cfs
Storm frequency	= 50 yrs	Time to peak	= 728 min
Time interval	= 2 min	Hyd. volume	= 102,279 cuft
Drainage area	= 9.740 ac	Curve number	= 65
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 22.00 min
Total precip.	= 6.66 in	Distribution	= Type II
Storm duration	= 24 hrs	Shape factor	= 484



# Hydrograph Report

Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2022

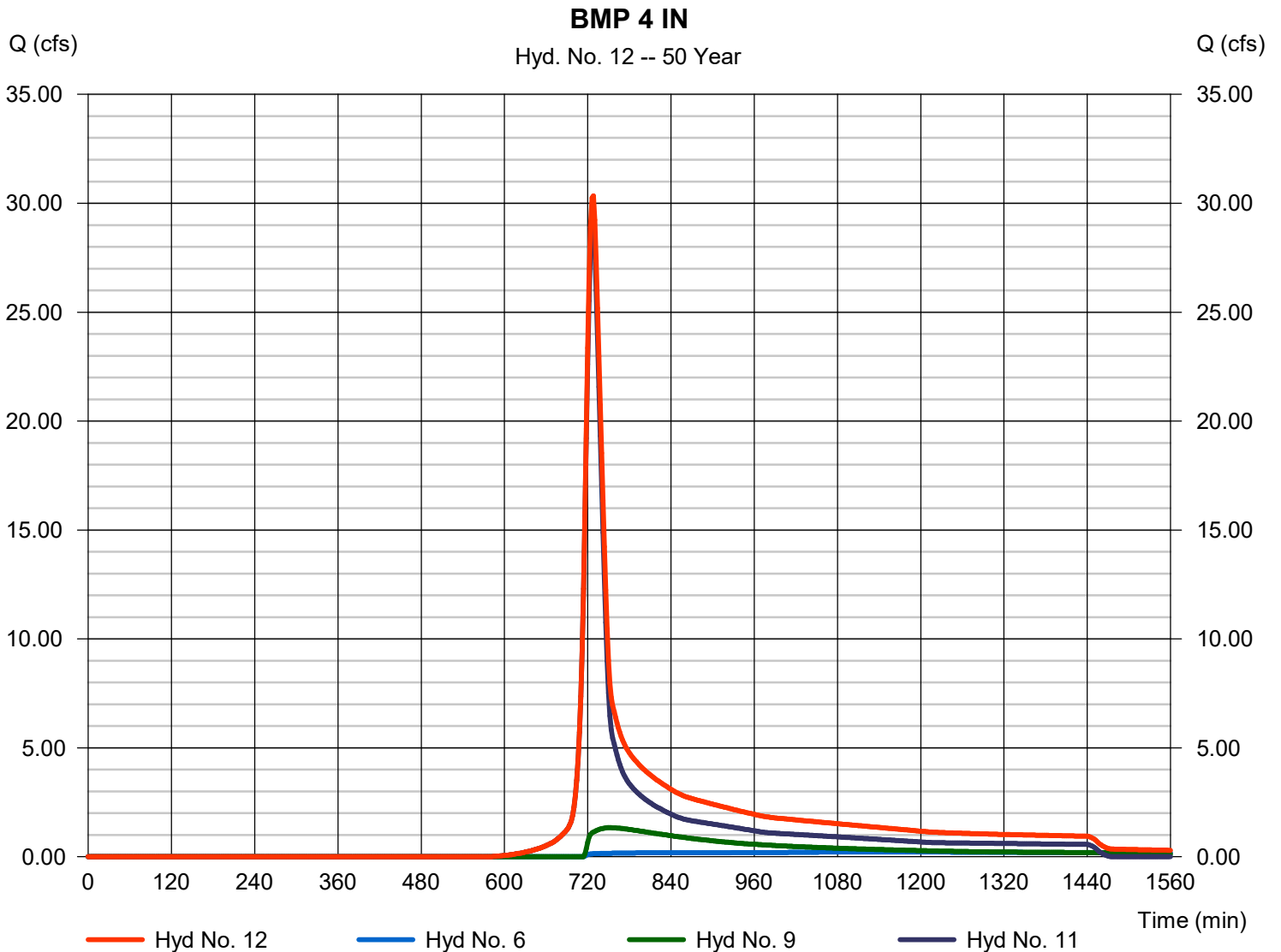
Monday, 01 / 16 / 2023

## Hyd. No. 12

BMP 4 IN

Hydrograph type = Combine  
Storm frequency = 50 yrs  
Time interval = 2 min  
Inflow hyds. = 6, 9, 11

Peak discharge = 30.34 cfs  
Time to peak = 728 min  
Hyd. volume = 153,197 cuft  
Contrib. drain. area = 9.740 ac



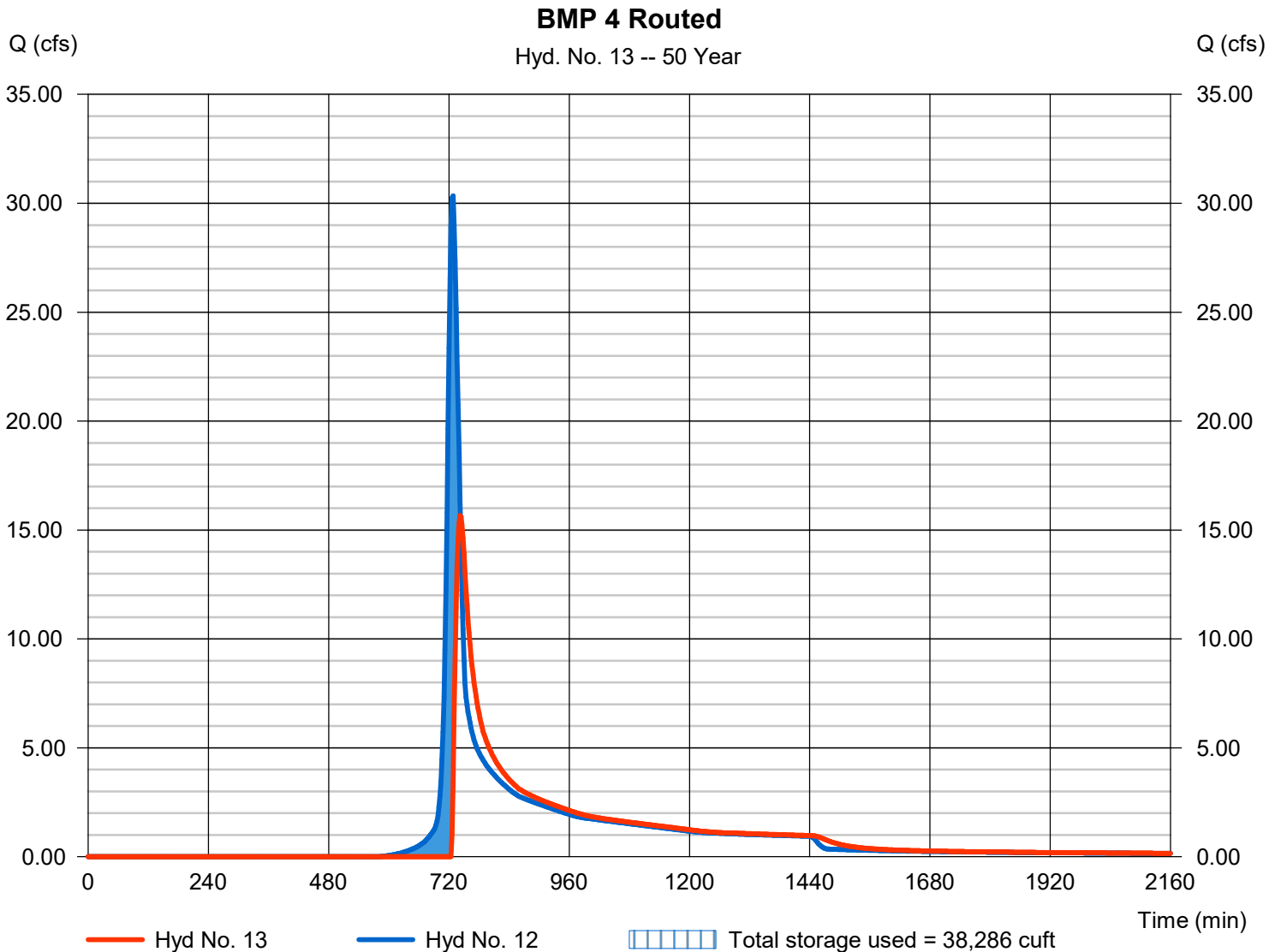
# Hydrograph Report

## Hyd. No. 13

### BMP 4 Routed

Hydrograph type	= Reservoir	Peak discharge	= 15.66 cfs
Storm frequency	= 50 yrs	Time to peak	= 742 min
Time interval	= 2 min	Hyd. volume	= 131,455 cuft
Inflow hyd. No.	= 12 - BMP 4 IN	Max. Elevation	= 311.58 ft
Reservoir name	= BMP 4	Max. Storage	= 38,286 cuft

Storage Indication method used.



# Hydrograph Report

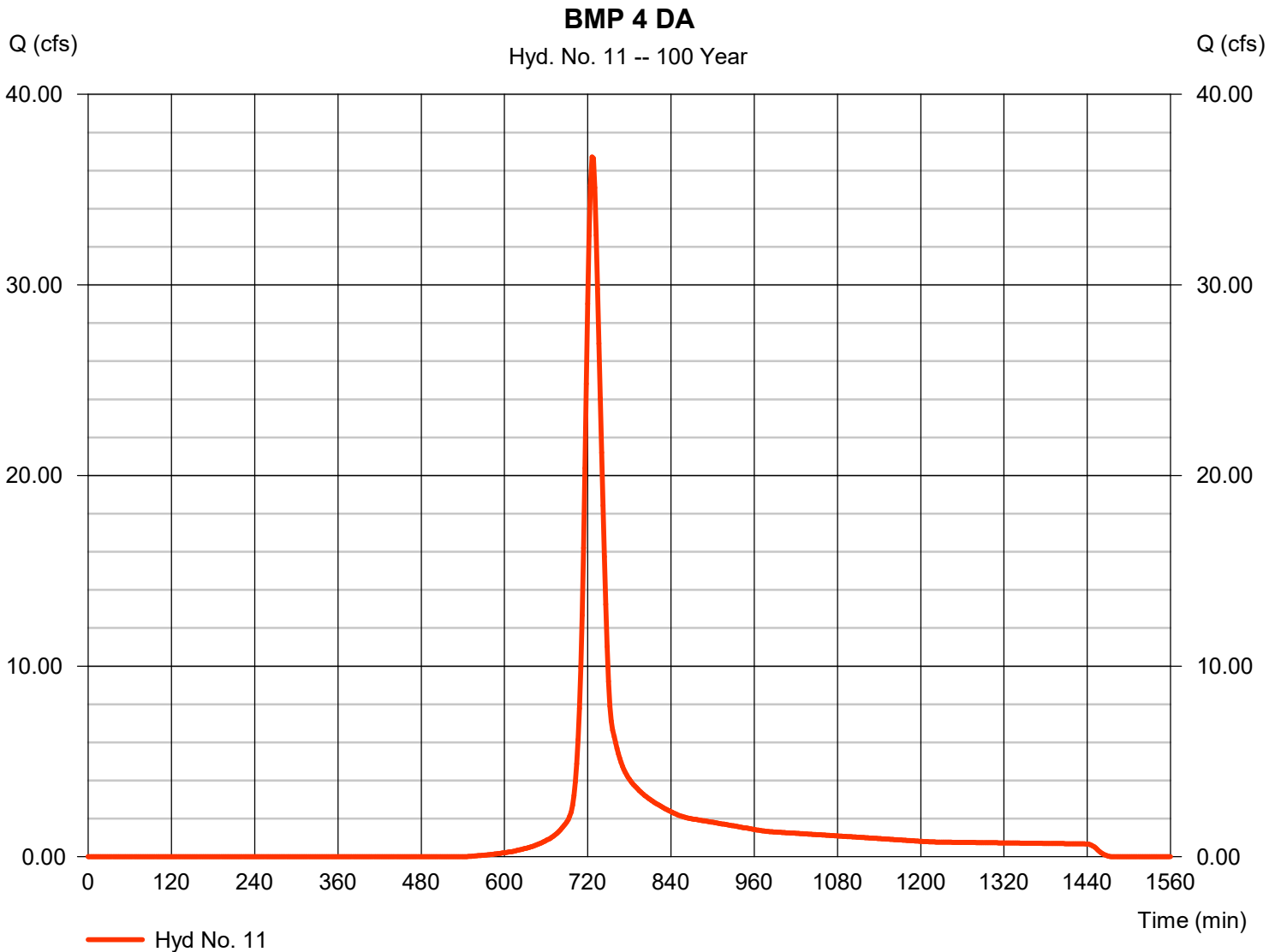
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2022

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## Hyd. No. 11

BMP 4 DA

Hydrograph type	= SCS Runoff	Peak discharge	= 36.71 cfs
Storm frequency	= 100 yrs	Time to peak	= 726 min
Time interval	= 2 min	Hyd. volume	= 128,024 cuft
Drainage area	= 9.740 ac	Curve number	= 65
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 22.00 min
Total precip.	= 7.58 in	Distribution	= Type II
Storm duration	= 24 hrs	Shape factor	= 484



# Hydrograph Report

Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2022

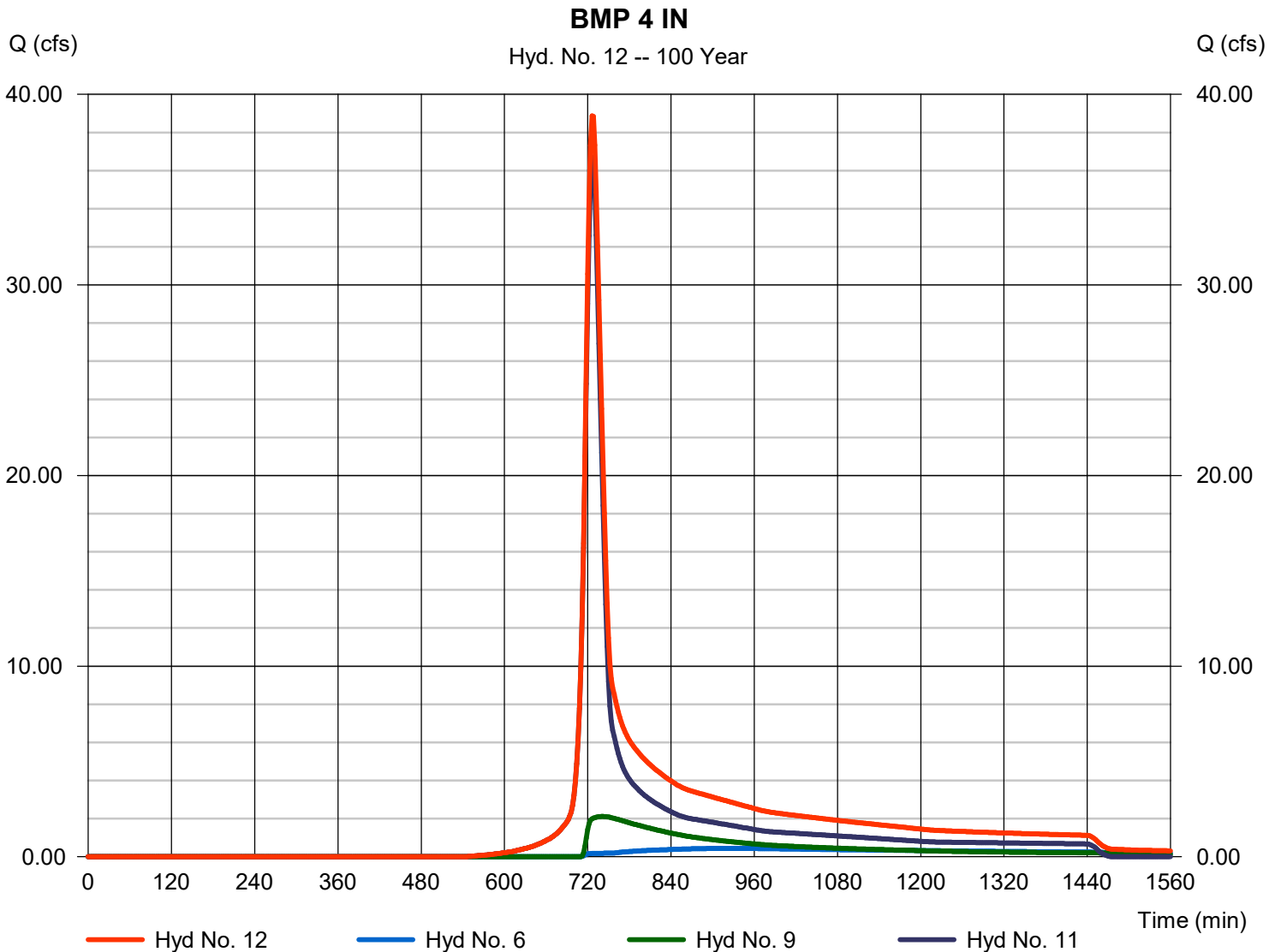
Monday, 01 / 16 / 2023

## Hyd. No. 12

BMP 4 IN

Hydrograph type = Combine  
Storm frequency = 100 yrs  
Time interval = 2 min  
Inflow hyds. = 6, 9, 11

Peak discharge = 38.87 cfs  
Time to peak = 726 min  
Hyd. volume = 192,802 cuft  
Contrib. drain. area = 9.740 ac



# Hydrograph Report

Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2022

Monday, 01 / 16 / 2023

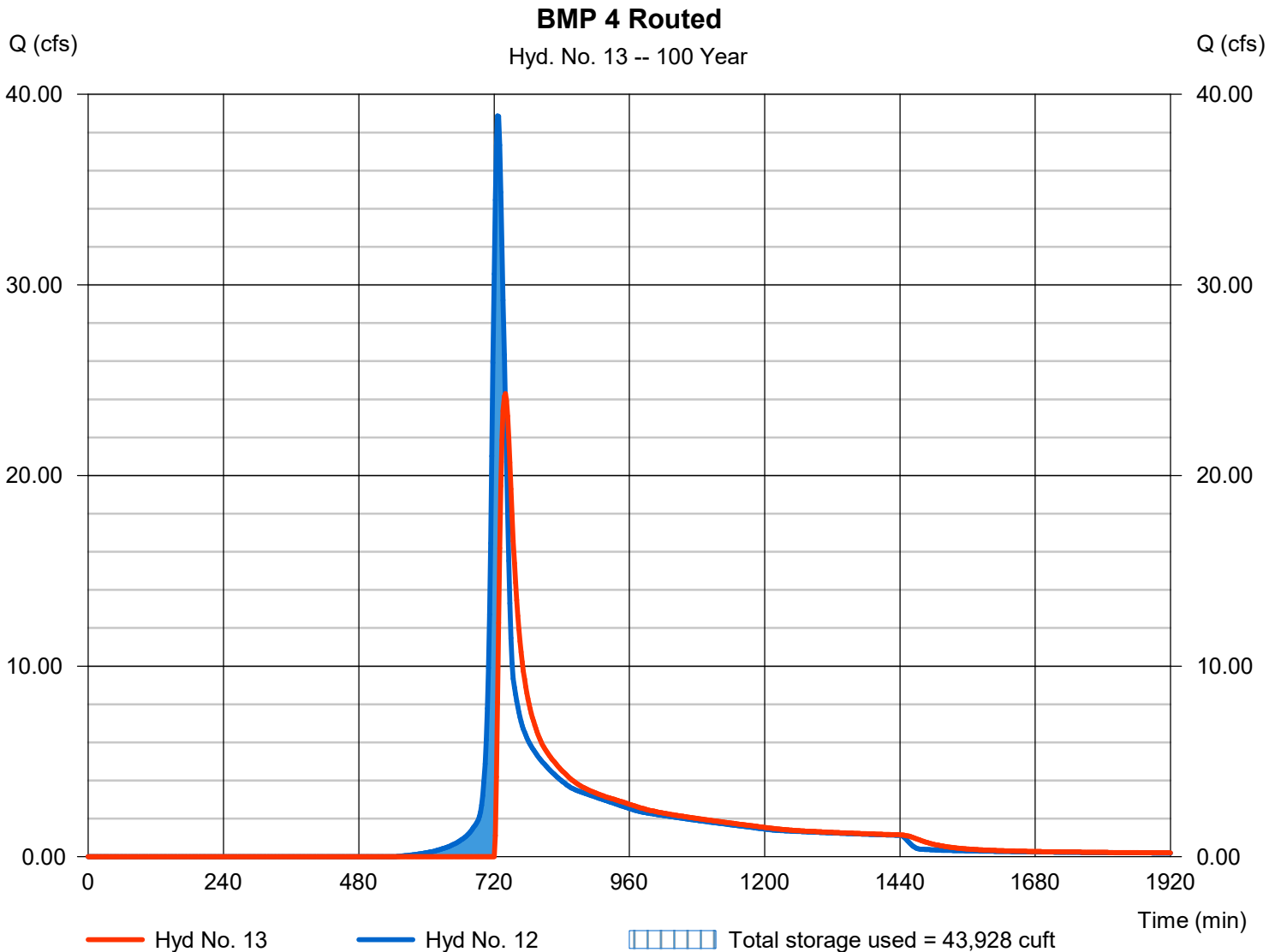
## Hyd. No. 13

BMP 4 Routed

Hydrograph type = Reservoir  
Storm frequency = 100 yrs  
Time interval = 2 min  
Inflow hyd. No. = 12 - BMP 4 IN  
Reservoir name = BMP 4

Peak discharge = 24.29 cfs  
Time to peak = 740 min  
Hyd. volume = 171,058 cuft  
Max. Elevation = 311.78 ft  
Max. Storage = 43,928 cuft

Storage Indication method used.

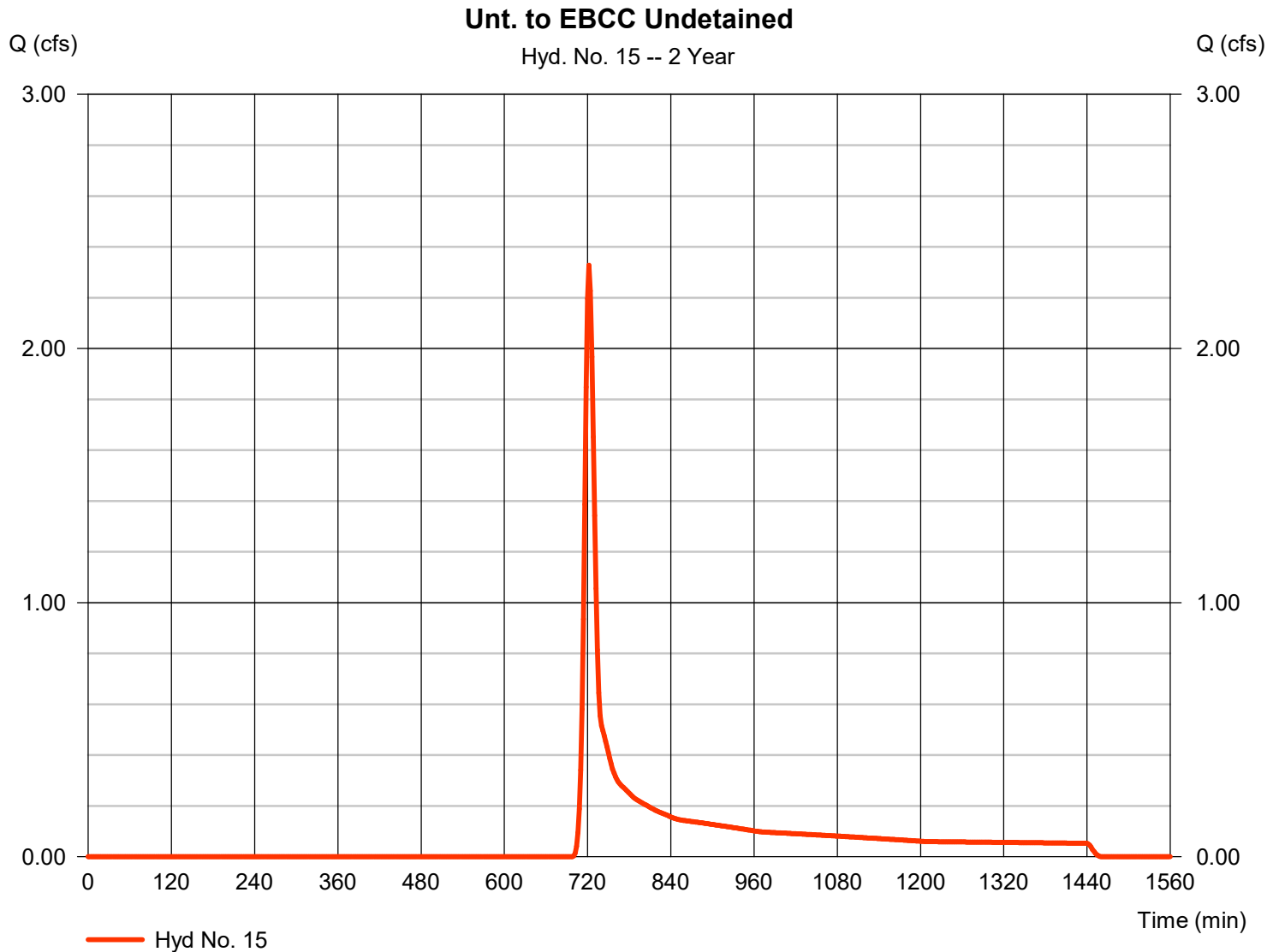


# Hydrograph Report

## Hyd. No. 15

Unt. to EBCC Undetained

Hydrograph type	= SCS Runoff	Peak discharge	= 2.328 cfs
Storm frequency	= 2 yrs	Time to peak	= 722 min
Time interval	= 2 min	Hyd. volume	= 6,908 cuft
Drainage area	= 2.740 ac	Curve number	= 66
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 12.00 min
Total precip.	= 3.26 in	Distribution	= Type II
Storm duration	= 24 hrs	Shape factor	= 484



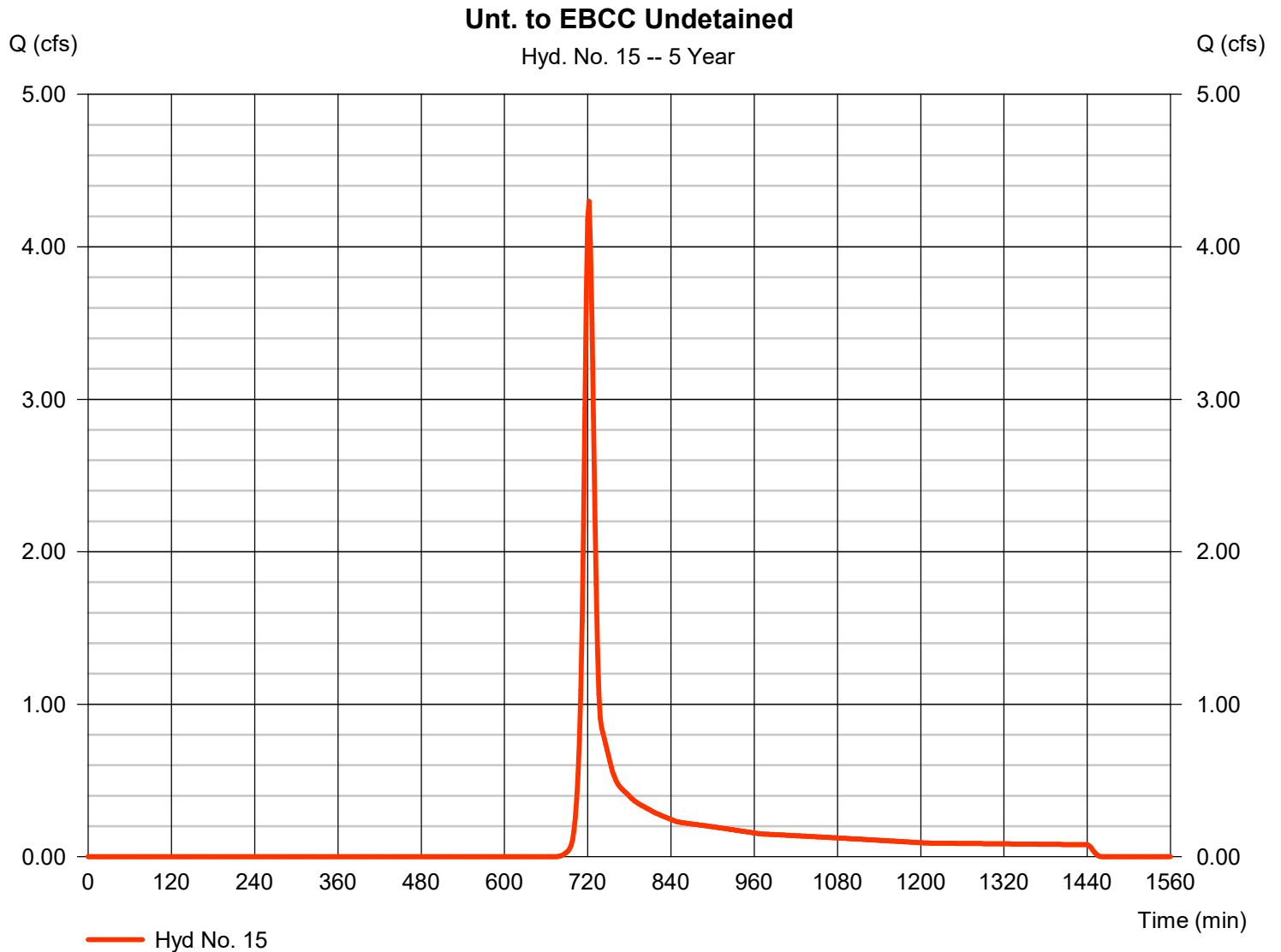


# Hydrograph Report

## Hyd. No. 15

Unt. to EBCC Undetained

Hydrograph type	= SCS Runoff	Peak discharge	= 4.298 cfs
Storm frequency	= 5 yrs	Time to peak	= 722 min
Time interval	= 2 min	Hyd. volume	= 11,756 cuft
Drainage area	= 2.740 ac	Curve number	= 66
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 12.00 min
Total precip.	= 4.10 in	Distribution	= Type II
Storm duration	= 24 hrs	Shape factor	= 484

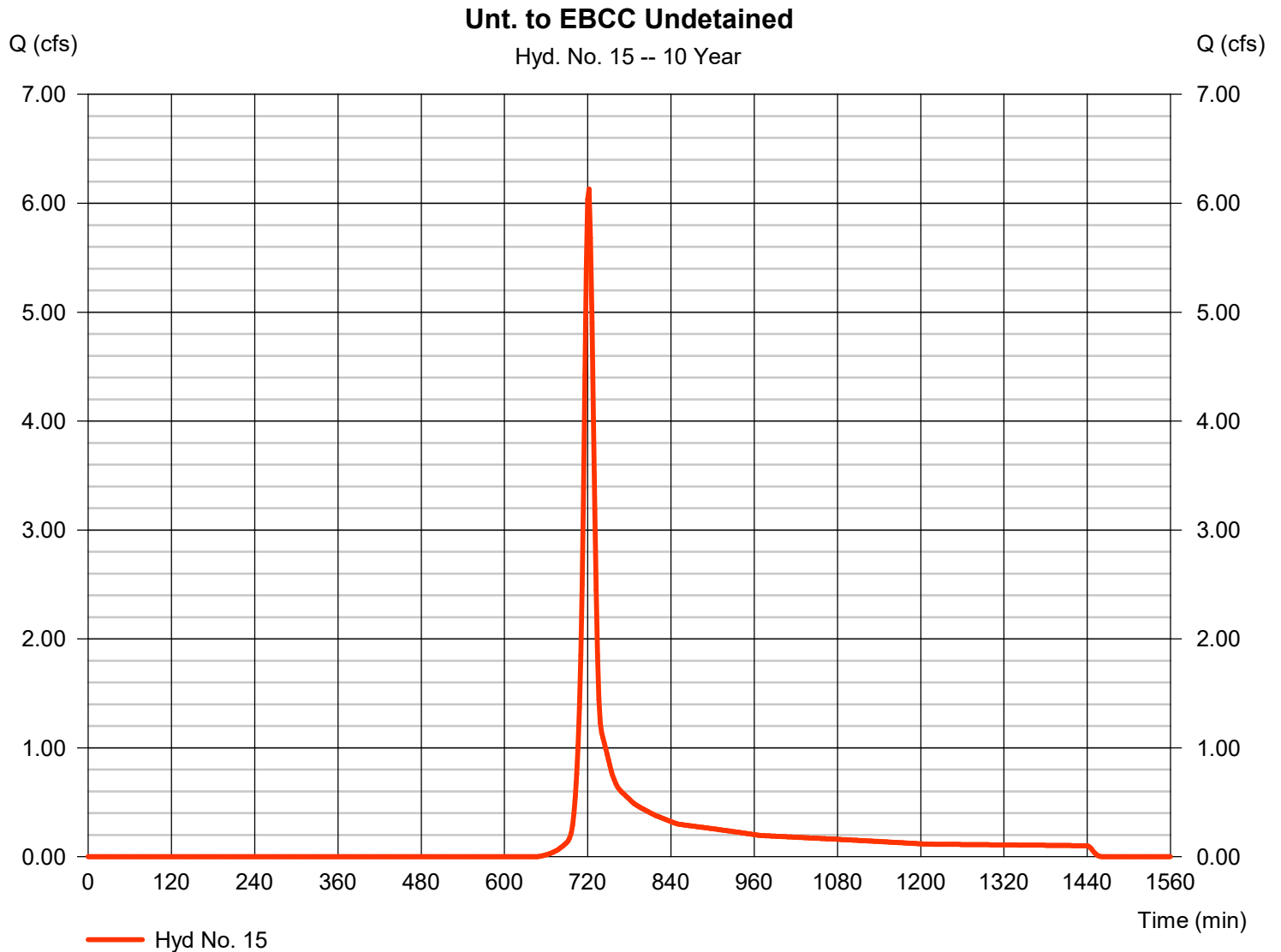


# Hydrograph Report

## Hyd. No. 15

Unt. to EBCC Undetained

Hydrograph type	= SCS Runoff	Peak discharge	= 6.130 cfs
Storm frequency	= 10 yrs	Time to peak	= 722 min
Time interval	= 2 min	Hyd. volume	= 16,338 cuft
Drainage area	= 2.740 ac	Curve number	= 66
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 12.00 min
Total precip.	= 4.80 in	Distribution	= Type II
Storm duration	= 24 hrs	Shape factor	= 484



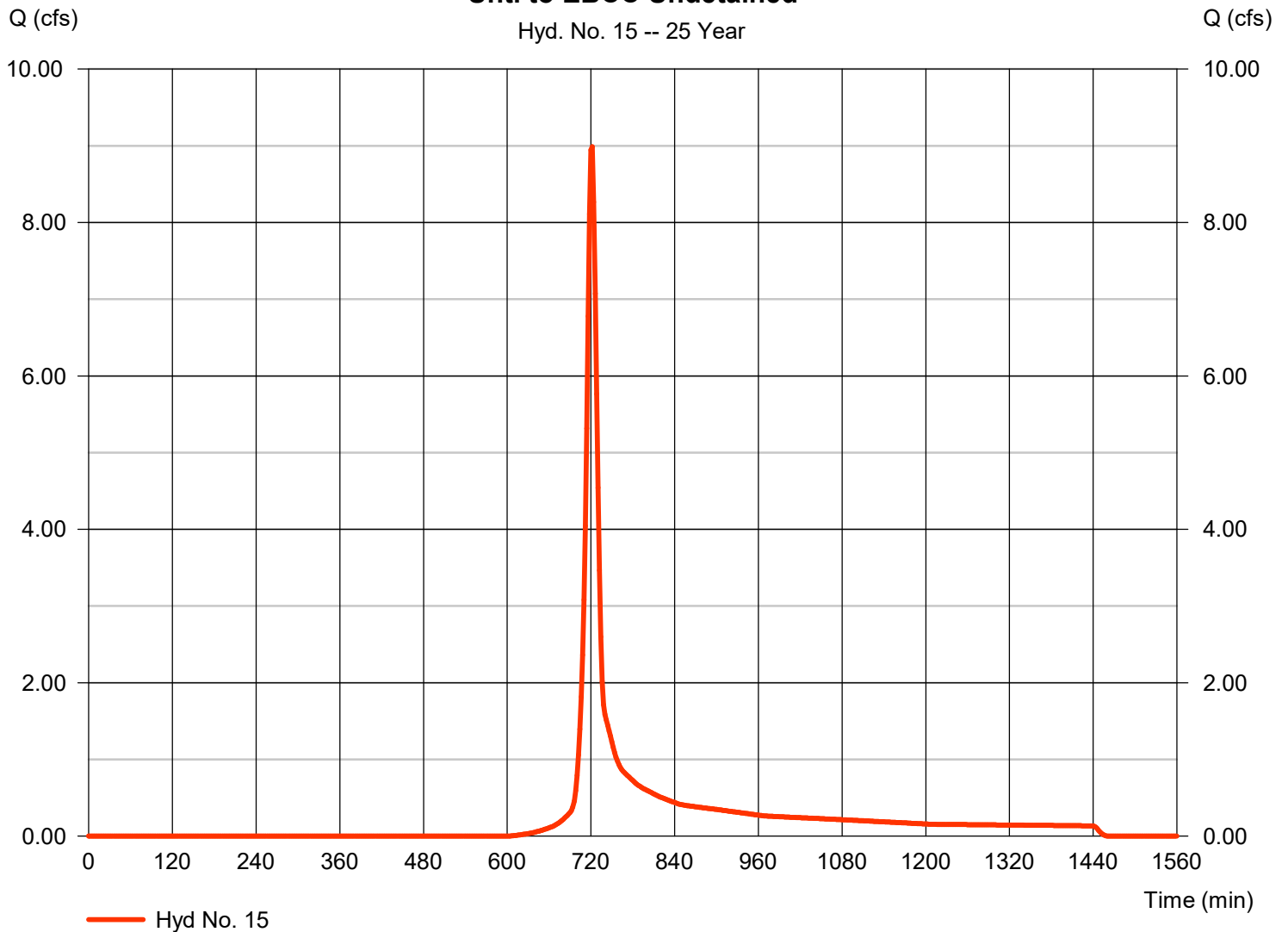
# Hydrograph Report

## Hyd. No. 15

Unt. to EBCC Undetained

Hydrograph type	= SCS Runoff	Peak discharge	= 8.988 cfs
Storm frequency	= 25 yrs	Time to peak	= 722 min
Time interval	= 2 min	Hyd. volume	= 23,595 cuft
Drainage area	= 2.740 ac	Curve number	= 66
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 12.00 min
Total precip.	= 5.81 in	Distribution	= Type II
Storm duration	= 24 hrs	Shape factor	= 484

### Unt. to EBCC Undetained

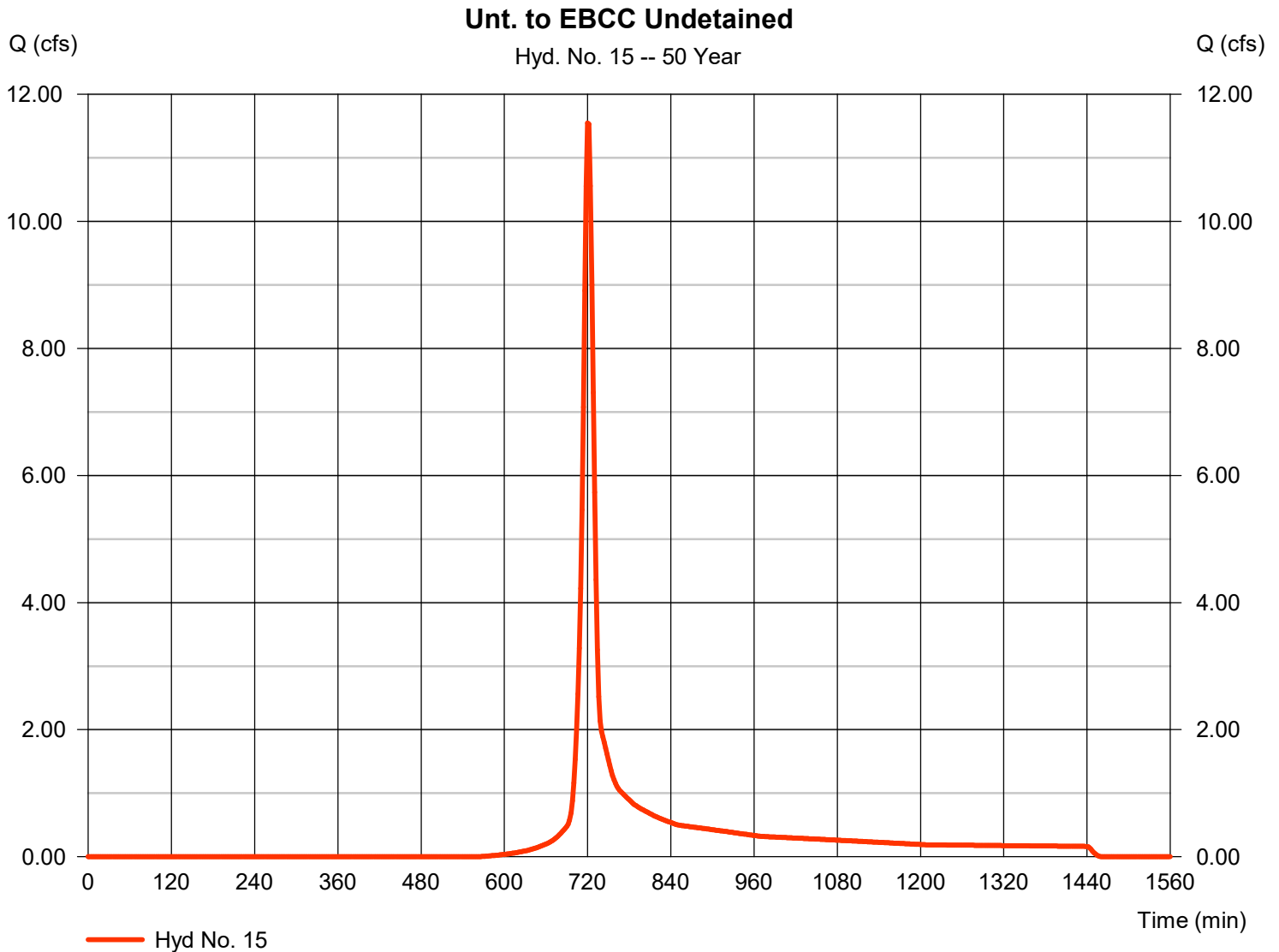


# Hydrograph Report

## Hyd. No. 15

Unt. to EBCC Undetained

Hydrograph type	= SCS Runoff	Peak discharge	= 11.55 cfs
Storm frequency	= 50 yrs	Time to peak	= 720 min
Time interval	= 2 min	Hyd. volume	= 30,153 cuft
Drainage area	= 2.740 ac	Curve number	= 66
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 12.00 min
Total precip.	= 6.66 in	Distribution	= Type II
Storm duration	= 24 hrs	Shape factor	= 484

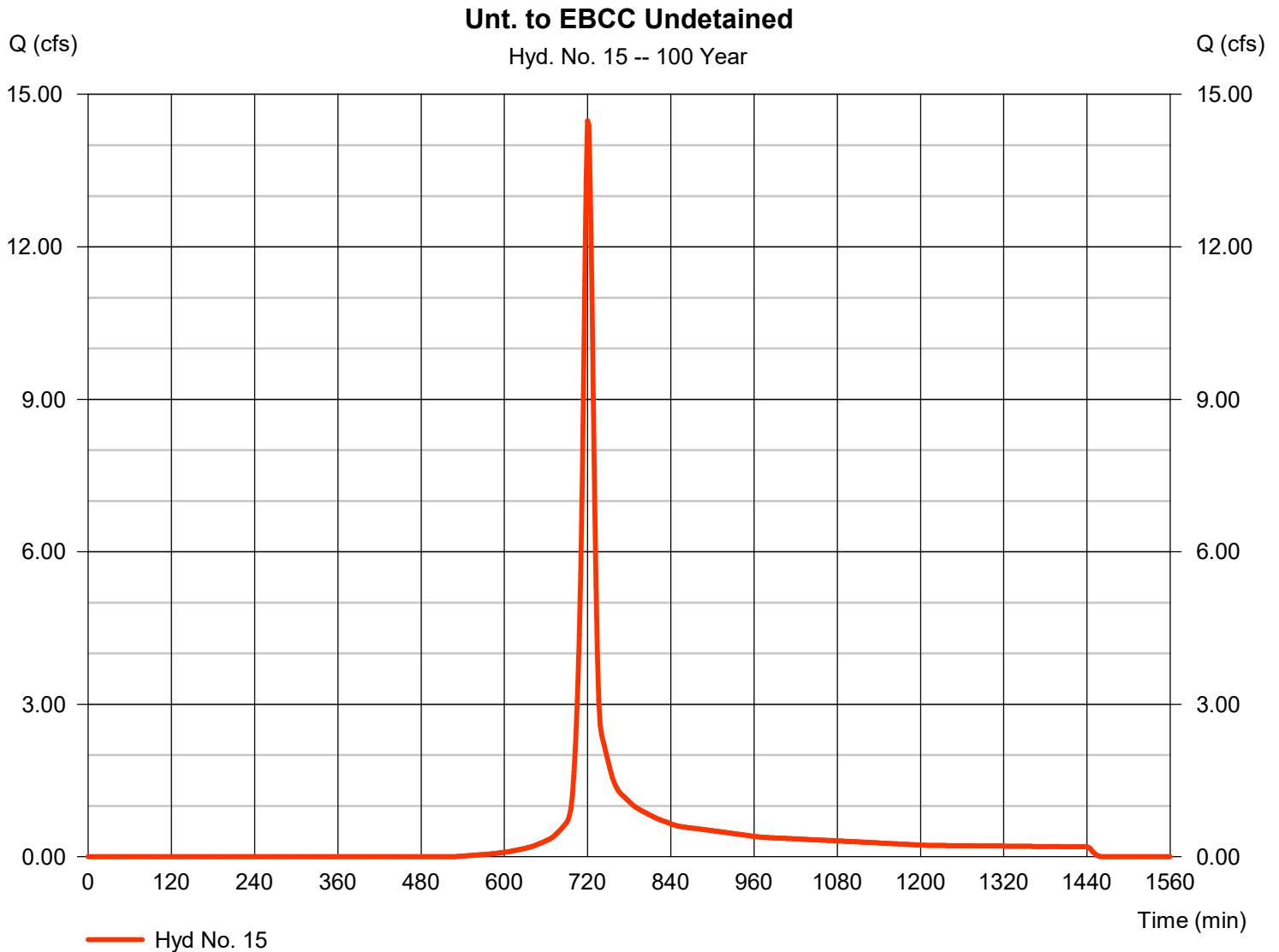


# Hydrograph Report

## Hyd. No. 15

Unt. to EBCC Undetained

Hydrograph type	= SCS Runoff	Peak discharge	= 14.48 cfs
Storm frequency	= 100 yrs	Time to peak	= 720 min
Time interval	= 2 min	Hyd. volume	= 37,604 cuft
Drainage area	= 2.740 ac	Curve number	= 66
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 12.00 min
Total precip.	= 7.58 in	Distribution	= Type II
Storm duration	= 24 hrs	Shape factor	= 484



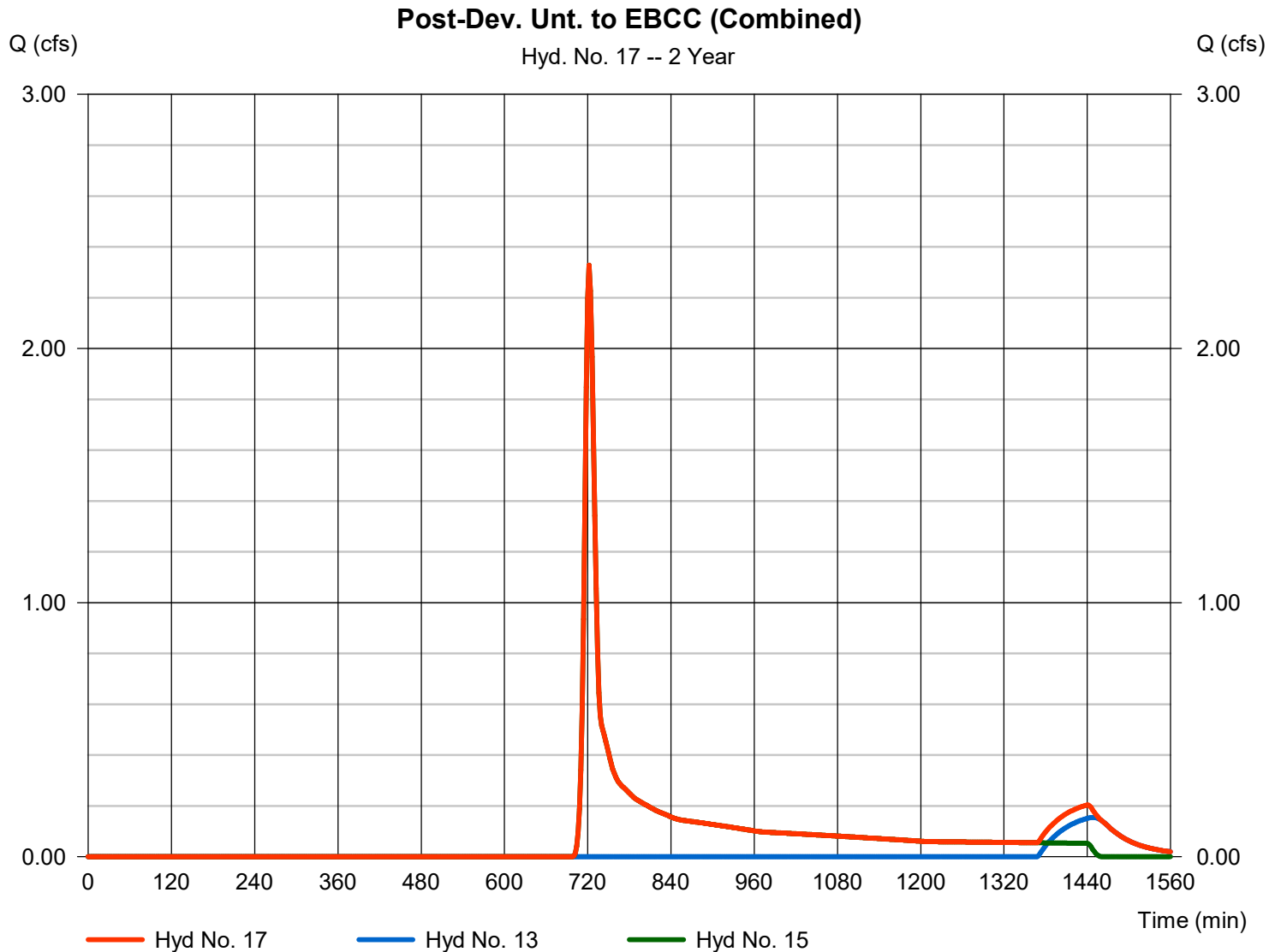
# Hydrograph Report

## Hyd. No. 17

Post-Dev. Unt. to EBCC (Combined)

Hydrograph type = Combine  
Storm frequency = 2 yrs  
Time interval = 2 min  
Inflow hyds. = 13, 15

Peak discharge = 2.328 cfs  
Time to peak = 722 min  
Hyd. volume = 8,615 cuft  
Contrib. drain. area = 2.740 ac



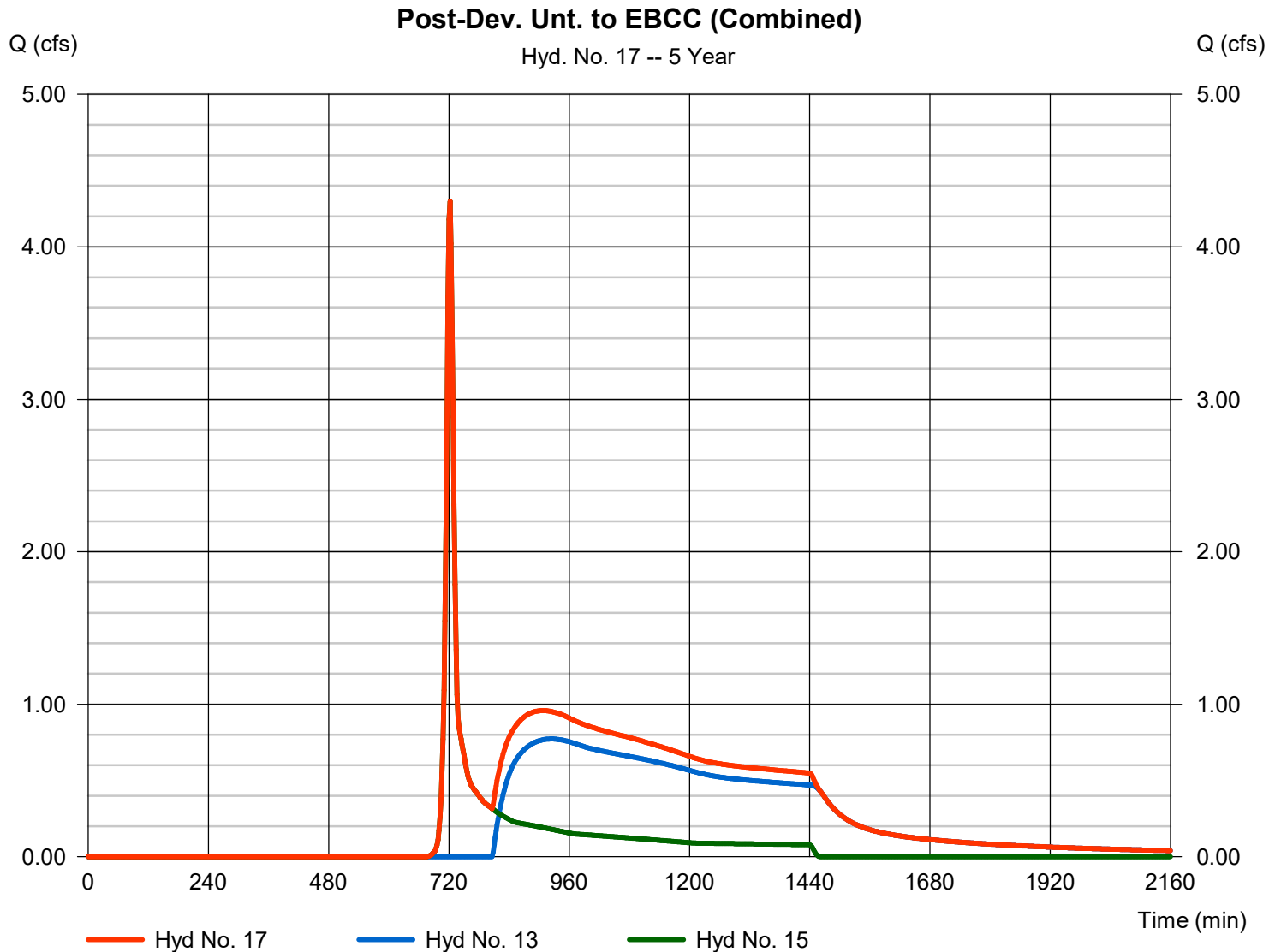
# Hydrograph Report

## Hyd. No. 17

Post-Dev. Unt. to EBCC (Combined)

Hydrograph type = Combine  
Storm frequency = 5 yrs  
Time interval = 2 min  
Inflow hyds. = 13, 15

Peak discharge = 4.298 cfs  
Time to peak = 722 min  
Hyd. volume = 41,946 cuft  
Contrib. drain. area = 2.740 ac



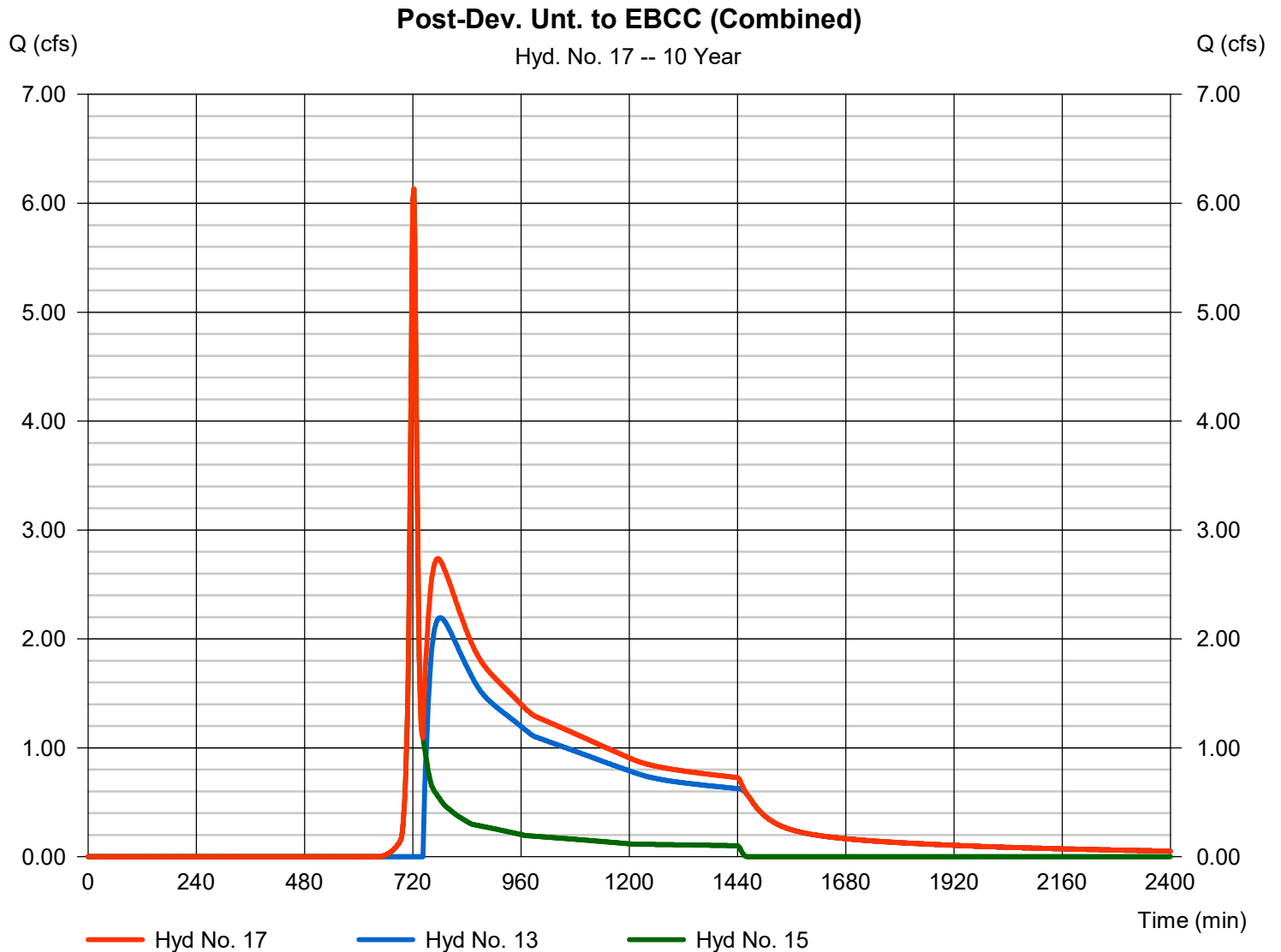
# Hydrograph Report

## Hyd. No. 17

Post-Dev. Unt. to EBCC (Combined)

Hydrograph type = Combine  
Storm frequency = 10 yrs  
Time interval = 2 min  
Inflow hyds. = 13, 15

Peak discharge = 6.130 cfs  
Time to peak = 722 min  
Hyd. volume = 72,598 cuft  
Contrib. drain. area = 2.740 ac





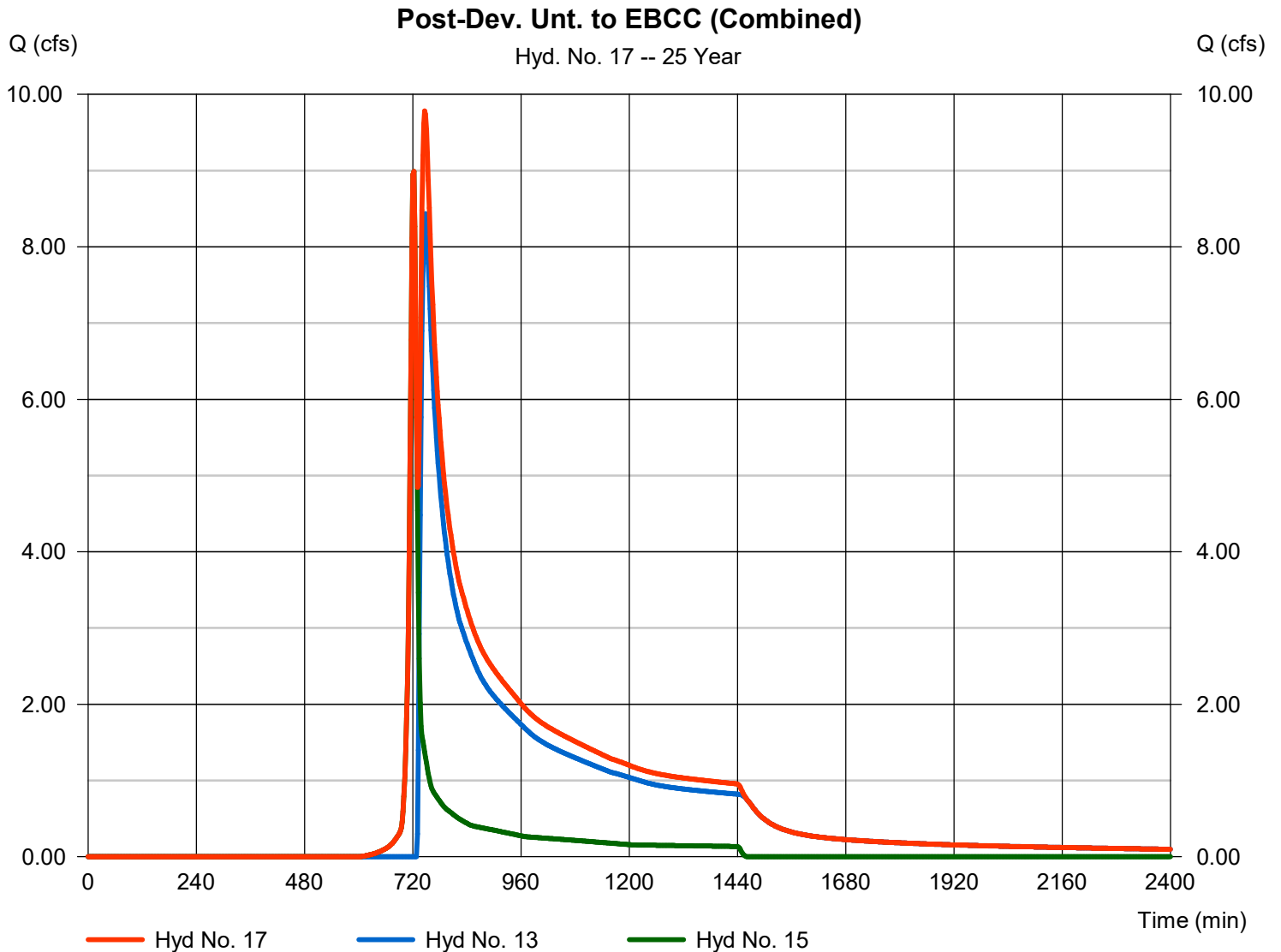
# Hydrograph Report

## Hyd. No. 17

Post-Dev. Unt. to EBCC (Combined)

Hydrograph type = Combine  
Storm frequency = 25 yrs  
Time interval = 2 min  
Inflow hyds. = 13, 15

Peak discharge = 9.782 cfs  
Time to peak = 746 min  
Hyd. volume = 119,801 cuft  
Contrib. drain. area = 2.740 ac



# Hydrograph Report

Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2022

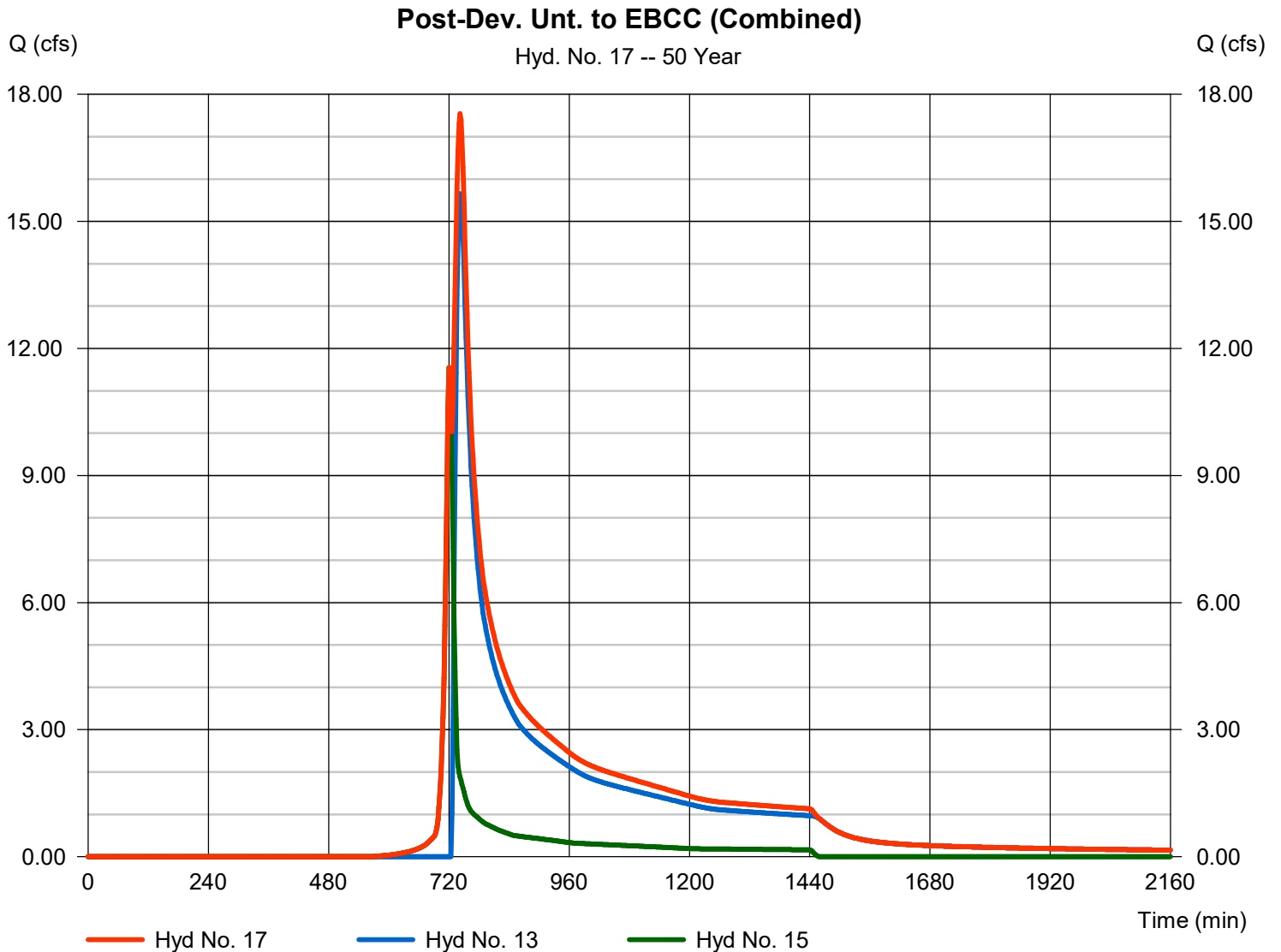
Monday, 01 / 16 / 2023

## Hyd. No. 17

Post-Dev. Unt. to EBCC (Combined)

Hydrograph type = Combine  
Storm frequency = 50 yrs  
Time interval = 2 min  
Inflow hyds. = 13, 15

Peak discharge = 17.54 cfs  
Time to peak = 742 min  
Hyd. volume = 161,607 cuft  
Contrib. drain. area = 2.740 ac



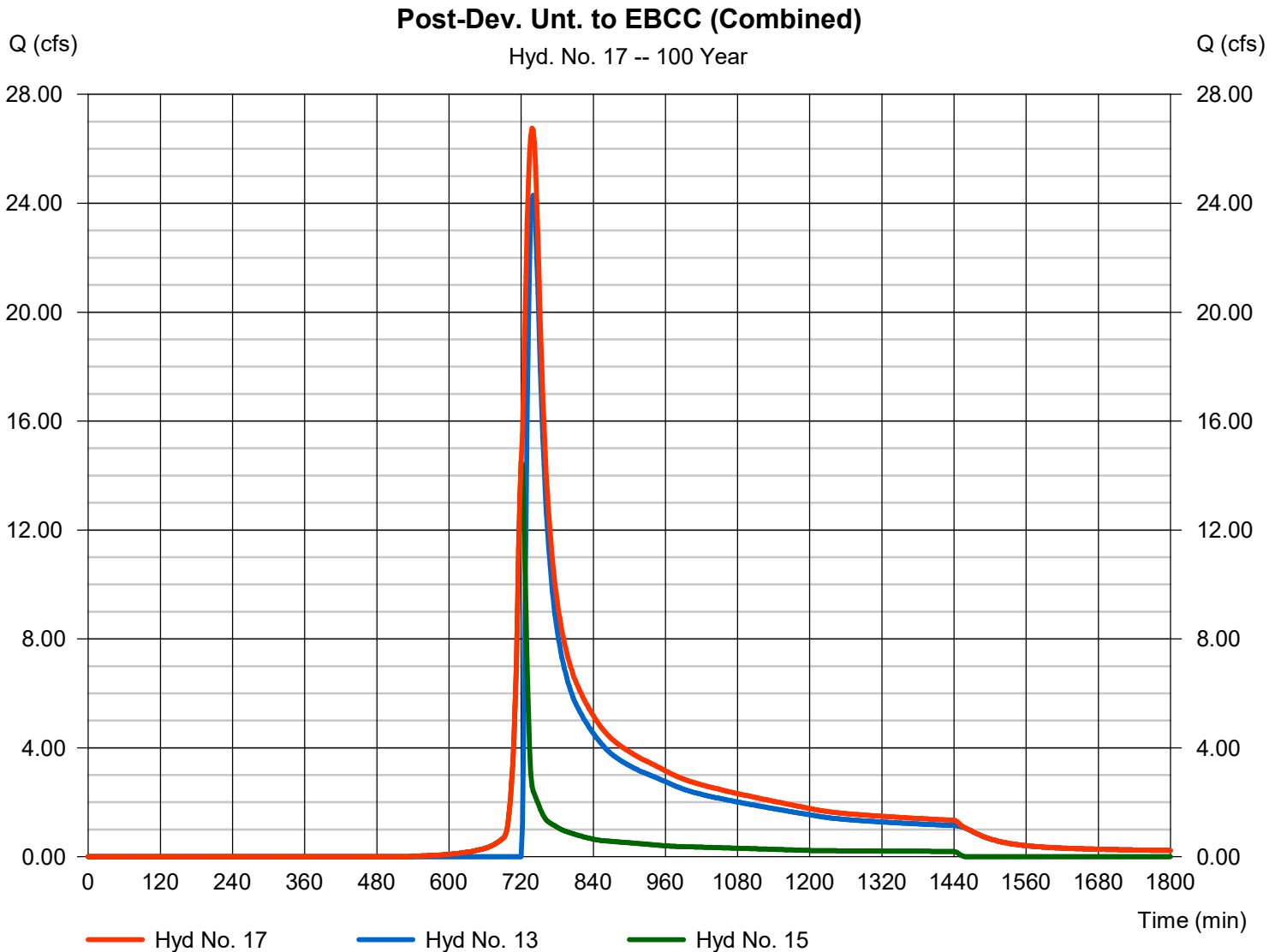
# Hydrograph Report

## Hyd. No. 17

Post-Dev. Unt. to EBCC (Combined)

Hydrograph type = Combine  
Storm frequency = 100 yrs  
Time interval = 2 min  
Inflow hyds. = 13, 15

Peak discharge = 26.76 cfs  
Time to peak = 738 min  
Hyd. volume = 208,663 cuft  
Contrib. drain. area = 2.740 ac



## **APPENDIX F**

### **STORM SEWER CALCULATIONS**



# INLET AREA COEFFICIENTS AND SURFACE FLOWS

PROJECT: The Westtown School - Oak Lane Project  
 LOCATION: Westtown Township  
 COUNTY: Chester

INLET COVER TYPE	B SOIL			D SOIL		AREA (ac.)	COMP. C	Tc (min)	COMMENTS
	IMP	LAWN	WOODS	LAWN	WOODS				
C COEFFICIENTS	0.99	0.25	0.34	0.65	0.7				
I-A3	0.06	1.72	0.00	0.00	0.00	1.79	0.28	5	
I-A5	0.15	0.58	0.00	0.00	0.00	0.73	0.40	5	
I-A6	0.26	0.09	0.00	0.00	0.00	0.35	0.80	5	
I-A7	0.06	0.00	0.00	0.00	0.00	0.06	0.96	5	
I-A8	0.31	0.18	0.00	0.00	0.00	0.48	0.72	5	
I-A9	0.12	0.03	0.00	0.00	0.00	0.15	0.85	5	
I-A10	0.06	0.05	0.00	0.00	0.00	0.11	0.65	5	
I-A11	0.10	0.27	0.00	0.00	0.00	0.37	0.45	5	

# Hydraflow Storm Sewers Extension for Autodesk® Civil 3D® Plan



# Storm Sewer Tabulation

Station	Line	To Line	Len (ft)	Drng Area (ac)		Rnoff coeff (C)	Area x C		Tc		Rain (l) (in/hr)	Total flow (cfs)	Cap full (cfs)	Vel (ft/s)	Pipe		Invert Elev (ft)		HGL Elev (ft)		Grnd / Rim Elev (ft)		Line ID
				Incr	Total		Incr	Total	Inlet (min)	Syst (min)					Size (in)	Slope (%)	Dn	Up	Dn	Up	Dn	Up	
1	End		59.980	1.79	4.04	0.28	0.50	1.84	5.0	7.4	6.6	12.08	10.06	7.09	18	0.92	289.50	290.05	290.82	291.68	0.00	292.80	A3 to A2
2	1		23.270	0.00	2.25	0.00	0.00	1.34	0.0	7.3	6.6	8.82	18.21	5.03	18	3.01	290.05	290.75	292.05	292.19	292.80	296.20	A4 to A3
3	2		89.010	0.73	2.25	0.40	0.29	1.34	5.0	7.1	6.7	8.92	9.57	5.79	18	0.83	291.00	291.74	292.31	292.89	296.20	295.34	A5 to A4
4	3		46.880	0.35	1.52	0.80	0.28	1.05	5.0	6.9	6.7	7.01	14.61	6.34	15	5.12	291.84	294.24	292.89	295.30	297.84	305.00	A6 to A5
5	4		184.000	0.06	1.17	0.96	0.06	0.77	5.0	6.4	6.9	5.27	12.29	5.30	15	3.62	294.34	301.00	295.30	301.93	305.00	306.00	A7 to A6
6	5		103.890	0.48	1.11	0.72	0.35	0.71	5.0	6.0	7.0	4.95	6.40	5.47	15	0.98	301.10	302.12	301.93	303.02	305.00	306.00	A8 to A7
7	6		71.110	0.15	0.63	0.85	0.13	0.37	5.0	5.8	7.1	2.58	4.65	4.15	12	1.70	302.22	303.43	303.02	304.12	306.00	307.13	A9 to A8
8	7		136.000	0.11	0.48	0.65	0.07	0.24	5.0	5.1	7.3	1.73	3.44	3.72	12	0.93	303.53	304.80	304.12	305.36	307.13	308.37	A10 to A9
9	8		29.850	0.37	0.37	0.45	0.17	0.17	5.0	5.0	7.3	1.22	3.51	3.43	12	0.97	304.90	305.19	305.36	305.65	308.37	308.73	A11 to A10
Project File: Westtown-PIPES_A.stm																Number of lines: 9						Run Date: 1/16/2023	

NOTES: Intensity = 50.00 / (Inlet time + 9.70) ^ 0.72; Return period = Yrs. 100 ; c = cir e = ellip b = box

# ELA GROUP

ENGINEERS &  
LANDSCAPE ARCHITECTS

737 S. BROAD STREET  
LITITZ, PA 17543  
(717) 626-72713



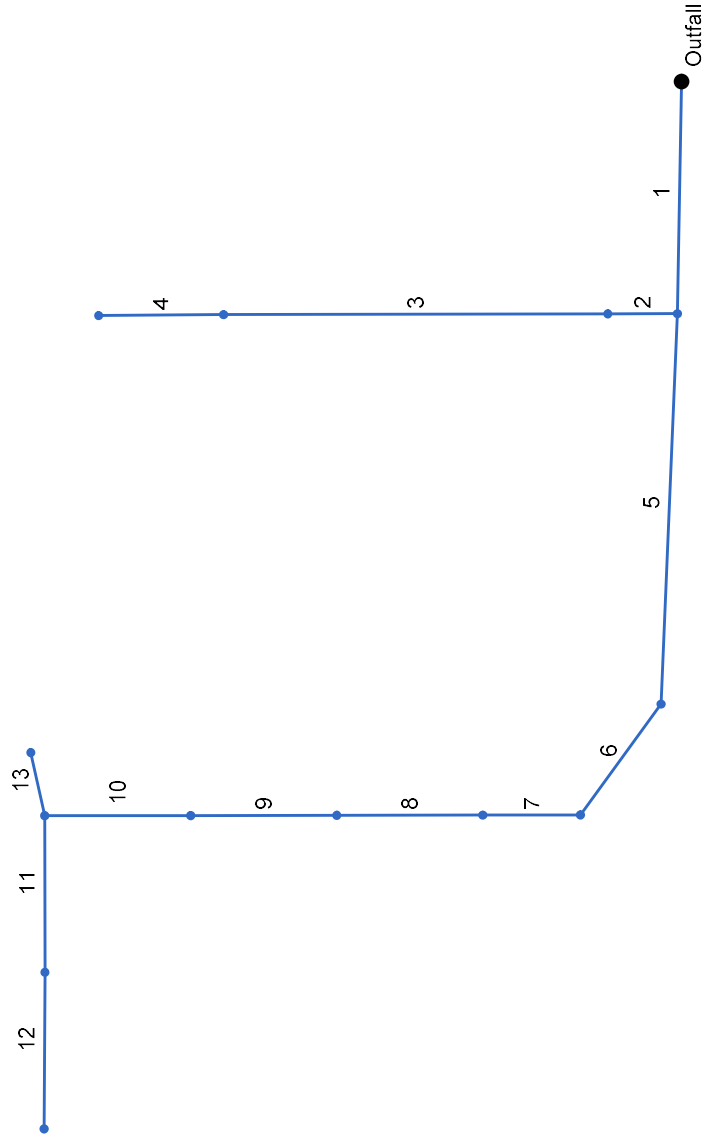
# INLET AREA COEFFICIENTS AND SURFACE FLOWS

PROJECT: The Westtown School - Oak Lane Project  
LOCATION: Westtown Township  
COUNTY: Chester

INLET	COVER TYPE	TYPE	B SOIL			D SOIL		AREA (ac.)	COMP. C	Tc (min)	COMMENTS
			IMP	LAWN	CULTIVATED	LAWN	CULTIVATED				
	C COEFFICIENTS		0.99	0.25	0.43	0.65	0.67				
I-B4			0.00	0.00	0.00	0.00	0.00	0.00		5	0.25 CFS FROM B-3
I-B5			0.00	0.04	0.00	0.00	0.00	0.04	0.25	5	
I-B6			0.00	0.04	0.00	0.00	0.00	0.04	0.25	5	
I-B8			0.00	0.08	0.00	0.00	0.00	0.08	0.25	5	0.92 CFS FROM B-2
I-B9			0.00	0.12	0.00	0.00	0.00	0.12	0.25	5	
I-B10			0.06	0.05	0.00	0.00	0.00	0.11	0.65	5	
I-B11			0.01	0.09	0.00	0.00	0.00	0.11	0.33	5	
I-B12			0.08	0.13	0.00	0.00	0.00	0.21	0.54	5	
I-B12A			0.01	0.02	0.00	0.00	0.00	0.03	0.57	5	
I-B13			0.01	0.04	0.00	0.00	0.00	0.05	0.45	5	
I-B14			0.02	0.02	0.00	0.00	0.00	0.03	0.61	5	
I-B18			0.15	0.86	0.35	0.00	0.00	1.35	0.38	5	



# Hydraflow Storm Sewers Extension for Autodesk® Civil 3D® Plan



# Storm Sewer Tabulation

Station	Line	To Line	Len (ft)	Drng Area		Rnoff coeff (C)	Area x C		Tc		Rain (l) (in/hr)	Total flow (cfs)	Cap full (cfs)	Vel (ft/s)	Pipe		Invert Elev		HGL Elev		Grnd / Rim Elev		Line ID
				Incr (ac)	Total (ac)		Incr (min)	Syst (min)	Incr (in)	Slope (%)					Dn (ft)	Up (ft)	Dn (ft)	Up (ft)	Dn (ft)	Up (ft)			
1	End		148.240	0.00	0.82	0.00	0.00	0.35	5.0	11.6	5.6	4.50	4.59	3.73	15	0.51	310.00	310.75	311.25	311.91	0.00	316.00	MH-B3 TO EW-B2
2	1		44.610	0.00	0.08	0.00	0.00	0.02	5.0	7.0	6.7	0.57	11.74	1.72	12	10.87	311.15	316.00	312.13	316.31	316.00	322.25	I-B4 TO MH-B3
3	2		246.000	0.04	0.08	0.25	0.01	0.02	5.0	5.7	7.1	0.58	1.22	3.25	8	1.02	316.25	318.75	316.57	319.11	322.25	322.25	I-B5 TO I-B4
4	3		80.000	0.04	0.04	0.25	0.01	0.01	5.0	5.0	7.3	0.07	1.22	1.79	8	1.01	319.19	320.00	319.30	320.12	322.25	322.00	I-B6 TO I-B5
5	1		249.540	0.00	0.74	0.00	0.00	0.33	5.0	10.4	5.8	4.03	4.57	3.48	15	0.50	310.75	312.00	312.13	313.05	316.00	321.00	MH-B7 TO MH-B3
6	5		87.620	0.08	0.74	0.25	0.02	0.33	5.0	10.1	5.9	4.06	4.88	3.73	15	0.57	312.00	312.50	313.17	313.45	321.00	317.00	I-B8 TO MH-B7
7	6		62.500	0.12	0.66	0.25	0.03	0.31	5.0	9.6	6.0	1.86	2.55	2.37	12	0.51	312.50	312.82	313.77	313.94	317.00	317.00	I-B9 TO I-B8
8	7		93.500	0.11	0.54	0.65	0.07	0.28	5.0	8.9	6.2	1.72	2.52	2.26	12	0.50	312.82	313.29	313.99	314.18	317.00	317.00	I-B10 TO I-B9
9	8		93.500	0.11	0.43	0.33	0.04	0.21	5.0	8.3	6.3	1.31	1.55	2.45	10	0.50	313.29	313.76	314.23	314.53	317.00	317.00	I-B11 TO I-B10
10	9		93.500	0.21	0.32	0.54	0.11	0.17	5.0	7.6	6.5	1.11	1.55	2.39	10	0.50	313.76	314.23	314.58	314.81	317.00	317.00	I-B12 TO I-B11
11	10		100.000	0.05	0.08	0.45	0.02	0.04	5.0	6.2	6.9	0.28	0.85	1.16	8	0.50	314.23	314.73	314.99	315.08	317.00	317.00	I-B13 TO I-B12
12	11		100.000	0.03	0.03	0.61	0.02	0.02	5.0	5.0	7.3	0.13	0.87	1.30	8	0.52	314.73	315.25	315.10	315.42	317.00	317.00	I-B14 TO I-B13
13	10		41.260	0.03	0.03	0.57	0.02	0.02	5.0	5.0	7.3	0.12	0.86	0.38	8	0.51	314.23	314.44	314.99	314.99	317.00	318.65	I-B12A TO I-B12

Project File: Westtown-PIPES\_B.stm

Number of lines: 13

Run Date: 1/16/2023

NOTES: Intensity = 50.00 / (Inlet time + 9.70) ^ 0.72; Return period = Yrs. 100 ; c = cir e = ellip b = box

## **APPENDIX G**

### **SPILLWAY/ANTI-SEEP COLLAR DESIGN CALCULATIONS**

# BMP 1 EMERGENCY SPILLWAY

PROJECT: The Westtown School - Oak Lane Project  
 LOCATION: Westtown Township  
 COUNTY: Chester

JOB # 1091-001  
 DATE: 1/12/2023  
 REVISED:

Flow into basin for 100-year storm frequency:

$$Q = 29.52 \text{ cfs} \text{ (From Post-Development analysis)}$$

Capacity of the Emergency Spillway:

$$Q = CLH^{1.5}$$

$$\begin{aligned} C &= 2.8 \\ L &= 30 \text{ ft.} \\ H &= 1.00 \end{aligned}$$

$$Q = 84.00 \text{ cfs} > 30 \text{ cfs cfs} \quad \text{OK}$$

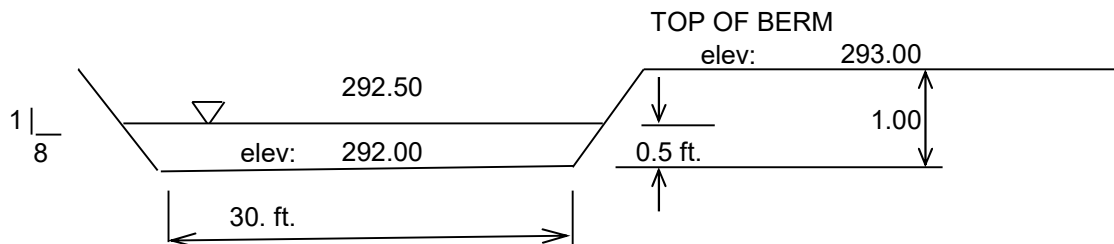
Check actual depth and velocity:

$$\begin{aligned} \text{Top of Berm Elevation} &= 293.00 \\ \text{Spillway Elevation} &= 292.00 \end{aligned}$$

$$\begin{aligned} H &= [Q/C*L]^{2/3} \\ &= 0.5 \text{ ft.} \quad \text{at elevation} \quad 292.50 \end{aligned}$$

$$\text{Freeboard:} \quad 293.00 - 292.50 = 0.5 \text{ ft.}$$

$$\begin{aligned} V &= Q/A \\ &= 1.7 \text{ fps} \end{aligned} \quad \text{Side Slope (H:V)} = 8$$



N.T.S.



North American Green  
 5401 St. Wendel-Cynthiana Rd.  
 Poseyville, Indiana 47633  
 Tel. 800.772.2040  
 >Fax 812.867.0247  
 www.nagreen.com  
 ECMDS v7.0

**SPILLWAY ANALYSIS**

>>> BMP 1

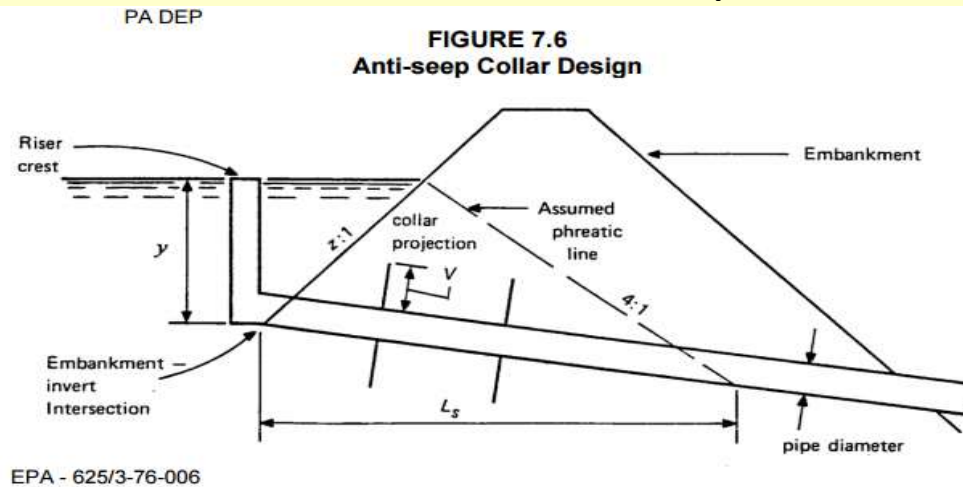
Name BMP 1  
 Discharge 29.52  
 Peak Flow Period 2  
 Channel Slope 0.167  
 Channel Bottom Width 30  
 Low Flow Liner  
 Retardence Class C 6-12 in  
 Vegetation Type Mix (Sod and Bunch)  
 Vegetation Density Very Good 80-95%  
 Soil Type Sand (SP)

**P300 - Class C - Mix (Sod & Bunch) - Very Good 80-95%**

Phase	Reach	Discharge	Velocity	Normal Depth	Mannings N	Permissible Shear Stress	Calculated Shear Stress	Safety Factor	Remarks	Staple Pattern
P300 Unvegetated	Straight	29.52 cfs	6.35 ft/s	0.15 ft	0.027	2.3 lbs/ft <sup>2</sup>	1.61 lbs/ft <sup>2</sup>	1.43	STABLE	E
Underlying Substrate	Straight	29.52 cfs	6.35 ft/s	0.15 ft	0.027	2.01 lbs/ft <sup>2</sup>	1.59 lbs/ft <sup>2</sup>	1.27	STABLE	E
P300 Reinforced Vegetation	Straight	29.52 cfs	5.34 ft/s	0.18 ft	0.036	10 lbs/ft <sup>2</sup>	1.91 lbs/ft <sup>2</sup>	5.25	STABLE	E
Underlying Substrate	Straight	29.52 cfs	5.34 ft/s	0.18 ft	0.036	2.66 lbs/ft <sup>2</sup>	1.89 lbs/ft <sup>2</sup>	1.41	STABLE	E

# ANTI-SEEP COLLAR DESIGN

## Infiltration BMP 1/Sediment Trap 1



1. Determine length of pipe in saturated zone ( $L_s$ )

$$L_s = y(z+4) \left[ 1 + \frac{S}{(0.25 - S)} \right]$$

$$\begin{aligned} y &= 6.25 \\ z &= 3 \\ S &= 0.005 \end{aligned}$$

Where  $y$  = Distance from upstream invert of spillway riser to top of dewatering volume (ft)  
 $z$  = Horizontal component of upstream embankment slope (ft)  
 $S$  = Pipe slope ft/ft

$$L_s = \underline{44.64} \text{ ft}$$

2. Determine the required increase in flow path

$$L_f = 1.15 * L_s = \underline{51.34} \text{ ft}$$

3. The minimum collar projection ( $V$ ) is equal to 1/2 the increase in flow length (for one collar). If more than one collar is used, it is the increase divided by twice the number of collars

$$\text{Number of collars: } \underline{2}$$

$$V_{\min} = \underline{1.67} \text{ ft}$$

4. The maximum spacing between collars should be  $14 \times V$  or  $L_s \div (\text{number of collars minus } 1)$

Minimum spacing should be  $5 \times V$

$$V = \underline{1.67} \text{ ft}$$

$$\text{Max} = 22 \text{ ft}$$

$$\text{Min} = 8.4 \text{ ft}$$

# BMP 4 EMERGENCY SPILLWAY

PROJECT: The Westtown School - Oak Lane Project  
 LOCATION: Westtown Township  
 COUNTY: Chester

JOB # 1091-001  
 DATE: 1/12/2023  
 REVISED:

Flow into basin for 100-year storm frequency:

$$Q = 38.87 \text{ cfs} \text{ (From Post-Development analysis)}$$

Capacity of the Emergency Spillway:

$$Q = CLH^{1.5}$$

$$C = 2.8$$

$$L = 40 \text{ ft.}$$

$$H = 1.00$$

$$Q = 112.00 \text{ cfs} > 39 \text{ cfs cfs} \quad \text{OK}$$

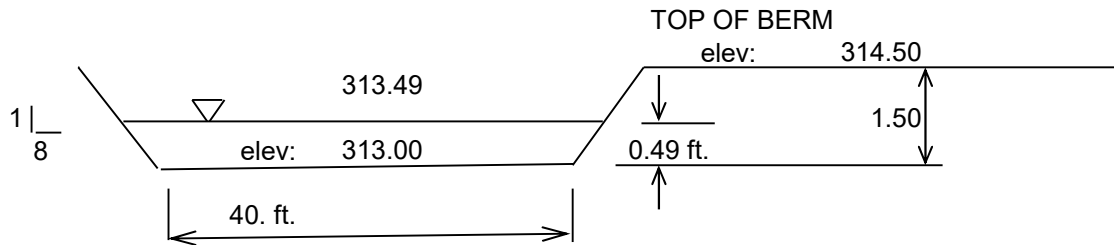
Check actual depth and velocity:

$$\begin{aligned} \text{Top of Berm Elevation} &= 314.50 \\ \text{Spillway Elevation} &= 313.00 \end{aligned}$$

$$\begin{aligned} H &= [Q/C*L]^{2/3} \\ &= 0.49 \text{ ft.} \quad \text{at elevation} \quad 313.49 \end{aligned}$$

$$\text{Freeboard:} \quad 314.50 - 313.49 = 1.01 \text{ ft.}$$

$$\begin{aligned} V &= Q/A \\ &= 1.8 \text{ fps} \end{aligned} \quad \text{Side Slope (H:V)} = 8$$





North American Green  
 5401 St. Wendel-Cynthiana Rd.  
 Poseyville, Indiana 47633  
 Tel. 800.772.2040  
 >Fax 812.867.0247  
 www.nagreen.com  
 ECMDS v7.0

**SPILLWAY ANALYSIS**

>>> BMP 4

Name BMP 4  
 Discharge 38.87  
 Peak Flow Period 2  
 Channel Slope 0.2  
 Channel Bottom Width 40  
 Low Flow Liner  
 Retardence Class C 6-12 in  
 Vegetation Type Mix (Sod and Bunch)  
 Vegetation Density Very Good 80-95%  
 Soil Type Sand (SP)

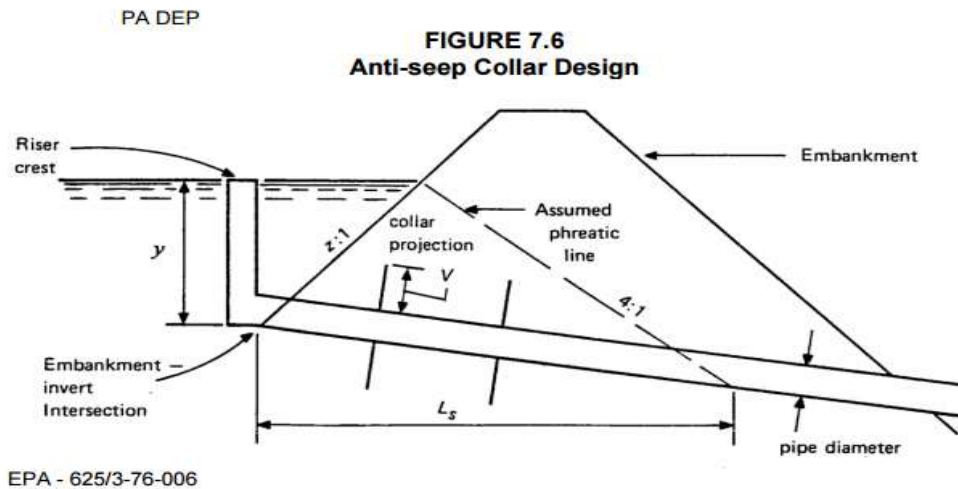
**P300 - Class C - Mix (Sod & Bunch) - Very Good 80-95%**

Phase	Reach	Discharge	Velocity	Normal Depth	Mannings N	Permissible Shear Stress	Calculated Shear Stress	Safety Factor	Remarks	Staple Pattern
P300 Unvegetated	Straight	38.87 cfs	6.74 ft/s	0.14 ft	0.027	2.3 lbs/ft <sup>2</sup>	1.79 lbs/ft <sup>2</sup>	1.28	STABLE	E
Underlying Substrate	Straight	38.87 cfs	6.74 ft/s	0.14 ft	0.027	2.01 lbs/ft <sup>2</sup>	1.78 lbs/ft <sup>2</sup>	1.13	STABLE	E
P300 Reinforced Vegetation	Straight	38.87 cfs	5.76 ft/s	0.17 ft	0.035	10 lbs/ft <sup>2</sup>	2.1 lbs/ft <sup>2</sup>	4.77	STABLE	E
Underlying Substrate	Straight	38.87 cfs	5.76 ft/s	0.17 ft	0.035	2.46 lbs/ft <sup>2</sup>	2.08 lbs/ft <sup>2</sup>	1.18	STABLE	E



# ANTI-SEEP COLLAR DESIGN

## Infiltration BMP 4/Sediment Basin 4



1. Determine length of pipe in saturated zone ( $L_s$ )

$$L_s = y(z+4) \left[ 1 + \frac{S}{(0.25 - S)} \right]$$

$$\begin{aligned} y &= 3.75 \\ z &= 3 \\ s &= 0.0069 \end{aligned}$$

Where  $y$  = Distance from upstream invert of spillway riser to top of dewatering volume (ft)  
 $z$  = Horizontal component of upstream embankment slope (ft)  
 $S$  = Pipe slope ft/ft

$$L_s = \underline{27.00} \text{ ft}$$

2. Determine the required increase in flow path

$$L_F = 1.15 * L_s = \underline{31.04} \text{ ft}$$

3. The minimum collar projection ( $V$ ) is equal to  $1/2$  the increase in flow length (for one collar). If more than one collar is used, it is the increase divided by twice the number of collars

Number of collars: 1

$$V_{\min} = \underline{2.00} \text{ ft}$$

4. The maximum spacing between collars should be  $14 \times V$  or  $L_s \div (\text{number of collars minus } 1)$

Minimum spacing should be  $5 \times V$

$$V = \underline{1} \text{ ft}$$

Max = 14 ft

Min = 5 ft

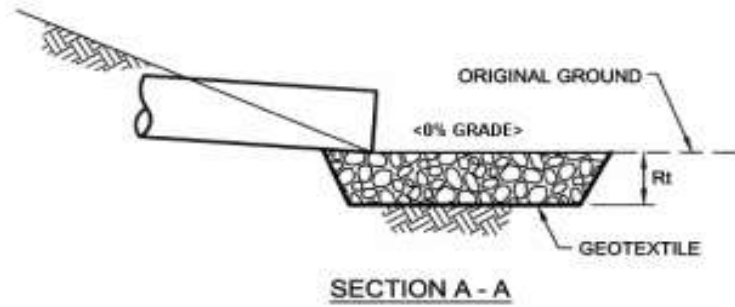
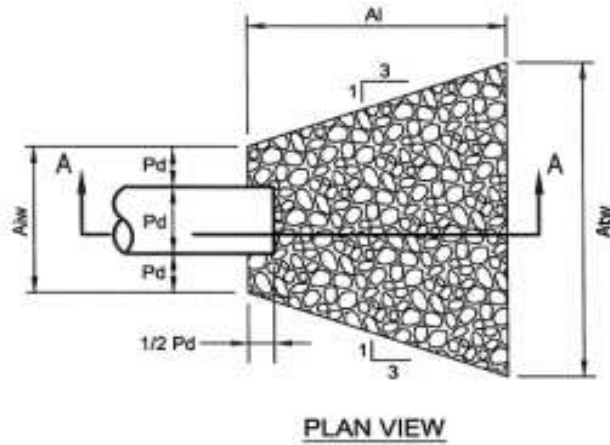
## **APPENDX H**

### **RIP-RAP DESIGN CALCULATIONS**

**EROSION AND SEDIMENT POLLUTION CONTROL**

**STANDARD E&S WORKSHEET #20  
Riprap Apron Outlet Protection**

PROJECT: <u>The Westtown School - Oak Lane Project</u>	JOB #	1091-001
LOCATION: <u>Westtown Township</u>	DATE:	1/16/2023
COUNTY: <u>Chester</u>	REVISED:	
CHECKED BY: <span style="background-color: yellow;">                    </span>		



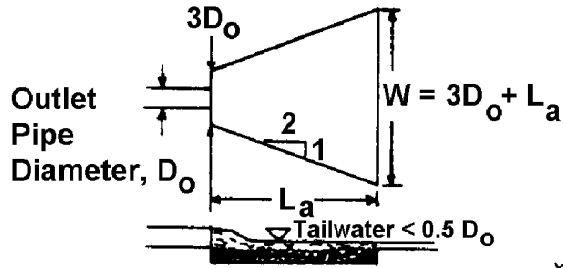
NO.	PIPE DIA. Do (in.)	TAIL WATER COND. (Max or Min.)	MAN. "n" FOR PIPE	PIPE SLOPE (%)	Q (CFS)	V* (FPS)	RIPRAP SIZE	Rt (in)	Al (ft)	Aiw (ft)	Atw (ft)
EW-A1	18	Min.	0.012	0.50	12.7	7.18	R-4	18	12	4.50	16.50
EW-A2	18	Min.	0.012	0.92	12.1	6.84	R-4	18	12	4.50	16.50
EW-B1	24	Min.	0.012	0.67	24.3	7.74	R-4	18	14	6.00	20.00
EW-B2	15	Min.	0.012	0.51	4.50	4.65	R-3	9	9	3.75	12.75

\*The anticipated velocity (V) should not exceed the maximum permissible shown in Table 6.6 for the proposed riprap protection. Adjust for less than full pipe flow. SEE TABLE 9, March 2000 E&S PROGRAM MANUAL. Use Manning's equation to calculate velocity for pipe slopes > 0.05 ft/ft. velocity for pipe slopes > 0.05 ft/ft.  
 \*\* Based on sediment basin flow through principle spillway  
 \*\*\* See attached Hydraflow Storm Sewers

# EW-A1

## DESIGN OF RIPRAP APRON OUTLET PROTECTION FROM A ROUND PIPE FLOWING FULL MINIMUM TAILWATER CONDITION ( $T_w < 0.5$ DIAMETER)

Adapted from USDA - NRCS



Not to be used for Box Culverts

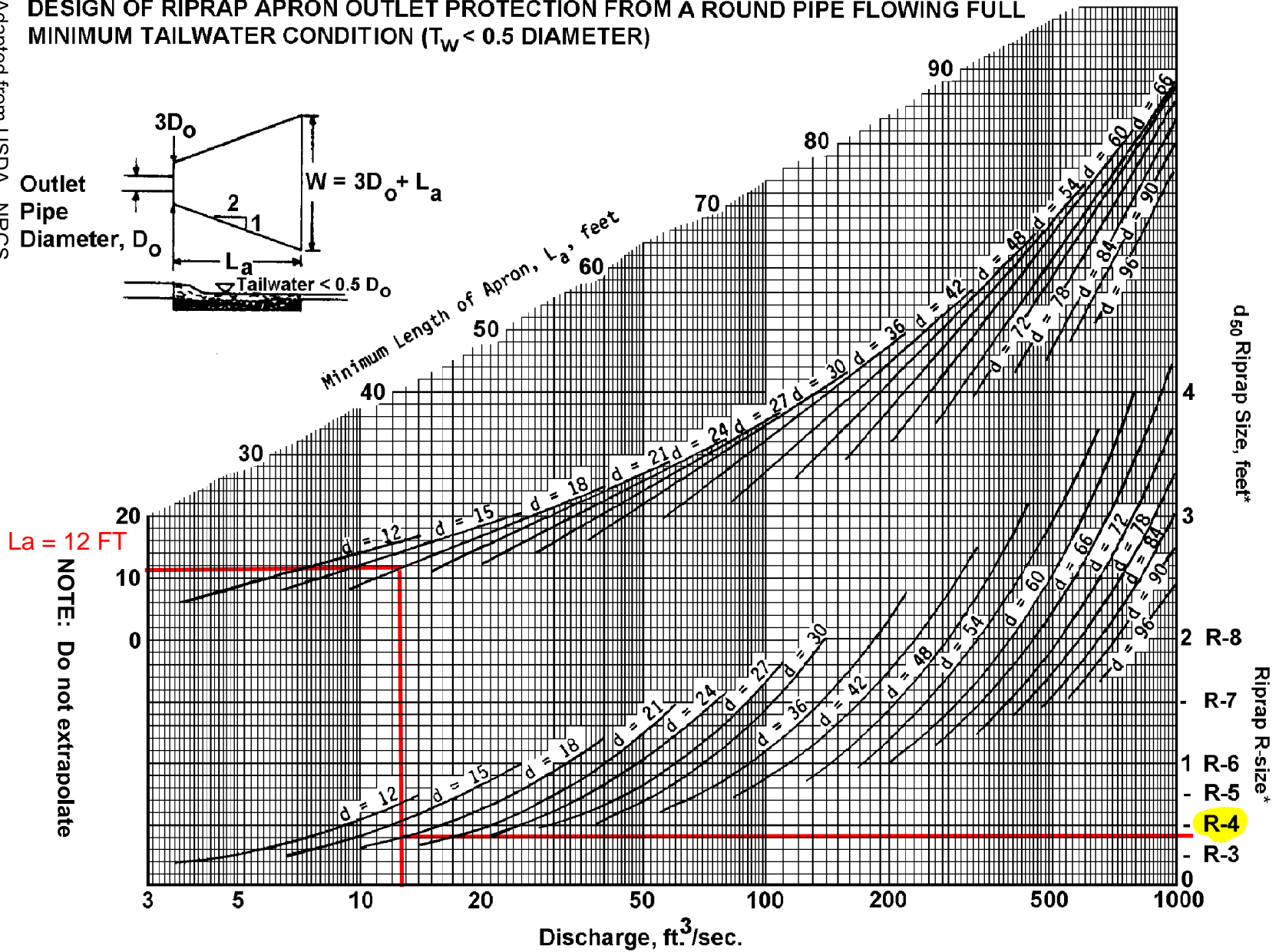


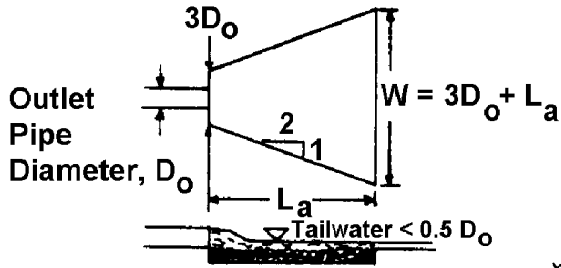
FIGURE 9.3  
Riprap Apron Design, Minimum Tailwater Condition

\* For discharge velocities exceeding Maximum Allowable for Riprap indicated, increase  $d_{50}$  stone size and/or provide velocity reduction device.

# EW-A2

## DESIGN OF RIPRAP APRON OUTLET PROTECTION FROM A ROUND PIPE FLOWING FULL MINIMUM TAILWATER CONDITION ( $T_w < 0.5$ DIAMETER)

Adapted from USDA - NRCS



Not to be used for Box Culverts

La = 12 FT

NOTE: Do not extrapolate

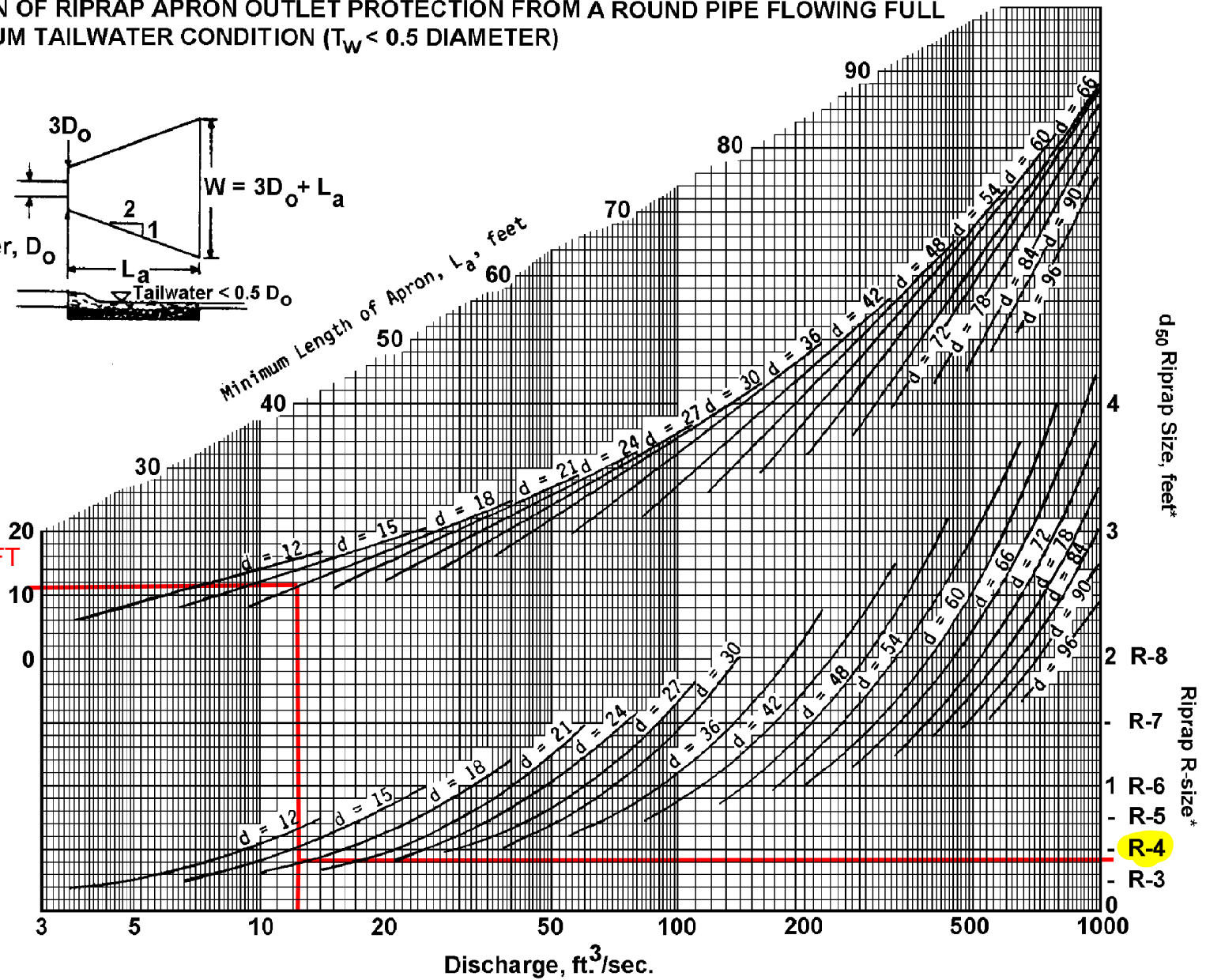


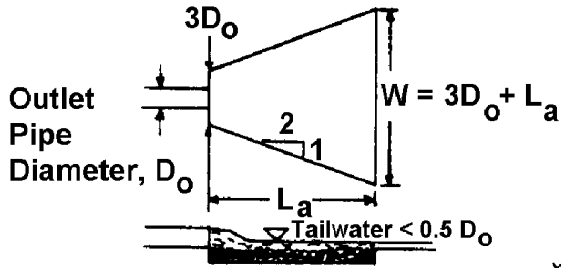
FIGURE 9.3  
Riprap Apron Design, Minimum Tailwater Condition

\* For discharge velocities exceeding Maximum Allowable for Riprap indicated, increase  $d_{50}$  stone size and/or provide velocity reduction device.

# EW-B1

## DESIGN OF RIPRAP APRON OUTLET PROTECTION FROM A ROUND PIPE FLOWING FULL MINIMUM TAILWATER CONDITION ( $T_w < 0.5$ DIAMETER)

Adapted from USDA - NRCS



Not to be used for Box Culverts

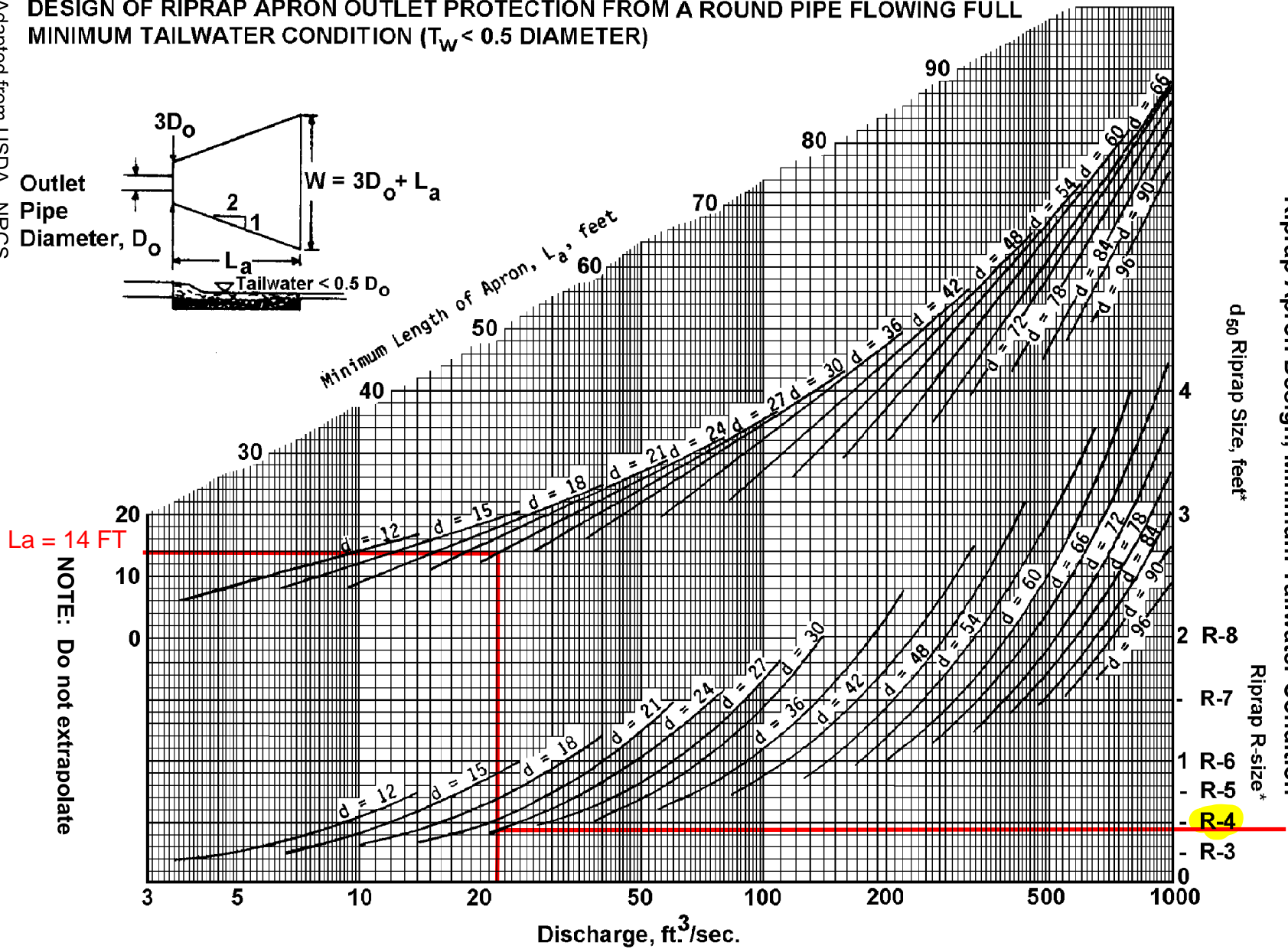


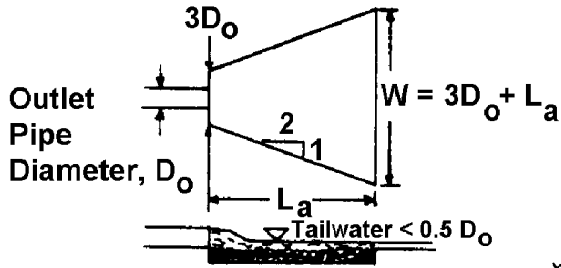
FIGURE 9.3  
Riprap Apron Design, Minimum Tailwater Condition

\* For discharge velocities exceeding Maximum Allowable for Riprap indicated, increase  $d_{50}$  stone size and/or provide velocity reduction device.

# EW-B2

## DESIGN OF RIPRAP APRON OUTLET PROTECTION FROM A ROUND PIPE FLOWING FULL MINIMUM TAILWATER CONDITION ( $T_w < 0.5$ DIAMETER)

Adapted from USDA - NRCS



Not to be used for Box Culverts

La = 9 FT

NOTE: Do not extrapolate

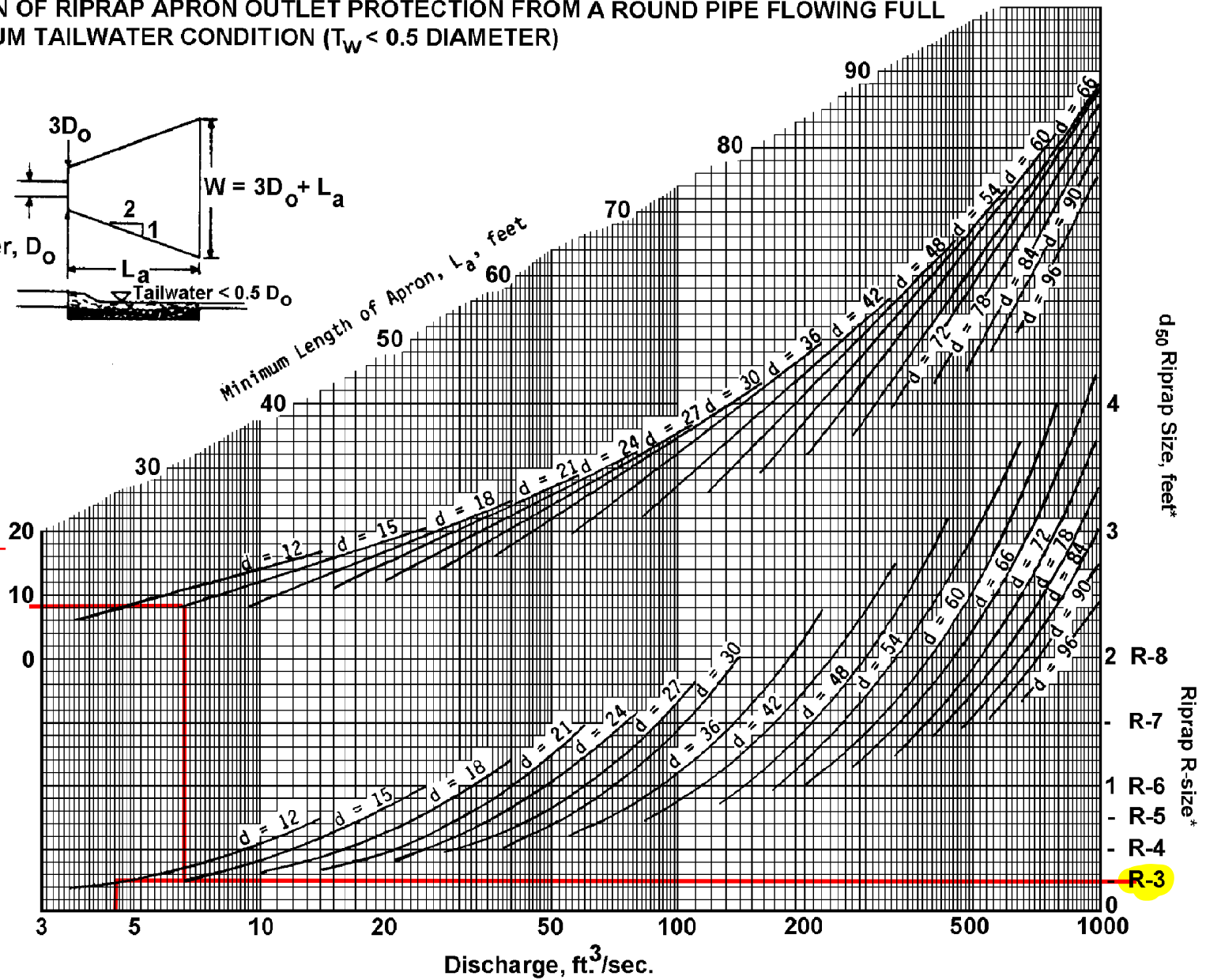


FIGURE 9.3  
Riprap Apron Design, Minimum Tailwater Condition

\* For discharge velocities exceeding Maximum Allowable for Riprap indicated, increase  $d_{50}$  stone size and/or provide velocity reduction device.

## Anticipated Velocity Calculation for Less Than Full Pipe Flow

### Outfall EW-B2

Full Flow Discharge:  $Q_f = \frac{0.464}{n} D^{8/3} S^{1/2} = 5.01 \text{ cfs}$

Continuity Equation to determine full-flow velocity:

$$V_f = \frac{Q_f}{A} = 4.08 \text{ ft/sec}$$

Where:  $A = 1.23 = \text{Cross Sectional Area (ft}^2\text{)}$

Ratio of Partial to Full-Flow Discharge:

$$d/D = \frac{Q_d}{Q_f} = 0.899$$

Where:  $d/D = 0.90 = \text{Ratio of Part-Full to Full-Flow Discharge}$   
 $Q_d = 4.50 = \text{Design Discharge (cfs)}$   
 $Q_f = 5.01 = \text{Full-Flow Discharge (cfs)}$   
 $D = 1.25 = \text{Diameter (ft)}$   
 $S = 0.01 = \text{Slope of pipe (ft/ft)}$   
 $n = 0.012 = \text{Mannings Coefficient}$

Velocity Ratio from Figure 9.1:  $1.14$

Design Velocity  $V_d = 4.65 \text{ ft/s}$



# EW-B2

CIRCULAR CHANNEL RATIOS

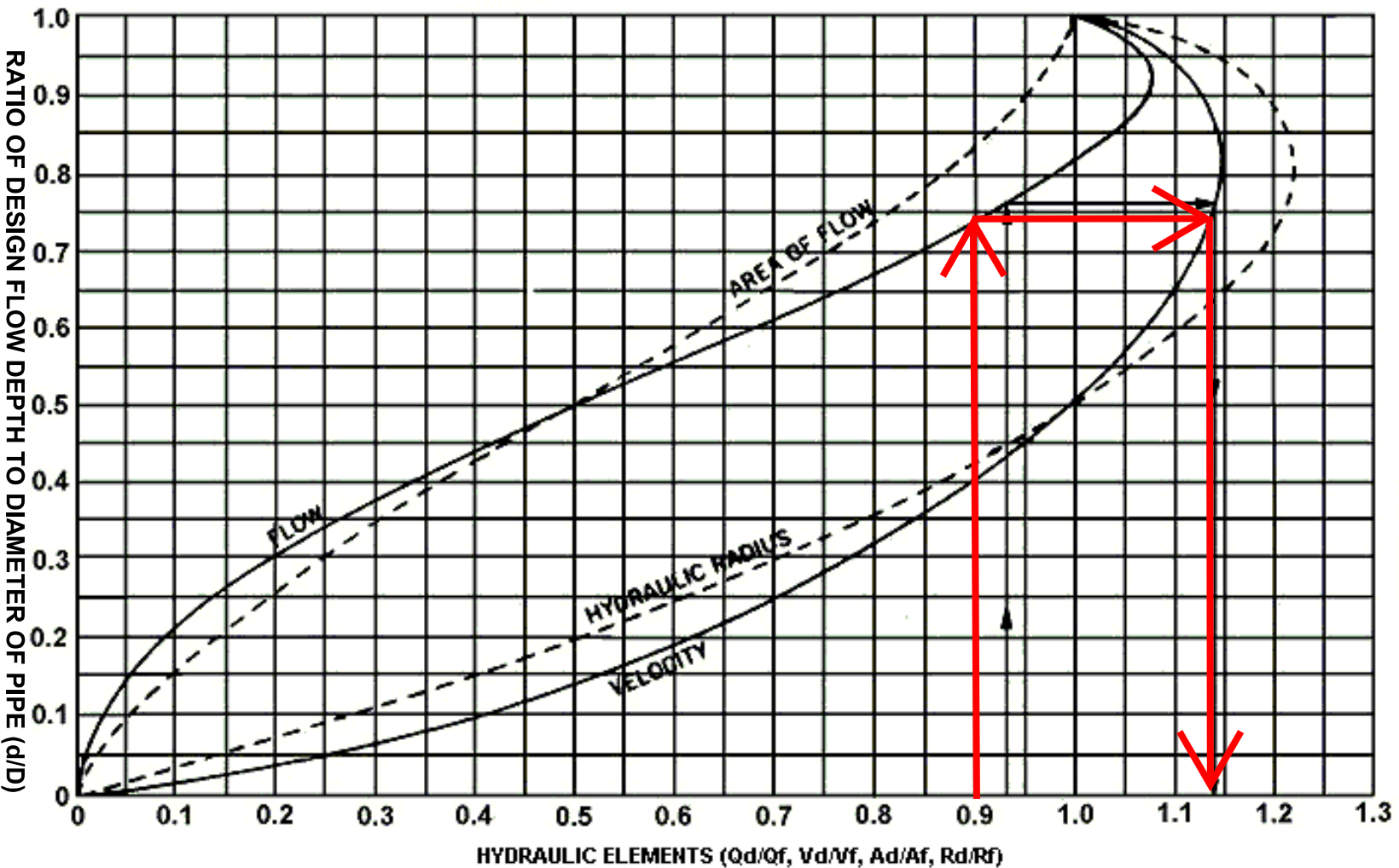


FIGURE 9.1  
Velocity Adjustment Nomograph for Less Than Full Pipe Flow

Adapted from *Design and Construction of Sanitary and Storm Sewers*, p. 87, ASCE, 1969

Do not use this nomograph to determine "equivalent pipe sizes" for discharges ( $Q_d$ ) that do not intersect curves corresponding to proposed pipe sizes on Figures 9.3 and 9.4.

## **APPENDIX I INFILTRATION REPORTS**



October 8, 2018

Westtown School  
975 Westtown Road  
West Chester, PA 19382

c/o

Mr. Charles R. Haley, Jr., P.E.  
ELA Group, Inc.  
743 South Broad Street  
Lititz, PA 17543

**RE: Stormwater Infiltration Feasibility Report  
Westtown School Oak Lane – Infiltration  
Westtown Township, Chester County, Pennsylvania  
Advantage Project Number: 1800331001**

Dear Mr. Haley:

In accordance with your request, Advantage Engineers (Advantage) has completed an engineering analysis of the above referenced project site in order to evaluate the suitability of the subsurface soils for the infiltration of stormwater. This correspondence serves to transmit the results of our evaluation.

## **SITE AND PROJECT DESCRIPTION**

The project site currently consists of outdoor athletic fields located east of Westtown Road in Westtown Township, Chester County, Pennsylvania. The site is bordered to the east by agricultural land and grass areas, to the south by Westtown School District buildings, to the west by Westtown Road and to the north by Westtown School District and wooded areas. The approximate location of the site in relation to the surrounding area is depicted on the *Topographic Map* (Figure 1) presented within the Appendix.

According to information provided by the Client, the improvements will include 2 synthetic turf multipurpose fields, 2 grass multipurpose fields, a softball field and a baseball field. Development of the site will also include new field lights, an outbuilding and new stormwater management facilities.

## **SCOPE OF WORK**

The objective of our work was to determine the permeability of the invert soils, identify any limiting zones (i.e. bedrock, groundwater, or seasonal high water table) within the proposed stormwater management facilities, and address PADEP requirements as they relate to stormwater management. This objective was accomplished through completion of a scope of work which included the completion of a subsurface field exploration, laboratory testing program and preparation of this report. This report presents a summary of the scope of work completed, conditions encountered, and results of our engineering analysis of subsurface conditions.

## **SUBSURFACE FIELD EXPLORATION**

In order to characterize subsurface conditions across the project site, 13 test pits were excavated on September 26 through 28, 2018. Supervision and monitoring of the field exploration was provided by a representative of Advantage. Test locations were marked out by ELA Group, Inc., based on the "Sketch Plan", dated July 24, 2017, prepared by Site Engineering Concepts, LLC. The approximate test locations, referenced as TP-1 through TP-13, are shown on the *Exploration Plan* (Figure 3) presented within the Appendix. Data pertaining to the subsurface exploration was documented in the field and is presented in detail on the *Test Pit Logs*, which contain detailed descriptions of the subsurface materials encountered and infiltration test depths. A general description of the soil conditions encountered is provided in the "Subsurface Conditions" section of this report.



## LABORATORY ANALYSIS

Soil samples retrieved from the site were visually reviewed and classified by Advantage Engineers. Representative soil samples were subjected to laboratory analyses to verify visual classifications in accordance with the following schedule:

- Natural Moisture Content (ASTM D2216)
- Sieve Analysis (ASTM D422)
- Atterberg Limits Determination (ASTM D4318)

Unified Soil Classification System (USCS) Group Symbols and ASTM Group Names has been assigned to the soils analyzed. Graphical depictions of the laboratory testing completed are presented in the table below and within the Appendix.

STANDARD CLASSIFICATION RESULTS											
Location	Depth (ft)	Soil Type	% Gravel	% Sand	% Fines	LL	PL	PI	Natural Moisture Content	USCS Group Symbol	ASTM Group Name
TP-2	3	Stratum I	7.2	54.4	38.4	36	33	3	21.9%	SM	Silty SAND
TP-5	4 – 6		45.6	42.5	11.9	36	35	1	10.7%	GP-GM	Poorly Graded GRAVEL with Silt and Sand

*LL-Liquid Limit; PL-Plastic Limit; PI-Plasticity Index*

## SUBSURFACE CONDITIONS

### Geology

According to the Pennsylvania Geologic Survey's, Geologic Map of the State of Pennsylvania, 1980, the project site is underlain by polyt schist of the Glenarm Wissahickon Formation (Geologic Symbol Xgw). This formation includes lenticular amphibolites bodies having ocean-floor basalt chemistry. The project site within its geologic setting is presented on the *Geologic Map* (Figure 2) found within the Appendix.

The Pennsylvania Geologic Survey publication, The Engineering Characteristics of the Rocks of Pennsylvania, Second Edition, 1982, describes the bedding in this formation as well developed, thin to fissile, and steeply dipping. Joints in this formation have an irregular pattern, are poorly formed, widely spaced, steeply dipping, and open. The schist of this formation is moderately resistant to weathering, and often weathers to a moderate depth. The resulting soil mantle is thin.

### Soil

#### Surficial Materials

Each test pit was covered by approximately 6 to 28 inches of topsoil or tilled soil; however, the thickness of surficial materials may differ in unexplored areas of the project site.

#### Stratum I – Brown to gray Silty SAND and GRAVEL with Silt and Sand

Stratum I was encountered within each test pit completed except for TP-12 and TP-13 and extended to depths ranging from approximately 4.5 to 10 feet below existing site grades. Laboratory testing conducted on representative samples of Stratum I show this soil to be well graded and non-plastic with natural moisture contents of 21.9% and 10.7%. Stratum I is described under the USCS as Silty SAND (SM) and Poorly Graded GRAVEL with Silt and Sand (GP-GM).



### **Stratum II – Brown Silty SAND with Gravel (highly weathered rock)**

Stratum II was encountered within test pits TP-10 and TP-11 and extended to depths of approximately 7.5 and 9.5 feet, respectively, below existing site grades. Upon review, the soils of Stratum II were found to be well graded, non-plastic and predominately comprised of Silty SAND with Gravel. The soils of Stratum II are anticipated to represent the highly weathered bedrock surface.

### **Stratum III – Orange brown to blue gray Sandy CLAY**

Stratum III was encountered within test pits TP-12 and TP-13 and extended to depths of approximately 6 feet below existing site grades. Upon review, the soils of Stratum III were found to be moderately graded, plastic and comprised of Sandy CLAY.

### **Bedrock**

The bedrock surface was encountered within test pits TP-10 and TP-11 at depths of approximately 7.5 and 9.5 feet below existing site grades, respectively. The bedrock surface was defined as the depth at which the bucket of the given excavation equipment could no longer excavate. Other equipment may yield different bedrock data.

### **Groundwater/Soil Mottling**

Groundwater was encountered within test pits TP-7, TP-8, TP-12 and TP-13 at depths ranging from approximately 1.5 to 6 feet below existing site grades. Additionally, soil mottling (indication of seasonal high water table and/or poorly draining soils) was encountered within test pits TP-12 and TP-13, starting at a depth of approximately 2.5 feet below existing site grades and extending to 6 feet below existing site grades. It should be noted that standing water was observed at several areas including the agricultural field located in the eastern portion of the site and the portion of the site located north of Oak Lane. These observations were made at the time of the field operation and the groundwater table elevation will vary with daily, seasonal, and climatological variations.

## **INFILTRATION ANALYSIS**

To evaluate the feasibility of infiltration of stormwater within the proposed stormwater management facilities, infiltration tests were completed utilizing the “double-ring” infiltrometer method in accordance with the Pennsylvania Stormwater Best Management Practices Manual, latest Edition. Based on the topsoil thickness encountered within test pit TP-4, the infiltration test was completed below the proposed test elevation. Based on the limiting zone encountered (groundwater and/or soil mottling) within test pits TP-8, TP-12 and TP-13, no infiltration tests were able to be completed. Based on the limiting zones encountered (groundwater/bedrock) within TP- 7, TP-10 and TP-11, the infiltration tests were completed above the proposed test elevations. The test pit locations, approximate surface elevation, proposed test elevation, actual test elevation(s), presence of limiting zones, and the infiltration rate(s) achieved at each location are presented in the table below.



INFILTRATION TEST RESULTS					
Test Location	Surface Elevation (ft)	Proposed Test Elevations (ft)	Actual Test Elevations (FT)	Limiting Zone Elevation (ft)	Infiltration Rate* (in/hr)
TP-1	319.5	316	316	Not Encountered @ 312	1.8
		314	314		6.0
TP-2	317	316	316	Not Encountered @ 312	0.0
		314	314		1.4
TP-3	321	317.5	317.5	Not Encountered @ 313.5	6.0
		315.5	315.5		12.0
TP-4	319.5	319	318.5	Not Encountered @ 315	1.2
		317	317		1.0
TP-5	321	319.5	319.5	Not Encountered @ 315	3.4
		317	317		4.8
TP-6	311	309	309	Not Encountered @ 305	1.0
		307	307		0.0
TP-7	313	309	311	Groundwater @ 307	0.0
		307	309		2.8
TP-8	311	309	No Test	Groundwater @ 309.5	No Test
		307	No Test		No Test
TP-9	303	292.5	295	Not Encountered @ 293	3.9
		291	295		4.0
TP-10	305	299	301	Bedrock @ 297.5	2.8
		297	299.5		4.8
TP-11	309	303	303	Bedrock @ 299.5	6.0
		301	301.5		5.4
TP-12	298	296	No Test	Soil Mottling @ 295.5-292 Groundwater @ 294.5	No Test
		294	No Test		No Test
TP-13	286	284	No Test	Groundwater @ 284.5 Soil Mottling @ 283.5-280	No Test
		282	No Test		No Test

\*Infiltration rates represent the rates recorded in the field and no safety factor has been applied

-Shaded cells represent infiltration tests completed above or below proposed invert due to a limiting zone or topsoil thickness

-Bold cells indicate infiltration testing completed at shallower depths due to safety concerns

## SUMMARY OF DATA & CONCLUSIONS

Based on the results of our field exploration and engineering analysis of the data obtained, we offer the following comments with regard to the infiltration of stormwater at the project site.

- The infiltration tests were conducted within the well graded, non-plastic, naturally-occurring soils of Stratum I and Stratum II.
- Groundwater was encountered within test pits TP-7, TP-8, TP-12 and TP-13 at depths ranging from approximately 1.5 to 6 feet below existing site grades.
- Soil mottling was encountered within test pits TP-12 and IT-13, starting at depths of approximately 2.5 feet below existing site grades and extending to 6 feet below existing site grades.



- The bedrock surface was encountered within test pits TP-10 and TP-11 at depths of approximately 7.5 and 9.5 feet below existing site grades, respectively
- Infiltration rates were found to range from no movement (0.0 inches per hour) to 12.0 inches per hour. These rates are unfactored. The PADEP recommended rate for infiltration of stormwater is 0.1 to 10 inches per hour.

## LIMITATIONS

The conclusions contained in this report are based upon the subsurface data collected and on details stated in this report. Should conditions arise which differ from those specifically stated herein, our office should be notified immediately, so that our recommendations can be reviewed and revised, if necessary.

The conclusions presented herein should be applied only to the infiltration tests as depicted on the *Exploration Plan* for the proposed stormwater management facilities to be constructed for Westtown School in Westtown Township, Chester County, Pennsylvania. Advantage takes no responsibility in utilizing this information for any other purposes.

The scope of work was limited to the exploration of the subsurface soils. Oil, hazardous waste, radioactivity, irritants, pollutants, radon or other dangerous substances and conditions were not the subject of this study. Their presence and/or absence are not implied, inferred or suggested by this report or results of this study.

We trust that this is the information you require. Should you have any questions or if we may be of further assistance, please don't hesitate to contact our office.

Respectfully,  
**advantage engineers**

A handwritten signature in black ink that reads "Bailey Jean Wildasin".

Bailey J. Wildasin  
Geotechnical Specialist I

A handwritten signature in black ink that reads "David J. Buckwalter".

David J. Buckwalter  
Senior Project Manager



# APPENDIX

FIGURE 1 – TOPOGRAPHIC MAP

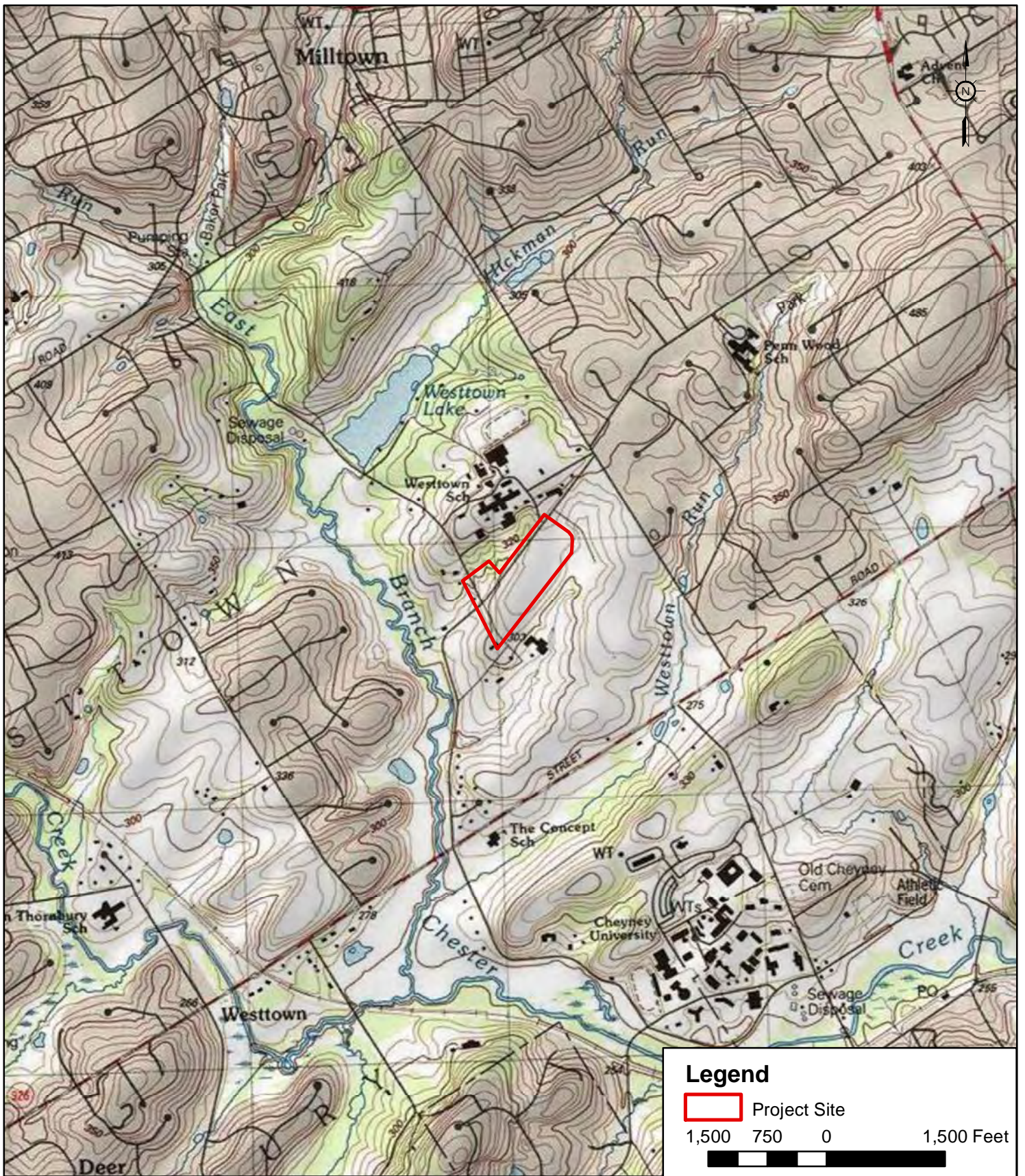
FIGURE 2 – GEOLOGIC MAP

FIGURE 3 – EXPLORATION PLAN

LABORATORY TEST RESULTS

TEST PIT LOGS





Service Layer Credits: Copyright:© 2013 National Geographic Society, i-cubed

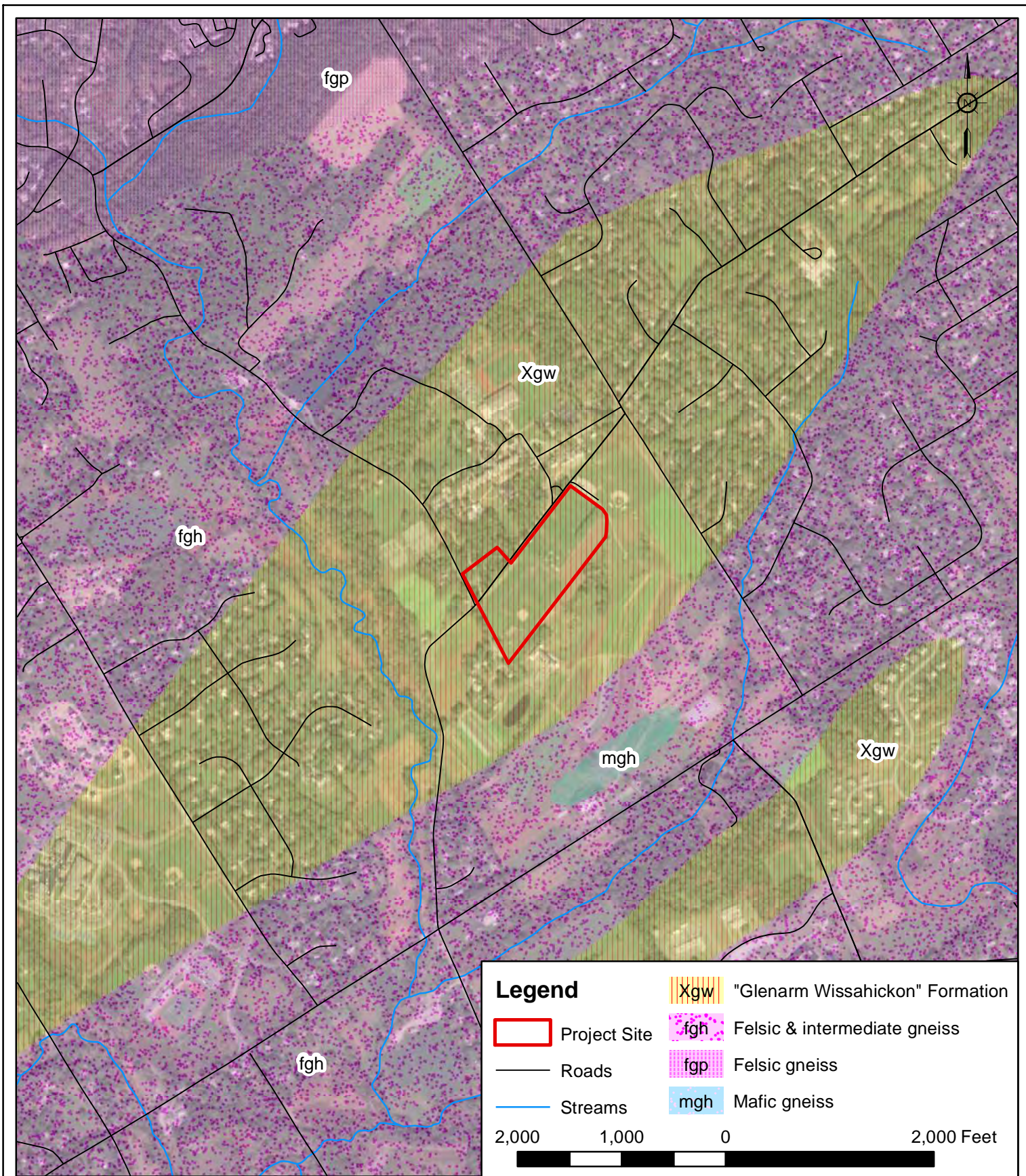
SCALE: AS SHOWN	DRAWING NUMBER: FIGURE 1
DRAWN BY: B. WILDASIN	CHECKED BY: D. BUCKWALTER
APPROVED BY: M. GIUNTA	DATE: 9-10-2018

**TOPOGRAPHIC MAP**  
PREPARED FOR  
**WESTTOWN SCHOOL OAK LANE - INFILTRATION**

WESTTOWN TOWNSHIP      CHESTER COUNTY      PENNSYLVANIA



**advantage engineers**  
435 INDEPENDENCE AVE., SUITE C  
MECHANICSBURG, PA 17055  
PH (717) 458-0800  
FAX (717) 458-0801



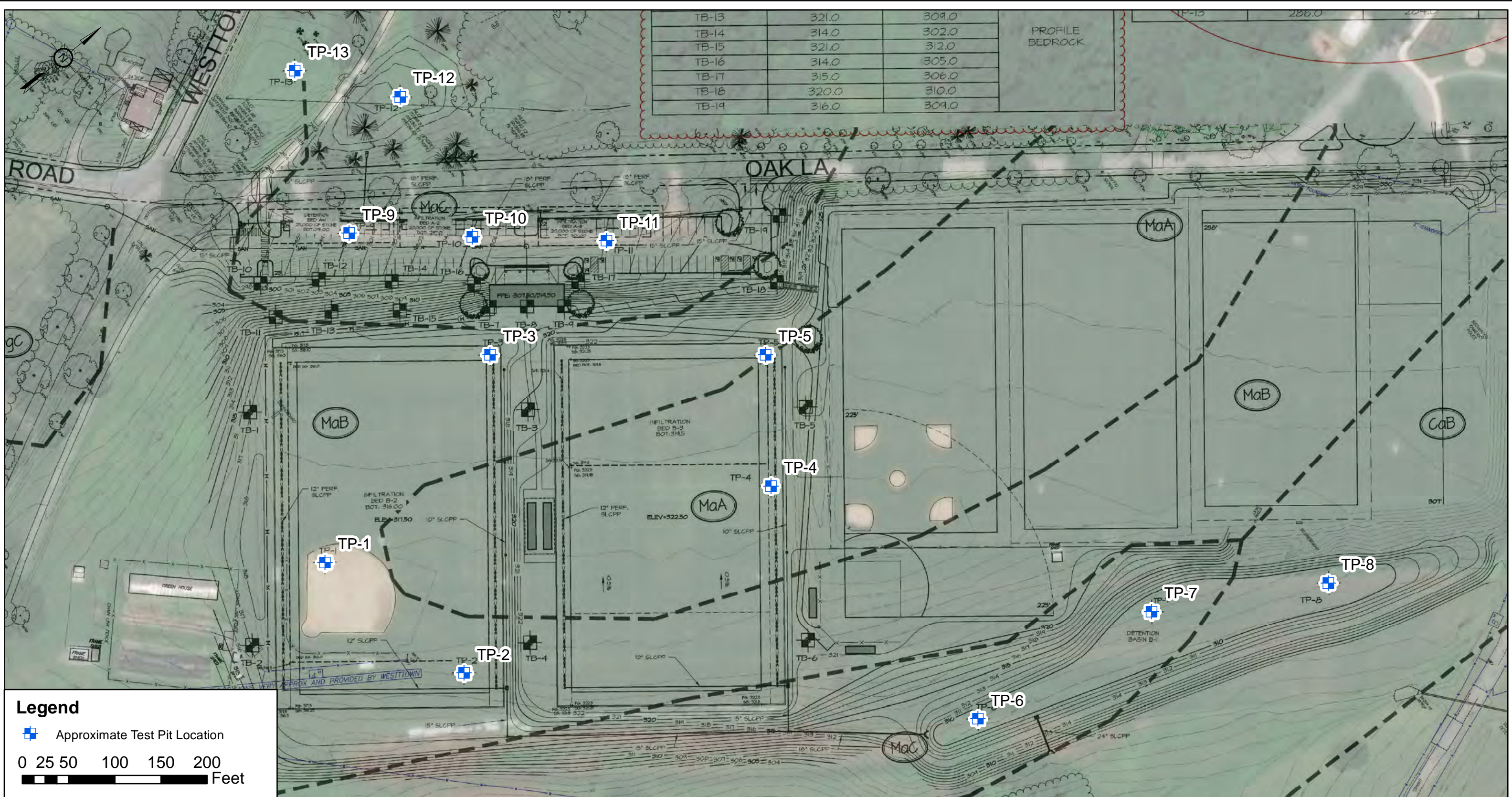
\*Source - Map 61 - Atlas of Preliminary Geologic Quadrangle Maps of Pennsylvania, 1981, Pa Geological Survey

SCALE: AS SHOWN	DRAWING NUMBER: FIGURE 2
DRAWN BY: B. WILDASIN	CHECKED BY: D. BUCKWALTER
APPROVED BY: M. GIUNTA	DATE: 9-10-2018

**GEOLOGIC MAP**  
PREPARED FOR  
**WESTTOWN SCHOOL OAK LANE - INFILTRATION**

WESTTOWN TOWNSHIP      CHESTER COUNTY      PENNSYLVANIA


**advantage engineers**  
 435 INDEPENDENCE AVE., SUITE C  
 MECHANICSBURG, PA 17055  
 PH (717) 458-0800  
 FAX (717) 458-0801



Service Layer Credits: Source: Esri, DigitalGlobe, GeoEye, i-cubed, USDA, USGS, AEX, Getmapping, Aerogrid, IGN, IGP, swisstopo, and the GIS User Community

SCALE: AS SHOWN	DRAWING NUMBER: FIGURE 3
DRAWN BY: B. WILDASIN	CHECKED BY: D. BUCKWALTER
APPROVED BY: M. GIUNTA	DATE: 9-10-2018

BASE PLAN: Sketch Plan
PROVIDED BY: Site Engineering Concepts, LLC
DATE: 7-24-2017

**EXPLORATION PLAN**  
PREPARED FOR  
**WESTTOWN SCHOOL OAK LANE - INFILTRATION**

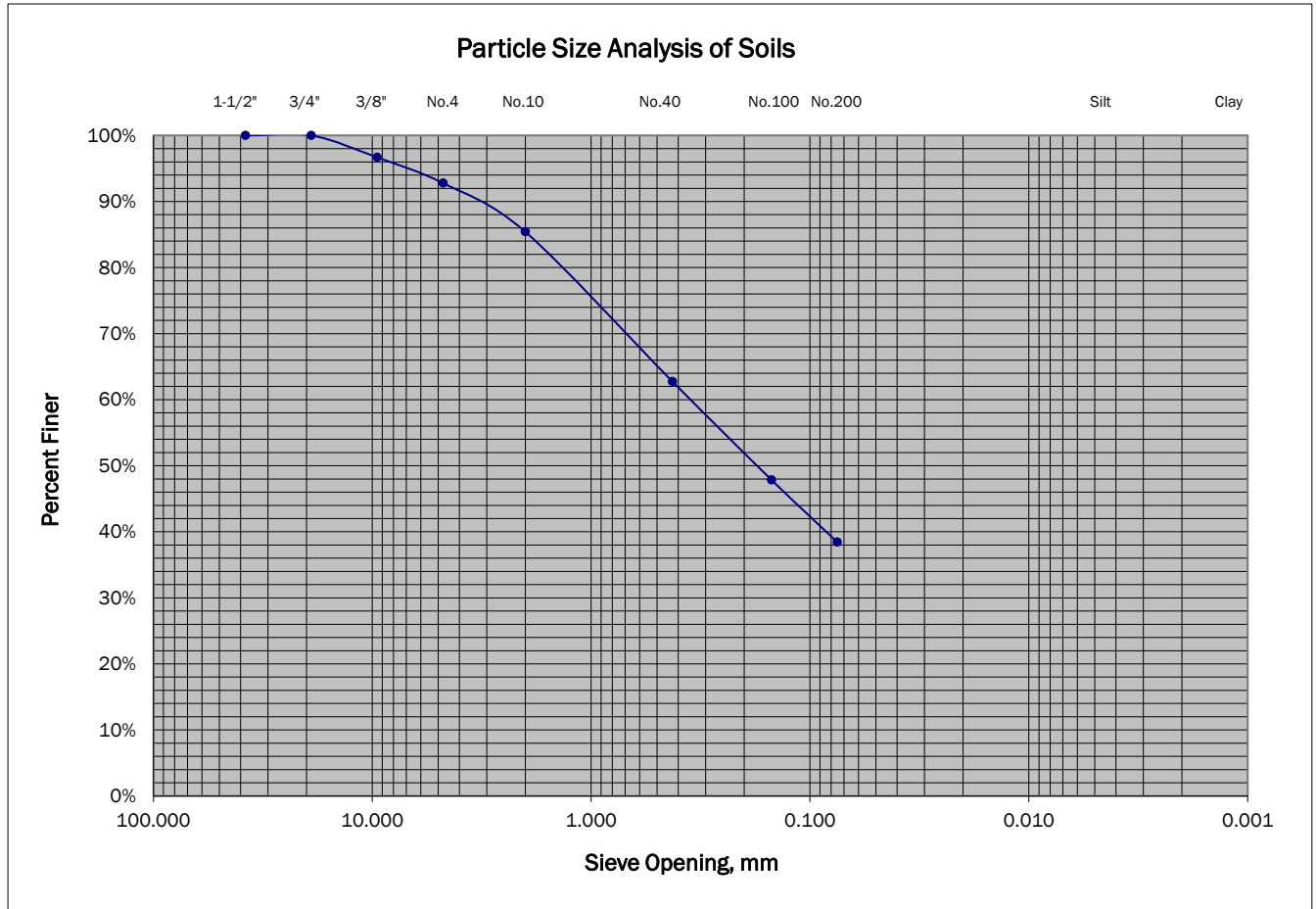
WESTTOWN TOWNSHIP      CHESTER COUNTY      PENNSYLVANIA



**advantage engineers**  
435 INDEPENDENCE AVE., SUITE C  
MECHANICSBURG, PA 17055  
PH (717) 458-0800  
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# Soil Classification Report

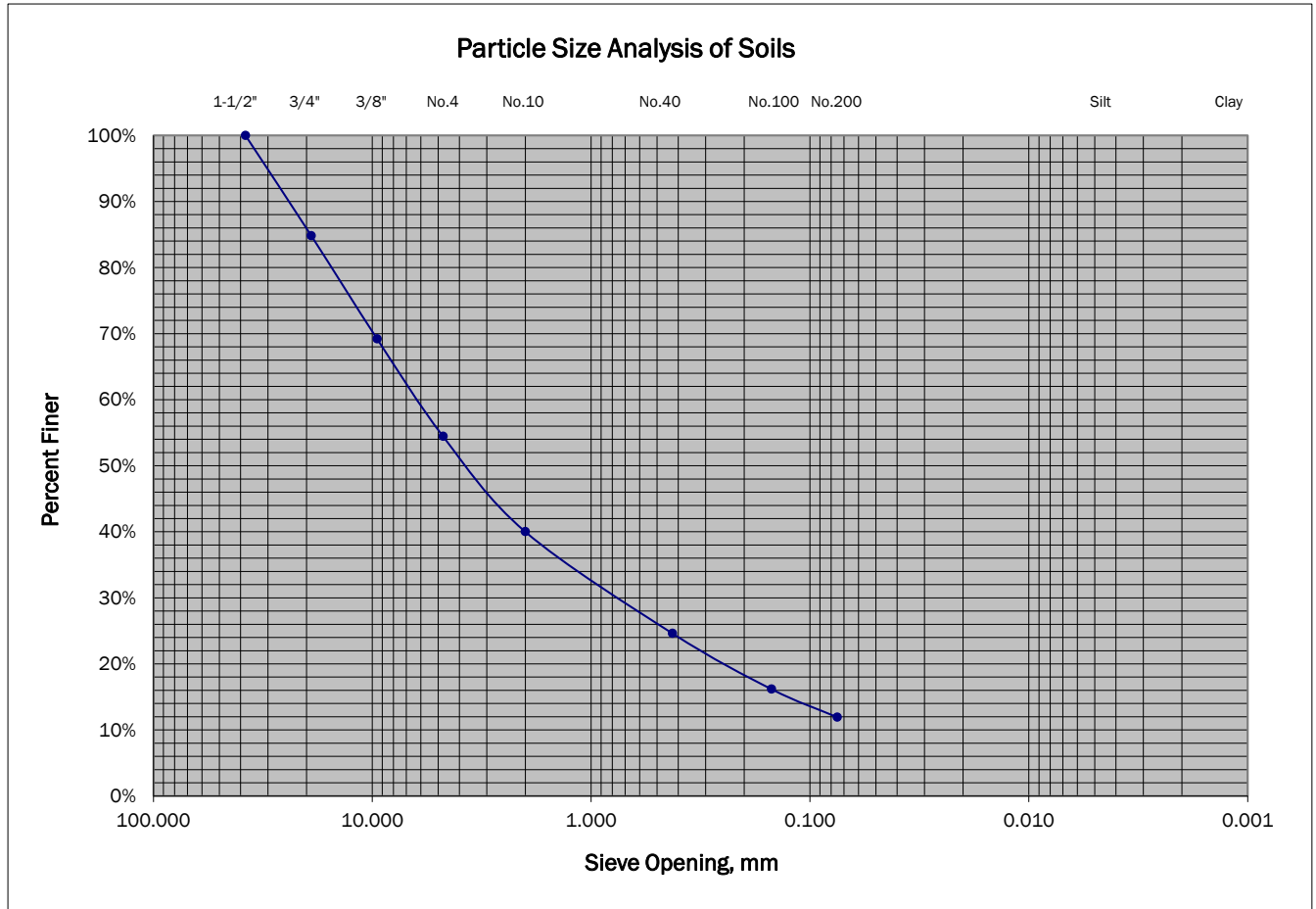
Per ASTM Designations D 2487 and D 2488



<b>As-Received Moisture</b> 21.9%		<b>Particle Size Distribution</b>						
<b>USCS Classification:</b> Silty SAND (SM)		US Standard Sieve Size		Opening (mm)	%Finer			
<b>Gravel:</b> 7.2%	<b>Coarse:</b> 0.0%	<b>GRAVEL</b>		Coarse	1-1/2"	38.0	100.0%	
<b>Fine:</b> 7.2%				Fine	3/4"	19.0	100.0%	
<b>Sand:</b> 54.4%	<b>Coarse:</b> 7.4%	<b>Medium:</b> 22.7%	<b>Fine:</b> 24.3%		3/8"	9.50	96.7%	
<b>Fines:</b> 38.4%	<b>Silt:</b>				No. 4	4.75	92.8%	
<b>Gravel Description:</b> Subangular to Subrounded					No. 10	2.00	85.4%	
<b>Sand Description:</b> Subangular				<b>SAND</b>	Medium	No. 40	0.425	62.7%
<b>Consistency:</b> N/A	<b>Dry Strength:</b> Low				Fine	No. 100	0.150	47.9%
<b>Dilatancy:</b> Rapid	<b>Toughness:</b> Low					No. 200	0.075	38.4%
<b>Structure:</b> Homogeneous	<b>Cementation:</b> N/A			Hydrometer Analysis	Silt Size	0.005		
					Clay Size	0.001		
				D <sub>60</sub> :	D <sub>30</sub> :	D <sub>10</sub> :	Cu:	Cc:
<b>Test Pit:</b> TP-2			<b>Atterberg Limits</b>		<b>LL:</b> 36	<b>PL:</b> 33	<b>PI:</b> 3	
<b>Sample:</b> S1	<b>Depth:</b> 3'			<b>Description:</b> Brown Silty SAND				
<b>Project:</b> Westtown School Oak Lane - Infiltration				<b>Remarks:</b> Stratum I				
<b>Client:</b> ELA Group, Inc.								
<b>Advantage Project Number:</b> 1800331001				<b>Report Date:</b> October 4, 2018				

# Soil Classification Report

Per ASTM Designations D 2487 and D 2488



As-Received Moisture 10.7%		Particle Size Distribution						
<b>USCS Classification:</b> Poorly Graded GRAVEL with Silt and Sand (GP-GM)		US Standard Sieve Size		Opening (mm)	%Finer			
<b>Gravel:</b> 45.6%	<b>Coarse:</b> 15.2%	<b>Fine:</b> 30.4%	<b>GRAVEL</b>	Coarse	1-1/2"	38.0	100.0%	
<b>Sand:</b> 42.5%	<b>Coarse:</b> 14.4%	<b>Medium:</b> 15.4%		<b>Fine:</b> 12.7%	Fine	3/4"	19.0	84.8%
<b>Fines:</b> 11.9%	<b>Silt:</b>	<b>Clay:</b>				3/8"	9.50	69.2%
<b>Gravel Description:</b> Subangular						No. 4	4.75	54.4%
<b>Sand Description:</b> Subangular			<b>SAND</b>	Coarse	No. 10	2.00	40.0%	
<b>Consistency:</b> N/A	<b>Dry Strength:</b> Low			Medium	No. 40	0.425	24.6%	
<b>Dilatancy:</b> Rapid	<b>Toughness:</b> Low			Fine	No. 100	0.150	16.2%	
<b>Structure:</b> Homogeneous	<b>Cementation:</b> N/A				No. 200	0.075	11.9%	
			Hydrometer Analysis	Silt Size	0.005			
				Clay Size	0.001			
			D <sub>60</sub> : 6.3	D <sub>30</sub> : 0.75	D <sub>10</sub> : 0.57	Cu: 11	Cc: 0.16	
<b>Test Pit:</b> TP-5			<b>Atterberg Limits</b>	<b>LL:</b> 36	<b>PL:</b> 35	<b>PI:</b> 1		
<b>Sample:</b> S1	<b>Depth:</b> 4' - 6'	<b>Description:</b> Brown GRAVEL with Silt and Sand						
<b>Project:</b> Westtown School Oak Lane - Infiltration	<b>Remarks:</b> Stratum I							
<b>Client:</b> ELA Group, Inc.								
<b>Advantage Project Number:</b> 1800331001	<b>Report Date:</b> October 4, 2018							

# TEST PIT LOG

PROJECT NAME: Westtown School Oak Lane - Infiltration

TEST PIT NO.: TP-1

PROJECT NO.: 1800331001 CLIENT: ELA Group, Inc.

TOP OF GROUND: ±319.5'

LOCATION: See Exploration Plan (Figure 3)

GROUNDWATER DATA: Dry

FIELD SURVEYED

TOPO ESTIMATE

DEPTH: Not Encountered Time: Completion

DEPTH (feet)	SOIL DESCRIPTION	REMARKS			
	0.0' - 0.5' Tan Clayey SAND	<b>Baseball Infield</b>			
	0.5' - 7.5' Brown Silty SAND				
5	Brown Silty SAND with Gravel	<b>Stratum I</b>			
	<b>-End of Test Pit at 7.5 Feet-</b>				
10	Infiltration Tests Conducted at 3.5 Feet (316') and 5.5 Feet (314')				
15					
	<b>DOUBLE RING INFILTRMETER DATA</b>				
	Test Depth:	3.5'	5.5'		
		Time (min)	Drop (inches')	Time (min)	Drop (inches)
20	Pre-soak 1	30	1.7	30	5.0
	Pre-soak 2	30	1.2	30	5.0
	Reading 1	30	1.0	10	1.0
	Reading 2	30	0.8	10	1.0
	Reading 3	30	0.8	10	1.0
25	Reading 4	30	1.0	10	1.0
	Reading 5			10	1.0
	Reading 6			10	1.0
	Reading 7				
	Reading 8				
30	Average Rate (inches per hour)		1.8		6.0



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 Office: (717) 458-0800 Fax: (717) 458-0801  
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EXCAVATION METHOD: Mini-excavator  
 ADVANTAGE REPRESENTATIVE: B. Wildasin  
 DATE EXCAVATED: September 27, 2018  
 DRAWN/COMPILED BY: B. Wildasin

# TEST PIT LOG

PROJECT NAME: Westtown School Oak Lane - Infiltration

TEST PIT NO.: TP-2

PROJECT NO.: 1800331001 CLIENT: ELA Group, Inc.

TOP OF GROUND: ±317'

LOCATION: See Exploration Plan (Figure 3)

GROUNDWATER DATA: Dry

FIELD SURVEYED

TOPO ESTIMATE

DEPTH: Not Encountered Time: Completion

DEPTH (feet)	SOIL DESCRIPTION	REMARKS																																																								
	0.0' - 0.8' Brown organic soil	<b>Topsoil</b>																																																								
	0.8' - 5.0' Brown Sandy SILT Brown Silty SAND																																																									
5		<b>Stratum I</b>																																																								
	<b>-End of Test Pit at 5 Feet-</b>																																																									
10	Infiltration Tests Conducted at 1 Foot (316') and 3 Feet (314')																																																									
	<table border="1" style="margin: auto; border-collapse: collapse;"> <thead> <tr> <th colspan="4" style="text-align: center;">DOUBLE RING INFILTROMETER DATA</th> </tr> <tr> <th style="text-align: center;">Test Depth:</th> <th colspan="2" style="text-align: center;">1'</th> <th style="text-align: center;">3'</th> </tr> <tr> <th></th> <th style="text-align: center;">Time (min)</th> <th style="text-align: center;">Drop (inches)</th> <th style="text-align: center;">Drop (inches)</th> </tr> </thead> <tbody> <tr> <td style="text-align: center;">Pre-soak 1</td> <td style="text-align: center;">30</td> <td style="text-align: center;">no movement</td> <td style="text-align: center;">1</td> </tr> <tr> <td style="text-align: center;">Pre-soak 2</td> <td style="text-align: center;">30</td> <td style="text-align: center;">no movement</td> <td style="text-align: center;">0.7</td> </tr> <tr> <td style="text-align: center;">Reading 1</td> <td style="text-align: center;">30</td> <td style="text-align: center;">no movement</td> <td style="text-align: center;">0.8</td> </tr> <tr> <td style="text-align: center;">Reading 2</td> <td style="text-align: center;">30</td> <td style="text-align: center;">no movement</td> <td style="text-align: center;">0.8</td> </tr> <tr> <td style="text-align: center;">Reading 3</td> <td style="text-align: center;">30</td> <td style="text-align: center;">no movement</td> <td style="text-align: center;">0.6</td> </tr> <tr> <td style="text-align: center;">Reading 4</td> <td style="text-align: center;">30</td> <td style="text-align: center;">no movement</td> <td style="text-align: center;">0.6</td> </tr> <tr> <td style="text-align: center;">Reading 5</td> <td></td> <td></td> <td></td> </tr> <tr> <td style="text-align: center;">Reading 6</td> <td></td> <td></td> <td></td> </tr> <tr> <td style="text-align: center;">Reading 7</td> <td></td> <td></td> <td></td> </tr> <tr> <td style="text-align: center;">Reading 8</td> <td></td> <td></td> <td></td> </tr> <tr> <td colspan="2" style="text-align: center;">Average Rate (inches per hour)</td> <td style="text-align: center;">0.0 (no movement)</td> <td style="text-align: center;">1.4</td> </tr> </tbody> </table>		DOUBLE RING INFILTROMETER DATA				Test Depth:	1'		3'		Time (min)	Drop (inches)	Drop (inches)	Pre-soak 1	30	no movement	1	Pre-soak 2	30	no movement	0.7	Reading 1	30	no movement	0.8	Reading 2	30	no movement	0.8	Reading 3	30	no movement	0.6	Reading 4	30	no movement	0.6	Reading 5				Reading 6				Reading 7				Reading 8				Average Rate (inches per hour)		0.0 (no movement)	1.4
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EXCAVATION METHOD: Mini-excavator

ADVANTAGE REPRESENTATIVE: B. Wildasin

DATE EXCAVATED: September 27, 2018

DRAWN/COMPILED BY: B. Wildasin

# TEST PIT LOG

PROJECT NAME: Westtown School Oak Lane - Infiltration

TEST PIT NO.: TP-3

PROJECT NO.: 1800331001 CLIENT: ELA Group, Inc.

TOP OF GROUND: ±321'

LOCATION: See Exploration Plan (Figure 3)

GROUNDWATER DATA: Dry

FIELD SURVEYED

TOPO ESTIMATE

DEPTH: Not Encountered Time: Completion

DEPTH (feet)	SOIL DESCRIPTION	REMARKS																																																								
	0.0' - 0.8' Brown organic soil	<b>Topsoil</b>																																																								
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**Stratum I**



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EXCAVATION METHOD: Mini-excavator  
 ADVANTAGE REPRESENTATIVE: B. Wildasin  
 DATE EXCAVATED: September 27, 2018  
 DRAWN/COMPILED BY: B. Wildasin



# TEST PIT LOG

PROJECT NAME: Westtown School Oak Lane - Infiltration

TEST PIT NO.: TP-4

PROJECT NO.: 1800331001 CLIENT: ELA Group, Inc.

TOP OF GROUND: ±319.5'

LOCATION: See Exploration Plan (Figure 3)

GROUNDWATER DATA: Dry

FIELD SURVEYED

TOPO ESTIMATE

DEPTH: Not Encountered Time: Completion

DEPTH (feet)	SOIL DESCRIPTION	REMARKS																																																								
	0.0' - 0.8' Brown organic soil	<b>Topsoil</b>																																																								
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5		<b>Stratum I</b>																																																								
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EXCAVATION METHOD: Mini-excavator  
 ADVANTAGE REPRESENTATIVE: B. Wildasin  
 DATE EXCAVATED: September 26, 2018  
 DRAWN/COMPILED BY: B. Wildasin

# TEST PIT LOG

PROJECT NAME: Westtown School Oak Lane - Infiltration

TEST PIT NO.: TP-5

PROJECT NO.: 1800331001 CLIENT: ELA Group, Inc.

TOP OF GROUND: ±321'

LOCATION: See Exploration Plan (Figure 3)

GROUNDWATER DATA: Dry

FIELD SURVEYED

TOPO ESTIMATE

DEPTH: Not Encountered Time: Completion

DEPTH (feet)	SOIL DESCRIPTION	REMARKS
	0.0' - 0.8' Dark brown Sandy CLAY with organic debris	<b>Topsoil</b>
	0.8' - 6.0' Brown Silty SAND	
	Brown GRAVEL with Silt and Sand	
5		<b>Stratum I</b>
	<b>-End of Test Pit at 6 Feet-</b>	
	Infiltration Tests Conducted at 1.5 Feet (319.5') and 4 Feet (317')	
10		
15		
	<b>DOUBLE RING INFILTRMETER DATA</b>	
	Test Depth:	1.5'
		4'
		Time (min)
		Drop (inches)
		Time (min)
		Drop (inches)
20	Pre-soak 1	30
		2.4
	Pre-soak 2	30
		1.8
	Reading 1	30
		1.8
	Reading 2	30
		1.7
	Reading 3	30
		1.7
25	Reading 4	30
		1.7
	Reading 5	10
		0.8
	Reading 6	
	Reading 7	
	Reading 8	
30	Average Rate (inches per hour)	3.4
		4.8



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EXCAVATION METHOD: Mini-excavator  
 ADVANTAGE REPRESENTATIVE: B. Wildasin  
 DATE EXCAVATED: September 26, 2018  
 DRAWN/COMPILED BY: B. Wildasin

# TEST PIT LOG

PROJECT NAME: Westtown School Oak Lane - Infiltration

TEST PIT NO.: TP-6

PROJECT NO.: 1800331001 CLIENT: ELA Group, Inc.

TOP OF GROUND: ±311'

LOCATION: See Exploration Plan (Figure 3)

GROUNDWATER DATA: Dry

FIELD SURVEYED

TOPO ESTIMATE

DEPTH: Not Encountered Time: Completion

DEPTH (feet)	SOIL DESCRIPTION	REMARKS																																																								
	0.0' - 1.5' Dark brown organic soil	<b>Tilled Soil</b>																																																								
	1.5' - 6.0' Brown Sandy SILT																																																									
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EXCAVATION METHOD: Mini-excavator  
 ADVANTAGE REPRESENTATIVE: B. Wildasin  
 DATE EXCAVATED: September 26, 2018  
 DRAWN/COMPILED BY: B. Wildasin

# TEST PIT LOG

PROJECT NAME: Westtown School Oak Lane - Infiltration

TEST PIT NO.: TP-7

PROJECT NO.: 1800331001 CLIENT: ELA Group, Inc.

TOP OF GROUND: ±313'

LOCATION: See Exploration Plan (Figure 3)

GROUNDWATER DATA: Wet

FIELD SURVEYED

TOPO ESTIMATE

DEPTH: 6'

Time: Completion

DEPTH (feet)	SOIL DESCRIPTION	REMARKS																																																								
	0.0' - 1.3' Brown organic soil	<b>Tilled Soil</b>																																																								
	1.3' - 8.0' Brown Sandy SILT Brown Silty SAND																																																									
5		<b>H<sub>2</sub>O @ 6'</b>																																																								
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EXCAVATION METHOD: Mini-excavator  
 ADVANTAGE REPRESENTATIVE: B. Wildasin  
 DATE EXCAVATED: September 26, 2018  
 DRAWN/COMPILED BY: B. Wildasin

# TEST PIT LOG

PROJECT NAME: Westtown School Oak Lane - Infiltration

TEST PIT NO.: TP-8

PROJECT NO.: 1800331001 CLIENT: ELA Group, Inc.

TOP OF GROUND: ±311'

LOCATION: See Exploration Plan (Figure 3)

GROUNDWATER DATA: Wet

FIELD SURVEYED

TOPO ESTIMATE

DEPTH: 1.5'

Time: Completion

DEPTH (feet)	SOIL DESCRIPTION	REMARKS
	0.0' - 1.5' Brown organic soil	
		<b>Tilled Soil</b>
	1.5' - 6.0' Brown Silty SAND	<b>H<sub>2</sub>O @ 1.5'</b>
5		
		<b>Stratum I</b>
	<b>-End of Test Pit at 6 Feet-</b>	
10		
	No infiltration tests conducted due to groundwater at 1.5 Feet (309.5')	
15		
20		
25		
30		



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 ADVANTAGE REPRESENTATIVE: B. Wildasin  
 DATE EXCAVATED: September 26, 2018  
 DRAWN/COMPILED BY: B. Wildasin

# TEST PIT LOG

PROJECT NAME: Westtown School Oak Lane - Infiltration

TEST PIT NO.: TP-9

PROJECT NO.: 1800331001 CLIENT: ELA Group, Inc.

TOP OF GROUND: ±303'

LOCATION: See Exploration Plan (Figure 3)

GROUNDWATER DATA: Dry

FIELD SURVEYED

TOPO ESTIMATE

DEPTH: Not Encountered Time: Completion

DEPTH (feet)	SOIL DESCRIPTION	REMARKS																																																				
	0.0' - 0.9' Brown organic soil	<b>Topsoil</b>																																																				
	0.9' - 10.0' Brown Silty SAND																																																					
5	Brown Silty SAND with Gravel																																																					
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EXCAVATION METHOD: Mini-excavator  
 ADVANTAGE REPRESENTATIVE: B. Wildasin  
 DATE EXCAVATED: September 28, 2018  
 DRAWN/COMPILED BY: B. Wildasin

# TEST PIT LOG

PROJECT NAME: Westtown School Oak Lane - Infiltration

TEST PIT NO.: TP-10

PROJECT NO.: 1800331001 CLIENT: ELA Group, Inc.

TOP OF GROUND: ±305'

LOCATION: See Exploration Plan (Figure 3)

GROUNDWATER DATA: Dry

FIELD SURVEYED

TOPO ESTIMATE

DEPTH: Not Encountered Time: Completion

DEPTH (feet)	SOIL DESCRIPTION	REMARKS			
	0.0' - 0.9' Brown organic soil	<b>Topsoil</b>			
	0.9' - 6.0' Brown Silty SAND	<b>Stratum I</b>			
5					
	6.0' - 7.5' Brown Silty SAND with Gravel (highly weathered rock)	<b>Stratum II</b>			
	<b>-Bucket Refusal at 7.5 Feet-</b> <b>-End of Test Pit at 7.5 Feet-</b>				
10					
	Infiltration Tests Conducted at 4 Feet (301') and 5.5 Feet (299.5')				
15					
<b>DOUBLE RING INFILTRMETER DATA</b>					
	Test Depth:	4'	5.5'		
		Time (min)	Drop (inches)	Time (min)	Drop (inches)
20	Pre-soak 1	30	2.2	30	3.5
	Pre-soak 2	30	1.5	30	2.7
	Reading 1	30	1.4	10	0.9
	Reading 2	30	1.4	10	0.6
	Reading 3	30	1.4	10	0.8
25	Reading 4	30	1.4	10	0.8
	Reading 5			10	0.8
	Reading 6			10	0.8
	Reading 7				
	Reading 8				
30	Average Rate (inches per hour)		2.8		4.8



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EXCAVATION METHOD: Mini-excavator  
 ADVANTAGE REPRESENTATIVE: B. Wildasin  
 DATE EXCAVATED: September 28, 2018  
 DRAWN/COMPILED BY: B. Wildasin

# TEST PIT LOG

PROJECT NAME: Westtown School Oak Lane - Infiltration

TEST PIT NO.: TP-11

PROJECT NO.: 1800331001 CLIENT: ELA Group, Inc.

TOP OF GROUND: ±309'

LOCATION: See Exploration Plan (Figure 3)

GROUNDWATER DATA: Dry

FIELD SURVEYED

TOPO ESTIMATE

DEPTH: Not Encountered Time: Completion

DEPTH (feet)	SOIL DESCRIPTION	REMARKS																																																				
	0.0' - 0.8' Brown organic soil	<b>Topsoil</b>																																																				
	0.8' - 6.0' Brown Silty SAND																																																					
5		<b>Stratum I</b>																																																				
	6.0' - 9.5' Brown Silty SAND with Gravel (highly weathered rock)																																																					
10		<b>Stratum II</b>																																																				
	<b>-Bucket Refusal at 9.5 Feet- -End of Test Pit at 9.5 Feet-</b>																																																					
	Infiltration Tests Conducted at 6 Feet (303') and 7.5 Feet (301.5')																																																					
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EXCAVATION METHOD: Mini-excavator  
 ADVANTAGE REPRESENTATIVE: B. Wildasin  
 DATE EXCAVATED: September 27, 2018  
 DRAWN/COMPILED BY: B. Wildasin



# TEST PIT LOG

PROJECT NAME: Westtown School Oak Lane - Infiltration

TEST PIT NO.: TP-12

PROJECT NO.: 1800331001 CLIENT: ELA Group, Inc.

TOP OF GROUND: ±298'

LOCATION: See Exploration Plan (Figure 3)

GROUNDWATER DATA: Wet

FIELD SURVEYED

TOPO ESTIMATE

DEPTH: 3.5'

Time: Completion

DEPTH (feet)	SOIL DESCRIPTION	REMARKS
	0.0' - 2.3' Brown organic soil	
		<b>Topsoil</b>
5	2.3' - 6.0' Brown to gray Sandy CLAY (Soil Mottling 2.5' - 6.0')	<b>H<sub>2</sub>O @ 3.5'</b>
		<b>Stratum III</b>
	<b>-End of Test Pit at 6 Feet-</b>	
10	No infiltration tests conducted due to Soil Mottling at 2.5 Feet (295.5') and Groundwater at 3.5 Feet (294.5')	
15		
20		
25		
30		



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EXCAVATION METHOD: Mini-excavator  
 ADVANTAGE REPRESENTATIVE: B. Wildasin  
 DATE EXCAVATED: September 28, 2018  
 DRAWN/COMPILED BY: B. Wildasin

# TEST PIT LOG

PROJECT NAME: Westtown School Oak Lane - Infiltration

TEST PIT NO.: TP-13

PROJECT NO.: 1800331001 CLIENT: ELA Group, Inc.

TOP OF GROUND: ±286'

LOCATION: See Exploration Plan (Figure 3)

GROUNDWATER DATA: Wet

FIELD SURVEYED

TOPO ESTIMATE

DEPTH: 1.5'

Time: Completion

DEPTH (feet)	SOIL DESCRIPTION	REMARKS
	0.0' - 1.5' Brown organic soil	<b>Topsoil</b>
	1.5' - 6.0' Brown to gray Sandy CLAY (Soil Mottling 2.5' - 6.0')	<b>H<sub>2</sub>O @ 1.5'</b>
5		<b>Stratum III</b>
	<b>-End of Test Pit at 6 Feet-</b>	
10	No infiltration tests conducted due to Groundwater at 1.5 Feet (284.5') and Soil Mottling at 2.5 Feet (283.5')	
15		
20		
25		
30		



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EXCAVATION METHOD: Mini-excavator  
 ADVANTAGE REPRESENTATIVE: B. Wildasin  
 DATE EXCAVATED: September 28, 2018  
 DRAWN/COMPILED BY: B. Wildasin



November 9, 2018

Westtown School  
975 Westtown Road  
West Chester, PA 19382

c/o

Mr. Charles R. Haley, Jr., P.E.  
ELA Group, Inc.  
743 South Broad Street  
Lititz, PA 17543

**RE: Supplemental Infiltration Feasibility Report  
Westtown School Oak Lane – Supplemental Infiltration  
Westtown Township, Chester County, Pennsylvania  
Advantage Project Number: 1800331001**

Dear Mr. Haley:

In accordance with your request, Advantage Engineers (Advantage) has completed supplemental infiltration testing for the above referenced project site. This correspondence serves to transmit the results of our supplemental evaluation.

## **SCOPE OF WORK**

The objective of our work was to determine the permeability of the invert soils, identify any limiting zones (i.e. bedrock, groundwater, or seasonal high water table) within the proposed stormwater management facility, and address PADEP requirements as they relate to stormwater management. Our scope of work included the completion of a subsurface exploration and preparation of this report. This report presents a summary of the scope of work completed, conditions encountered, and results of the supplemental infiltration testing engineering analysis of subsurface conditions.

## **SUBSURFACE FIELD EXPLORATION**

In order to characterize subsurface conditions, 3 test pits were excavated on October 31, 2018. Supervision and monitoring of the field exploration was provided by a representative of Advantage who field located the test locations based on the "Updated Sketch Plan", prepared by Site Engineering Concepts, LLC. The approximate test locations, referenced as TP-14 through TP-16, are shown on the attached *Exploration Plan* (Figure 1). Data pertaining to the subsurface exploration was documented in the field and is presented in detail on the *Test Pit Logs*, which contain detailed descriptions of the subsurface materials encountered and infiltration test depths/elevations. A general description of the soil conditions encountered is provided in the "Subsurface Conditions" section of this report.

## **SUBSURFACE CONDITIONS**

### **Soil**

#### **Surficial Materials**

Each test pit was covered by approximately 16 inches of tilled soil; however, the thickness of surficial materials may differ in unexplored areas of the project site.



**Stratum I – Brown Silty SAND/Sandy SILT**

Stratum I was encountered within test pits TP-14 and TP-16 and extended to depths of approximately 5 feet below existing site grades. Upon review, the soils of Stratum I were found to be moderately well graded, non-plastic and comprised of Silty SAND and Sandy SILT.

**Stratum II – Brown Silty SAND with Gravel (highly weathered rock)**

Stratum II was only encountered within test pit TP-16 and extended to its termination depth of approximately 7 feet below existing site grades. Upon review, the soils of Stratum II were found to be well graded, non-plastic and predominately comprised of Silty SAND with Gravel. The soils of Stratum II represent the highly weathered bedrock surface.

**Stratum III – Brown Sandy CLAY**

Stratum III was only encountered within test pit TP-15 and extended to its termination depth of approximately 5 feet below existing site grades. Upon review, the soils of Stratum III were found to be poorly graded, plastic and comprised of Sandy CLAY.

**Bedrock**

The bedrock surface was not encountered within the test pits excavated. The bedrock surface would have been defined as the depth at which the bucket of the given excavation equipment could no longer excavate.

**Groundwater/Soil Mottling**

Neither groundwater nor soil mottling was encountered within the test pits excavated. These observations were made at the time of the field operation and groundwater table elevations will vary with daily, seasonal, and climatological variations.

**INFILTRATION ANALYSIS**

To evaluate the feasibility of stormwater infiltration within the proposed stormwater management facility, infiltration tests were completed utilizing the “double-ring” infiltrometer method in accordance with the Pennsylvania Stormwater Best Management Practices Manual, latest Edition. It should be noted that the shallow tests in both TP-14 and TP-15 were completed 6-inches below the proposed test elevations due to the thickness of the tilled soil. The test pit locations, approximate surface elevations, proposed test elevations, actual test elevations, presence of limiting zones, and the infiltration rates achieved at each location are presented in the table below.

INFILTRATION TEST RESULTS					
Test Location	Surface Elevation (ft)	Proposed Test Elevations (ft)	Actual Test Elevations (FT)	Limiting Zone Elevation (ft)	Infiltration Rate* (in/hr)
TP-14	290	289	288.5	Not Encountered @ 285	0.2
		287	287		1.0
TP-15	290	289	288.5	Not Encountered @ 285	0.0
		287	287		0.0
TP-16	292	289	289	Not Encountered @ 285	2.7
		287	287		6.0

*\*Infiltration rates represent the rates recorded in the field and no safety factor has been applied*



## SUMMARY OF DATA & CONCLUSIONS

Based on the results of our field exploration and engineering analysis of the data obtained, we offer the following comments with regard to the infiltration of stormwater at the project site.

- The infiltration tests were conducted within the naturally-occurring soils of Stratum I, Stratum II and Stratum III.
- No limiting zones (i.e. bedrock, groundwater and/or soil mottling) were encountered within the test pits excavated.
- The unfactored infiltration rates were found to range from no movement (0.0 inches per hour) to 6.0 inches per hour. The PADEP recommended rate for infiltration of stormwater is 0.1 to 10 inches per hour.

## LIMITATIONS

The conclusions contained in this report are based upon the subsurface data collected and on details stated in this report. Should conditions arise which differ from those specifically stated herein, our office should be notified immediately, so that our recommendations can be reviewed and revised, if necessary.

The conclusions presented herein should be applied only to the infiltration tests as depicted on the *Exploration Plan* for the proposed Westtown School improvements in Westtown Township, Chester County, Pennsylvania. Advantage takes no responsibility in utilizing this information for any other purposes.

The scope of work was limited to the exploration of the subsurface subsoils. Oil, hazardous waste, radioactivity, irritants, pollutants, radon or other dangerous substances and conditions were not the subject of this study. Their presence and/or absence are not implied, inferred or suggested by this report or results of this study.

We trust that this is the information you require. Should you have any questions or if we may be of further assistance, please don't hesitate to contact our office.

Respectfully,  
**advantage engineers**

A handwritten signature in black ink that reads "Bailey Jean Wildasin".

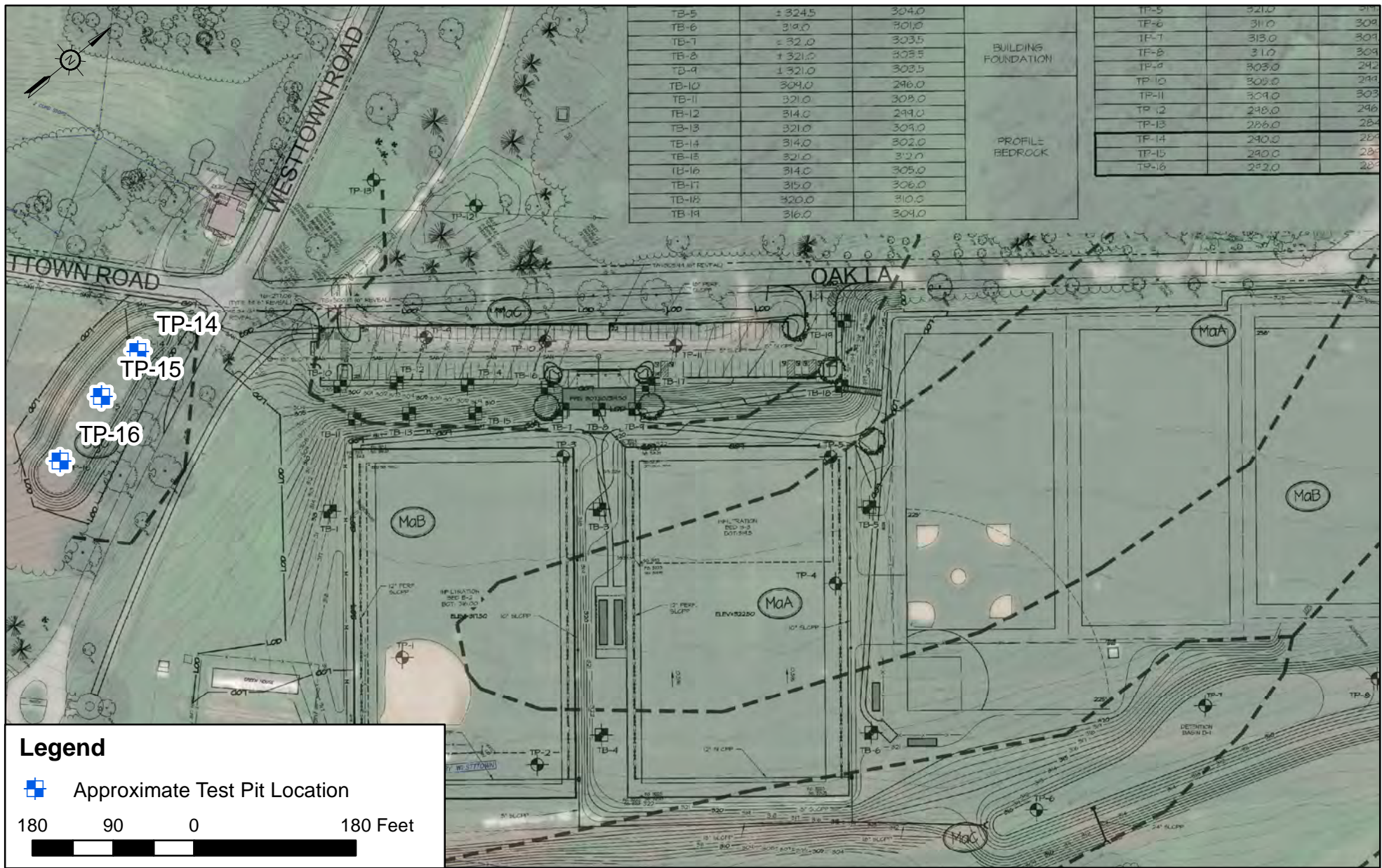
Bailey J. Wildasin  
Geotechnical Specialist I

A handwritten signature in black ink that reads "David J. Buckwalter".

David J. Buckwalter  
Senior Project Manager

### Attachments:

Exploration Plan – Figure 1  
Test Pit Logs



TB-5	± 324.5	304.0
TB-6	319.0	301.0
TB-7	± 32.0	303.5
TB-8	± 321.0	303.5
TB-9	1 321.0	303.5
TB-10	309.0	296.0
TB-11	321.0	303.0
TB-12	314.0	299.0
TB-13	321.0	309.0
TB-14	314.0	302.0
TB-15	321.0	312.0
TB-16	314.0	305.0
TB-17	315.0	306.0
TB-18	320.0	310.0
TB-19	316.0	304.0

TP-5	321.0	311.0
TP-6	311.0	309.0
TP-7	313.0	309.0
TP-8	311.0	309.0
TP-9	303.0	292.0
TP-10	309.0	299.0
TP-11	309.0	303.0
TP-12	298.0	296.0
TP-13	286.0	284.0
TP-14	290.0	284.0
TP-15	290.0	284.0
TP-16	282.0	284.0

**Legend**

Approximate Test Pit Location

180      90      0      180 Feet

\*Source - "Updated Sketch Plan" provided by Site Engineering Concepts, LLC, received 10-24-2018

SCALE: AS SHOWN	DRAWING NUMBER: FIGURE 1
DRAWN BY: B. WILDASIN	CHECKED BY: D. BUCKWALTER
APPROVED BY: M. GIUNTA	DATE: 10-26-2018

**EXPLORATION PLAN**

PREPARED FOR  
**WESTTOWN SCHOOL OAK LANE - SUPPLEMENTAL INFILTRATION**

WESTTOWN TOWNSHIP      CHESTER COUNTY      PENNSYLVANIA



**advantage engineers**

435 INDEPENDENCE AVE., SUITE C  
MECHANICSBURG, PA 17055  
PH (717) 458-0800  
FAX (717)458-0801

# TEST PIT LOG

PROJECT NAME: Westtown School Oak Lane - Supplemental Infiltration

TEST PIT NO.: TP-14

PROJECT NO.: 1800331001 CLIENT: ELA Group, Inc.

TOP OF GROUND: ±290'

LOCATION: See Exploration Plan (Figure 3)

GROUNDWATER DATA: Dry

FIELD SURVEYED

TOPO ESTIMATE

DEPTH: Not Encountered Time: Completion

DEPTH (feet)	SOIL DESCRIPTION	REMARKS																																																								
	0.0' - 1.3' Brown organic soil	<b>Tilled Soil</b>																																																								
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[www.advantageengineers.com](http://www.advantageengineers.com)

EXCAVATION METHOD: Backhoe  
 ADVANTAGE REPRESENTATIVE: B. Wildasin  
 DATE EXCAVATED: October 31, 2018  
 DRAWN/COMPILED BY: B. Wildasin

# TEST PIT LOG

PROJECT NAME: Westtown School Oak Lane - Supplemental Infiltration

TEST PIT NO.: TP-15

PROJECT NO.: 1800331001 CLIENT: ELA Group, Inc.

TOP OF GROUND: ±290'

LOCATION: See Exploration Plan (Figure 3)

GROUNDWATER DATA: Dry

FIELD SURVEYED

TOPO ESTIMATE

DEPTH: Not Encountered Time: Completion

DEPTH (feet)	SOIL DESCRIPTION	REMARKS																																																								
	0.0' - 1.3' Brown organic soil	<b>Tilled Soil</b>																																																								
	1.3' - 5.0' Brown Sandy CLAY																																																									
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EXCAVATION METHOD: Backhoe  
 ADVANTAGE REPRESENTATIVE: B. Wildasin  
 DATE EXCAVATED: October 31, 2018  
 DRAWN/COMPILED BY: B. Wildasin



# TEST PIT LOG

PROJECT NAME: Westtown School Oak Lane - Supplemental Infiltration

TEST PIT NO.: TP-16

PROJECT NO.: 1800331001 CLIENT: ELA Group, Inc.

TOP OF GROUND: ±292'

LOCATION: See Exploration Plan (Figure 3)

GROUNDWATER DATA: Dry

FIELD SURVEYED

TOPO ESTIMATE

DEPTH: Not Encountered Time: Completion

DEPTH (feet)	SOIL DESCRIPTION	REMARKS
	0.0' - 1.3' Brown organic soil	<b>Tilled Soil</b>
	1.3' - 5.0' Brown Silty SAND	
5		<b>Stratum I</b>
	5.0' - 7.0' Brown Silty SAND with Gravel (highly weathered rock)	<b>Stratum II</b>
	<b>-End of Test Pit at 7 Feet-</b>	
10		
	Infiltration Tests Conducted at 3 Feet (289') and 5 Feet (287')	
15		
	<b>DOUBLE RING INFILTROMETER DATA</b>	
	Test Depth:	3'
		5'
		Time (min)
		Drop (inches)
		Time (min)
		Drop (inches)
20	Pre-soak 1	30
		1.9
	Pre-soak 2	30
		1.4
	Reading 1	30
		1.4
	Reading 2	30
		1.3
	Reading 3	30
		1.3
25	Reading 4	30
		1.4
	Reading 5	10
		1.0
	Reading 6	
	Reading 7	
	Reading 8	
30	Average Rate (inches per hour)	2.7
		6.0



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