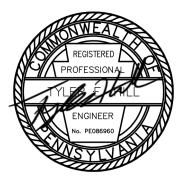
EROSION AND SEDIMENT CONTROL REPORT

FOR

THE WESTTOWN SCHOOL OAK LANE PROJECT WESTTOWN TOWNSHIP CHESTER COUNTY, PA

PROJECT NO: 1091-001



January 27, 2023 Revised: October 27, 2023

Prepared By:



ELA GROUP, INC.

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Central PA Office 2013 Sandy Drive, Suite 103 State College, PA 16803 (814) 861-6328

DEPARTMENT OF ENVIRONMENTAL PROTECTION

COMMONWEALTH OF PENNSYLVANIA DEPARTMENT OF ENVIRONMENTAL PROTECTION BUREAU OF CLEAN WATER

NATIONAL POLLUTANT DISCHARGE ELIMINATION SYSTEM (NPDES) DISCHARGES OF STORMWATER ASSOCIATED WITH CONSTRUCTION ACTIVITIES EROSION AND SEDIMENT CONTROL (E&S) MODULE 1

Applicant: The Westtown School

Project Site Name: The Westtown School - Oak Lane Project

TSF, MF

Surface Water Name(s): East Branch Chester Creek

E&S PLAN INFORMATION

Surface Water Use(s):

1. Describe the existing topographic features of the project site and the immediate surrounding area.

The project site is located near the center of the Westtown School campus, just south of Oak Lane. The site largely comprised of existing grass athletic fields which are bordered to the north by a partially forested area and the school's academic centers; to the east by a baseball field and residential area; the south by agricultural fields and a partially forested riparian area; and to the west by the school's working farm and agricultural area.

2.	Complete t	the following table for soils present at the project site					
	Map Unit Symbol	Map Unit Name	Acres	HSG	% of Disturbed Area	Depth (ft)	Hydric
	CaB	Califon loam	1.14	D	6.48	8-12	
	GgC	Glenelg silt loam	0.87	В	4.95	7+	\boxtimes
	MaA/B/ C	Manor loam	15.58	В	88.57	5-12	

Discuss any soil limitations and how the E&S Plan was designed to address those limitations.

See plan sheet 5 for the soil limitations information.

If Hydric soils are present, is a wetland determination attached to this module? Xes No N/A

If soils are known to be contaminated, 1) identify the pollutants exceeding Act 2 standards in the space provided below, 2) identify the extent of soil contamination on an E&S Plan Drawing that is attached to this module, and 3) describe the methods that will be used to avoid or minimize disturbance of the contaminated soils in the space provided below.

n/a

3. Describe the characteristics of the earth disturbance activity, including the past, present and proposed land uses and the proposed alteration to the project site.

The proposed improvements primarily involve the conversion of two (2) grass athletic fields to synthetic turf fields, construction of a paved parking lot in an existing gravel parking area, as well as additional access improvements, concession building, and a comprehensive stormwater management system

4. Describe the volume and rate of runoff from the project site and its upstream watershed area.

The project site consists primarily of grass athletic fields, with some existing gravel parking and a small portion of agricultural area. Runoff from the site generally flows to the southeast (DP001/EBCC) or southwest (DP002/UNT to EBCC) prior to entering the receiving surface waters.

Discharge point 001 (DP001) is considered to be a point in a roadside swale that receives surface runoff from the eastern portion of the project site. The calculated change in runoff for the 2-yr/24-hr storm from pre- to post-

development is approximately 10,516 CF, which is being fully mitigated by the proposed infiltration facilities. Peak flow rates for the 2-yr/24-hr storm is being reduced from 2.38 cfs to 1.27 CFS from pre- to post-developmetn as a result of the implementation of the proposed PCSM BMP's.

DP002 is considered to be a point in a natural drainageway upgradient of the headwaters of the reciving Unnamed Tributary to East Branch Chester Creek. The calculated change in runoff for the 2-yr/24-hr storm from pre- to post-development is approximately 49,535 CF, which is being fully mitigated by the proposed infiltration facilities. Peak flow rates for the 2-yr/24-hr storm is being reduced from 5.02 cfs to 2.51 CFS from pre- to post-development as a result of the implementation of the proposed PCSM BMP's.

For complete information regarding the rate and volume of stormater from the project area refer to the Post Construction Stormwater Management Report.

3800-PM-BCW0406a Rev. 12/2019 E&S Module 1

Identified	Plan No(s). for O&M	Deviation(s) from E&S Manual
18, 19, 32	32	
33	33	
18, 32	32	
18, 19, 33	33	
33	33	Modified for use w/ compost filter sock
	18, 32 18, 19, 33	18, 32 32 18, 19, 33 33

	E&S BMPs	Plan No(s). Identified	Plan No(s). for O&M	Deviation(s) from E&S Manual
	Sediment Filter Log (Fiber Log)			
	Wood Chip Filter Berm			
	Straw Bale Barrier			
	Rock Filter			
	Vegetative Filter Strip			
	Inlet Filter Bag			
	Stone Inlet Protection			
	Runoff Conveyance (Channel)			
	Bench			
	Top-of-Slope Berm			
	Temporary Slope Pipe			
\square	Sediment Basin	18, 19, 34	34	
\square	Sediment Trap	18, 34	34	
\square	Riprap Apron	18, 19, 37	37	
	Flow Transition Mat			
	Stilling Basin (Plunge Pool)			
	Stilling Well			
	Energy Dissipater			
	Drop Structure			
	Earthen Level Spreader			
	Structural Level Spreader			
	Surface Roughening			
\square	Vegetative Stabilization	35	4 & 5	
\square	Erosion Control Blanket	18, 19, 32	4 & 5	
	Soil Binders			
	Sodding			
	Cellular Confinement Systems			
	Alternative:			
	Alternative:			

Table 1 – For PAG-01 applicants, complete the requested information for each selected E&S BMP, where applicable.

Site Access BMPs										
BMP Name	No.	Length (ft)	Width (ft)	% Slope	Spacing (ft)	Length of Upslope Drainage (ft)	Culvert Diameter (in)	Soil Ty	vpe in Ditch	E&S Manual Figure/Detail No.
Rock Construction Entrance (RCE)										
RCE with Wash Rack										
Temporary and Permanent Access Roads – Crowned Roadway										
Temporary and Permanent Access Roads – Insloped Roadway										
Waterbar										
Broad-based Dip										
Open-top Culvert										
Water Deflector										
Roadside Ditch										
Ditch Relief Culvert										
Sediment Barriers / Filters	1	I	1				1	1		
BMP Name	DA (a	c) Dian	neter (in)	Storage Capacity (cf)	Trap Heig (in)	ht % Slope	Slope I Above B		Barrier Height (in)	E&S Manual Figure/Detail No.
Compost Sock Sediment Trap										
Compost Filter Sock										
Compost Filter Berm										
Silt Fence (Filter Fabric Fence)										
Super Silt Fence										
Sediment Filter Log										
Weighted Sediment Filter Tube										
Straw Bale Barrier										
Wood Chip Filter Berm										
Toe-of-Slope Berm										

Table 1 – For PAG-01 applicants, complete the requested information for each selected E&S BMP, where applicable.

Runoff Conveyanc	e BMPs			-		-											
BMP Name	Temporary	Desigr Storm		ac) Multip	olier	Qr (cfs)	Q (cfs	;) <mark> </mark>	Mannin n	g's	Va (fps)	V (fps)	D (f	t) d (f	t) De	ow epth atio	E&S Manual Figure/Detail No.
Vegetated Channel																	
Sodded Channel																	
Riprap Channel																	
Energy Reduction	BMPs											·					
BMP Name	Downstread to Drainage			nstream % Slope		DA (ac)		char (cfs)		Mani Depti			w Pipe eter (in		let Pipe neter (ir		E&S Manual Figure/Detail No.
Level Spreader																	
Drop Structure																	
Stilling Basins / W	ells		•									·					
BMP Name	Pipe Diameter (in) Dischar	ge (cfs)	Well Diar (in)			n of Wel Invert (Basin D)epth ((ft)	Median Ri Size (ii		Discha to Basi		е	E&S Manual Figure/Detail No.
Stilling Basin															-		
Stilling Well																	
Other BMPs	1	•		•		-											
BMP Name	DA (ac)	Pipe Diameter (in)	Berm Height (in)	Length (ft)	% Slo		cing	Chai Dept	nnel th (ft)	Ripi Siz		Riprap Thicknes (in)		Initial /idth (ft)	Term Widt		E&S Manual Figure/Detail No.
Temporary Slope Pipe																	
Bench																	
Rock Filter																	
Riprap Apron																	

For selected BMPs not identified in will be used for design and impleme		the BMP and the Figure or Detail No	b. from the E&S Manual that				
BMP Name	E&S Manual Figure/Detail No.	BMP Name	E&S Manual Figure/Detail No.				
6. All applicable Standard E&S	Worksheets from Appendix	x B of the E&S Manual have been co	mpleted and are attached.				
7. Other worksheets or calcula	tions equivalent to Appendi	x B of the E&S Manual have been co	mpleted and are attached.				
		he sequence of BMP installation an g and after earth disturbance activi					
Plan sheet 5							
9. Supporting E&S calculation:	s have been completed and	are available upon request (PAG-01	only).				
10. 🛛 Supporting E&S calculation:	s are attached to the NOI/ap	oplication.					
11. 🗌 Plan drawings consist of sta	ndard Figures/Construction	Details in E&S Manual (PAG-01 only	/).				
12. 🛛 Plan drawings have been de	2. 🛛 Plan drawings have been developed for the project and are attached to the NOI/application.						
13. 🛛 BMPs will be inspected on a	B. 🛛 BMPs will be inspected on a weekly basis and after measurable storm events (i.e., at least 0.25 inch).						
Drawing No. below: 1) vegeta	 Identify the following information relating to temporary stabilization measures on an E&S Plan Drawing and identify the Drawing No. below: 1) vegetative species, 2) % pure live seed, 3) seed application rate, 4) fertilizer type, 5) fertilizer application rate, 6) mulch type, 7) mulching rate, and 8) liming rate. 						
E&S Plan Drawing No(s).: 35							
Drawing No. below: 1) vegeta	tive species, 2) % pure liv 7) mulching rate, 8) liming ra	abilization measures on an E&S Plate re seed, 3) seed application rate, 4 ate, 9) anchor material, 10) anchoring eeding season dates.) fertilizer type, 5) fertilizer				
E&S Plan Drawing No(s).: 35							
16. Describe the procedures that we project site will be conducted pr		t recycling or disposal of materials	associated with or from the				
See plan sheet 4							
pollution during earth disturband	7. Identify the presence of any naturally occurring geologic formations or soil conditions that may have the potential to cause pollution during earth disturbance activities. If such formations or conditions exist, identify BMPs that will be implemented to avoid or minimize potential pollution.						
See plan sheet 5							
		to surface waters from the earth d void, minimize, or mitigate potential t					
oee high sheet a							

19. 🛛 The E&S Plan has been planned, designed, and will be implemented to be consistent with the PCSM Plan.									
	 If applicable, identify existing and proposed riparian forest buffers on E&S and PCSM Plan Drawings and identify the Drawing No(s) below (select N/A if not applicable). 								
E&S Plan Dra	awing No(s):	N/A							
PCSM Plan	Drawing No(s):								
	E&S PLAN	DEVELOPER							
I am trained a	nd experienced in E&S control methods.	🛛 I am a licen	sed professional.						
Name:	Tyler E. Hill	Title:	Project Manager						
Company:	ELA Group, Inc.	Phone No.:	717-726-7271						
Address:	743 S Broad Street	Email:	tehill@elagroup.com						
City, State, ZIP:	Lititz, PA 17543	License No.:	PE086960						
License Type:	Professional Engineer	Exp. Date:	09/30/2023						
Jerta 9/19/2023									
E&S	Plan Developer Signature	D	late						

APPENDIX A EROSION & SEDIMENT CONTROL NARRATIVE

Corporate Office 743 South Broad Street Lititz, PA 17543 (717) 626-7271 Central PA Office 2013 Sandy Drive, Suite 103 State College, PA 16803 (814) 861-6328



EROSION & SEDIMENT CONTROL NARRATIVE

Site Description

The project site is located near the center of the Westtown School campus, just south of Oak Lane. The existing site is largely comprised of existing grass athletic fields which are bordered to the north by a partially forested area and the school's academic centers; to the east by a baseball field and residential area; the south by agricultural fields (i.e. row crops) and a partially forested riparian area; and to the west by the school's working farm and agricultural area.

During the past 50 years, the site's primary use has been agricultural (i.e. row crops). The site is currently utilized primarily for athletic fields, with row crops along the southeastern portion of the project site. The site has been utilized as such for at least the past five years, with no significant improvements being constructed during that time.

The Westtown School is proposing to improve upon the existing athletic facilities on campus by constructing two new synthetic turf multipurpose fields, along with reconfiguring the remaining area to maximize field space. Additional components of the project involve the construction of a field house, parking lot, improved pedestrian access and a comprehensive stormwater management system.

102.4(b)(5)(vi) Narrative description of perimeter and onsite BMPs

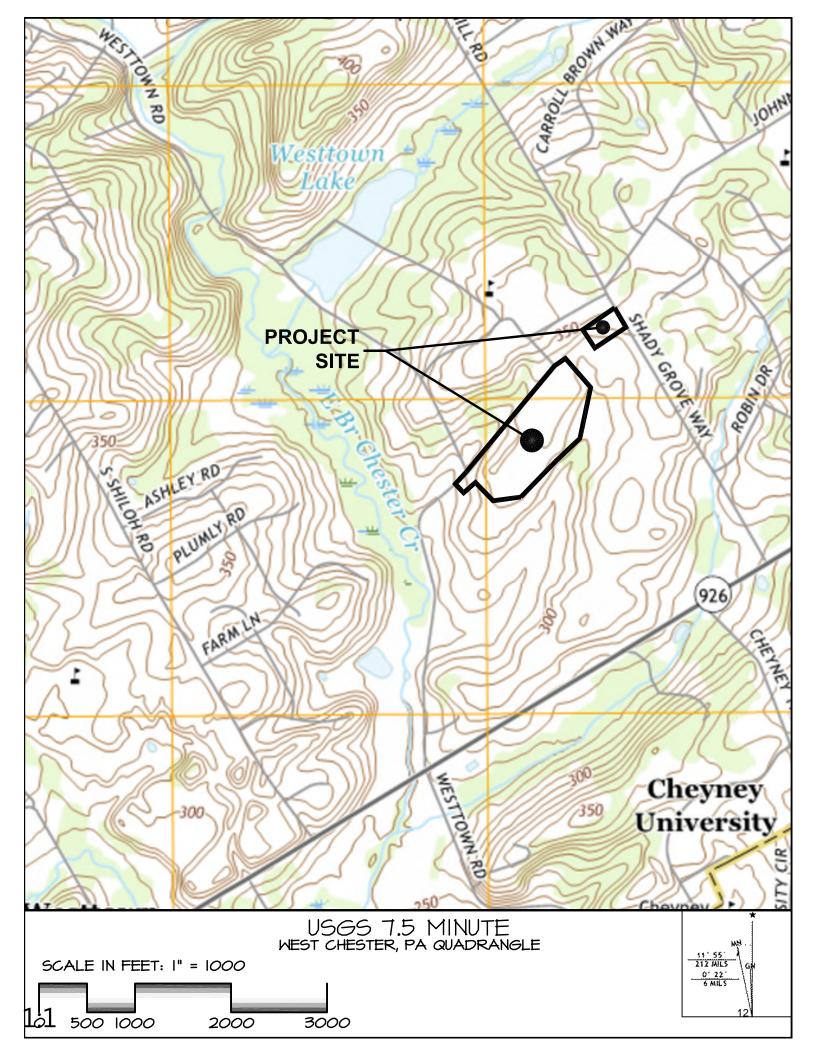
In order to prevent and control sediment pollution resulting from the proposed earthwork operations several onsite BMPs are being proposed. These BMPs include multiple rock construction entrances, compost filter sock, silt fence, erosion control matting/slope stabilization, a sediment trap, and a sediment basin.

Based on the topography of the site, along with the intentional sequencing of earthmoving activities, the proposed BMPs are adequate to protect the receiving watercourse and offsite locations from sediment or other pollution produced during construction.

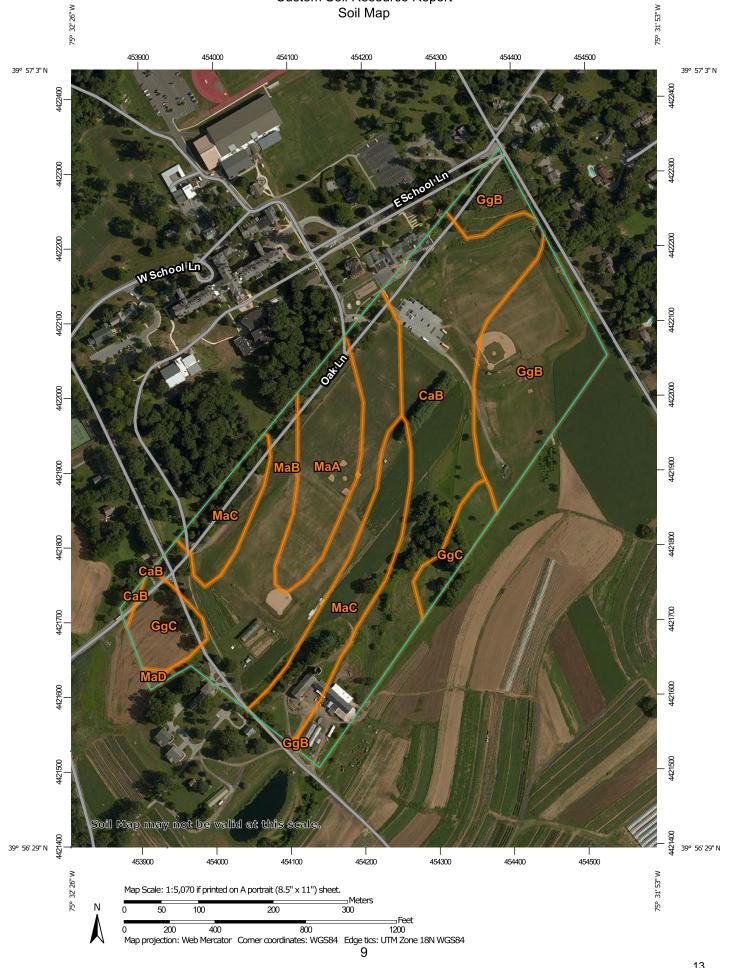
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APPENDIX B REFERENCE MATERIAL AND SUPPORTING DOCUMENTS

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Custom Soil Resource Report Soil Map



Map Unit Symbol	Map Unit Name	Acres in AOI	Percent of AOI
СаВ	Califon loam, 3 to 8 percent slopes	16.5	28.4%
GgB	Glenelg silt loam, 3 to 8 percent slopes	10.4	17.9%
GgC	Glenelg silt loam, 8 to 15 percent slopes	4.0	6.9%
MaA	Manor loam, 0 to 3 percent slopes	5.5	9.4%
МаВ	Manor loam, 3 to 8 percent slopes	12.9	22.2%
MaC	Manor loam, 8 to 15 percent slopes	8.7	15.0%
MaD	Manor loam, 15 to 25 percent slopes	0.1	0.2%
Totals for Area of Interest		58.1	100.0%

Map Unit Legend

Map Unit Descriptions

The map units delineated on the detailed soil maps in a soil survey represent the soils or miscellaneous areas in the survey area. The map unit descriptions, along with the maps, can be used to determine the composition and properties of a unit.

A map unit delineation on a soil map represents an area dominated by one or more major kinds of soil or miscellaneous areas. A map unit is identified and named according to the taxonomic classification of the dominant soils. Within a taxonomic class there are precisely defined limits for the properties of the soils. On the landscape, however, the soils are natural phenomena, and they have the characteristic variability of all natural phenomena. Thus, the range of some observed properties may extend beyond the limits defined for a taxonomic class. Areas of soils of a single taxonomic class rarely, if ever, can be mapped without including areas of other taxonomic classes. Consequently, every map unit is made up of the soils or miscellaneous areas for which it is named and some minor components that belong to taxonomic classes other than those of the major soils.

Most minor soils have properties similar to those of the dominant soil or soils in the map unit, and thus they do not affect use and management. These are called noncontrasting, or similar, components. They may or may not be mentioned in a particular map unit description. Other minor components, however, have properties and behavioral characteristics divergent enough to affect use or to require different management. These are called contrasting, or dissimilar, components. They generally are in small areas and could not be mapped separately because of the scale used. Some small areas of strongly contrasting soils or miscellaneous areas are identified by a special symbol on the maps. If included in the database for a given area, the contrasting minor components are identified in the map unit

Job Number: 1091-001 Date: 10/25/2018

SOILS INFORMATION FACT SHEET

			•				
TION	TOPSOIL	Fair	Fair	Fair	Fair	Fair	Poor
SOIL CONDITIONS FOR CONSTRUCTION	ROADFILL	Fair	Fair	Fair	Poor	Poor	Poor
IDITIONS FO	BUILDING SITE	Very Limited	Somewhat Limited	Very Limited	Somewhat Limited	Somewhat Limited	Very Limited
SOIL CON	SURFACE WATER MANAGEMENT	Somewhat Limited	Very Limited	Very Limited	Not Limited	Very Limited	Very Limited
	FROST ACTION	High	Moderate	Moderate	Moderate	Moderate	Moderate
SUITABILITY	WINTER GRADING	Limited	Somewhat Limited	Somewhat Limited	Somewhat Limited	Somewhat Limited	Somewhat Limited
SUITA	DEPTH TO BEDROCK (IN)	72 to 99	80+	80+	72 to 99	72 to 99	59 to 100
SUITAB	DEPTH OF WATER TABLE (IN)	6 to 36	+08	80+	+08	+08	+08
	ERODIBILITY (K)	0.32	0.37	0.37	0.28	0.28	0.28
	HYDRIC (INCLUSIONS)						
	HYDRO. SOIL GROUP	D	В	В	В	В	В
SOIL	SLOPE, %	3 to 8	3 to 8	8 to 15	0 to 3	3 to 8	8 to 15
	TEXTURE	Loam	Silt Loam	Silt Loam	Loam	Loam	Loam
	SYMBOL NAME	CaB Califon	GgB Glenelg	GgC Glenelg	MaA Manor	MaB Manor	MaC Manor

Job Number: 1091-001 Date: 10/25/2018

				ONS & RESOLUTIONS	Date: 10/25/20
SOIL	LIN	IITATIONS	CHARACTERISTICS	RESOLUTIONS	COMMENTS
	-	1		It is imperative that appropriate precautions be taken to	COMMENTS
CaB	Cutbanks Cave	Excavations	The walls of excavations tend	safeguard workers during all trenching and excavation	All applicable OSHA standards and regulations
GgB			to cave in or slough	operations.	must be implemented at all times.
GgC					
MaA					
MaB					
MaC					
CaB (C/S)	Corrosive to	Foundation and other	Weakening or dissolution of	Suitable precautions should be taken to protect all	Refer to the Geotechnical Report
GgB (C)	Concrete/ Steel	infrastructural materials that	concrete or uncoated steel	underground pipes, conduits, and storage tanks from	
GgC (C)		may contact the soil	caused by soil-induced	concrete and steel corrosion. If potential corrosive	
MaA (C)			electrochemical or chemical action.	properties are encountered during construction, impacted utilities in that area shall be backfilled with processed	
MaB (C)			action.	aggregate to reduce the potential of corrosion from soil	
MaC (C)					
	r - dhan	• 1997 -	Easily Erodible	Excavation should occur during low-rainfall periods when	See Erosion and Sediment Control Plan
GgB	Erodibility	Grassed Waterways		possible	See crosion and Sediment Control Plan
GgC		Terraces	Rill and/or Gully Erosion	Minimize duration of earth disturbance	
MaA		Slopes			
MaB		Stabilization		Immediately stabilize with erosion control matting, mulch, or sod.	
MaC		Landscaping			
a -			11 ab tabla	Avoid concentrating runoff in disturbed areas	Contest Costashairal Frankrish II
CaB	Depth to Saturated	Buildings w/ basements	High table	Suitable precautions should be taken if water is	Contact Geotechnical Engineer if shallow groundwater is encountered
	Zone/ Seasonal High	Excavations	Wetness	Contractor is to utilize pumping techniques and other	groundwater is encountered
	Water Table	Stormwater Facilities	Soil mottling	methods as recommended by a Geotechnical Engineer.	
CaB	Frost Action	Winter Grading	Frost heaving or upward swelling of soil during freezing	Do not grade, fill, or backfill during periods of freezing temperatures.	
GgB			conditons.		
GgC			conditions.	Proper precautions should be taken to prevent damage,	
MaA				especially to roadways.	
MaB					
MaC					
GgB	Hydric/	unless authorized by DEP	Wetlands	Delineate and Protect Wetlands	See wetland delineation repot
GgC	Hydric Inclusions	and/or ACOE if wetlands	Wetness	Obtain all permits/authorizations	
Cap	Law Chronoth /	present Steep Slopes	Low strength soils are prone	Utilize pumping techniques where appropriate Precautions should be taken to prevent slope failures due to	See gestechnical angineering report or concul
CaB GgB	Low Strength/ Landslide Prone	Structural Fill	failure on steep slopes.	improper construction practices such as over-steepening	the geotechnical professional on record
GgC	Editusitae Frone	Structurarrin		and overloading of slopes, removal of lateral support, and	8 F
MaA				failure to prevent saturation of slopes.	
MaB				Setbacks should comply with the standards contained in	
MaC				Chapter 16 unless it can be shown that proposed cuts and	
				fills do not pose a hazard to public safety or to surface	
				Road fill/other structural fill material will likely need to be	
				imported in areas where soils have low strength.	
CaB	Slow Percolation	Stormwater Infiltration	Wetness	Soil testing should be performed if infiltration BMPs or on-	See geotechnical engineering report or consul
GgB		On-lot Sewage Facilities	Soil mottling	lot sewage facilities are proposed.	the geotechnical professional on record
GgC			Shallow groundwater	Ammend soils with compost and/or sand.	See Appendix A of the PA Stormwater BMP
MaA					Manual
MaB					
MaC	Disian		Formation of sub-surface	Avoid concentrating supoff	See alars
GgB GgC	Piping		Formation of subsurface tunnels or pipelike cavities by	Avoid concentrating runoff. Avoid infiltrating in areas with excessive infiltration rates.	See plans See geotechnical engineering report or consul
MaA			water moving through the soil	Install trench plugs, anti-seep collars, key trenches, etc.	the geotechnical professional on record
MaB					g
MaC					
GgB	Poor Source of Topsoil	Vegetative Growth/	Low Fertility	Soil Testsing and appropriate supplementation.	See plan notes
GgC		Stabilization	Droughty or Wet	Soil amendment/restoration practices	
MaA			High Acidity		
MaB					
MaC					
CaB	Wetness	Site work/grading	Slow percolation	Concrete stabilization	See geotechnical report or consult geotechnic
GgB		Fill operations	Soil Mottling	Undercut and replace with suitable material	engineer on record
GgC	1		Shallow groundwater	Provide positive drainage	

APPENDIX C PERIMETER CONTROLS

Corporate Office 743 South Broad Street Lititz, PA 17543 (717) 626-7271 Central PA Office 2013 Sandy Drive, Suite 103 State College, PA 16803 (814) 861-6328

STANDARD E&S WORKSHEET #1 Compost Filter Socks

PROJECT: <u>The Westtown School - Oak Lane Project</u>	JOB#	<u>1091-001</u>
LOCATION: <u>Westtown Township</u>	DATE:	<u>1/11/2023</u>
COUNTY: <u>Chester</u>	REVISED:	<u>9/18/2023</u>
2" X 2" WOODEN S COMPOST FILT UNDISTURBED AREA		

т

BARRIER NO.	SOCK SIZE (IN.)	LOCATION	SLOPE %	SLOPE LENGTH ABOVE BARRIER (FT)
12-1	12	Below Sediment Trap 1	33	27
12-2	12	Below Sediment Trap 1	33	22
12-3	12	Below Sediment Trap 1	33	33
12-4	12	NW of Oak Lane	10	12
18-1	18	NE of RCE #1	5,23	159,64
18-2	18	NE of CFS 18-1	9, 21	53, 71
18-3	18	NE of CFS 18-2	7,18,1.3	44,74,43
18-4	18	NE of CFS 18-3	7,12,25,1.3	42,58,24,43
18-5	18	NE of CFS 18-4	9	193
18-6	18	NE of CFS 18-5	3, 33	65, 45
18-7	18	NE of CF 18-6	33	31
18-8	18	Around Topsoil Stockpile	33	50
24-1	24	Below Sediment Basin 4	5,15,1.5	122,52,375
24-2	24	Below Sediment Basin 4	5,10,1.5	145,77,375
24-3	24	Below Sediment Basin 4	7,1.2	253,375
24-4	24	SW of CFS 24-3	13,8,1.5	55,165,407
24-5	24	SW of CFS 24-4	12,1.5	102,380
24-6	24	SW of CFS 24-5	7,1.5	165,335

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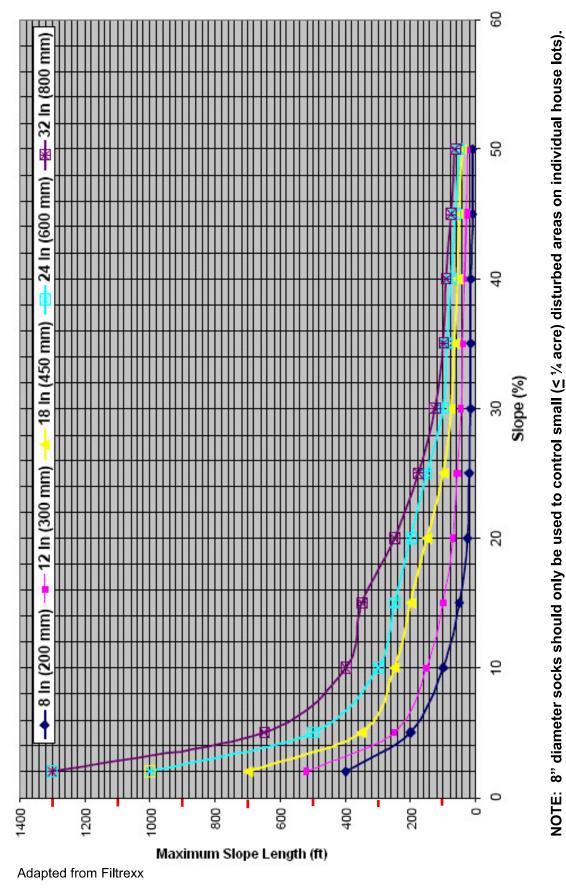


FIGURE 4.2 MAXIMUM PERMISSIBLE SLOPE LENGTH ABOVE COMPOST FILTER SOCKS

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APPEND D SEDIMENT TRAP DESIGN

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STANDARD E&S WORKSHEET #14

Sediment Basin/Sediment Trap Storage Data

PROJECT: LOCATION: COUNTY: CHECKED BY:	<u>Chester</u>		<u>Oak Lan</u>	<u>e Project</u>		RE	JOB #: DATE: VISED:	1091-001 1/11/2023 9/19/2023
ONEORED DT.		SE	DIMENT .	TRAP #1				
WATER SURFACE	AREA	AVERAGE			STORAGE VOLUN	ΛE		
ELEVATION (FEET)	(SQ.FT.)	AREA (SQ.FT.)	ELEV. (FEET)	INCR.	Σ (CU.FT.)	(AC.FT.)		
288.5	10675				0	0		
000	44400	11087	0.50	5,543	5 5 40	0.4070		
289	11498	11927	0.50	5,964	5,543	0.1273		
289.5	12356	11327	0.00	5,504	11,507	0.2642		
		12784	0.50	6,392				
290	13211				17,899	0.4109		
		14118	1.00	14,118				
291	15025				32,017	0.735		
		15977	1.00	15,977				
292	16928				47,993	1.1018		
		18020	1.00	18,020				
293	19112				66,013	1.5154		

WESTTOWN-ESC (2022).xlsx - WS-14(ST-1)

EROSION AND SEDIMENT POLLUTION CONTROL

STANDARD WORK SHEET # 17 SEDIMENT BASIN DISCHARGE CAPACITY

PROJECT: <u>The Westtown School - Oak Lane Project</u> LOCATION: <u>Westtown Township</u>

COUNTY: Chester

JOB #	1091-001
DATE:	1/12/2023
REVISED.	10/23/2023

FLOW

					SEDIMEN	TTRAP #1					
		PRINCIP	AL SPILLW	AY DISC	HARGE		CITY				
		Flow Into To TEMPORARY			ow Into Top MANENT R		BAR PIPE I		PRINCIPAL	EMERGENCY	
WATER		ORIFICE	WEIR		ORIFICE	WEIR			SPILLWAY	SPILLWAY WEIR FLOW	TOTAL FLO
SURFACE	HEAD	FLOW	FLOW	HEAD	FLOW	FLOW	HEAD ²	Q	CAPACITY ³	Q (cfs) ****	Q (cfs) ****
ELEVATION	ft.	Q (cfs) ¹	Q (cfs)	ft.	Q (cfs) ¹	Q (cfs) ¹	ft.	(cfs)	(cfs)	Q (CIS)	
290.75							5.75	21.8	. ,		
290.85	0.10	0.3	0.2				5.85	22.0	0.2		0.15
290.95	0.20	0.4	0.4				5.95	22.1	0.4		0.42
291.05	0.30	0.5	0.8	0.05	8.12	0.39	6.05	22.3	0.9		0.91
291.15	0.40	0.6	1.2	0.15	14.06	2.03	6.15	22.5	2.6		2.63
291.25	0.50	0.7	1.7	0.25	18.15	4.37	6.25	22.7	5.0		5.04
291.35	0.60	0.7	2.3	0.35	21.48	7.24	6.35	22.9	8.0	2.66	10.63
291.45	0.70	0.8	2.9	0.45	24.35	10.55	6.45	23.1	11.3	7.51	18.85
291.55	0.80	0.8	3.5	0.55	26.92	14.26	6.55	23.2	15.1	13.8	28.91
291.65	0.90	0.9	4.2	0.65	29.27	18.32	6.65	23.4	19.2	21.25	40.47
291.75	1.00	0.9	4.9	0.75	31.44	22.71	6.75	23.6	23.7	29.7	53.35
291.85	1.10	1.0	5.6	0.85	33.47	27.40	6.85	23.8	24.7	39.04	63.78
291.95	1.20	1.0	6.4	0.95	35.39	32.38	6.95	23.9	25.0	49.2	74.15
292.05	1.30	1.1	7.2	1.05	37.20	37.62	7.05	24.1	25.2	60.11	85.28
292.15	1.40	1.1	8.1	1.15	38.93	43.12	7.15	24.3	25.4	71.72	97.11
292.25	1.50	1.2	8.9	1.25	40.59	48.87	7.25	24.4	25.6	84	109.59
292.35	1.60	1.2	9.9	1.35	42.18	54.84	7.35	24.6	25.8	96.91	122.70
292.45	1.70	1.2	10.8	1.45	43.72	61.05	7.45	24.8	26.0	110.42	136.42
292.55	1.80	1.3	11.8	1.55	45.20	67.47	7.55	24.9	26.2	124.51	150.71
292.65	1.90	1.3	12.7	1.65	46.63	74.11	7.65	25.1	26.4	139.15	165.55
292.75	2.00	1.3	13.8	1.75	48.03	80.95	7.75	25.3	26.6	154.32	180.91
292.85	2.10	1.4	14.8	1.85	49.38	87.98	7.85	25.4	26.8	170	196.80
292.95	2.20	1.4	15.9	1.95	50.70	95.21	7.95	25.6	27.0	186.19	213.18
293.05	2.30	1.4	17.0	2.05	51.98	102.63	8.05	25.8	27.2	202.86	230.04
293.15	2.40	1.5	18.1	2.15	53.23	110.23	8.15	25.9	27.4	219.99	247.36
293.25	2.50	1.5	19.2	2.25	54.46	118.01	8.25	26.1	27.6	237.59	265.14
293.35	2.60	1.5	20.4	2.35	55.65	125.96	8.35	26.2	27.7	255.63	283.37
293.45	2.70	1.6	21.6	2.45	56.83	134.09	8.45	26.4	27.9	274.1	302.03

* Flow into top of riser only (Flow through perforations not included)

** Water surface elevation minus elevation at centerline of pipe outlet

*** Least of orifice, weir or pipe flow

PARAMETERS		
ORIFICE FLOW Q=CA(2gH)^ ^{1/2}	WEIR FLOW Q=CLH^3/2	2
TOP OF RISER: 290.75	RISER DIAMETER (IN)=	6
CO1= <mark>0.6</mark>	C=	3.1
EMERGENCY SPILLWAY		
Q=CLH ^{A3/2}	BROAD-CRESTED WEIR ⁶ : C= 2.8	
ELEVATION: 291.25	WIDTH ⁵ : <mark>30</mark> SIDE SLOPES:	4.5
TOP OF BERM: 293.00	STEP INCREMENT: 0.1	
PIPE FLOW		
Q=a[(2gH)/(1+Km+KpL)]^1/2	PIPE SIZE (IN) : <mark>18</mark> MANNING'S N= <mark>(</mark>	0.012
Kp=(5087*N^2)/D^4/3	Kp= (0.0155
INVERT OUT= 284.25	SLOPE: 0.0053 ft/ft Km= 1	
PIPE LENGTH (Lb) = 28.5		

PERMANENT RISER PARAMETERS

ORIFICE FLOW	Q=CA(2g	μ)^ ^{1/2}	WEIR FLOW Q=CLH ^{A3}	2
	TOP OF OSC:	291.00	RISER LENGTH (FT)=	3.77
			RISER WIDTH	2
	CO1=	0.6	C=	3.33

1. Flow into top of riser only (Flow through perforations not included)

2. Water surface elevation minus elevation at centerline of pipe outlet.

3. Least of orifice, weir or pipe flow (Peak flow from 10 yr/24 hr storm Min.)

4. 24" below top of embankment (12" if 100-yr storm routed through basin)

5. 8 Ft minimum

Use Tables 7.5 through 7.8 or equation for broad-crested weir [Q=CLH^{1.5}, where C ≤ 2.8 (MAX)]; for Riprap larger than R-3 or flows less than 1.5' deep adjust C downward]

7. Principal Spillway Capacity + Emergency Spillway Capacity

EROSION AND SEDIMENT POLLUTION CONTROL

STANDARD E&S WORKSHEET #19 Sediment Trap Design Data

PROJECT: The Westtown School - Oak Lane Project	<u>JOB #</u>	1091-001
LOCATION: Westtown Township	DATE:	1/12/23
COUNTY: <u>Chester</u>	REVISED:	10/23/2023
CHECKED BY:		

TRAP NUMBER		ST #1		
DRAINAGE AREA (5 ACRES MAX)	(AC)	4.98		
REQUIRED CAPACITY (2000 CF/AC)	(CF)	9,960		
CAPACITY PROVIDED AT ELEVATION h	(CF)	28,488		
SOIL TYPES IN DRAINAGE AREA		Silt Loam		
REQUIRED SURFACE AREA (5,300 X AC) ¹	(SF)	-	-	
*AVERAGE BOTTOM LENGTH	(FT)	165		
*AVERAGE BOTTOM WIDTH	(FT)	43		
*AVERAGE TRAP LENGTH AT ELEVATION h	(FT)	165		
*AVERAGE TRAP WIDTH AT ELEVATION h	(FT)	49		
SURFACE AREA AT ELEVATION h	(SF)	14571		
BOTTOM ELEVATION	(FT)	288.50		
CLEAN-OUT ELEVATION (@700 CF/AC) ²	(FT)	289.50		
TOP OF EMBANKMENT ELEVATION ³	(FT)	293.00		
EMBANKMENT HEIGHT	(FT)	4.50		
CREST OF SPILLWAY ELEVATION, h ⁴	(FT)	290.75		
FLOW LENGTH AT ELEVATION h	(FT)	125		
FLOW LENGTH/WIDTH RATIO AT ELEV. h ⁵	(2:1 MIN)	2.6 :1		

1. If sandy clays, silty clays, silty clay loams, clay loams, or clays predominate soil types.

2. Minimum 12" above bottom of trap

3. Minimum 12" above elevation at which 1.5 cfs/acre discharge capacity is provided.

4. Minimum 24" above bottom of trap.

5. 4:1 Flow Length: Width ratio required for HQ and EV watersheds.

	6" Perf.			
	Riser +			
(IN)	Permanent			
	2'x4' Conc.			
	OCS			
(IN)	18			
(CFS)	8.4			
(FT)	284.25			
(FT)	291.35			
_	(IN) (CFS) (FT)	Riser + Rermanent (IN) Permanent 2'x4' Conc. OCS (IN) 18 (CFS) 8.4 (FT) 284.25	Riser + Permanent 2'x4' Conc. OCS Riser + Permanent 2'x4' Conc. (IN) 18 (CFS) 8.4 (FT) 284.25	(IN) Riser + Permanent 2'x4' Conc. OCS Permanent 2'x4' Conc. OCS (IN) 18 (CFS) 8.4 (FT) 284.25

APPENDIX E SEDIMENT BASIN DESIGN

Corporate Office 743 South Broad Street Lititz, PA 17543 (717) 626-7271 Central PA Office 2013 Sandy Drive, Suite 103 State College, PA 16803 (814) 861-6328

STANDARD E&S WORKSHEET # 12

Sediment Basin Capacity Requirements

PROJECT: LOCATION: COUNTY: CH <mark>ECKED BY:</mark>	<u>The Westtown School - Oak Lane Project</u> <u>Westtown Township</u> <u>Chester</u>			JOB # DATE: REVISED:	1091-001 1/11/2023 9/19/2023
BASIN NUMBER				#4	
PERMANENT OR	TEMPORARY BASIN?	(P or	r T)	Р	
SPECIAL PROTEC	CTION WATERSHED?	(YES OR N	10)	NO	
KARST SOILS?		(YES OR N	1 0)	NO	
(A) MAXIMUM TO	TAL DRAINAGE AREA (AC)	(A	AC)	9.74	
IS DRAINAGE AR	EA (A) MORE THAN 10% LARGER THAN THE				
PRECONSTRUC	CTION CONDITION?	(YES OR N	1 0)	YES	
(A1) DISTURBED	ACRES IN DRAINAGE AREA	(A	AC)	7.24	
(I) INITIAL REQUI	RED SETTLING VOLUME (5000 X A)	((CF)	48,700	
(T) REDUCTION F	OR TOP DEWATERING (-700 X A)	((CF)	6,818	
(P) REDUCTION F	OR PERMANENT POOL (-700 X A)	((CF)		
(L) REDUCTION F	OR 4:1 FLOW LENGTH:WIDTH (-350 X A)	((CF)		
(D) REDUCTION F	FOR 4 TO 7 DAY DEWATERING (-350 X A)	((CF)		
(Sv) REQUIRED [DEWATERING ZONE [I - (T+P+L+D)] ¹	((CF)	41,882	
(Sd) REQUIRED S	SEDIMENT STORAGE VOLUME (1000 X A ₁)	((CF)	7,240	
(St) TOTAL REQU	JIRED STORAGE VOLUME (Sv+Sd)	((CF)	49,122	
SEDIMENT STOR	AGE VOLUME PROVIDED (@ ELEV 2)	((CF)	22,536	
TOTAL STORAGE	VOLUME PROVIDED (@ ELEV 3) ²	((CF)	68,686	
DEWATERING TH	ME FOR DEWATERING ZONE	(DA)	YS)	3.06	
REQUIRED DISCH	HARGE CAPACITY (2 X A)	(CF	S) ³	19.48	
PRINCIPAL SPILL	WAY TYPE (PERFORATED RISER, SKIMMER, e	tc.)		Type 'M' w/ Extension	
PEAK FLOW FRO	M 10YR/24HR STORM FOR DRAINAGE AREA (A	(CF	FS)	14.9	
PRINCIPAL SPILL	WAY CAPACITY (@ ELEV 5)	(CF	S) ⁴	0.52 (see routing)	
EMERGENCY SPI	LLWAY CAPACITY (@ ELEV 5)	(CF	S) ⁴	n/a	
TOTAL BASIN DIS	CHARGE CAPACITY (@ ELEV 5)	(CF	FS)	0.52 (see routing)	
EMERGENCY SPI	LLWAY PROTECTIVE LINING ⁵			Flexamat	
OUTLET TO A SU	RFACE WATER?	(YES OR N	O) ⁶	NO	
PEAK FLOW FRO	M A 100 YR/24 HR STORM FOR DRAINAGE ARE	EA (A) (CF	FS)	36.71	

1 The minimum dewatering zone capacity for sediment basins is (3,600 X A). No reduction is permitted in Special Protection (HQ and EV) Watersheds.

2 Total Storage Volume provided at riser crest.

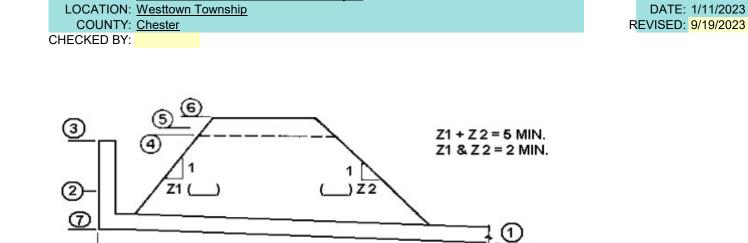
3 Or provide calculations to show peak flow from 25 yr./24 hr. storm for area (A) is routed through the basin.

4 Provide supporting computations.

- 5 If grass lining is proposed, spillway should be constructed in original ground unless a suitable TRM lining is used. Wherever a TRM is used, riprap should be placed at the bottom of the embankment to prevent scour.
- 6 If no, and basin is permanent or drainage area is more than 10% larger than pre-construction, provide supporting calculations to show accelerated erosion will not result from the proposed discharge. For discharges increasing volume or rate of flow onto a neighboring property prior to entering a surface water, an easement should be obtained prior to plan submittal.

PROJECT: The Westtown School - Oak Lane Project

Lb



STANDARD E&S WORKSHEET #13 Sediment Basin Dimensions and Elevations

BASIN NUMBER		#4	
1. DISCHARGE PIPE ELEVATION	(FT)	307.25	
2. ELEVATION AT TOP OF SEDIMENT STORAGE ZONE (@Sd)	(FT)	311.00	
(MIN. 1.0' ABOVE ELEVATION 7)		511.00	
3. ELEVATION AT TOP OF DEWATERING ZONE (St)	(FT)	312.50	
(CREST OF PRINCIPAL SPILLWAY)		312.50	
4. EMERGENCY SPILLWAY CREST ELEVATION	(FT)	313.00	
(MIN. 0.5' ABOVE ELEVATION 3)		313.00	
5. 2 CFS/ACRE OR <u>25-YR/24-HR</u> FLOW ELEVATION	(FT)	312.55	
6. TOP OF EMBANKMENT ELEVATION	(FT)		
(MIN. 24" ABOVE ELEVATION 5		315.00	
OR 12" WITH ROUTED 100-YR/24-HR STORM)			
7. BASIN BOTTOM ELEVATION	(FT)	310.00	
AVERAGE BOTTOM WIDTH	(FT)	40	
AVERAGE BOTTOM LENGTH	(FT)	400	
(SAmin) REQUIRED SURFACE AREA AT ELEVATION 2	(SF)	1,858	
SURFACE AREA PROVIDED AT ELEVATION 2	(SF)	25,262	
AVERAGE BASIN WIDTH (W) AT ELEVATION 3	(FT)	55	
FLOW LENGTH (L) AT ELEVATION 3	(FT)	516	
FLOW LENGTH: WIDTH RATIO AT ELEVATION 3	(L:W)	9.4 :1	
SILT CURTAIN OR FOREBAY? (IF YES INDICATE WHICH)		NO	
EMBANKMENT TOP WIDTH	(FT, 8' MIN)	8	
EMBANKMENT SOIL TYPE(S)		SILT/ LOAM	
KEY TRENCH DEPTH	(FT, 2' MIN)	2'	
KEY TRENCH WIDTH	(FT, 4' MIN)	4'	
RISER DIAMETER/TYPE	(15" MIN)	2'X4' CONC	
BARREL DIAMETER/TYPE	(12" MIN)	24" SLCPP	
Lb (BARREL LENGTH)	(FT)	37'	
EMERGENCY SPILLWAY WIDTH	(FT)	50	
EMERGENCY SPILLWAY SIDE SLOPES	(H:V)	6 :1	
EMERGENCY SPILLWAY DEPTH	(FT)	1.5'	

JOB # 1091-001

STANDARD E&S WORKSHEET #14

Sediment Basin/Sediment Trap Storage Data

PROJECT: LOCATION: COUNTY: CHECKED BY:	Westtown T		<u>Oak Lan</u>	<u>e Project</u>		RE	JOB #: DATE: EVISED:	1091-001 1/11/2023 9/19/2023			
SEDIMENT BASIN #4											
WATER SURFACE	AREA	AVERAGE			STORAGE VOLUM	1E					
ELEVATION (FEET)	(SQ.FT.)	AREA (SQ.FT.)	ELEV. (FEET)	INCR.	Σ (CU.FT.)	(AC.FT.)					
310	19809				0	0					
311	25262	22536	1.00	22,536	22,536	0.5173					
312	31631	28447	1.00	28,447	50,982	1.1704					
		35407	1.00	35,407							
313	39183	42922	1.00	42,922	86,389	1.9832					
314	46661	42922	1.00	42,922	129,311	2.9686					
		48071	0.50	24,036							
314.5	49481				153,347	3.5204					
		50870	0.50	25,435							
315	52258				178,781	4.1043					

WESTTOWN-ESC (2022).xlsx - WS-14(SB-4)

STANDARD WORK SHEET # 17 SEDIMENT BASIN DISCHARGE CAPACITY

PROJECT: <u>The Westtown School - Oak Lane Project</u> LOCATION: <u>Westtown Township</u> COUNTY: <u>Chester</u>

JOB # 1091-001 DATE: 10/29/2022 REVISED: 9/19/2023

SEDIMENT BASIN 4 PRINCIPAL SPILLWAY DISCHARGE CAPACITY

		Flow Into To				Flow Into Top of PERMANENT RISER		REL	PRINCIPAL		
		TEMPORARY		PERM			PIPE	FLOW		SPILLWAY	TOTAL FLOW
WATER		ORIFICE	WEIR		ORIFICE	WEIR			SPILLWAY	WEIR FLOW	Q (cfs) ****
SURFACE	HEAD	FLOW	FLOW	HEAD	FLOW	FLOW	HEAD ²	Q	CAPACITY ³	Q (cfs) ****	
ELEVATION	ft.	Q (cfs) ¹	Q (cfs)	ft.	Q (cfs) ¹	Q (cfs) ¹	ft.	(cfs)	(cfs)	G (010)	
312.50							4.25	33.6			
312.60	0.10			0.10	11.48	1.11	4.35	34.0	1.1		1.11
312.70	0.20			0.20	16.24	3.13	4.45	34.4	3.1		3.13
312.80	0.30			0.30	19.89	5.75	4.55	34.8	5.7		5.75
312.90	0.4			0.40	22.96	8.85	4.65	35.2	8.8		8.85
313.00	0.5			0.50	25.67	12.36	4.75	35.5	12.4		12.36
313.10	0.6			0.60	28.12	16.25	4.85	35.9	16.3	3.54	19.79
313.20	0.7			0.70	30.37	20.48	4.95	36.3	20.5	10.02	30.50
313.30	0.8			0.80	32.47	25.02	5.05	36.6	25.02	18.40	43.42
313.40	0.9			0.90	34.44	29.85	5.15	37.0	29.9	28.33	58.18
313.50	1.0			1.00	36.30	34.97	5.25	37.4	35.0	39.6	74.57
313.60	1.1			1.10	38.08	40.34	5.35	37.7	37.7	52.05	89.76
313.70	1.2			1.20	39.77	45.96	5.45	38.1	38.1	65.59	103.65
313.80	1.3			1.30	41.39	51.83	5.55	38.4	38.4	80.14	118.55
313.90	1.4			1.40	42.96	57.92	5.65	38.8	38.8	95.63	134.38
314.00	1.5			1.50	44.46	64.23	5.75	39.1	39.1	112	151.09
314.10	1.6			1.60	45.92	70.76	5.85	39.4	39.4	129.21	168.64
314.20	1.7			1.70	47.34	77.50	5.95	39.8	39.8	147.23	187.00
314.30	1.8			1.80	48.71	84.44	6.05	40.1	40.1	166.01	206.11
314.40	1.9			1.90	50.04	91.57	6.15	40.4	40.4	185.53	225.96
314.50	2.0			2.00	51.34	98.90	6.25	40.8	40.8	205.76	246.52
314.60	2.1			2.10	52.61	106.41	6.35	41.1	41.1	226.67	267.75
314.70	2.2			2.20	53.85	114.10	6.45	41.4	41.4	248.25	289.65
314.80	2.3			2.30	55.06	121.96	6.55	41.7	41.7	270.47	312.19
314.90	2.4			2.40	56.24	130.00	6.65	42.0	42.0	293.32	335.36
315.00	2.5			2.50	57.40	138.21	6.75	42.4	42.4	316.78	359.13
315.10	2.6			2.60	58.54	146.59	6.85	42.7	42.7	340.84	383.51
315.20	2.7			2.70	59.66	155.12	6.95	43.0	43.0	365.47	408.45

* Flow into top of riser only (Flow through perforations not included)

** Water surface elevation minus elevation at centerline of pipe outlet

*** Least of orifice, weir or pipe flow

PARAMETERS - TEMPORARY RISER		
ORIFICE FLOW Q=CA(2gH)^1/2		WEIR FLOW Q=CLH^3/2
TOP OF RISER:		RISER LENGTH (FT)=
CO1= 0.6		Č= 3.1
EMERGENCY SPILLWAY		
Q=CLH ^{^3/2}	BROAD-CRESTED WEIR ⁶ : C= 2.8	
ELEVATION: 313.00	WIDTH⁵: <mark>40</mark>	SIDE SLOPES: 6
TOP OF BERM: 315.00	STEP INCREMENT: 0.1	
PIPE FLOW		
Q=a[(2gH)/(1+Km+KpL)]^ ^{1/2}	PIPE SIZE (IN) : <mark>24</mark>	MANNING'S N= <mark>0.012</mark>
Kp=(5087*N^2)/D^4/3		Kp= 0.0106
INVERT OUT= 307.25	SLOPE: 0.0067	ft/ft Km= 1
PIPE LENGTH (Lb) = <mark>37</mark>		

1. Flow into top of riser only (Flow through perforations not included)

2. Water surface elevation minus elevation at centerline of pipe outlet.

3. Least of orifice, weir or pipe flow (Peak flow from 10 yr/24 hr storm Min.)

4. 24" below top of embankment (12" if 100-yr storm routed through basin)

5.8 Ft minimum

6. Use Tables 7.5 through 7.8 or equation for broad-crested weir [Q=CLH^{1.5}, where C <2.8 (MAX)]; for Riprap larger than R-3

or flows less than 1.5' deep adjust C downward]

7. Principal Spillway Capacity + Emergency Spillway Capacity

PARAMETERS - PERMANENT RISER

PARAMETERS -	PERMANENT RISER				
ORIFICE FLOW	Q=CA(2gH)^1/2	WEIR FLOW Q=CLH ^{A3/2}			
	TOP OF OSC: 312.50	RISER LENGTH (FT)=	3.77		
		RISER WIDTH	2		
	CO1= <mark>0.6</mark>	C=	3.33		

ATHLETIC FAGLITIES DESIGN & CONSULTING

ELA SPORT ATHLETIC FACILITIES DESIGN & CONSULTING

NRCS (SCS) TR-55- WATERSHED WEIGHTED CURVE NUMBER FOR

SEDIMENT TRAPS/BASINS

7 S. BROAD STRE	'ITZ, PA 17543	7) 626-72713
737 5	E	(717)

PROJECT: The Westtown School - Oak Lane Project LOCATION: Westtown Township COUNTY: Chester

	_					_	
			Tc	Min.	22	22	
			Composite		65	87	
			Total Area	(ac.)	9.74	9.74	
Bare Soil	D	2-6%	94		0.00	7.24	
956q2 n9qO b9d1u12bnU) Area)	D	2-6%	80		0.56	0.56	
Open Space (Disturbed Area)	D	< 2%	80		0.87	0.00	
Open Space (Undsturbed (6a)	В	%9<	61	Area (ac)	1.94	1.94	
Open Space (Disturbed Area)	В	2-6%	61		6.01	00.0	
Area) Parking, Other Impervious Undisturbed Area)	В	< 2%	98		0.00	00.0	
Parking, Other Impervious Disturbed Area)	В	< 2%	98		0.36	0.00	
IAND USE	BSH	Slope	"CN" Value				
				WATERSHED	Basin B-1	B-1 Bare Earth	

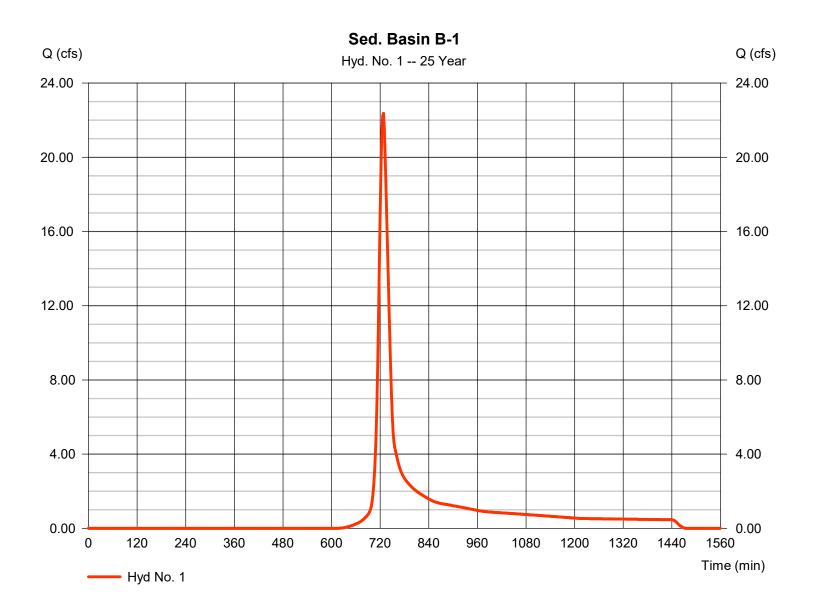
Hydrograph Report

Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2022

Hyd. No. 1

Sed. Basin B-1

Hydrograph type	= SCS Runoff	Peak discharge	= 22.37 cfs
Storm frequency	= 25 yrs	Time to peak	= 728 min
Time interval	= 2 min	Hyd. volume	= 79,682 cuft
Drainage area	= 9.740 ac	Curve number	= 65
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 22.00 min
Total precip.	= 5.81 in	Distribution	= Type II
Storm duration	= 24 hrs	Shape factor	= 484



Tuesday, 09 / 19 / 2023

Hydrograph Report

Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2022

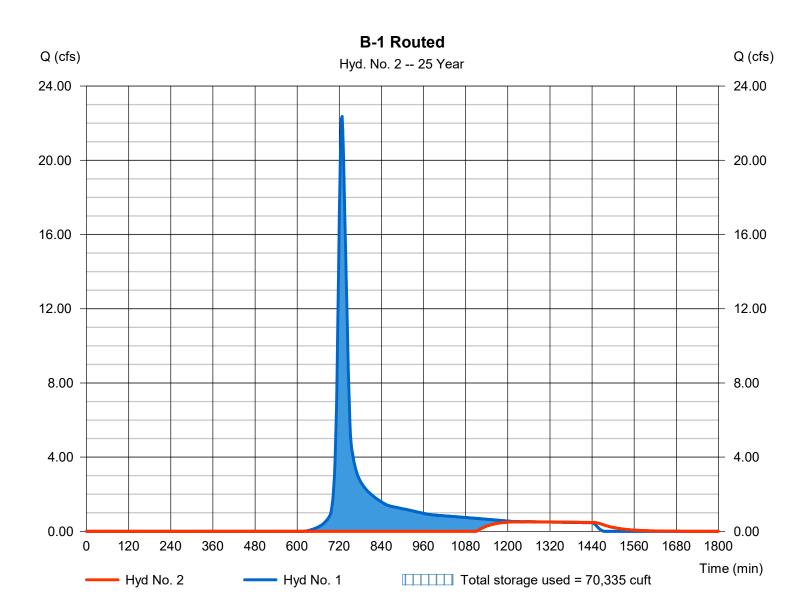
Tuesday, 09 / 19 / 2023

Hyd. No. 2

B-1 Routed

ischarge = 0.515 cfs
peak = 1264 min
olume = 10,993 cuft
levation = 312.55 ft
torage = 70,335 cuft

Storage Indication method used.



Pond Report

Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2022

Pond No. 5 - Sed. Basin 4

Pond Data

Contours -User-defined contour areas. Average end area method used for volume calculation. Begining Elevation = 310.00 ft

Stage / Storage Table

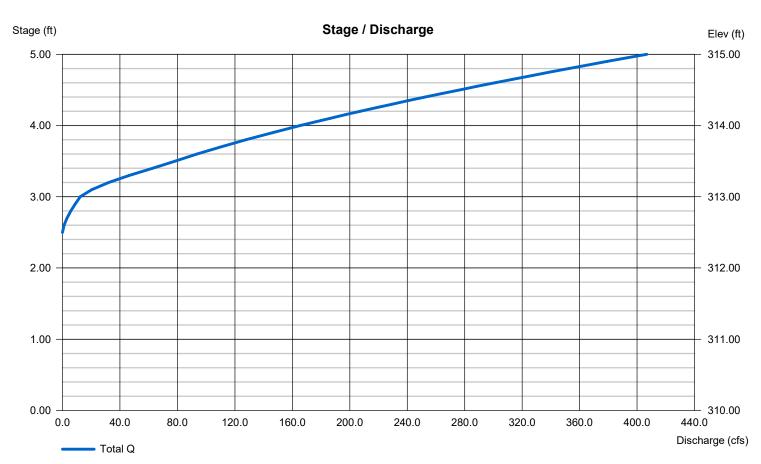
Stage (ft)	Elevation (ft)	Contour area (sqft)	Incr. Storage (cuft)	Total storage (cuft)
0.00	310.00	19,809	0	0
1.00	311.00	25,262	22,536	22,536
2.00	312.00	31,631	28,447	50,982
3.00	313.00	39,183	35,407	86,389
4.00	314.00	46,661	42,922	129,311
4.50	314.50	49,481	24,036	153,347
5.00	315.00	52,258	25,435	178,781

Culvert / Orifice Structures

	[A]	[B]	[C]	[PrfRsr]		[A]	[B]	[C]	[D]
Rise (in)	= 24.00	0.00	0.00	0.00	Crest Len (ft)	= 10.50	Inactive	50.00	0.00
Span (in)	= 24.00	0.00	0.00	0.00	Crest El. (ft)	= 312.50	311.00	313.00	0.00
No. Barrels	= 1	0	0	0	Weir Coeff.	= 3.33	3.33	2.60	3.33
Invert El. (ft)	= 307.25	0.00	0.00	0.00	Weir Type	= 1	Rect	Broad	
Length (ft)	= 36.00	0.00	0.00	0.00	Multi-Stage	= Yes	Yes	No	No
Slope (%)	= 0.69	0.00	0.00	n/a					
N-Value	= .013	.013	.013	n/a					
Orifice Coeff.	= 0.60	0.60	0.60	0.60	Exfil.(in/hr)	= 0.000 (by	Contour)		
Multi-Stage	= n/a	No	No	No	TW Elev. (ft)	= 0.00			

Note: Culvert/Orifice outflows are analyzed under inlet (ic) and outlet (oc) control. Weir risers checked for orifice conditions (ic) and submergence (s).

Weir Structures



SEDIMENT BASIN #4

FLOW CAPACITIES (IN CU. FT.) FOR THE FAIRCLOTH SKIMMER®

Skimmer size	1.5"	2"	2.5"	3"	4"	5"	6"	8"
24 hours	1,728	3,283	6,234	9,774	20,109	32,832	51,840	97,978
2 day	3,456	6,566	12,468	19,548	40,218	65,664	103,680	195,956
3 day	5,184	9,849	18,702	29,322	60,327	98,496	155,520	293,934
4 day	6,912	13,132	24,936	39,096	80,436	131,328	207,360	391,912
5 day	8, <mark>640</mark>	16,415	31,170	48, <mark>870</mark>	100,545	164,160	259,200	489,890
6 day	10,368	19,698	37,404	58,644	120,654	196,992	311,040	587,868
7 day	12,096	22,981	43,638	68,418	140,763	229,824	362,880	685,846

Important note: The orifice sizing chart in the Pennsylvania Erosion Control Manual DOES NOT APPLY to Faircloth Skimmer® surface drains. It will give the wrong size skimmer. Please use these instructions to choose the size skimmer required for the basin volume and the orifice size.

Dewatering Volume = 68,686 - 7,240 CF = 61,446 CF Dewatering Time = $\frac{61,446}{20,109}$ CF/Day 3.06 Days

APPENDIX F SPILLWAY/ANTI-SEEP COLLAR DESIGN

Corporate Office 743 South Broad Street Lititz, PA 17543 (717) 626-7271 Central PA Office 2013 Sandy Drive, Suite 103 State College, PA 16803 (814) 861-6328 Western PA Office 408 North Main Street, Suite 200 Butler, PA 16001 (717) 201-5334

BMP 1 EMERGENCY SPILLWAY

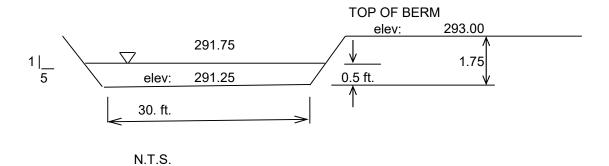
PROJECT: The Westtown School - Oak Lane Project LOCATION: Westtown Township COUNTY: Chester JOB # 1091-001 DATE: 1/12/2023 REVISED: 9/17/2023

Flow into basin for 100-year storm frequency:

Q = 29.58 cfs (From Post-Development analysis)

Capacity of the Emergency Spillway:

	Q = CL	H^1.5			C = L = H =		
	Q =	84.00 cfs		>	30 cfs	cfs	ОК
Check actual dep	oth and ve	elocity:					
Top of Berm Spillway Elev		ן =			293.00 291.25		
	H = [Q/	C*L]^2/3					
	= 0.5	ft.		at ele	evation	291.75	
Freeboard:			293.00	-	291.75	=	1.25 ft.
	V = Q//	4			Side Slope	e (H:V) =	4.5
	=	1.8 fps					



BMP 4 EMERGENCY SPILLWAY

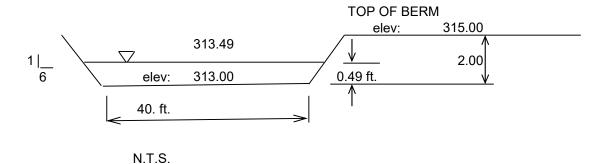
PROJECT: The Westtown School - Oak Lane Project LOCATION: Westtown Township COUNTY: Chester JOB # 1091-001 DATE: 1/12/2023 REVISED: 9/17/2023

Flow into basin for 100-year storm frequency:

Q = <u>38.87 cfs</u> cfs (From Post-Development analysis)

Capacity of the Emergency Spillway:

	Q = CI	LH^1.5			C = L = H =		
	Q =	112.00 cfs		>	39 cfs c	fs	ОК
Check actual dept	th and v	elocity:					
Top of Berm Spillway Eleva		on =			315.00 313.00		
	H = [C)/C*L]^2/3					
	= 0.4	49 ft.		at ele	vation	313.49	
Freeboard:			315.00	-	313.49	=	1.51 ft.
	V = Q/	/A			Side Slope	(H:V) =	6
	=	1.8 fps					



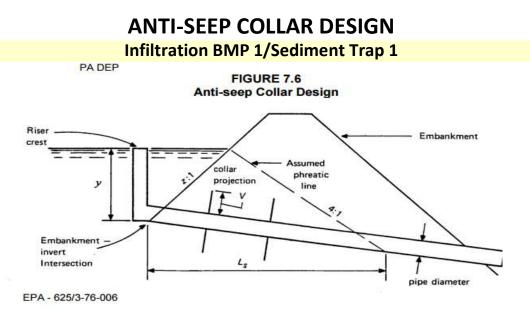
F:\Data\1091- Westtown School\1091-001 - Oak Lane Project\Civil\Stormwater\Worksheets\WESTTOWN-STORM.xlsx - SPILLWAY-BASIN_BMP 4

MODIFIED WORK SHEET # 11 SPILLWAY STABILITY CALCULATIONS

PROJECT: The Westtown School - Oak Lane Project JOB #	1091-001
LOCATION: Westtown Township Date	9/18/23
COUNTY: Chester Revised	

x	BASIN SPILLWAY ID		BMP 1	BMP 4	
	TEMPORARY OR PERMANENT?	(T OR P)	Р	Р	
	DESIGN STORM		100	100	
	Qr (REQUIRED CAPACITY)*	(CFS)	29.58	38.61	
	Q (CALCULATED AT FLOW DEPTH d)	(CFS)	29.59	38.62	
x	PROTECTIVE LINING ²		Flexamat	Flexamat	
	n (MANNING'S COEFFICIENT) ²		0.058	0.059	
	Va (ALLOWABLE VELOCITY)	(FPS)	19	19	
	V (CALCULATED AT FLOW DEPTH d)	(FPS)	4.05	4.69	
	ta (MAX ALLOWABLE SHEAR STRESS)	(LB/FT ²)	24.00	24.00	
	td (CALC'D SHEAR STRESS AT FLOW DEPTH d)	(LB/FT ²)	2.49	3.62	
	SPILLWAY BOTTOM WIDTH	(FT)	30.0	40.0	
	SIDE SLOPES	(H:V)	4.5:1	6:1	
	D (TOTAL DEPTH)	(FT)	1.75	2.00	
	d (CALCULATED FLOW DEPTH)	(FT)	0.24	0.20	
х	d ₅₀ STONE SIZE (IN)	(IN)	N/A	N/A	
x	A (CROSS-SECTIONAL AREA)	(SQ. FT.)	7.30	8.23	
x	R (HYDRAULIC RADIUS)		0.24	0.20	
x	S (BED SLOPE) ³	(FT/FT)	0.167	0.286	
	FREEBOARD PROVIDED	(FT)	1.51	1.80	
x	DESIGN METHOD FOR PROTECTIVE LINING **** PERMISS VELOCITY (V) OR SHEAR STRESS (S)	S	S		

* Required capacity based on the 100-year in flow. Refer to the PCSM Report/NPDES Module 2.



1. Determine length of pipe in saturated zone (Ls)

$$L_{s} = y(z+4) \begin{bmatrix} 1 + \frac{S}{(0.25-S)} \end{bmatrix}$$

$$y = \begin{array}{c} 6.25 \\ z = \\ S = \begin{array}{c} 3 \\ 0.005 \end{array}$$

Where y = Distance from upstream invert of spillway riser to top of dewatering volume (ft) z = Horizontal component of upstream embankment slope (ft) S = Pipe slope ft/ft

L_s = 44.64 ft

2. Determine the required increase in flow path

 $L_F = 1.15*L_s = 51.34$ ft

3. The minimum collar projection (V) is equal to 1/2 the increase in flow length (for one collary). If more than one collar is used, it is the increase divided by twice the number of collars

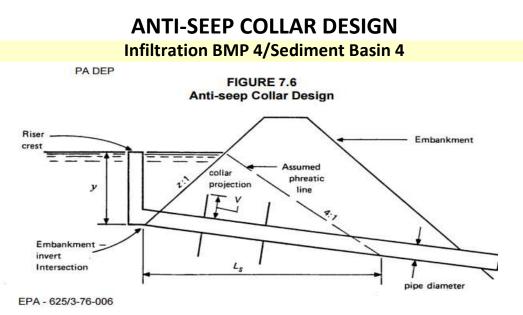
Number of collars: 2 Vmin = 1.67 ft

ft

4. The maximum spacing between collars should be 14 x V or Ls ÷ (number of collars minus 1)

Minimum spacing should be 5 X V

V = 1.67 Max = 22 ft Min = 8.4 ft



1. Determine length of pipe in saturated zone (Ls)

$$L_{s} = y(z+4) \begin{bmatrix} 1 + \frac{S}{(0.25-S)} \end{bmatrix}$$

$$y = \frac{3.75}{z} = \frac{3}{0.0069}$$

Where y = Distance from upstream invert of spillway riser to top of dewatering volume (ft) z = Horizontal component of upstream embankment slope (ft) S = Pipe slope ft/ft

2. Determine the required increase in flow path

 $L_F = 1.15*L_s = 31.04$ ft

3. The minimum collar projection (V) is equal to 1/2 the increase in flow length (for one collary). If more than one collar is used, it is the increase divided by twice the number of collars

Number of collars: 1 Vmin = 2.00 ft

4. The maximum spacing between collars should be 14 x V or Ls ÷ (number of collars minus 1)

Minimum spacing should be 5 X V

2 75



APPENDIX G RIP-RAP DESIGN

Corporate Office 743 South Broad Street Lititz, PA 17543 (717) 626-7271 Central PA Office 2013 Sandy Drive, Suite 103 State College, PA 16803 (814) 861-6328 Western PA Office 408 North Main Street, Suite 200 Butler, PA 16001 (717) 201-5334

STANDARD E&S WORKSHEET #20 Riprap Apron Outlet Protection

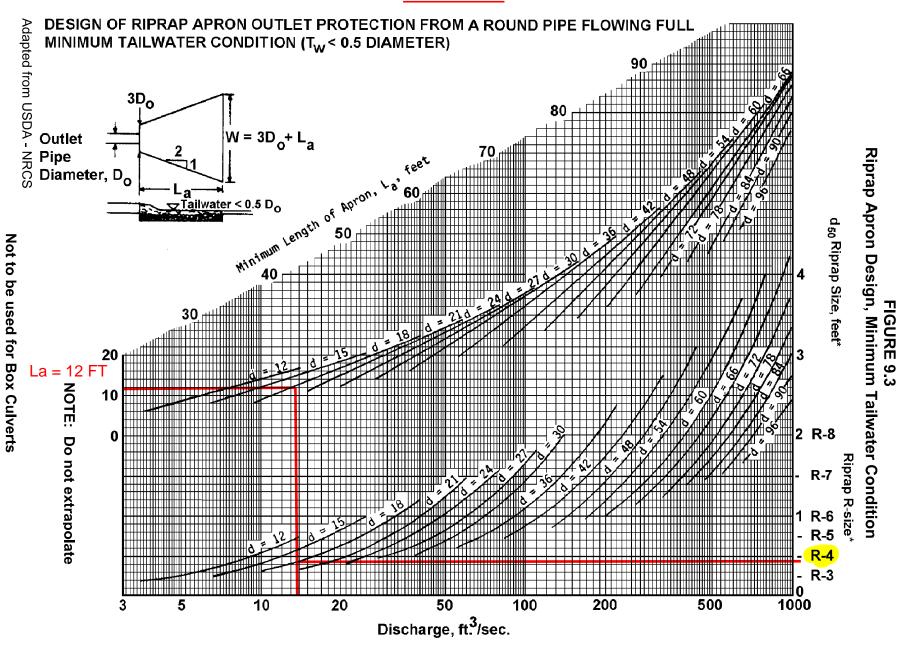
PROJECT: LOCATION: COUNTY: CHECH	Westtov	<u>vn Townsh</u>		i <u>k Lane F</u>	Project			F	JOB # DATE: REVISED:		-001 2023 /2023
A Pd Pd 1/2 Pd 1/2 Pd 1/2 Pd 1/2 Pd 1/2 Pd 1/2 Pd 1/2 Pd 1/2 Pd 1/2 Pd 1/2 Pd 1/3 1/3 1/3 1/3 1/3 1/3 1/3 1/3											
PLAN VIEW											
ORIGINAL GROUND ON GRADE> Rt GEOTEXTILE SECTION A - A											
	PIPE	TAIL WATER COND.	MAN. "n"	PIPE							
NO.	DIA. Do (in.)	(Max or Min.)	FOR PIPE	SLOPE (%)	Q (CFS)	V* (FPS)	RIPRAP SIZE	Rt (in)	AI (ft)	Aiw (ft)	Atw (ft)
EW-A1	18	Min.	0.012	0.50	13.7	7.75	R-4	18	12	4.50	16.50
EW-A2	18	Min.	0.012	1.00	12.0	6.83	R-4	18	12	4.50	16.50
EW-B1 EW-B2	24 15	Min. Min.	0.012	0.67	23.7 4.51	7.56	R-4	18 9	14 9	6.00 3.75	20.00
EVV-D2	15	IVIII1.	0.012	0.51	4.31	3.73	R-3	9	9	3.10	12.75

*The anticipated velocity (V) should not exceed the maximum permissible shown in Table 6.6 for the proposed riprap protection. Adjust for less than full pipe flow. SEE TABLE 9, March 2000 E&S PROGAM MANUAL. Use Manning's equation to calculate velocity for pipe slopes > 0.05 ft/ft.velocity for pipe slopes > 0.05 ft/ft.

** Based on sediment basin flow through principle spillway

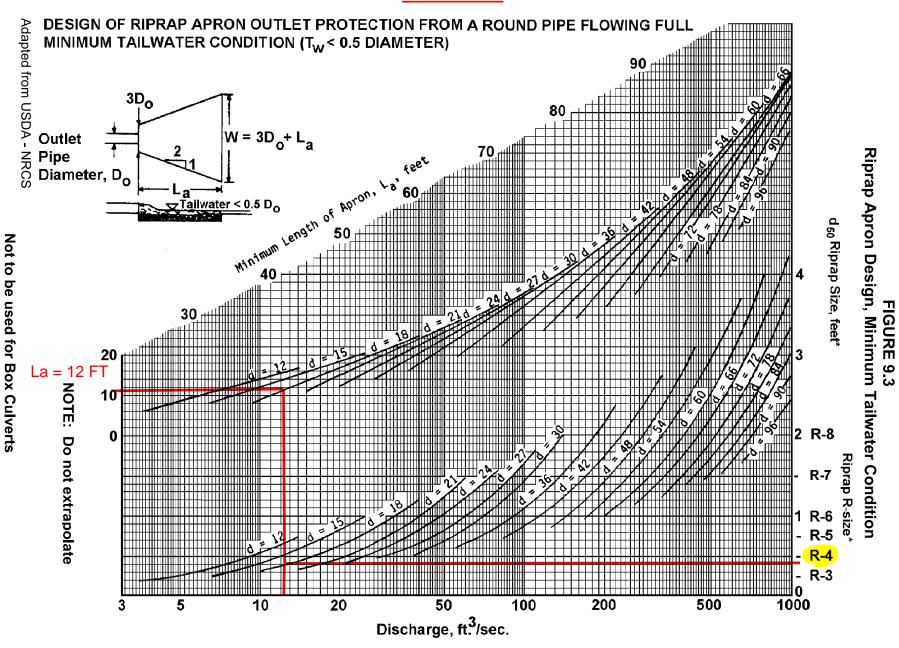
*** See attached Hydraflow Storm Sewers

EW-A1



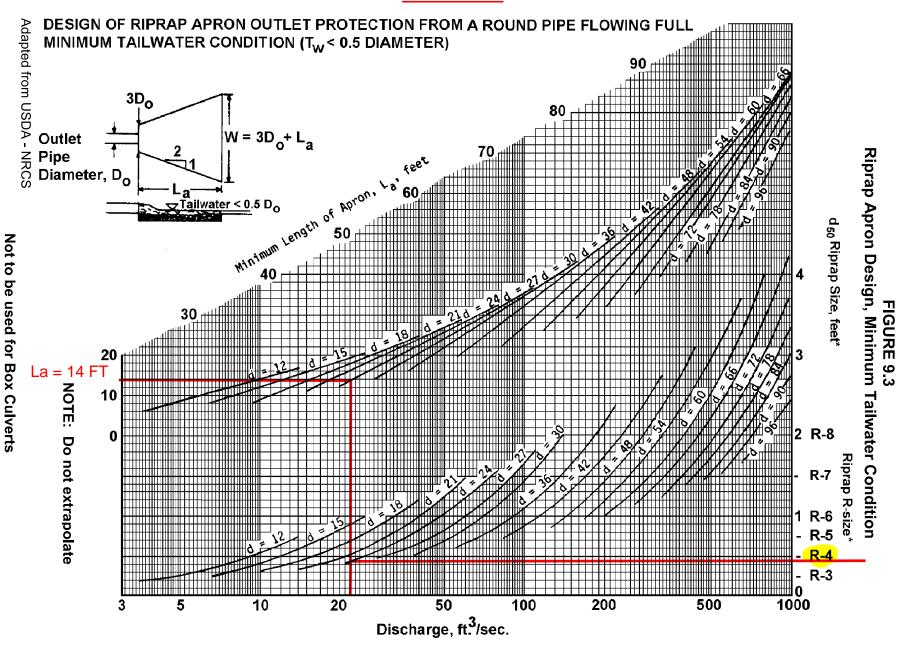
* For discharge velocities exceeding Maximum Allowable for Riprap indicated, increase d₅₀ stone size and/or provide velocity reduction device.

EW-A2



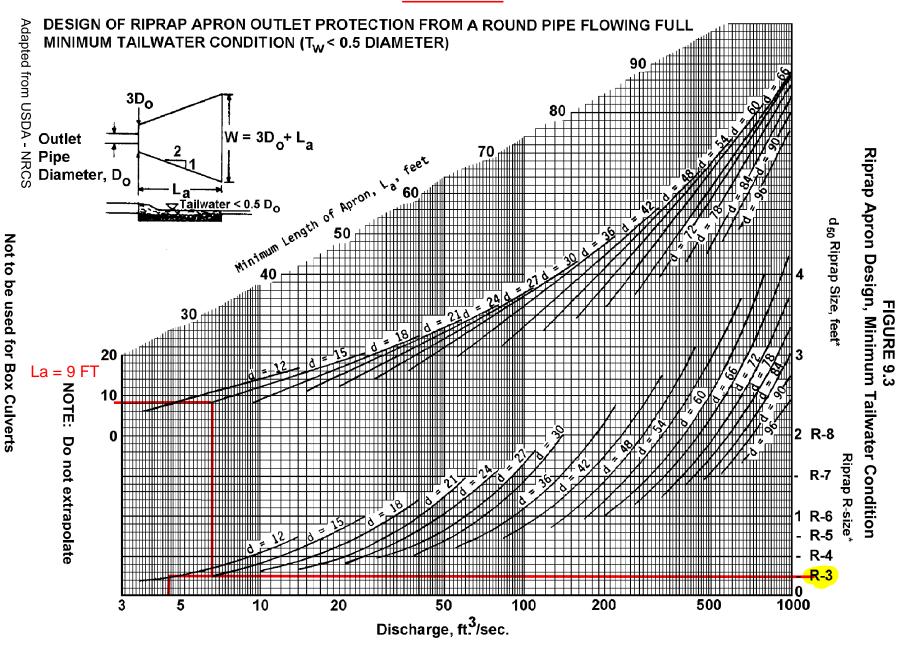
* For discharge velocities exceeding Maximum Allowable for Riprap indicated, increase d₅₀ stone size and/or provide velocity reduction device.

EW-B1



* For discharge velocities exceeding Maximum Allowable for Riprap indicated, increase d₅₀ stone size and/or provide velocity reduction device.

EW-B2



* For discharge velocities exceeding Maximum Allowable for Riprap indicated, increase d₅₀ stone size and/or provide velocity reduction device.

45

Anticipated Velocity Calculation for Less Than Full Pipe Flow

Outfall EW-B2

Full Flow Discharge:
$$Q_f = \frac{0.464}{n} D^{8/3} S^{1/2} = 5.01 \text{ cfs}$$

Continuity Equation to determine full-flow velocity:

$$V_f = \frac{Q_f}{A} = 4.08 \text{ ft/sec}$$

Where:

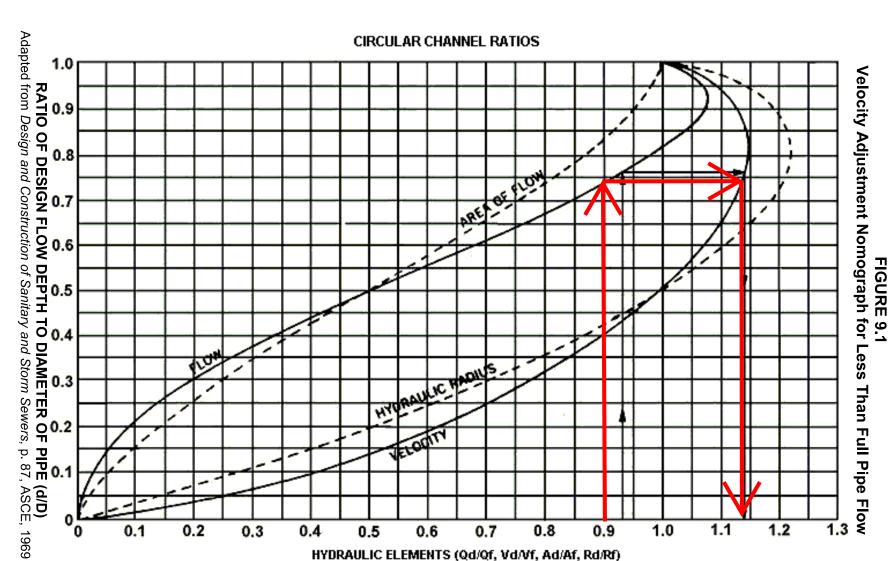
A = <u>1.23</u> = Cross Sectional Area (ft^2)

Ratio of Partial to Full-Flow Discharge:

$$d/D = \frac{Q_d}{Q_f} = 0.899$$
Where: $d/D = 0.90$ = Ratio of Part-Full to Full-Flow Discharge
 $Qd = 4.50$ = Design Discharge (cfs)
 $Qf = 5.01$ = Full-Flow Discharge (cfs)
 $D = 1.25$ = Diameter (ft)
 $S = 0.01$ = Slope of pipe (ft/ft)
 $n = 0.012$ = Mannings Coefficient
Velocity Ratio from Figure 9.1: 1.14
Design Velocity V_d = 4.65 ft/s



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EW-B2