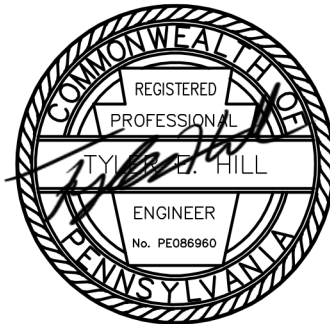


**NPDES PCSM MODULE 2/
POST CONSTRUCTION
STORM WATER MANAGEMENT REPORT**

FOR

**THE WESTTOWN SCHOOL
OAK LANE PROJECT
WESTTOWN TOWNSHIP
CHESTER COUNTY, PA**

PROJECT NO: 1091-001



January 27, 2023

Revised: October 27, 2023

This report is intended to provide supporting information and calculations associated with the approved PCSM Plans. Refer to the Approved Preliminary/Final Land Development Plan for Westtown School – Oak Lane Project, dated, January 27, 2023, last revised October 27, 2023

Prepared By:



ELA GROUP, INC.

743 S. Broad Street • Lititz, PA 17543
(717) 626-7271 • Fax (717) 626-7040

Website: www.elagroup.com • Email: staff@elagroup.com

Central PA Office • State College, PA
Western PA Office • Butler, PA

TABLE OF CONTENTS

NPDES PCSM MODULE 2	1
APPENDIX A – STORMWATER MANAGEMENT NARRATIVE.....	7
Site Description	
Summary of Proposed Improvements	
Soil Description, Limitations and Resolutions	
Geotechnical Assessment	
Narrative Description of Stormwater Management Concept	
BMP Design Notes	
Volume Management Summary	
Peak Rate Summary	
Offsite Discharge Analysis	
APPENDIX B – PADEP PCSM SPREADSHEETS	15
APPENDIX C – REFERENCE & SUPPORTING DOCUMENTS	32
APPENDIX D – SUPPORTING VOLUME CALCULATIONS	54
APPENDIX E – RATE CONTROL ANALYSIS.....	67
APPENDIX F – STORM SEWER CALCULATIONS	191
APPENDIX G – SPILLWAY/ANTI-SEEP COLLAR DESIGN CALCULATIONS.....	198
APPENDIX H – RIP RAP DESIGN CALCULATIONS.....	203
APPENDIX I – INFILTRATION REPORTS	
Infiltration Feasibility Report	213
Supplemental Infiltration Feasibility Report.....	239
WATERSHED MAPS	BACK
POCKET	

See plan sheet 4.

3. Plan drawings have been developed for the project and will be available on-site.

4. Plan drawings have been developed for the project and are attached to the NOI/application.

5. Recycling and proper disposal of materials associated with PCSM BMPs are addressed as part of long-term operation and maintenance of the PCSM BMPs.

6. Identify naturally occurring geologic formations or soil conditions that may have the potential to cause pollution after earth disturbance activities are completed and PCSM BMPs are operational and the applicant's plan to avoid or minimize potential pollution and its impacts.

See plan sheet 4.

7. Identify whether the potential exists for thermal impacts to surface waters from post-construction stormwater. If such potential exists, identify BMPs that will be implemented to avoid, minimize, or mitigate potential thermal impacts.

See plan sheet 4.

8. The PCSM Plan has been planned, designed, and will be implemented to be consistent with the E&S Plan.

9. A pre-development site characterization has been performed.

STORMWATER ANALYSIS – RUNOFF VOLUME

Surface Water Name: **East Branch Chester Creek**

Discharge Point(s): **001**

1. The design standard is based on volume management requirements in an Act 167 Plan approved by DEP within the past five years.
2. The design standard is based on managing the net change for storms up to and including the 2-year/24-hour storm.
3. An alternative design standard is being used.
4. A printout of DEP's PCSM Spreadsheet – Volume Worksheet is attached.
5. 2-Year/24-Hour Storm Event: **3.26** inches Source of precipitation data: **NOAA Atlas 14**
6. Stormwater Runoff Volume, Pre-Construction Conditions: **8,282** CF Calculations attached
7. Stormwater Runoff Volume, Post-Construction Conditions: **18,798** CF Calculations attached
8. Net Change (Post-Construction – Pre-Construction Volumes): **10,516** CF
9. Identify all selected structural PCSM BMPs and provide the information requested. Calculations attached

DP No.	BMP ID	Series	Vol. Routed to BMP (CF)	Inf. Area (SF)	Inf. Rate (in/hr)	Inf. Period (hrs)	Veg?	Media Depth (ft)	Storage Vol. (CF)	Inf. Credit (CF)	ET Credit (CF)
							<input type="checkbox"/>				
							<input type="checkbox"/>				
							<input type="checkbox"/>				
							<input type="checkbox"/>				
							<input type="checkbox"/>				
							<input type="checkbox"/>				
							<input type="checkbox"/>				
							<input type="checkbox"/>				
							<input type="checkbox"/>				
							<input type="checkbox"/>				

Total Infiltration & ET Credits (CF): 14,438

Non-Structural BMP Volume Credits (CF) (Attach Calculations):

Managed Release Credits (CF) (Attach MRC Design Summary):

Volume Required to Reduce/Manage (CF): 10,516

Total Credits (CF): 14,438

INFILTRATION INFORMATION	
BMP ID: 1	<input checked="" type="checkbox"/> Soil/geologic test results are attached.
1. No. of infiltration tests completed:	3
2. Method(s) used for infiltration testing:	double ring infiltrometer
3. Test Pit Identifiers (from PCSM Plan Drawings):	14A, 14B, & 16A
4. Avg Infiltration Rate:	0.81 in/hr
5. FOS:	2 : 1
6. Infiltration rate used for design:	0.41 in/hr
7. Separation distance between the BMP bottom and bedrock:	>3.5' feet
8. Separation distance between the BMP bottom and seasonal high-water table:	>3.5' feet
9. Comments:	
BMP ID:	<input type="checkbox"/> Soil/geologic test results are attached.
1. No. of infiltration tests completed:	
2. Method(s) used for infiltration testing:	
3. Test Pit Identifiers (from PCSM Plan Drawings):	
4. Avg Infiltration Rate:	in/hr
5. FOS:	: 1
6. Infiltration Rate Used for Design:	in/hr
7. Separation distance between the BMP bottom and bedrock:	feet
8. Separation distance between the BMP bottom and seasonal high-water table:	feet
9. Comments:	
BMP ID:	<input type="checkbox"/> Soil/geologic test results are attached.
1. No. of infiltration tests completed:	
2. Method(s) used for infiltration testing:	
3. Test Pit Identifiers (from PCSM Plan Drawings):	
4. Avg Infiltration Rate:	in/hr
5. FOS:	: 1
6. Infiltration Rate Used for Design:	in/hr
7. Separation distance between the BMP bottom and bedrock:	feet
8. Separation distance between the BMP bottom and seasonal high-water table:	feet
9. Comments:	

INFILTRATION INFORMATION	
BMP ID: 2	<input checked="" type="checkbox"/> Soil/geologic test results are attached.
1. No. of infiltration tests completed: 2	
2. Method(s) used for infiltration testing: double ring infiltrometer	
3. Test Pit Identifiers (from PCSM Plan Drawings): 1A & 3B	
4. Avg Infiltration Rate: 4.65 in/hr	5. FOS: 2 : 1
6. Infiltration rate used for design: 2.32 in/hr	
7. Separation distance between the BMP bottom and bedrock: >4' feet	
8. Separation distance between the BMP bottom and seasonal high-water table: >4' feet	
9. Comments:	
<hr/>	
BMP ID: 3	<input checked="" type="checkbox"/> Soil/geologic test results are attached.
1. No. of infiltration tests completed: 2	
2. Method(s) used for infiltration testing: double ring infiltrometer	
3. Test Pit Identifiers (from PCSM Plan Drawings): 4A & 5A	
4. Avg Infiltration Rate: 2.02 in/hr	5. FOS: 2 : 1
6. Infiltration Rate Used for Design: 1.01 in/hr	
7. Separation distance between the BMP bottom and bedrock: >4' feet	
8. Separation distance between the BMP bottom and seasonal high-water table: >4' feet	
9. Comments:	
<hr/>	
BMP ID: 4	<input type="checkbox"/> Soil/geologic test results are attached.
1. No. of infiltration tests completed: 2	
2. Method(s) used for infiltration testing: double ring infiltrometer	
3. Test Pit Identifiers (from PCSM Plan Drawings): 6A & 7B	
4. Avg Infiltration Rate: 1.67 in/hr	5. FOS: 2 : 1
6. Infiltration Rate Used for Design: 0.84 in/hr	
7. Separation distance between the BMP bottom and bedrock: >2' feet	
8. Separation distance between the BMP bottom and seasonal high-water table: 2' feet	
9. Comments:	

STORMWATER ANALYSIS – PEAK RATE

Surface Water Name: East Branch Chester Creek **Discharge Point(s):** 001

1. The design standard is based on rate requirements in an Act 167 Plan approved by DEP within the past five years.
2. The design standard is based on managing the net change for 2-, 10-, 50-, and 100-year/24-hour storms.
3. An alternative design standard is being used.
4. A printout of DEP's PCSM Spreadsheet – Rate Worksheet is attached.
5. Alternative rate calculations are attached.

6. Identify precipitation amounts. Source of precipitation data:

2-Year/24-Hour Storm: 10-Year/24-Hour Storm

50-Year/24-Hour Storm: 100-Year/24-Hour Storm

7. Report peak discharge rates, pre- and post-construction (without BMPs), based on a time of concentration analysis.

Design Storm	Pre-Construction Peak Rate (cfs)	Post-Construction Peak Rate (cfs)	Difference (cfs)
2-Year/24-Hour			
10-Year/24-Hour			
50-Year/24-Hour			
100-Year/24-Hour			

8. Identify all BMPs used to mitigate peak rate differences and provide the requested information.

BMP ID	Inflow to BMP (cfs)				Outflow from BMP (cfs)			
	2-Yr	10-Yr	50-Yr	100-Yr	2-Yr	10-Yr	50-Yr	100-Yr

9. Report peak rates for pre-construction and post-construction with BMPs and identify the differences.

Design Storm	Pre-Construction Peak Rate (cfs)	Post-Construction Peak Rate (with BMPs) (cfs)	Difference (cfs)
2-Year/24-Hour	2.38	1.27	-1.11
10-Year/24-Hour	8.96	3.28	-5.68
50-Year/24-Hour	19.09	8.40	-10.69
100-Year/24-Hour	24.73	12.51	-12.22

APPENDIX A

STORMWATER MANAGEMENT NARRATIVE

STORMWATER MANAGEMENT NARRATIVE

SITE DESCRIPTION

The project site is located near the center of the Westtown School campus, just south of Oak Lane. The existing site is largely comprised of existing grass athletic fields which are bordered to the north by a partially forested area and the school's academic centers; to the east by a baseball field and residential area; the south by agricultural fields (i.e. row crops) and a partially forested riparian area; and to the west by the school's working farm and agricultural area.

During the past 50 years, the site's primary use has been agricultural (i.e. row crops). The site is currently utilized primarily for athletic fields, with row crops along the southeastern portion of the project site. The site has been utilized as such for at least the past five years, with no significant improvements being constructed during that time.

SUMMARY OF PROPOSED IMPROVEMENTS

The Westtown School is proposing to improve upon the existing athletic facilities on campus by constructing two new synthetic turf multipurpose fields, along with reconfiguring the remaining area to maximize field space. Additional components of the project involve the construction of a support building, parking lot and improved pedestrian access.

SOIL DESCRIPTIONS, LIMITATIONS AND RESOLUTIONS

As per the USDA NRCS Web Soil Survey, the soils within the project area (Limit of Disturbance) are classified as follows:

- CaB – Califon Loam (3-8% slopes, Hydrologic Soil Group "D")
- GgC – Glenelg Silt Loam (8-15% slopes, Hydrologic Soil Group "B")
- MaA – Manor Loam (0-3% slopes, Hydrologic Soil Group "B")
- MaB – Manor Loam (3-8% slopes, Hydrologic Soil Group "B")
- MaC – Manor Loam (8-15% slopes, Hydrologic Soil Group "B")

See the *Supplemental Design Information* section for a summary of the Soil Facts, Use Limitations and Resolutions.

GEOTECHNICAL ASSESSMENT

A geotechnical investigation was performed on site to evaluate the site for infiltration of post-construction stormwater. The investigation determined that the site is underlain by the polytactic schist of the Glenarm Wissahickon Formation. This formation includes lenticular amphibolite bodies having ocean-floor basalt chemistry and is not considered karst. Infiltration tests performed on site found suitable infiltration rates in nearly every test pit, but not at all depths. In general, the site was found to be well drained and suitable for infiltration.

The complete Stormwater Infiltration Feasibility Report, dated October 8, 2018, and Supplemental Infiltration Feasibility Report, dated November 9, 2018, has been provided as an attachment to this report.

NARRATIVE DESCRIPTION OF STORMWATER MANAGEMENT CONCEPT

The project site generally sits along a watershed drainage boundary and thus has been analyzed as two drainage areas. The south/western portion of the site generally drains to the southwest towards East Branch Chester Creek (TSF, MF). In post development there is one proposed discharge point (DP001) in this watershed. The eastern portion of the site drains to an existing riparian area consisting of wetlands, forested area and the headwaters of an unnamed tributary to East Branch Chester Creek. In post development, there is one proposed discharge point (DP002) in this watershed. See the Pre and Post Watershed Mapping in this report for watershed delineation.

In order to address rate control, volume control, and water quality requirements the following structural and non-structural BMPs are being proposed:

Infiltration Basin (BMP 1 & BMP 4)

- An infiltration basin is a constructed impoundment intended to capture and infiltrate stormwater runoff.
- Infiltration basin typically contains a layer of installed amended soils which typically contain a high percent of organic matter and additional large grained materials (such as sand) to provide an improved cation exchange rate and assure permeability.
- Infiltration basins are often planted with water-tolerant, native vegetation in order to increase water uptake via the vegetation's root system and increase pollutant removal.

Subsurface Infiltration Bed (BMP 2 and BMP 3)

- A subsurface detention bed is a void space, typically angular stone and/or manufactured chamber system, constructed beneath the surface on virgin material with the intent to capture and infiltrate stormwater runoff.
- Infiltration Beds BMP 2 and BMP 3 are to be installed beneath the synthetic turf fields and consist of crushed angular stone with perforated distribution pipes

BMP DESIGN NOTES

The proposed structural BMPs have been designed in general accordance with the PADEP Stormwater BMP Manual. Given the site topography and location of existing improvements, the design of Basin A required a slightly modified approach with minor deviations from the BMP Manual. First, as the only feasible location for infiltration within the East Branch Chester Creek watershed, impervious and overall loading ratios exceed the recommended values of 5:1 and 8:1, respectively. Loading ratios of approximately 7:1 and 28:1 are proposed. These loading ratios are acceptable as the contributing area does not present a high potential for pollution, the geology is not karst and thus sinkholes and groundwater contamination are not of concern, and the site is general well-drained.

Additionally, three (3) infiltration tests were performed within the infiltration footprint of BMP 1 at the infiltration invert elevation and yielded results of 0.0 in/hr, 1.0 in/hr, and 6.0 in/hr. Based on the results, and the general soil characteristics of the site the area is feasible for infiltration, however determination of a design infiltration rate is not straightforward due to the wide range and the presence of test with zero infiltration. As a result, the design infiltration rate has been determined by removing the highest and lowest recorded infiltration

rates and applying a safety factor of two (2) to the remaining infiltration rate. This approach is reasonable as the recorded infiltration rates in the other proposed infiltration facilities ranged from 1.00 in/hr to 6.00 in/hr, which suggests the site as a whole consists of relatively variable soils but is generally conducive for infiltration. The recorded rates of TP-14 and TP-16 of 1.00 in/hr and 6.00 in/hr are within the range of recorded values elsewhere onsite and thus utilizing the lower of the two would produce a conservative design rate. Additionally, notes have been added to the plan regarding the potentially unsuitable soils within BMP 1 which outline in-situ testing protocol to determine the extent of unsuitable soils and a remediation plan.

VOLUME MANAGEMENT SUMMARY

A geotechnical evaluation was performed by Advantage Engineers to determine the suitability of the site for infiltration practices. Based upon the analysis, the site is generally well-drained and suitable for infiltration. See the *Stormwater Infiltration Feasibility Report*, dated October 8, 2018 and the Supplemental Infiltration Feasibility Report, dated November 9, 2018, for more information and a complete list of infiltration test pit results.

The volume removal requirements have been analyzed separately for compliance with NPDES PAG-02 and the municipal requirements. NPDES PAG-02 requires that 20% of existing impervious area be considered meadow in good condition, whereas the Westtown Township Stormwater Management Ordinance (SWMO) requires that 40% of existing impervious area be considered meadow in good condition.

NPDES volume management calculations can be found in Appendix B – PADEP PCSM Spreadsheets and the volume management calculations for Westtown Township can be found in Appendix D – Supporting Volume Calculations.

A summary of the volume removal calculations considering NPDES and municipal requirements can be found for each watershed in the tables below.

East Branch Chester Creek

The increase in runoff for the 2-year/24-hour storm for East Branch Chester Creek is being fully mitigated within the Infiltration Basin (BMP 1). A summary of the volume calculations can be seen in the following tables:

NPDES:

VOLUME SUMMARY East Branch Chester Creek

PROJECT: The Westtown School - Oak Lane Project
 LOCATION: Westtown Township
 COUNTY: Chester

JOB # : 1091-001
 DATE: 1/13/2023
 REVISED: 9/17/2023

Req'd Infiltration Volume		10,516 CF							
STRUCTURAL BMPs									
BMP ID	Infiltration Area (sf)	Impervious		Overall		2 YR Runoff Volume (cf)	Storage		Infiltration & ET Credit (CF)*
		Area (sf)	LR	Area (sf)	LR		Vol. (cf) @	Elev.	
BMP 1	10,675	53,560	5.0:1	217,187	20:1	15,663	11,503	289.50	14,438
Total	10,675	53,560	5.0:1	217,187	20:1	15,663	11,503		14,438

*See Infiltration Volume Worksheets

Westtown Township:

VOLUME SUMMARY (Twp. Analysis) East Branch Chester Creek

PROJECT: The Westtown School - Oak Lane Project
 LOCATION: Westtown Township
 COUNTY: Chester

JOB # : 1091-001
 DATE: 9/17/2023
 REVISED:

Req'd Infiltration Volume		10,971 CF							
STRUCTURAL BMPs									
BMP ID	Infiltration Area (sf)	Impervious		Overall		2 YR Runoff Volume (cf)	Storage		Infiltration & ET Credit (CF)*
		Area (sf)	LR	Area (sf)	LR		Vol. (cf) @	Elev.	
BMP 1	10,675	53,560	5.0:1	217,187	20:1	15,663	11,503	289.50	14,438
Total	10,675	53,560	5.0:1	217,187	20:1	15,663	11,503		14,438

*See Infiltration Volume Worksheets

Unt. to East Branch Chester Creek

The increase in volume for the 2-year/24-hour storm for the Unnamed Tributary to East Branch Chester Creek is being controlled through two (2) subsurface infiltration beds (BMP's 2&3) and an infiltration basin (BMP 4). A summary of the volume calculations can be seen in the following tables:

NPDES:

VOLUME SUMMARY UNT. TO EAST BRANCH CHESTER CREEK

PROJECT: The Westtown School - Oak Lane Project
 LOCATION: Westtown Township
 COUNTY: Chester

JOB #: 1091-001
 DATE: 1/13/2023
 REVISED: 9/17/2023

Req'd Infiltration Volume (from WS 4)				49,535 CF					
STRUCTURAL BMPS									
BMP ID	Infiltration Area (sf)	Impervious		Overall		2 YR Runoff Volume (cf)	Storage		Volume Credits (cf)*
		Area (sf)	LR	Area (sf)	LR		Vol. (cf) @	Elev.	
2	75,725	96,824	1.3:1	96,824	1.3:1	24,426	23,035	316.75	24,426
3	26,795	96,824	3.6:1	96,824	3.6:1	24,426	21,916	321.00	24,357
4	19,809	12,972	0.7:1	421,241	21.3:1	14,912	22,478	311.00	14,912
Total	122,329	206,620	1.7:1	614,889	5:1	63,764	67,429		63,695

*See Infiltration Volume Worksheets

Westtown Township:

VOLUME SUMMARY UNT. TO EAST BRANCH CHESTER CREEK

PROJECT: The Westtown School - Oak Lane Project
 LOCATION: Westtown Township
 COUNTY: Chester

JOB #: 1091-001
 DATE: 1/13/2023
 REVISED:

Req'd Infiltration Volume (from WS 4)				49,557 CF					
STRUCTURAL BMPS									
BMP ID	Infiltration Area (sf)	Impervious		Overall		2 YR Runoff Volume (cf)	Storage		Infiltration Volume *
		Area (sf)	LR	Area (sf)	LR		Vol. (cf) @	Elev.	
2	75,725	96,824	1.3:1	96,824	1.3:1	24,426	23,035	316.75	24,426
3	26,795	96,824	3.6:1	96,824	3.6:1	24,426	21,916	321.00	24,357
4	19,809	12,972	0.7:1	421,241	21.3:1	14,912	22,478	311.00	14,912
Total	122,329	206,620	1.7:1	614,889	5:1	63,764	67,429		63,695

*See Infiltration Volume Worksheets

See Appendix B for complete volume calculations.

PEAK RATE SUMMARY CALCULATIONS

The peak rate calculations have been provided to show compliance with the Westtown Township SWMO as well as NPDES PAG-02 requirements. The Township requires that all non-impervious areas be treated as meadow and 40% of impervious areas be treated as meadow in pre-development conditions. Since this requirement is more stringent than NPDES requirements it has been used as the standard for peak rate calculations.

Additionally, the Township requires a 50% reduction in onsite peak flows from pre- to post-development.

The following tables summarize the calculations for the pre-development peak flows, allowable post-development outflows, and the calculated outflow from each BMP and subdrainage area. Post development flows assume hydraulic routing through the proposed detention/infiltration facilities. All flows are in cfs. See Appendix E within this report for complete area calculations and hydrographs.

SUMMARY OF FLOWS - NRCS Rainfall-Runoff East Branch Chester Creek

PROJECT: The Westtown School - Oak Lane Project	JOB #: 1091-001
LOCATION: Westtown Township	DATE: 1/13/2023
COUNTY: Chester	REVISED: 9/17/2023

WATERSHEDS	2 yr	5 yr	10 yr	25 yr	50 yr	100 yr
PRE-DEVELOPMENT	Flows (cfs)					
Pre-Dev. (E. Branch Chester Creek (EBCC))	2.38	5.68	8.96	14.25	19.09	24.73
Total Pre-Development						
EBCC Onsite (Reduction Factor)	1.53	3.84	6.21	10.05	13.58	17.68
50% Reduction	0.76	1.92	3.11	5.03	6.79	8.84
Allowable Post-Development Flow (Pre-Dev. - 50% Reduction)	1.62	3.76	5.86	9.23	12.30	15.89
POST-DEVELOPMENT						
EBCC-Undetained	1.27	2.31	3.28	4.79	6.12	7.62
BMP 1	0.16	0.62	1.63	4.43	7.56	11.46
Total Post-Development(Combined Hydrographs)	1.27	2.31	3.28	5.06	8.40	12.51

SUMMARY OF FLOWS - NRCS Rainfall-Runoff Unt. to East Branch Chester Creek

PROJECT: The Westtown School - Oak Lane Project	JOB #: 1091-001
LOCATION: Westtown Township	DATE: 1/13/2023
COUNTY: Chester	REVISED: 9/17/2023

WATERSHEDS	2 yr	5 yr	10 yr	25 yr	50 yr	100 yr
PRE-DEVELOPMENT	Flows (cfs)					
Pre-Dev. UNT. to East Branch Chester Creek (EBCC)	5.02	12.03	19.34	31.25	42.19	54.74
Total Pre-Development						
Unt. to EBCC Onsite (Reduction Factor)	3.66	8.78	14.12	22.81	30.80	39.96
50% Reduction	1.83	4.39	7.06	11.41	15.40	19.98
Allowable Post-Development Flow	3.19	7.64	12.28	19.85	26.79	34.76
POST-DEVELOPMENT						
BMP 3	0.01	0.08	0.12	0.17	0.22	0.44
BMP 2	0.00	0.15	0.32	0.76	1.33	2.11
BMP 4	0.02	0.75	2.04	7.99	15.12	23.74
Unt. to EBCC Undetained	2.51	4.94	7.23	10.84	14.08	17.79
Total Post-Development(Combined Hydrographs)	2.51	4.94	7.23	10.84	17.45	26.78

OFFSITE DISCHARGE ANALYSIS

DP001

Discharge Point (DP)001 is considered to be the proposed outfall of BMP 1. In order to reduce the risk of downstream erosion a rip-rap apron will be employed to dissipate the energy and spread out the concentrated discharge of the endwall. The rip-rap has been designed using current design standards based on pipe size, outflow and anticipated velocity. Approximately 100 feet downslope of the discharge point the outflow enters and existing roadside swale. The flowpath between the discharge path and drainage swale is a well vegetated open area. The relatively short flowpath should reduce the amount of re-concentration of runoff. After the runoff enters the swale it continues on to an existing culvert which discharges to another reach of swale that enters the receiving surface water (refer to the Overall Drainage Map, sheet 44 of 44). Since the post-development rate and volume of runoff from the project site tributary to the existing drainage swale is being reduced from pre- to post development there is no risk of accelerated erosion to the downstream flowpath of runoff leaving the site at DP001. Further, mitigation is being provided in the form of a rip-rap apron to prevent erosion prior to runoff entering the existing drainage swale.

DP002

Discharge Point (DP)002 is considered to be the proposed outfall of BMP 4. DP002 discharges to an existing, well vegetated natural draw. This natural draw becomes the headwaters of the receiving watercourse approximately 350' downslope of DP002. In order to reduce the risk of downstream erosion a rip-rap apron will be employed to dissipate the energy and spread out the concentrated discharge of the endwall. The rip-rap has been designed using current design standards based on pipe size, outflow and anticipated velocity. Given the mild slope of the draw, quality and density of the vegetation, and the proposed outlet protection (rip-rap) there is no anticipated risk of accelerated erosion to the downstream flowpath.

APPENDIX B

PADEP PCSM SPREADSHEETS

APPENDIX B
PADEP PCSM SPREADSHEETS
(EAST BRANCH CHESTER CREEK)

General Information

- Instructions
- General**
- Volume
- Rate
- Quality

Project Name:	The Westtown School - Oak Lane Project	Application Type:	PAG-02 NOI
County:	Chester	Municipality:	Westtown Township
Project Type:	Other	<input checked="" type="radio"/> New Project <input type="radio"/> Minor / Major Amendment	
Area: <i>(In Watershed)</i>	6.60 acres	Total Earth Disturbance: <i>(In Watershed)</i>	4.91 acres
No. of Post-Construction Discharge Points:	1	Start DP Numbering at:	001

Discharge Point (DP) No.	Drainage Area (DA) (acres)	Earth Disturbance in DA (acres)	Existing Impervious in DA (acres)	Proposed Impervious in DA (acres)	Receiving Waters	Ch. 93 Class	Structural BMP(s)
001	4.99	3.36	0.34	1.23	Discharge to MS4	TSF, MF	Yes
Undetained Areas	1.27	1.21	0.08	0.15	Discharge to MS4	TSF, MF	
Totals:	6.26	4.57	0.42	1.38			

Volume Management

Project: The Westtown School - Oak Lane Project

Instructions General **Volume** Rate Quality

2-Year / 24-Hour Storm Event (NOAA Atlas 14): inches Alternative 2-Year / 24-Hour Storm Event inches
Alternative Source:

Pre-Construction Conditions: No. Rows: Exempt from Meadow in Good Condition Automatically Calculate CN, Ia, Runoff and Volume

Land Cover	Area (acres)	Soil Group	CN	Ia (in)	Q Runoff (in)	Runoff Volume (cf)
Impervious Areas: Paved Parking Lots, Roofs, Driveways, Etc. (Excluding ROW)	0.19	B	98	0.041	3.03	2,066
Pervious as Meadow	4.68	B	58	1.448	0.36	6,154
Impervious as Meadow	0.05	B	58	1.448	0.36	62
TOTAL (ACRES):		4.91			TOTAL (CF):	8,282

Post-Construction Conditions: No. Rows:

Land Cover	Area (acres)	Soil Group	CN	Ia (in)	Q Runoff (in)	Runoff Volume (cf)
Impervious Areas: Paved Parking Lots, Roofs, Driveways, Etc. (Excluding ROW)	1.19	B	98	0.041	3.03	13,033
Open Space (Lawns, Parks, Golf Courses, Cemeteries, Etc.) - Good Condition (Grass Cover > 75%)	3.39	B	61	1.279	0.47	5,765
TOTAL (ACRES):		4.57			TOTAL (CF):	18,798

NET CHANGE IN VOLUME TO MANAGE (CF):

Non-Structural BMP Volume Credits:

Tree Planting Credit

Other (attach calculations):

Structural BMP Volume Credits:

No. Structural BMPs:

Start BMP Numbering at:

DP No.	BMP No.	BMP Name	MRC?	Discharge	Incremental BMP DA (acres)	Volume Routed to BMP (CF)	Infiltration / Vegetated Area (SF)	Infiltration Rate (in/hr)	Infiltration Period (hrs)	Vegetated?	Media Depth (ft)	Storage Volume (CF)	Infiltration Credit (CF)	ET Credit (CF)
001	1	Infiltration Basin		Off-Site	3.36	15,663	10,675	0.41	34	Yes	1.0	11,503	11,161	3,277

Totals: 11,161 3,277

INFILTRATION & ET CREDITS (CF):

NET CHANGE IN VOLUME TO MANAGE (CF):

TOTAL CREDITS (CF):

VOLUME REQUIREMENT SATISFIED

Rate Control

Project: The Westtown School - Oak Lane Project

Instructions
General
Volume
Rate
Quality

Precipitation Amounts:

NOAA 2-Year 24-Hour Storm Event (in):	3.26
NOAA 10-Year 24-Hour Storm Event (in):	4.8
NOAA 50-Year 24-Hour Storm Event (in):	6.66
NOAA 100-Year 24-Hour Storm Event (in):	7.58

Alternative 2-Year 24-Hour Storm Event (in):	
Alternative 10-Year 24-Hour Storm Event (in):	
Alternative 50-Year 24-Hour Storm Event (in):	
Alternative 100-Year 24-Hour Storm Event (in):	

Report Summary of Peak Rates Only

Attach model input and output data or other calculations to support the rates reported below.

	<i>Peak Discharge Rates (cfs)</i>			
	Pre-Construction	Post-Construction	Net Change	
2-Year Storm:	2.38	1.27	-1.11	<i>Rate Control Satisfied</i>
10-Year Storm:	8.96	3.28	-5.68	<i>Rate Control Satisfied</i>
50-Year Storm:	19.09	8.40	-10.69	<i>Rate Control Satisfied</i>
100-Year Storm:	24.73	12.51	-12.22	<i>Rate Control Satisfied</i>

Water Quality

Project: The Westtown School - Oak Lane Project

PRINT

Instructions

General

Volume

Rate

Quality

Pre-Construction Pollutant Loads:

Land Cover (from Volume Worksheet)	Land Cover for Water Quality	Area (acres)	Soil Group	Runoff Volume (cf)	Pollutant Conc. (mg/L)			Pollutant Loads (lbs)		
					TSS	TP	TN	TSS	TP	TN
Impervious Areas: Paved Parking Lots, Roofs, Driveways, Etc. (Excluding ROW)	Residential	0.19	B	2,066	65.0	0.29	2.05	8.39	0.04	0.26
Pervious as Meadow	Grassland/Herbaceous	4.68	B	6,154	48.8	0.22	2.30	18.75	0.08	0.88
Impervious as Meadow	Grassland/Herbaceous	0.05	B	62	48.8	0.22	2.30	0.19	0.00	0.01
TOTAL (ACRES):		4.91			TOTALS:			27.33	0.12	1.16

Post-Construction Pollutant Loads (without BMPs):

Land Cover (from Volume Worksheet)	Land Cover for Water Quality	Area (acres)	Soil Group	Runoff Volume (cf)	Pollutant Conc. (mg/L)			Pollutant Loads (lbs)		
					TSS	TP	TN	TSS	TP	TN
Impervious Areas: Paved Parking Lots, Roofs, Driveways, Etc. (Excluding ROW)	Residential	1.19	B	13,033	65.0	0.29	2.05	52.90	0.24	1.67
Open Space (Lawns, Parks, Golf Courses, Cemeteries, Etc.) - Good Condition (Grass Cover > 75%)	Open Space	3.39	B	5,765	78.0	0.25	1.25	28.08	0.09	0.45

TOTAL (ACRES): 4.57

TOTALS: 80.98 0.33 2.12

POLLUTANT LOAD REDUCTION REQUIREMENTS (LBS): **53.65 0.20 0.96**

Characterize Undetained Areas (for Untreated Stormwater)

Land Cover	Area (acres)	Soil Group	CN	Ia (in)	Q Runoff (in)	Runoff Volume (cf)

Non-Structural BMP Water Quality Credits:

Pervious Undetained Area Credit

Other (attach calculations)

Structural BMP Water Quality Credits:

Use default BMP Outflows and Median BMP Outflow Concentrations

DP No.	BMP No.	BMP Name	MRC?	BMP DA (acres)	Vol. Routed to BMP (CF)	Inf. & ET Credits (CF)	Capture & Buffer Credits (CF)	Outflow (CF)	Outflow Conc. (mg/L)			Pollutant Loads (lbs)		
									TSS	TP	TN	TSS	TP	TN
001	1	Infiltration Basin		3.36	15,663	14,438		1,225	10.00	0.24	0.96	0.76	0.02	0.07

POLLUTANT LOADS FROM STRUCTURAL BMP (TREATED) OUTFLOWS (LBS):

POLLUTANT LOADS FROM UNTREATED STORMWATER (LBS):

NON-STRUCTURAL BMP WATER QUALITY CREDITS (LBS):

NET POLLUTANT LOADS FROM SITE, POST-CONSTRUCTION (LBS):

POLLUTANT LOADS FROM SITE, PRE-CONSTRUCTION (LBS):

TSS	TP	TN
0.76	0.02	0.07
13.50	0.05	0.35
14.27	0.07	0.43
27.33	0.12	1.16

WATER QUALITY REQUIREMENT SATISFIED

CERTIFICATION

I certify under penalty of law and subject to the penalties of 18 Pa.C.S. § 4904 (relating to unsworn falsification to authorities) that this document and all attachments were prepared under my direction or supervision in accordance with a system designed to assure that qualified personnel properly gathered and evaluated the information submitted. Based on my inquiry of the person or persons who manage the system, or those persons directly responsible for gathering the information, the information submitted is, to the best of my knowledge and belief, true, accurate, and complete. I further certify that the structure, function, and calculations contained in this spreadsheet have not been modified in comparison to the spreadsheet DEP has posted to its website or, if modifications were made, an explanation of the modifications made is attached to this spreadsheet.

Tyler E. Hill, PE

Spreadsheet User Name

9/17/2023

Date

**UNT. TO
EAST BRANCH CHESTER CREEK**

General Information

Instructions
General
Volume
Rate
Quality

Project Name:	The Westtown School - Oak Lane Project	Application Type:	PAG-02 NOI
County:	Chester	Municipality:	Westtown Township
Project Type:	Other	<input checked="" type="radio"/> New Project <input type="radio"/> Minor / Major Amendment	
Area: <i>(In Watershed)</i>	17.70 acres	Total Earth Disturbance: <i>(In Watershed)</i>	13.02 acres
No. of Post-Construction Discharge Points:	1	Start DP Numbering at:	002

Discharge Point (DP) No.	Drainage Area (DA) (acres)	Earth Disturbance in DA (acres)	Existing Impervious in DA (acres)	Proposed Impervious in DA (acres)	Receiving Waters	Ch. 93 Class	Structural BMP(s)
002	14.11	10.41	0.01	4.74	Unt. to E. Branch Chester Creek	TSF, MF	Yes
Undetained Areas	3.59	2.61	0.01	0.00	Unt. to E. Branch Chester Creek	TSF, MF	
Totals:	17.70	13.02	0.02	4.74			

IET CHANGE IN VOLUME TO MANAGE (CF): 49,535

Non-Structural BMP Volume Credits:

- Tree Planting Credit
- Other (attach calculations):

Structural BMP Volume Credits:

No. Structural BMPs: 3

Start BMP Numbering at: 2

DP No.	BMP No.	BMP Name	MRC?	Discharge	Incremental BMP DA (acres)	Volume Routed to BMP (CF)	Infiltration / Vegetated Area (SF)	Infiltration Rate (in/hr)	Infiltration Period (hrs)	Vegetated?	Media Depth (ft)	Storage Volume (CF)	Infiltration Credit (CF)	ET Credit (CF)
002	2	Infiltration Bed		to BMP No. 4	2.22	24,426	75,725	2.32	12	No		23,035	24,426	
002	3	Infiltration Bed		to BMP No. 4	2.22	24,426	26,795	1.01	12	No		21,916	24,357	
002	4	Infiltration Basin		Off-Site	9.67	14,912	19,809	0.84	16	Yes	1.0	14,912	14,912	0

Totals: 63,695

INFILTRATION & ET CREDITS (CF): 63,695

NET CHANGE IN VOLUME TO MANAGE (CF): 49,535

TOTAL CREDITS (CF): 63,695

VOLUME REQUIREMENT SATISFIED

Rate Control

Project: The Westtown School - Oak Lane Project

Instructions
General
Volume
Rate
Quality

Precipitation Amounts:

NOAA 2-Year 24-Hour Storm Event (in):	3.26	Alternative 2-Year 24-Hour Storm Event (in):	
NOAA 10-Year 24-Hour Storm Event (in):	4.8	Alternative 10-Year 24-Hour Storm Event (in):	
NOAA 50-Year 24-Hour Storm Event (in):	6.66	Alternative 50-Year 24-Hour Storm Event (in):	
NOAA 100-Year 24-Hour Storm Event (in):	7.58	Alternative 100-Year 24-Hour Storm Event (in):	

Report Summary of Peak Rates Only

Attach model input and output data or other calculations to support the rates reported below.

	<i>Peak Discharge Rates (cfs)</i>			
	Pre-Construction	Post-Construction	Net Change	
2-Year Storm:	5.02	2.51	-2.51	<i>Rate Control Satisfied</i>
10-Year Storm:	19.34	7.23	-12.11	<i>Rate Control Satisfied</i>
50-Year Storm:	42.19	17.45	-24.74	<i>Rate Control Satisfied</i>
100-Year Storm:	54.74	26.78	-27.96	<i>Rate Control Satisfied</i>

Water Quality

Project: The Westtown School - Oak Lane Project

PRINT

Instructions

General

Volume

Rate

Quality

Pre-Construction Pollutant Loads:

Land Cover (from Volume Worksheet)	Land Cover for Water Quality	Area (acres)	Soil Group	Runoff Volume (cf)	Pollutant Conc. (mg/L)			Pollutant Loads (lbs)		
					TSS	TP	TN	TSS	TP	TN
Impervious Areas: Paved Parking Lots, Roofs, Driveways, Etc. (Excluding ROW)	Residential	0.01	B	88	65.0	0.29	2.05	0.36	0.00	0.01
Pervious as Meadow	Grassland/Herbaceous	11.53	B	15,168	48.8	0.22	2.30	46.22	0.21	2.18
Impervious as Meadow	Grassland/Herbaceous	0.00	B	3	48.8	0.22	2.30	0.01	0.00	0.00
Pervious as Meadow	Grassland/Herbaceous	1.14	D	5,471	48.8	0.22	2.30	16.67	0.08	0.79
TOTAL (ACRES):		12.68			TOTALS:			63.26	0.29	2.98

Post-Construction Pollutant Loads (without BMPs):

Land Cover (from Volume Worksheet)	Land Cover for Water Quality	Area (acres)	Soil Group	Runoff Volume (cf)	Pollutant Conc. (mg/L)			Pollutant Loads (lbs)		
					TSS	TP	TN	TSS	TP	TN
Impervious Areas: Paved Parking Lots, Roofs, Driveways, Etc. (Excluding ROW)	Residential	4.74	B	52,121	65.0	0.29	2.05	211.55	0.94	6.67

Open Space (Lawns, Parks, Golf Courses, Cemeteries, Etc.) - Good Condition (Grass Cover > 75%)	Open Space	7.13	B	12,130	78.0	0.25	1.25	59.08	0.19	0.95
Open Space (Lawns, Parks, Golf Courses, Cemeteries, Etc.) - Good Condition (Grass Cover > 75%)	Open Space	1.14	D	6,014	78.0	0.25	1.25	29.29	0.09	0.47

TOTAL (ACRES): 13.02

TOTALS: 299.92 1.23 8.09

POLLUTANT LOAD REDUCTION REQUIREMENTS (LBS): 236.66 0.94 5.11

Characterize Undetained Areas (for Untreated Stormwater)

Land Cover	Area (acres)	Soil Group	CN	Ia (in)	Q Runoff (in)	Runoff Volume (cf)

Non-Structural BMP Water Quality Credits:

- Pervious Undetained Area Credit
- Other (attach calculations)

Structural BMP Water Quality Credits:

Use default BMP Outflows and Median BMP Outflow Concentrations

DP No.	BMP No.	BMP Name	MRC?	BMP DA (acres)	Vol. Routed to BMP (CF)	Inf. & ET Credits (CF)	Capture & Buffer Credits (CF)	Outflow (CF)	Outflow Conc. (mg/L)			Pollutant Loads (lbs)		
									TSS	TP	TN	TSS	TP	TN
002	2	Infiltration Bed		2.22	24,426	24,426		0	-	-	-	-	-	-
002	3	Infiltration Bed		2.22	24,426	24,357		69	-	-	-	-	-	-
002	4	Infiltration Basin		9.74	14,912	14,912		0	10.00	0.24	0.96	0.00	0.00	0.00

	TSS	TP	TN
POLLUTANT LOADS FROM STRUCTURAL BMP (TREATED) OUTFLOWS (LBS):	0.00	0.00	0.00
POLLUTANT LOADS FROM UNTREATED STORMWATER (LBS):	28.04	0.11	0.76
NON-STRUCTURAL BMP WATER QUALITY CREDITS (LBS):			
NET POLLUTANT LOADS FROM SITE, POST-CONSTRUCTION (LBS):	28.04	0.11	0.76
POLLUTANT LOADS FROM SITE, PRE-CONSTRUCTION (LBS):	63.26	0.29	2.98

WATER QUALITY REQUIREMENT SATISFIED

CERTIFICATION

I certify under penalty of law and subject to the penalties of 18 Pa.C.S. § 4904 (relating to unsworn falsification to authorities) that this document and all attachments were prepared under my direction or supervision in accordance with a system designed to assure that qualified personnel properly gathered and evaluated the information submitted. Based on my inquiry of the person or persons who manage the system, or those persons directly responsible for gathering the information, the information submitted is, to the best of my knowledge and belief, true, accurate, and complete. I further certify that the structure, function, and calculations contained in this spreadsheet have not been modified in comparison to the spreadsheet DEP has posted to its website or, if modifications were made, an explanation of the modifications made is attached to this spreadsheet.

Tyler E. Hill, PE

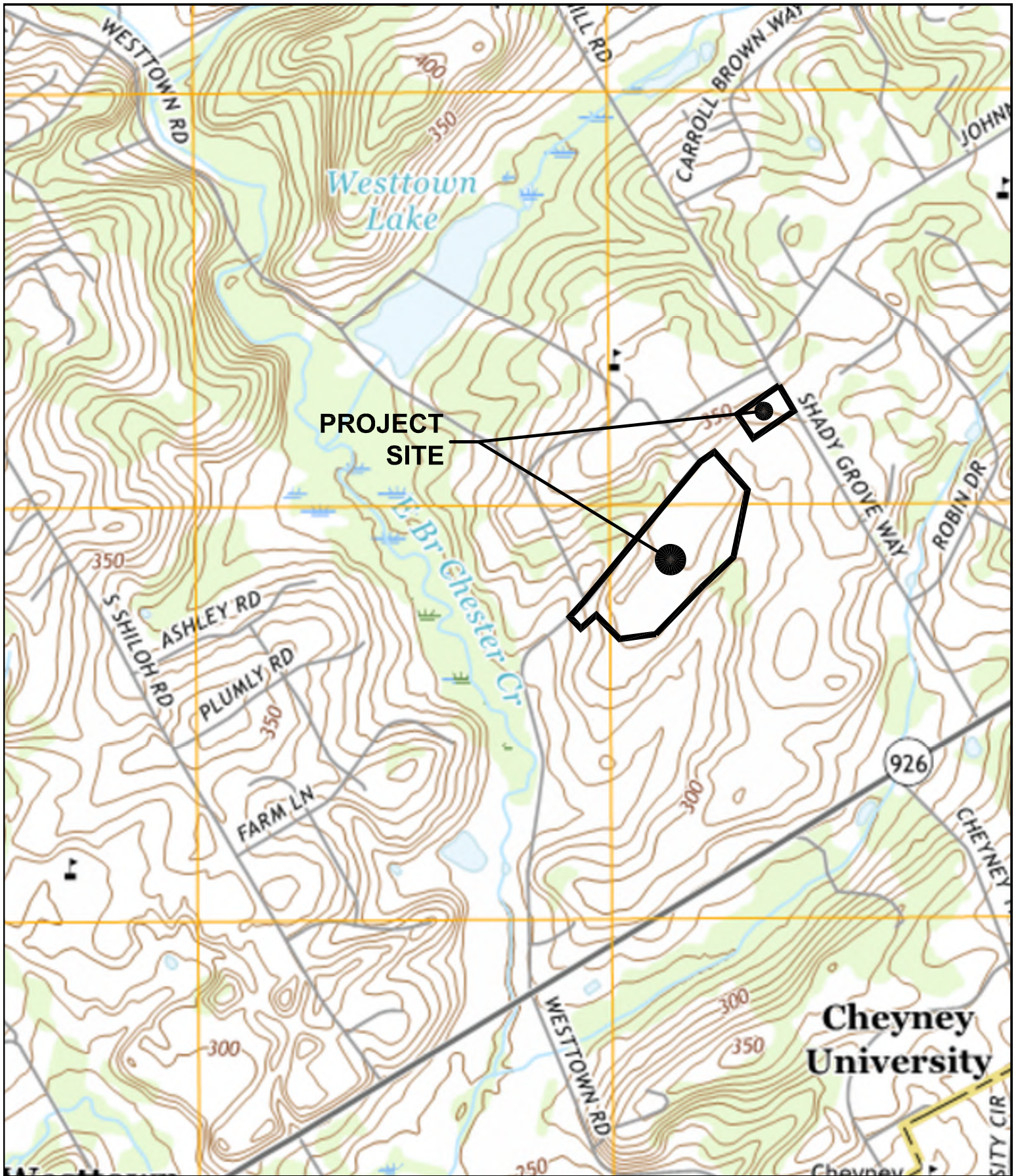
Spreadsheet User Name

9/17/2023

Date

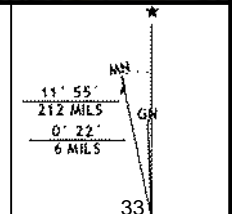
APPENDIX C

REFERENCE & SUPPORTING DOCUMENTS

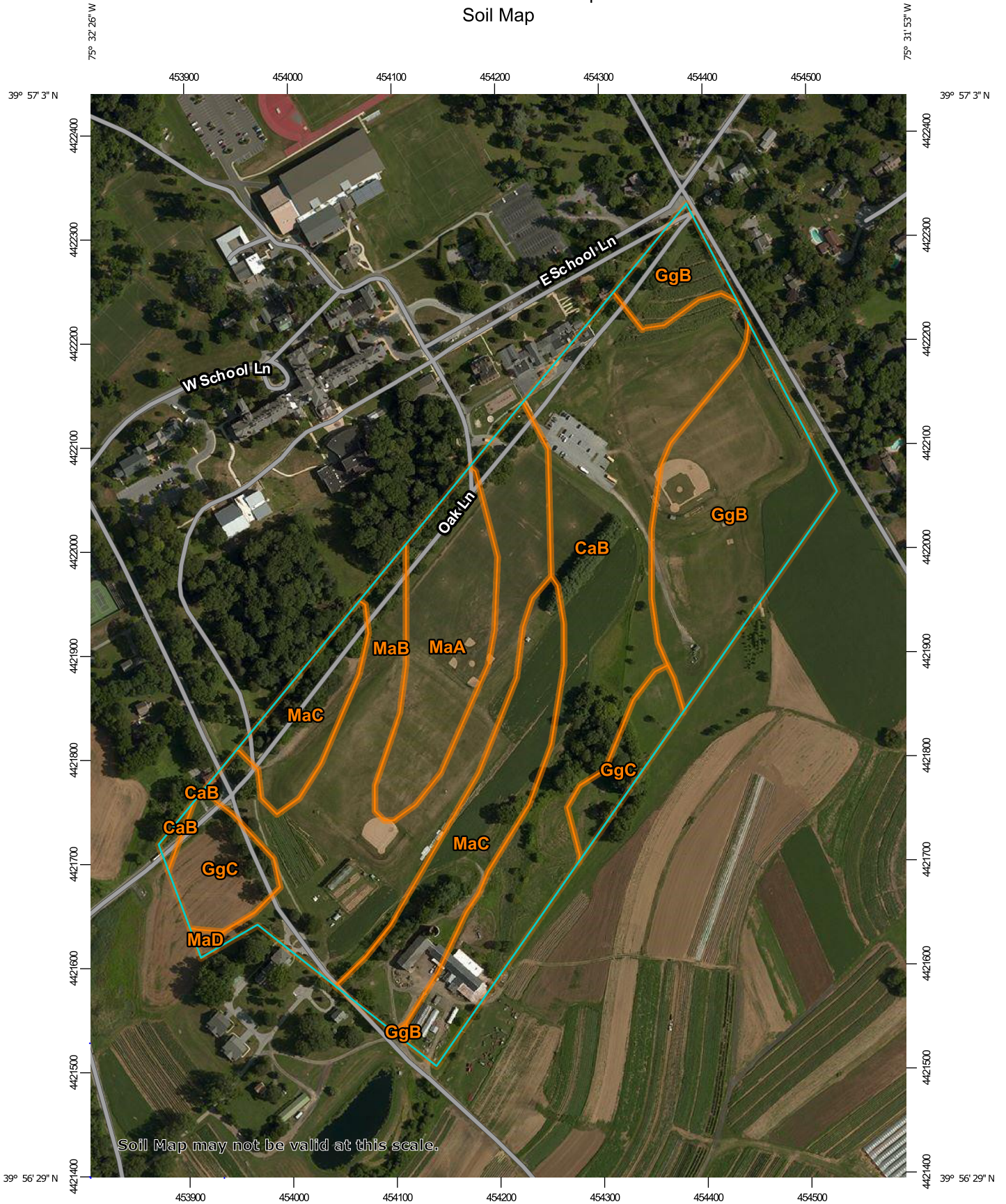


USGS 7.5 MINUTE
WEST CHESTER, PA QUADRANGLE

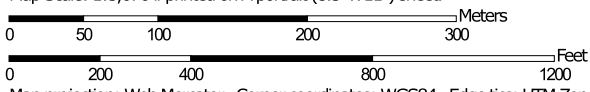
SCALE IN FEET: 1" = 1000



Custom Soil Resource Report Soil Map



Map Scale: 1:5,070 if printed on A portrait (8.5" x 11") sheet.



Map projection: Web Mercator Corner coordinates: WGS84 Edge tics: UTM Zone 18N WGS84

Map Unit Legend

Map Unit Symbol	Map Unit Name	Acres in AOI	Percent of AOI
CaB	Califon loam, 3 to 8 percent slopes	16.5	28.4%
GgB	Glenelg silt loam, 3 to 8 percent slopes	10.4	17.9%
GgC	Glenelg silt loam, 8 to 15 percent slopes	4.0	6.9%
MaA	Manor loam, 0 to 3 percent slopes	5.5	9.4%
MaB	Manor loam, 3 to 8 percent slopes	12.9	22.2%
MaC	Manor loam, 8 to 15 percent slopes	8.7	15.0%
MaD	Manor loam, 15 to 25 percent slopes	0.1	0.2%
Totals for Area of Interest		58.1	100.0%

Map Unit Descriptions

The map units delineated on the detailed soil maps in a soil survey represent the soils or miscellaneous areas in the survey area. The map unit descriptions, along with the maps, can be used to determine the composition and properties of a unit.

A map unit delineation on a soil map represents an area dominated by one or more major kinds of soil or miscellaneous areas. A map unit is identified and named according to the taxonomic classification of the dominant soils. Within a taxonomic class there are precisely defined limits for the properties of the soils. On the landscape, however, the soils are natural phenomena, and they have the characteristic variability of all natural phenomena. Thus, the range of some observed properties may extend beyond the limits defined for a taxonomic class. Areas of soils of a single taxonomic class rarely, if ever, can be mapped without including areas of other taxonomic classes. Consequently, every map unit is made up of the soils or miscellaneous areas for which it is named and some minor components that belong to taxonomic classes other than those of the major soils.

Most minor soils have properties similar to those of the dominant soil or soils in the map unit, and thus they do not affect use and management. These are called noncontrasting, or similar, components. They may or may not be mentioned in a particular map unit description. Other minor components, however, have properties and behavioral characteristics divergent enough to affect use or to require different management. These are called contrasting, or dissimilar, components. They generally are in small areas and could not be mapped separately because of the scale used. Some small areas of strongly contrasting soils or miscellaneous areas are identified by a special symbol on the maps. If included in the database for a given area, the contrasting minor components are identified in the map unit

Job Number: 1091-001

Date: 10/25/2018

SOILS INFORMATION FACT SHEET

SOIL							SUITABILITY					SOIL CONDITIONS FOR CONSTRUCTION			
SYMBOL NAME	TEXTURE	SLOPE, %	HYDRO. SOIL GROUP	HYDRIC (INCLUSIONS)	ERODIBILITY (K)	DEPTH OF WATER TABLE (IN)	DEPTH TO BEDROCK (IN)	WINTER GRADING	FROST ACTION	SURFACE WATER MANAGEMENT	BUILDING SITE	ROADFILL	TOPSOIL		
CaB Califon	Loam	3 to 8	D		0.32	6 to 36	72 to 99	Limited	High	Somewhat Limited	Very Limited	Fair	Fair		
GgC Glenelg	Silt Loam	8 to 15	B		0.37	80+	80+	Somewhat Limited	Moderate	Very Limited	Very Limited	Fair	Fair		
MaA Manor	Loam	0 to 3	B		0.28	80+	72 to 99	Somewhat Limited	Moderate	Not Limited	Somewhat Limited	Poor	Fair		
MaB Manor	Loam	3 to 8	B		0.28	80+	72 to 99	Somewhat Limited	Moderate	Very Limited	Somewhat Limited	Poor	Fair		
MaC Manor	Loam	8 to 15	B		0.28	80+	59 to 100	Somewhat Limited	Moderate	Very Limited	Very Limited	Poor	Poor		

SOIL LIMITATIONS & RESOLUTIONS					
SOIL	LIMITATIONS		CHARACTERISTICS	RESOLUTIONS	COMMENTS
CaB GgC MaA MaB Mac	Cutbanks Cave	Excavations	The walls of excavations tend to cave in or slough	It is imperative that appropriate precautions be taken to safeguard workers during all trenching and excavation operations.	All applicable OSHA standards and regulations must be implemented at all times.
CaB (C/S) GgC (C) MaA (C) MaB (C) MaC (C)	Corrosive to Concrete/ Steel	Foundation and other infrastructural materials that may contact the soil	Weakening or dissolution of concrete or uncoated steel caused by soil-induced electrochemical or chemical action.	Suitable precautions should be taken to protect all underground pipes, conduits, and storage tanks from concrete and steel corrosion. If potential corrosive properties are encountered during construction, impacted utilities in that area shall be backfilled with processed aggregate to reduce the potential of corrosion from soil backfill.	Refer to the Geotechnical Report
GgC MaA MaB MaC	Erodibility	Grassed Waterways Terraces Slopes Stabilization Landscaping	Easily Erodible Rill and/or Gully Erosion	Excavation should occur during low-rainfall periods when possible Minimize duration of earth disturbance Immediately stabilize with erosion control matting, mulch, or sod. Avoid concentrating runoff in disturbed areas	See Erosion and Sediment Control Plan
CaB	Depth to Saturated Zone/ Seasonal High Water Table	Buildings w/ basements Excavations Stormwater Facilities	High table Wetness Soil mottling	Suitable precautions should be taken if water is encountered Contractor is to utilize pumping techniques and other methods as recommended by a Geotechnical Engineer.	Contact Geotechnical Engineer if shallow groundwater is encountered
CaB GgC MaA MaB Mac	Frost Action	Winter Grading	Frost heaving or upward swelling of soil during freezing conditons.	Do not grade, fill, or backfill during periods of freezing temperatures. Proper precautions should be taken to prevent damage, especially to roadways.	
GgC	Hydric/ Hydric Inclusions	unless authorized by DEP and/or ACOE if wetlands present	Wetlands Wetness	Delineate and Protect Wetlands Obtain all permits/authorizations Utilize pumping techniques where appropriate	See wetland delineation report
CaB GgC MaA MaB MaC	Low Strength/ Landslide Prone	Steep Slopes Structural Fill	Low strength soils are prone failure on steep slopes.	Precautions should be taken to prevent slope failures due to improper construction practices such as over-steepening and overloading of slopes, removal of lateral support, and failure to prevent saturation of slopes. Setbacks should comply with the standards contained in Chapter 16 unless it can be shown that proposed cuts and fills do not pose a hazard to public safety or to surface waters. Road fill/other structural fill material will likely need to be imported in areas where soils have low strength.	See geotechnical engineering report or consult the geotechnical professional on record
CaB GgC MaA MaB MaC	Slow Percolation	Stormwater Infiltration On-lot Sewage Facilities	Wetness Soil mottling Shallow groundwater	Soil testing should be performed if infiltration BMPs or on-lot sewage facilities are proposed. Ammend soils with compost and/or sand.	See geotechnical engineering report or consult the geotechnical professional on record See Appendix A of the PA Stormwater BMP Manual
GgC MaA MaB MaC	Piping		Formation of subsurface tunnels or pipelike cavities by water moving through the soil	Avoid concentrating runoff. Avoid infiltrating in areas with excessive infiltration rates. Install trench plugs, anti-seep collars, key trenches, etc.	See plans See geotechnical engineering report or consult the geotechnical professional on record
GgC MaA MaB MaC	Poor Source of Topsoil	Vegetative Growth/ Stabilization	Low Fertility Droughty or Wet High Acidity	Soil Testing and appropriate supplementation. Soil amendment/restoration practices	See plan notes
CaB GgC GgC	Wetness	Site work/grading Fill operations	Slow percolation Soil Mottling Shallow groundwater	Concrete stabilization Undercut and replace with suitable material Provide positive drainage	See geotechnical report or consult geotechnical engineer on record

ORDINANCE APPENDIX C

RUNOFF COEFFICIENTS AND CURVE NUMBERS

TABLE C-1. RUNOFF CURVE NUMBERS

Source: Table 2-2a, Table 2-2b, and Table 2-2c from U. S. Department of Agriculture, Natural Resources Conservation Service, June 1986, Urban Hydrology for Small Watersheds, Technical Release No. 55 (TR-55), Second Edition.

TABLE C-2. RATIONAL RUNOFF COEFFICIENTS

Source: Table F.2 from Delaware County Planning Department, December 2011, Crum Creek Watershed Act 167 Stormwater Management Plan.

TABLE C-3. MANNING'S 'n' VALUES

Source: Table 3-1 from United States Army Corps of Engineers, January 2010, HEC-RAS River Analysis System, Hydraulic Reference Manual, Version 4.1.

FIGURE C-1. REDEVELOPMENT PROJECTS RUNOFF CRITERIA ADJUSTMENT FOR PRE-DEVELOPMENT CONDITIONS

Source: Figure B-3 from the Delaware County Planning Department and Chester County Planning Commission, June 2002, Act 167 Stormwater Management Plan Chester Creek Watershed.

TABLE C-1. RUNOFF CURVE NUMBERS

(3 pages)

Source: Table 2-2a, Table 2-2b, and Table 2-2c from U. S. Department of Agriculture, Natural Resources Conservation Service, June 1986, Urban Hydrology for Small Watersheds, Technical Release No. 55 (TR-55), Second Edition.

TABLE C-2. RATIONAL RUNOFF COEFFICIENTS

(1 page)

Source: Table F.2 from Delaware County Planning Department, December 2011,
Crum Creek Watershed Act 167 Stormwater Management Plan.

TABLE C-3. MANNING'S 'n' VALUES
(3 pages)

Source: Table 3-1 from United States Army Corps of Engineers, January 2010,
HEC-RAS River Analysis System, Hydraulic Reference Manual, Version 4.1.

Table 2-2a Runoff curve numbers for urban areas ^{1/}

Cover description	Average percent impervious area ^{2/}	Curve numbers for hydrologic soil group			
		A	B	C	D
<i>Fully developed urban areas (vegetation established)</i>					
Open space (lawns, parks, golf courses, cemeteries, etc.) ^{3/} :					
Poor condition (grass cover < 50%)		68	79	86	89
Fair condition (grass cover 50% to 75%)		49	69	79	84
Good condition (grass cover > 75%)		39	61	74	80
Impervious areas:					
Paved parking lots, roofs, driveways, etc. (excluding right-of-way)		98	98	98	98
Streets and roads:					
Paved; curbs and storm sewers (excluding right-of-way)		98	98	98	98
Paved; open ditches (including right-of-way)		83	89	92	93
Gravel (including right-of-way)		76	85	89	91
Dirt (including right-of-way)		72	82	87	89
Western desert urban areas:					
Natural desert landscaping (pervious areas only) ^{4/}		63	77	85	88
Artificial desert landscaping (impervious weed barrier, desert shrub with 1- to 2-inch sand or gravel mulch and basin borders)		96	96	96	96
Urban districts:					
Commercial and business	85	89	92	94	95
Industrial	72	81	88	91	93
Residential districts by average lot size:					
1/8 acre or less (town houses)	65	77	85	90	92
1/4 acre	38	61	75	83	87
1/3 acre	30	57	72	81	86
1/2 acre	25	54	70	80	85
1 acre	20	51	68	79	84
2 acres	12	46	65	77	82
<i>Developing urban areas</i>					
Newly graded areas (pervious areas only, no vegetation) ^{5/}		77	86	91	94
Idle lands (CN's are determined using cover types similar to those in table 2-2c).					

¹ Average runoff condition, and $I_a = 0.2S$.² The average percent impervious area shown was used to develop the composite CN's. Other assumptions are as follows: impervious areas are directly connected to the drainage system, impervious areas have a CN of 98, and pervious areas are considered equivalent to open space in good hydrologic condition. CN's for other combinations of conditions may be computed using figure 2-3 or 2-4.³ CN's shown are equivalent to those of pasture. Composite CN's may be computed for other combinations of open space cover type.⁴ Composite CN's for natural desert landscaping should be computed using figures 2-3 or 2-4 based on the impervious area percentage (CN = 98) and the pervious area CN. The pervious area CN's are assumed equivalent to desert shrub in poor hydrologic condition.⁵ Composite CN's to use for the design of temporary measures during grading and construction should be computed using figure 2-3 or 2-4 based on the degree of development (impervious area percentage) and the CN's for the newly graded pervious areas.

Table 2-2b Runoff curve numbers for cultivated agricultural lands ^{1/}

Cover description			Curve numbers for hydrologic soil group			
Cover type	Treatment ^{2/}	Hydrologic condition ^{3/}	A	B	C	D
Fallow	Bare soil	—	77	86	91	94
	Crop residue cover (CR)	Poor	76	85	90	93
		Good	74	83	88	90
Row crops	Straight row (SR)	Poor	72	81	88	91
		Good	67	78	85	89
	SR + CR	Poor	71	80	87	90
		Good	64	75	82	85
	Contoured (C)	Poor	70	79	84	88
		Good	65	75	82	86
	C + CR	Poor	69	78	83	87
		Good	64	74	81	85
	Contoured & terraced (C&T)	Poor	66	74	80	82
		Good	62	71	78	81
C&T+ CR	Poor	65	73	79	81	
	Good	61	70	77	80	
Small grain	SR	Poor	65	76	84	88
		Good	63	75	83	87
	SR + CR	Poor	64	75	83	86
		Good	60	72	80	84
	C	Poor	63	74	82	85
		Good	61	73	81	84
	C + CR	Poor	62	73	81	84
		Good	60	72	80	83
	C&T	Poor	61	72	79	82
		Good	59	70	78	81
C&T+ CR	Poor	60	71	78	81	
	Good	58	69	77	80	
Close-seeded or broadcast legumes or rotation meadow	SR	Poor	66	77	85	89
		Good	58	72	81	85
	C	Poor	64	75	83	85
		Good	55	69	78	83
	C&T	Poor	63	73	80	83
Good	51	67	76	80		

¹ Average runoff condition, and $I_a=0.2S$

² Crop residue cover applies only if residue is on at least 5% of the surface throughout the year.

³ Hydraulic condition is based on combination factors that affect infiltration and runoff, including (a) density and canopy of vegetative areas, (b) amount of year-round cover, (c) amount of grass or close-seeded legumes, (d) percent of residue cover on the land surface (good $\geq 20\%$), and (e) degree of surface roughness.

Poor: Factors impair infiltration and tend to increase runoff.

Good: Factors encourage average and better than average infiltration and tend to decrease runoff.

Table 2-2c Runoff curve numbers for other agricultural lands ^{1/}

Cover description	Hydrologic condition	Curve numbers for hydrologic soil group			
		A	B	C	D
Pasture, grassland, or range—continuous forage for grazing. ^{2/}	Poor	68	79	86	89
	Fair	49	69	79	84
	Good	39	61	74	80
Meadow—continuous grass, protected from grazing and generally mowed for hay.	—	30	58	71	78
Brush—brush-weed-grass mixture with brush the major element. ^{3/}	Poor	48	67	77	83
	Fair	35	56	70	77
	Good	30 ^{4/}	48	65	73
Woods—grass combination (orchard or tree farm). ^{5/}	Poor	57	73	82	86
	Fair	43	65	76	82
	Good	32	58	72	79
Woods. ^{6/}	Poor	45	66	77	83
	Fair	36	60	73	79
	Good	30 ^{4/}	55	70	77
Farmsteads—buildings, lanes, driveways, and surrounding lots.	—	59	74	82	86

^{1/} Average runoff condition, and $I_a = 0.2S$.^{2/} *Poor*: <50% ground cover or heavily grazed with no mulch.*Fair*: 50 to 75% ground cover and not heavily grazed.*Good*: > 75% ground cover and lightly or only occasionally grazed.^{3/} *Poor*: <50% ground cover.*Fair*: 50 to 75% ground cover.*Good*: >75% ground cover.^{4/} Actual curve number is less than 30; use CN = 30 for runoff computations.^{5/} CN's shown were computed for areas with 50% woods and 50% grass (pasture) cover. Other combinations of conditions may be computed from the CN's for woods and pasture.^{6/} *Poor*: Forest litter, small trees, and brush are destroyed by heavy grazing or regular burning.*Fair*: Woods are grazed but not burned, and some forest litter covers the soil.*Good*: Woods are protected from grazing, and litter and brush adequately cover the soil.

Table 3-1 Manning's 'n' Values

Type of Channel and Description	Minimum	Normal	Maximum
A. Natural Streams			
1. Main Channels			
a. Clean, straight, full, no rifts or deep pools			
b. Same as above, but more stones and weeds	0.025	0.030	0.033
c. Clean, winding, some pools and shoals	0.030	0.035	0.040
d. Same as above, but some weeds and stones	0.033	0.040	0.045
e. Same as above, lower stages, more ineffective slopes and sections	0.035	0.045	0.050
f. Same as "d" but more stones	0.040	0.048	0.055
g. Sluggish reaches, weedy, deep pools	0.045	0.050	0.060
h. Very weedy reaches, deep pools, or floodways with heavy stands of timber and brush	0.050	0.070	0.080
	0.070	0.100	0.150
2. Flood Plains			
a. Pasture no brush			
1. Short grass	0.025	0.030	0.035
2. High grass	0.030	0.035	0.050
b. Cultivated areas			
1. No crop	0.020	0.030	0.040
2. Mature row crops	0.025	0.035	0.045
3. Mature field crops	0.030	0.040	0.050
c. Brush			
1. Scattered brush, heavy weeds	0.035	0.050	0.070
2. Light brush and trees, in winter	0.035	0.050	0.060
3. Light brush and trees, in summer	0.040	0.060	0.080
4. Medium to dense brush, in winter	0.045	0.070	0.110
5. Medium to dense brush, in summer	0.070	0.100	0.160
d. Trees			
1. Cleared land with tree stumps, no sprouts	0.030	0.040	0.050
2. Same as above, but heavy sprouts	0.050	0.060	0.080
3. Heavy stand of timber, few down trees, little undergrowth, flow below branches	0.080	0.100	0.120
4. Same as above, but with flow into branches	0.100	0.120	0.160
5. Dense willows, summer, straight	0.110	0.150	0.200
3. Mountain Streams, no vegetation in channel, banks usually steep, with trees and brush on banks submerged			
a. Bottom: gravels, cobbles, and few boulders	0.030	0.040	0.050
b. Bottom: cobbles with large boulders	0.040	0.050	0.070

Table 3-1 (Continued) Manning's 'n' Values

Type of Channel and Description	Minimum	Normal	Maximum
B. Lined or Built-Up Channels			
1. Concrete			
a. Trowel finish	0.011	0.013	0.015
b. Float Finish	0.013	0.015	0.016
c. Finished, with gravel bottom	0.015	0.017	0.020
d. Unfinished	0.014	0.017	0.020
e. Gunit, good section	0.016	0.019	0.023
f. Gunit, wavy section	0.018	0.022	0.025
g. On good excavated rock	0.017	0.020	
h. On irregular excavated rock	0.022	0.027	
2. Concrete bottom float finished with sides of:			
a. Dressed stone in mortar	0.015	0.017	0.020
b. Random stone in mortar	0.017	0.020	0.024
c. Cement rubble masonry, plastered	0.016	0.020	0.024
d. Cement rubble masonry	0.020	0.025	0.030
e. Dry rubble on riprap	0.020	0.030	0.035
3. Gravel bottom with sides of:			
a. Formed concrete	0.017	0.020	0.025
b. Random stone in mortar	0.020	0.023	0.026
c. Dry rubble or riprap	0.023	0.033	0.036
4. Brick			
a. Glazed	0.011	0.013	0.015
b. In cement mortar	0.012	0.015	0.018
5. Metal			
a. Smooth steel surfaces	0.011	0.012	0.014
b. Corrugated metal	0.021	0.025	0.030
6. Asphalt			
a. Smooth	0.013	0.013	
b. Rough	0.016	0.016	
7. Vegetal lining			
	0.030		0.500

Table 3-1 (Continued) Manning's 'n' Values

Type of Channel and Description	Minimum	Normal	Maximum
<i>C. Excavated or Dredged Channels</i>			
1. Earth, straight and uniform			
a. Clean, recently completed	0.016	0.018	0.020
b. Clean, after weathering	0.018	0.022	0.025
c. Gravel, uniform section, clean	0.022	0.025	0.030
d. With short grass, few weeds	0.022	0.027	0.033
2. Earth, winding and sluggish			
a. No vegetation	0.023	0.025	0.030
b. Grass, some weeds	0.025	0.030	0.033
c. Dense weeds or aquatic plants in deep channels	0.030	0.035	0.040
d. Earth bottom and rubble side	0.028	0.030	0.035
e. Stony bottom and weedy banks	0.025	0.035	0.040
f. Cobble bottom and clean sides	0.030	0.040	0.050
3. Dragline-excavated or dredged			
a. No vegetation	0.025	0.028	0.033
b. Light brush on banks	0.035	0.050	0.060
4. Rock cuts			
a. Smooth and uniform	0.025	0.035	0.040
b. Jagged and irregular	0.035	0.040	0.050
5. Channels not maintained, weeds and brush			
a. Clean bottom, brush on sides	0.040	0.050	0.080
b. Same as above, highest stage of flow	0.045	0.070	0.110
c. Dense weeds, high as flow depth	0.050	0.080	0.120
d. Dense brush, high stage	0.080	0.100	0.140

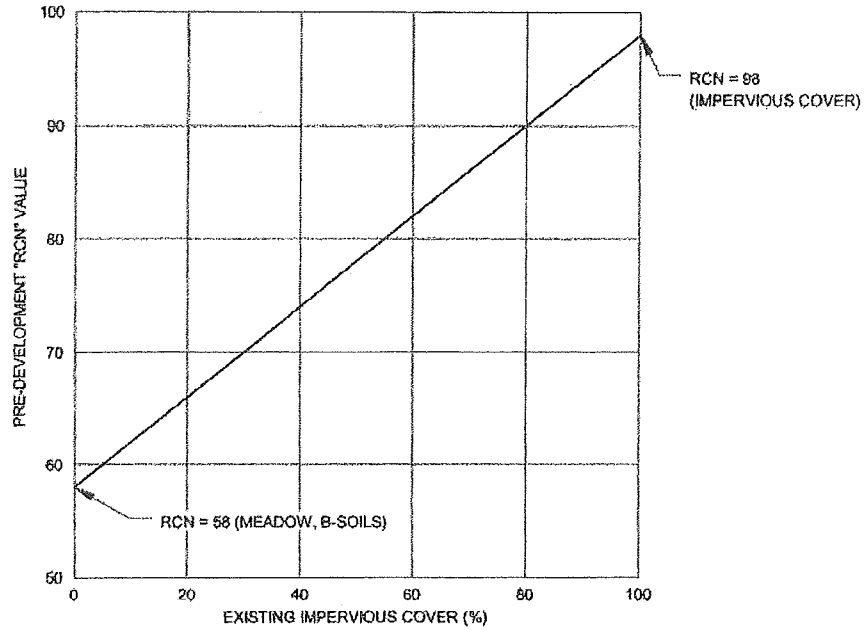
Other sources that include pictures of selected streams as a guide to n value determination are available (Fasken, 1963; Barnes, 1967; and Hicks and Mason, 1991). In general, these references provide color photos with tables of calibrated n values for a range of flows.

Although there are many factors that affect the selection of the n value for the channel, some of the most important factors are the type and size of materials that compose the bed and banks of a channel, and the shape of the channel. Cowan (1956) developed a procedure for estimating the effects of these factors to determine the value of Manning's n of a channel. In Cowan's procedure, the value of n is computed by the following equation:

FIGURE C-1

REDEVELOPMENT PROJECTS
RUNOFF CRITERIA ADJUSTMENT FOR PRE-DEVELOPMENT CONDITIONS

NRCS METHODOLOGY
RCN ADJUSTMENT



RATIONAL FORMULA
C ADJUSTMENT

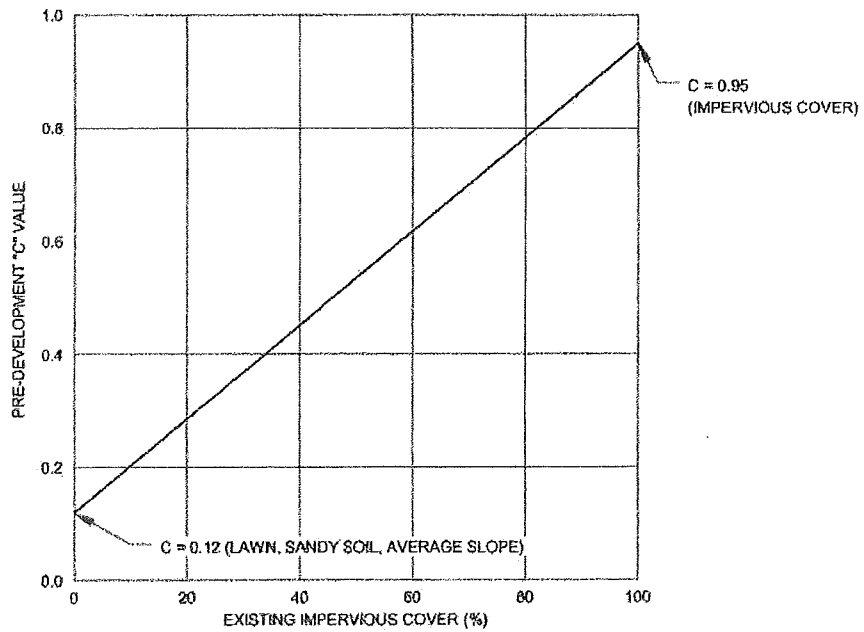
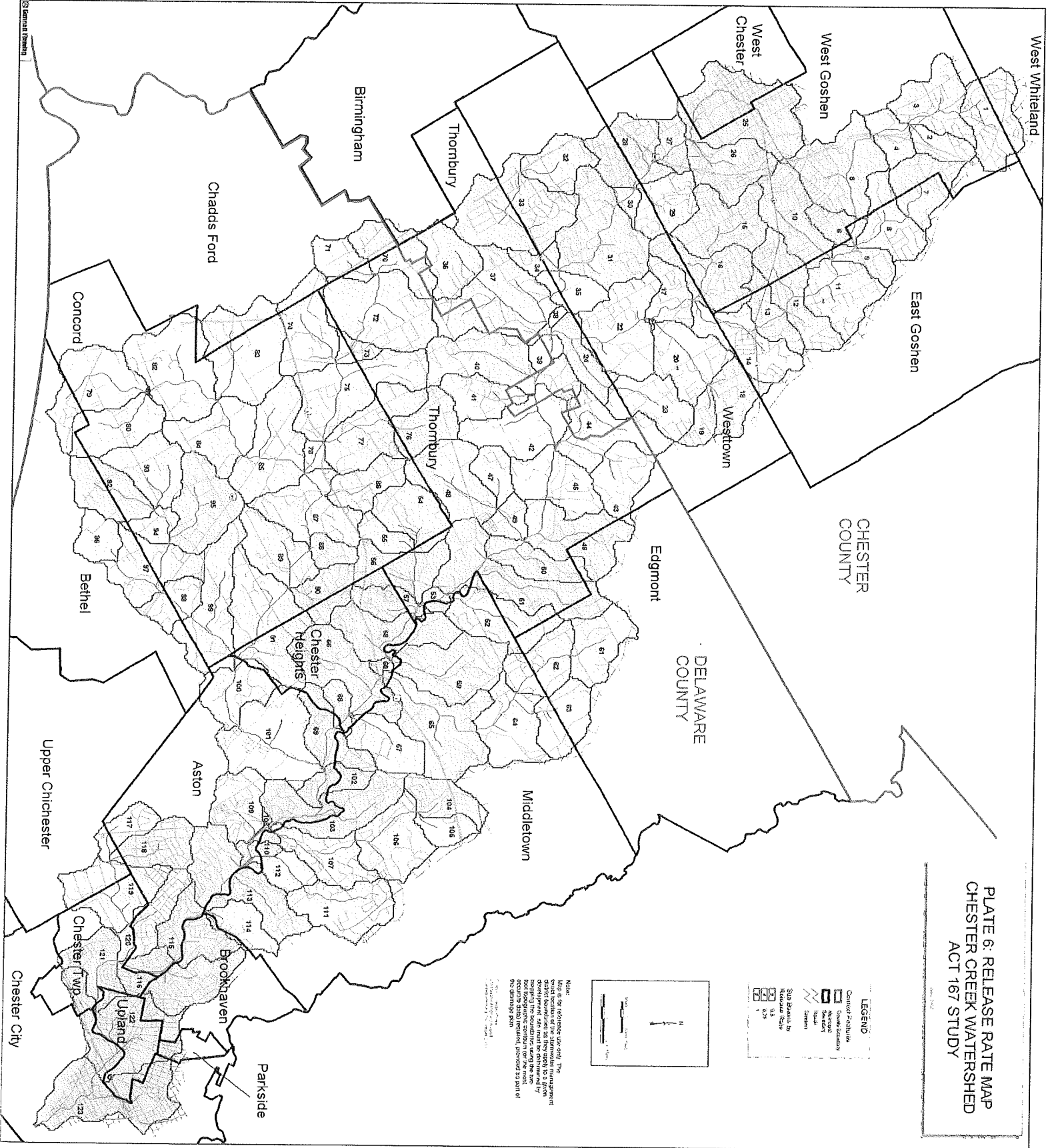
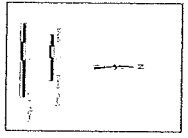


PLATE 6: RELEASE RATE MAP
 CHESTER CREEK WATERSHED
 ACT 167 STUDY



LEGEND

Control Structure	1:50,000 Scale
Service Station	1:50,000 Scale
Manhole	1:50,000 Scale
Head	1:50,000 Scale
Stream	1:50,000 Scale
State Boundary by Release Act	1:50,000 Scale
1	1:50,000 Scale
2	1:50,000 Scale
3	1:50,000 Scale
4	1:50,000 Scale
5	1:50,000 Scale
6	1:50,000 Scale
7	1:50,000 Scale
8	1:50,000 Scale
9	1:50,000 Scale
10	1:50,000 Scale
11	1:50,000 Scale
12	1:50,000 Scale
13	1:50,000 Scale
14	1:50,000 Scale
15	1:50,000 Scale
16	1:50,000 Scale
17	1:50,000 Scale
18	1:50,000 Scale
19	1:50,000 Scale
20	1:50,000 Scale
21	1:50,000 Scale
22	1:50,000 Scale
23	1:50,000 Scale
24	1:50,000 Scale
25	1:50,000 Scale
26	1:50,000 Scale
27	1:50,000 Scale
28	1:50,000 Scale
29	1:50,000 Scale
30	1:50,000 Scale
31	1:50,000 Scale
32	1:50,000 Scale
33	1:50,000 Scale
34	1:50,000 Scale
35	1:50,000 Scale
36	1:50,000 Scale
37	1:50,000 Scale
38	1:50,000 Scale
39	1:50,000 Scale
40	1:50,000 Scale
41	1:50,000 Scale
42	1:50,000 Scale
43	1:50,000 Scale
44	1:50,000 Scale
45	1:50,000 Scale
46	1:50,000 Scale
47	1:50,000 Scale
48	1:50,000 Scale
49	1:50,000 Scale
50	1:50,000 Scale
51	1:50,000 Scale
52	1:50,000 Scale
53	1:50,000 Scale
54	1:50,000 Scale
55	1:50,000 Scale
56	1:50,000 Scale
57	1:50,000 Scale
58	1:50,000 Scale
59	1:50,000 Scale
60	1:50,000 Scale
61	1:50,000 Scale
62	1:50,000 Scale
63	1:50,000 Scale
64	1:50,000 Scale
65	1:50,000 Scale
66	1:50,000 Scale
67	1:50,000 Scale
68	1:50,000 Scale
69	1:50,000 Scale
70	1:50,000 Scale
71	1:50,000 Scale
72	1:50,000 Scale
73	1:50,000 Scale
74	1:50,000 Scale
75	1:50,000 Scale
76	1:50,000 Scale
77	1:50,000 Scale
78	1:50,000 Scale
79	1:50,000 Scale
80	1:50,000 Scale
81	1:50,000 Scale
82	1:50,000 Scale
83	1:50,000 Scale
84	1:50,000 Scale
85	1:50,000 Scale
86	1:50,000 Scale
87	1:50,000 Scale
88	1:50,000 Scale
89	1:50,000 Scale
90	1:50,000 Scale
91	1:50,000 Scale
92	1:50,000 Scale
93	1:50,000 Scale
94	1:50,000 Scale
95	1:50,000 Scale
96	1:50,000 Scale
97	1:50,000 Scale
98	1:50,000 Scale
99	1:50,000 Scale
100	1:50,000 Scale
101	1:50,000 Scale
102	1:50,000 Scale
103	1:50,000 Scale
104	1:50,000 Scale
105	1:50,000 Scale
106	1:50,000 Scale
107	1:50,000 Scale
108	1:50,000 Scale
109	1:50,000 Scale
110	1:50,000 Scale
111	1:50,000 Scale
112	1:50,000 Scale
113	1:50,000 Scale
114	1:50,000 Scale
115	1:50,000 Scale
116	1:50,000 Scale
117	1:50,000 Scale
118	1:50,000 Scale
119	1:50,000 Scale
120	1:50,000 Scale
121	1:50,000 Scale
122	1:50,000 Scale
123	1:50,000 Scale



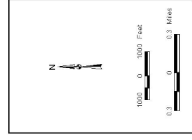
Note:
 Map is for reference use only. The
 exact location of the structure to be
 developed, the location of the
 development site must be determined by
 field investigation. Contact with the
 appropriate authority must be made
 before any construction is started.
 The release rate is based on the
 design flow.

**PLATE 6: RELEASE RATE MAP
CHESTER CREEK WATERSHED
ACT 167 STUDY**

June, 2002

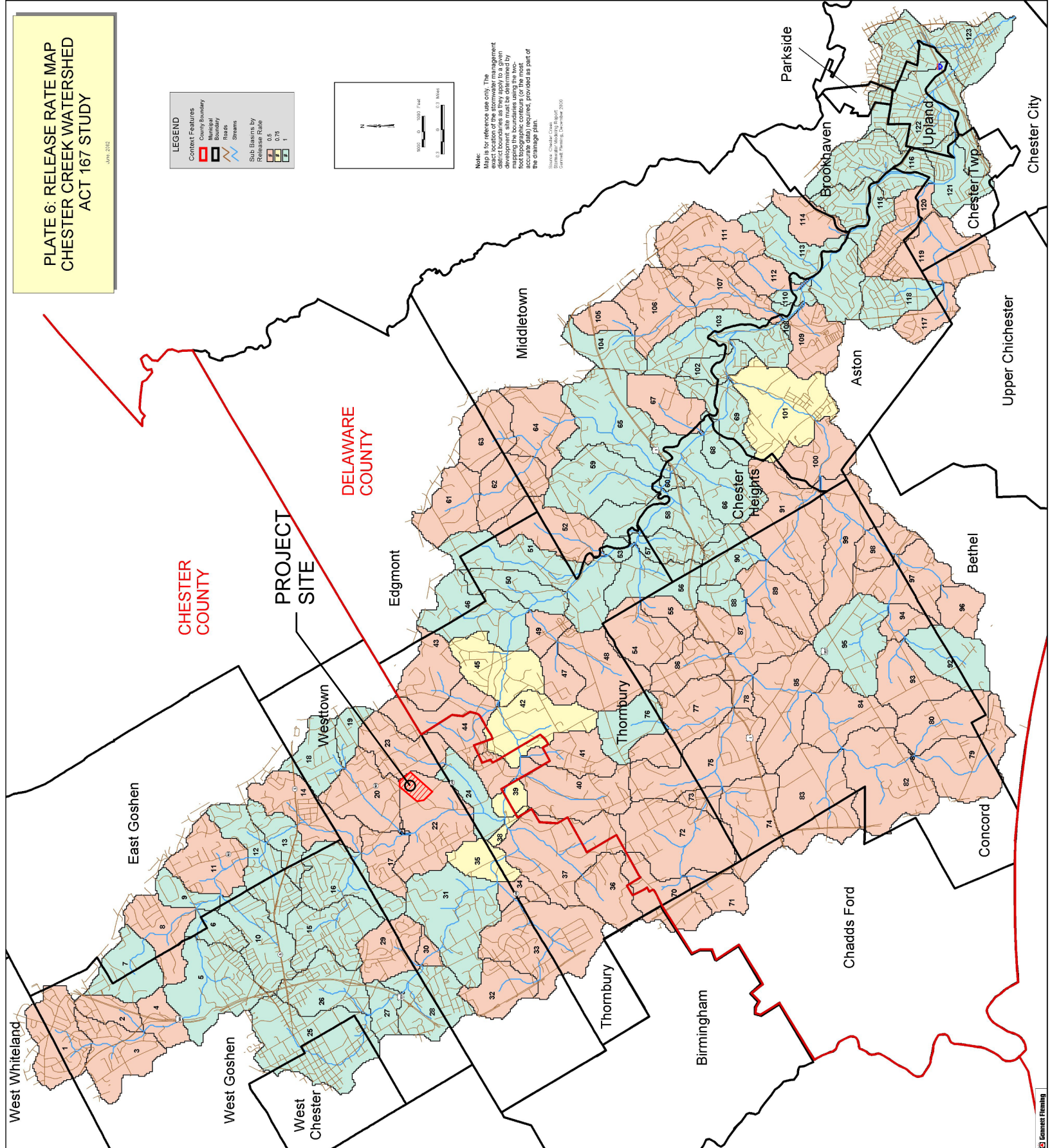
LEGEND

	Context Features
	County Boundary
	Municipal Boundary
	Streams
	Sub Basins by Release Rate
	0.5
	1
	1



Note: Map is for reference use only. The management district boundaries as they apply to a given development site must be determined by foot topographic contours (or the most accurate data) required, provided as part of the drainage plan.

Source: Chester Creek
General Permit, December 2010





NOAA Atlas 14, Volume 2, Version 3
Location name: West Chester, Pennsylvania, USA*
Latitude: 39.9456°, Longitude: -75.5371°
Elevation: 319.37 ft**



* source: ESRI Maps
 ** source: USGS

POINT PRECIPITATION FREQUENCY ESTIMATES

G.M. Bonnin, D. Martin, B. Lin, T. Parzybok, M.Yekta, and D. Riley

NOAA, National Weather Service, Silver Spring, Maryland

[PF tabular](#) | [PF graphical](#) | [Maps & aerials](#)

PF tabular

PDS-based point precipitation frequency estimates with 90% confidence intervals (in inches)¹										
Duration	Average recurrence interval (years)									
	1	2	5	10	25	50	100	200	500	1000
5-min	0.353 (0.323-0.385)	0.421 (0.386-0.459)	0.492 (0.450-0.537)	0.542 (0.495-0.591)	0.600 (0.546-0.655)	0.640 (0.578-0.699)	0.679 (0.611-0.742)	0.712 (0.637-0.781)	0.750 (0.665-0.825)	0.778 (0.684-0.860)
10-min	0.563 (0.517-0.615)	0.673 (0.617-0.734)	0.788 (0.720-0.859)	0.866 (0.791-0.946)	0.957 (0.870-1.04)	1.02 (0.921-1.11)	1.08 (0.971-1.18)	1.13 (1.01-1.24)	1.19 (1.05-1.31)	1.23 (1.08-1.36)
15-min	0.704 (0.646-0.769)	0.846 (0.775-0.923)	0.996 (0.911-1.09)	1.10 (1.00-1.20)	1.21 (1.10-1.32)	1.29 (1.17-1.41)	1.36 (1.23-1.49)	1.42 (1.27-1.56)	1.49 (1.32-1.64)	1.54 (1.35-1.70)
30-min	0.966 (0.885-1.06)	1.17 (1.07-1.27)	1.42 (1.30-1.54)	1.59 (1.45-1.73)	1.80 (1.63-1.96)	1.94 (1.76-2.12)	2.09 (1.88-2.28)	2.22 (1.98-2.43)	2.38 (2.11-2.62)	2.49 (2.19-2.75)
60-min	1.20 (1.10-1.32)	1.47 (1.34-1.60)	1.82 (1.66-1.98)	2.07 (1.89-2.26)	2.39 (2.17-2.61)	2.63 (2.38-2.88)	2.88 (2.59-3.15)	3.11 (2.78-3.41)	3.41 (3.02-3.75)	3.64 (3.20-4.02)
2-hr	1.44 (1.31-1.59)	1.75 (1.59-1.93)	2.17 (1.97-2.40)	2.50 (2.26-2.76)	2.93 (2.63-3.22)	3.27 (2.92-3.60)	3.60 (3.20-3.97)	3.94 (3.47-4.35)	4.39 (3.83-4.86)	4.74 (4.09-5.27)
3-hr	1.56 (1.42-1.73)	1.90 (1.73-2.09)	2.37 (2.15-2.61)	2.73 (2.47-3.01)	3.20 (2.88-3.53)	3.58 (3.20-3.94)	3.96 (3.52-4.36)	4.34 (3.82-4.79)	4.86 (4.22-5.38)	5.25 (4.51-5.83)
6-hr	1.93 (1.75-2.14)	2.33 (2.12-2.58)	2.90 (2.63-3.21)	3.36 (3.03-3.71)	3.99 (3.58-4.41)	4.51 (4.01-4.97)	5.05 (4.45-5.57)	5.61 (4.89-6.19)	6.39 (5.48-7.09)	7.01 (5.93-7.82)
12-hr	2.35 (2.13-2.62)	2.83 (2.57-3.16)	3.55 (3.21-3.95)	4.14 (3.73-4.60)	4.99 (4.45-5.54)	5.71 (5.05-6.33)	6.48 (5.66-7.19)	7.32 (6.30-8.14)	8.53 (7.19-9.51)	9.53 (7.89-10.7)
24-hr	2.71 (2.49-2.96)	3.26 (3.00-3.56)	4.10 (3.76-4.48)	4.80 (4.39-5.23)	5.81 (5.29-6.33)	6.66 (6.03-7.24)	7.58 (6.82-8.23)	8.57 (7.67-9.30)	10.0 (8.87-10.9)	11.2 (9.85-12.2)
2-day	3.13 (2.87-3.43)	3.78 (3.47-4.14)	4.76 (4.36-5.20)	5.55 (5.08-6.07)	6.69 (6.09-7.31)	7.63 (6.92-8.33)	8.64 (7.79-9.42)	9.71 (8.70-10.6)	11.3 (9.99-12.3)	12.5 (11.0-13.7)
3-day	3.30 (3.03-3.62)	3.98 (3.66-4.36)	5.00 (4.59-5.46)	5.83 (5.33-6.37)	7.00 (6.38-7.65)	7.98 (7.24-8.70)	9.02 (8.14-9.83)	10.1 (9.08-11.0)	11.7 (10.4-12.8)	13.0 (11.5-14.2)
4-day	3.47 (3.19-3.80)	4.19 (3.85-4.58)	5.24 (4.81-5.73)	6.10 (5.59-6.66)	7.32 (6.67-7.99)	8.33 (7.56-9.08)	9.40 (8.49-10.2)	10.5 (9.46-11.5)	12.2 (10.8-13.3)	13.5 (11.9-14.7)
7-day	4.06 (3.77-4.41)	4.87 (4.51-5.29)	6.03 (5.58-6.55)	6.98 (6.45-7.57)	8.34 (7.68-9.04)	9.47 (8.67-10.2)	10.7 (9.72-11.5)	12.0 (10.8-12.9)	13.8 (12.4-14.9)	15.3 (13.6-16.6)
10-day	4.62 (4.30-4.98)	5.52 (5.14-5.95)	6.73 (6.26-7.26)	7.71 (7.16-8.31)	9.08 (8.40-9.77)	10.2 (9.40-11.0)	11.3 (10.4-12.2)	12.5 (11.4-13.5)	14.2 (12.9-15.3)	15.6 (14.0-16.8)
20-day	6.24 (5.84-6.69)	7.41 (6.94-7.93)	8.84 (8.27-9.47)	9.97 (9.31-10.7)	11.5 (10.7-12.3)	12.7 (11.8-13.6)	13.9 (12.9-14.9)	15.1 (13.9-16.2)	16.8 (15.4-18.0)	18.0 (16.4-19.4)
30-day	7.77 (7.32-8.24)	9.16 (8.63-9.72)	10.7 (10.1-11.3)	11.9 (11.2-12.6)	13.4 (12.6-14.3)	14.6 (13.7-15.5)	15.8 (14.8-16.8)	17.0 (15.8-18.0)	18.5 (17.1-19.6)	19.6 (18.1-20.9)
45-day	9.86 (9.35-10.4)	11.6 (11.0-12.2)	13.3 (12.6-14.1)	14.6 (13.9-15.5)	16.3 (15.4-17.2)	17.6 (16.6-18.5)	18.7 (17.7-19.8)	19.8 (18.7-21.0)	21.2 (19.9-22.4)	22.2 (20.8-23.5)
60-day	11.8 (11.2-12.4)	13.8 (13.2-14.6)	15.8 (15.0-16.6)	17.3 (16.4-18.2)	19.1 (18.1-20.1)	20.4 (19.4-21.5)	21.7 (20.5-22.8)	22.8 (21.6-24.0)	24.2 (22.9-25.5)	25.2 (23.8-26.6)

¹ Precipitation frequency (PF) estimates in this table are based on frequency analysis of partial duration series (PDS). Numbers in parenthesis are PF estimates at lower and upper bounds of the 90% confidence interval. The probability that precipitation frequency estimates (for a given duration and average recurrence interval) will be greater than the upper bound (or less than the lower bound) is 5%. Estimates at upper bounds are not checked against probable maximum precipitation (PMP) estimates and may be higher than currently valid PMP values. Please refer to NOAA Atlas 14 document for more information.

[Back to Top](#)



NOAA Atlas 14, Volume 2, Version 3
Location name: West Chester, Pennsylvania, USA*
Latitude: 39.9456°, Longitude: -75.5371°
Elevation: 319.37 ft**



* source: ESRI Maps
 ** source: USGS

POINT PRECIPITATION FREQUENCY ESTIMATES

G.M. Bonnin, D. Martin, B. Lin, T. Parzybok, M. Yekta, and D. Riley

NOAA, National Weather Service, Silver Spring, Maryland

[PF_tabular](#) | [PF_graphical](#) | [Maps & aerials](#)

PF tabular

PDS-based point precipitation frequency estimates with 90% confidence intervals (in inches/hour)¹										
Duration	Average recurrence interval (years)									
	1	2	5	10	25	50	100	200	500	1000
5-min	4.24 (3.88-4.62)	5.05 (4.63-5.51)	5.90 (5.40-6.44)	6.50 (5.94-7.09)	7.20 (6.55-7.86)	7.68 (6.94-8.39)	8.15 (7.33-8.90)	8.54 (7.64-9.37)	9.00 (7.98-9.90)	9.34 (8.21-10.3)
10-min	3.38 (3.10-3.69)	4.04 (3.70-4.40)	4.73 (4.32-5.15)	5.20 (4.75-5.68)	5.74 (5.22-6.26)	6.11 (5.53-6.68)	6.47 (5.83-7.08)	6.77 (6.06-7.43)	7.12 (6.31-7.84)	7.35 (6.46-8.13)
15-min	2.82 (2.58-3.08)	3.38 (3.10-3.69)	3.98 (3.64-4.35)	4.38 (4.00-4.78)	4.85 (4.41-5.29)	5.16 (4.66-5.64)	5.46 (4.91-5.96)	5.70 (5.10-6.25)	5.97 (5.29-6.57)	6.15 (5.41-6.80)
30-min	1.93 (1.77-2.11)	2.34 (2.14-2.55)	2.83 (2.59-3.09)	3.17 (2.90-3.47)	3.59 (3.27-3.92)	3.89 (3.51-4.24)	4.18 (3.76-4.57)	4.43 (3.97-4.86)	4.75 (4.21-5.23)	4.98 (4.38-5.51)
60-min	1.20 (1.10-1.32)	1.47 (1.34-1.60)	1.82 (1.66-1.98)	2.07 (1.89-2.26)	2.39 (2.17-2.61)	2.63 (2.38-2.88)	2.88 (2.59-3.15)	3.11 (2.78-3.41)	3.41 (3.02-3.75)	3.64 (3.20-4.02)
2-hr	0.719 (0.652-0.792)	0.874 (0.794-0.964)	1.09 (0.986-1.20)	1.25 (1.13-1.38)	1.47 (1.32-1.61)	1.63 (1.46-1.80)	1.80 (1.60-1.99)	1.97 (1.74-2.17)	2.20 (1.91-2.43)	2.37 (2.04-2.63)
3-hr	0.521 (0.474-0.575)	0.632 (0.575-0.697)	0.789 (0.716-0.869)	0.908 (0.822-1.00)	1.07 (0.959-1.17)	1.19 (1.07-1.31)	1.32 (1.17-1.45)	1.45 (1.27-1.60)	1.62 (1.40-1.79)	1.75 (1.50-1.94)
6-hr	0.322 (0.293-0.357)	0.389 (0.354-0.431)	0.484 (0.439-0.536)	0.560 (0.507-0.620)	0.667 (0.598-0.736)	0.752 (0.670-0.830)	0.843 (0.743-0.930)	0.937 (0.817-1.03)	1.07 (0.915-1.18)	1.17 (0.990-1.31)
12-hr	0.195 (0.177-0.218)	0.235 (0.213-0.262)	0.294 (0.267-0.328)	0.343 (0.309-0.382)	0.415 (0.370-0.460)	0.474 (0.419-0.525)	0.538 (0.470-0.597)	0.607 (0.523-0.675)	0.708 (0.597-0.789)	0.791 (0.655-0.885)
24-hr	0.113 (0.104-0.123)	0.136 (0.125-0.149)	0.171 (0.157-0.187)	0.200 (0.183-0.218)	0.242 (0.220-0.264)	0.277 (0.251-0.302)	0.316 (0.284-0.343)	0.357 (0.319-0.388)	0.418 (0.370-0.453)	0.468 (0.410-0.508)
2-day	0.065 (0.060-0.071)	0.079 (0.072-0.086)	0.099 (0.091-0.108)	0.116 (0.106-0.127)	0.139 (0.127-0.152)	0.159 (0.144-0.173)	0.180 (0.162-0.196)	0.202 (0.181-0.221)	0.234 (0.208-0.256)	0.261 (0.230-0.284)
3-day	0.046 (0.042-0.050)	0.055 (0.051-0.061)	0.069 (0.064-0.076)	0.081 (0.074-0.088)	0.097 (0.089-0.106)	0.111 (0.101-0.121)	0.125 (0.113-0.137)	0.141 (0.126-0.153)	0.163 (0.145-0.177)	0.181 (0.159-0.197)
4-day	0.036 (0.033-0.040)	0.044 (0.040-0.048)	0.055 (0.050-0.060)	0.064 (0.058-0.069)	0.076 (0.070-0.083)	0.087 (0.079-0.095)	0.098 (0.088-0.107)	0.110 (0.099-0.120)	0.127 (0.113-0.138)	0.141 (0.124-0.153)
7-day	0.024 (0.022-0.026)	0.029 (0.027-0.031)	0.036 (0.033-0.039)	0.042 (0.038-0.045)	0.050 (0.046-0.054)	0.056 (0.052-0.061)	0.064 (0.058-0.069)	0.071 (0.064-0.077)	0.082 (0.074-0.089)	0.091 (0.081-0.099)
10-day	0.019 (0.018-0.021)	0.023 (0.021-0.025)	0.028 (0.026-0.030)	0.032 (0.030-0.035)	0.038 (0.035-0.041)	0.042 (0.039-0.046)	0.047 (0.043-0.051)	0.052 (0.048-0.056)	0.059 (0.054-0.064)	0.065 (0.058-0.070)
20-day	0.013 (0.012-0.014)	0.015 (0.014-0.017)	0.018 (0.017-0.020)	0.021 (0.019-0.022)	0.024 (0.022-0.026)	0.026 (0.025-0.028)	0.029 (0.027-0.031)	0.032 (0.029-0.034)	0.035 (0.032-0.037)	0.038 (0.034-0.040)
30-day	0.011 (0.010-0.011)	0.013 (0.012-0.013)	0.015 (0.014-0.016)	0.016 (0.016-0.017)	0.019 (0.018-0.020)	0.020 (0.019-0.022)	0.022 (0.020-0.023)	0.024 (0.022-0.025)	0.026 (0.024-0.027)	0.027 (0.025-0.029)
45-day	0.009 (0.009-0.010)	0.011 (0.010-0.011)	0.012 (0.012-0.013)	0.014 (0.013-0.014)	0.015 (0.014-0.016)	0.016 (0.015-0.017)	0.017 (0.016-0.018)	0.018 (0.017-0.019)	0.020 (0.018-0.021)	0.021 (0.019-0.022)
60-day	0.008 (0.008-0.009)	0.010 (0.009-0.010)	0.011 (0.010-0.012)	0.012 (0.011-0.013)	0.013 (0.013-0.014)	0.014 (0.013-0.015)	0.015 (0.014-0.016)	0.016 (0.015-0.017)	0.017 (0.016-0.018)	0.018 (0.016-0.018)

¹ Precipitation frequency (PF) estimates in this table are based on frequency analysis of partial duration series (PDS). Numbers in parenthesis are PF estimates at lower and upper bounds of the 90% confidence interval. The probability that precipitation frequency estimates (for a given duration and average recurrence interval) will be greater than the upper bound (or less than the lower bound) is 5%. Estimates at upper bounds are not checked against probable maximum precipitation (PMP) estimates and may be higher than currently valid PMP values. Please refer to NOAA Atlas 14 document for more information.

[Back to Top](#)

APPENDIX D
SUPPORTING VOLUME CALCULATIONS
(EAST BRANCH CHESTER CREEK)

Worksheet 4. Change in Runoff Volume for 2-YR Storm Event

East Branch Chester Creek

PROJECT: The Westtown School - Oak Lane Project
Drainage Area East Branch Chester Creek
2-Year Rainfall: 3.26 in

Existing Conditions:

Cover Type/Condition	Soil Type	Area (sf)	Area (ac)	CN	S	la (0.2*S)	Q Runoff ¹ (in)	Runoff Volume ² (ft ³)
Paved/Impervious Areas	B	6,143	0.141	98	0.20	0.04	3.03	1,550
Meadow	B	203,696	4.676	58	7.24	1.45	0.36	6,154
40% Impervious Area as Meadow	B	4095	0.094	58	7.24	1.45	0.36	124
TOTAL:		213,934	4.911				3.75	7,828

Developed Conditions:

Cover Type/Condition	Soil Type	Area (sf)	Area (ac)	CN	S	la (0.2*S)	Q Runoff ¹ (in)	Runoff Volume ² (ft ³)
Paved/Impervious Areas	B	51,664	1.186	98	0.20	0.04	3.03	13,033
Lawn (Good condition)	B	147,588	3.388	61	6.39	1.28	0.47	5,765
TOTAL:		199,252	4.574				3.50	18,798

2-Year Volume Increase (ft³): **10,971**

2-Year Volume Increase = Developed Conditions Runoff Volume - Existing Conditions Runoff Volume

- Runoff (in) = $Q = (P-0.2S)^2 / (P+0.8S)$ where P = 2-Year Rainfall (in) S = (1000 / CN) - 10
- Runoff Volume (CF) = Q x Area x 1/12 Q = Runoff (in) Area = Land use area (sq. ft)

Note: Runoff Volume must be calculated for EACH land use type/condition and HSGI. The use of a weighted CN value for volume calculations is not acceptable.

BMP Volume Calculation Worksheet

PROJECT: The Westtown School - Oak Lane Project
2-Year Rainfall: 3.26 in

Drainage Area Name: Infiltration BMP 1

Cover Type/Condition	Soil Type	Area (sf)	Area (ac)	CN	S	Ia ((0.2*S)	Q Runoff ¹ (in)	Runoff Volume ² (ft ³)
Disturbed Area								
Lawn (Good condition)	B	99734	2.29	61	6.39	1.28	0.47	3,896
Paved/Impervious Areas	B	46644	1.07	98	0.20	0.04	3.03	11,767
TOTAL ONSITE:		146378	3.36					15,663
Undisturbed Area								
Lawn (Good condition)	B	63893	1.47	61	6.39	1.28	0.47	2,496
Paved/Impervious Areas	B	6916	0.16	98	0.20	0.04	3.03	1,745
TOTAL:		217187	4.99					19,903

1. Runoff (in) = $Q = (P - 0.2S)^2 / (P + 0.8S)$ where
 P = 2-Year Rainfall (in)
 S = $(1000 / CN) - 10$
2. Runoff Volume (CF) = $Q \times \text{Area} \times 1/12$
 Q = Runoff (in)
 Area = Land use area (sq. ft)

Infiltration BMP 1 Calculations

Infiltration Volume

Inf Rate:	0.41 in/hr
Inf Area:	10,675 sf

Storage Volume = 11,503 cf at elev: 289.50

Infiltration Volume = Inf. Rate x Inf Area X Inf Period
 = 0.41 in/hr x 10,675 sf x 2 hr x (1ft/12in)
 = 724 CF

Total Inf. Volume¹ = Storage Volume + Infiltration Volume
 = 12,227 cf at elev: 289.5

Volume Captured = 15,663 cf

Infiltration Credit = 11,161 cf²
ET Credit = 3277 cf²
Total Credits 14,438

Test Pit	Infiltration Rate (in/hr)
TP-14A	0.20
TP-14B	1.00
TP-15A*	0.00
TP-15B*	0.00
TP-16A	2.70
TP-16B*	6.00
Geomean	0.81
Safety Factor	2.00
Adjusted Rate	0.41

*The highest and lowest recorded rates were removed from the calculation.

Loading Ratios

Total Drainage Area = 217,187 sf
 Impervious Area = 53,560 sf
 Infiltration Area = 10,675 sf
 Impervious Loading Ratio = 5.0:1
 Overall Loading Ratio = 20.3:1

Dewatering Time (After Rainfall Event)

$T = \frac{\text{Infiltration Volume}}{(\text{Inf. Rate}/12 \times \text{Inf. Area})}$
 = **33.8 hrs**

¹ For dewatering calculation analysis

² See PADEP PCSM Volume Spreadsheet

**UNT. TO
EAST BRANCH CHESTER CREEK**

Worksheet 4. Change in Runoff Volume for 2-YR Storm Event

UNT to East Branch Chester Creek

PROJECT: The Westtown School - Oak Lane Project
Drainage Area Unt. to East Branch Chester Creek
2-Year Rainfall: 3.26 in

Existing Conditions:

Cover Type/Condition	Soil Type	Area (sf)	Area (ac)	CN	S	Ia (0.2*S)	Q Runoff ¹ (in)	Runoff Volume ² (ft ³)
Paved/Impervious Areas	B	263	0.006	98	0.20	0.04	3.03	66
Meadow	B	502,049	11.525	58	7.24	1.45	0.36	15,169
40% Impervious Area as Meadow	B	175	0.004	58	7.24	1.45	0.36	5
Meadow	D	49,830	1.144	78	2.82	0.56	1.32	5,471
TOTAL:		552,317	12.679				3.75	20,711

Developed Conditions:

Cover Type/Condition	Soil Type	Area (sf)	Area (ac)	CN	S	Ia (0.2*S)	Q Runoff ¹ (in)	Runoff Volume ² (ft ³)
Paved/Impervious Areas	B	206,620	4.743	98	0.20	0.04	3.03	52,125
Lawn (Good condition)	B	310,539	7.129	61	6.39	1.28	0.47	12,130
Lawn (Good condition)	D	49,830	1.144	80	2.50	0.50	1.45	6,014
TOTAL:		566,989	13.016				4.94	70,268

2-Year Volume Increase (ft³): **49,557**

2-Year Volume Increase = Developed Conditions Runoff Volume - Existing Conditions Runoff Volume

- Runoff (in) = $Q = (P-0.2S)^2 / (P+0.8S)$ where P = 2-Year Rainfall (in) S = (1000 / CN) - 10
- Runoff Volume (CF) = Q x Area x 1/12 Q = Runoff (in) Area = Land use area (sq. ft)

Note: Runoff Volume must be calculated for EACH land use type/condition and HSGI. The use of a weighted CN value for volume calculations is not acceptable.

BMP Volume Calculation Worksheet

PROJECT: The Westtown School - Oak Lane Project

2-Year Rainfall: 3.26 in

Drainage Area Name: Infiltration Bed - BMP 2

Cover Type/Condition	Soil Type	Area (sf)	Area (ac)	CN	S	Ia ((0.2*S)	Q Runoff ¹ (in)	Runoff Volume ² (ft ³)
Disturbed Area								
Paved/Impervious Areas	B	96824	2.22	98	0.20	0.04	3.03	24,426
Lawn (Good condition)	B			61	6.39	1.28	0.47	0
Lawn (Good condition)	D			80	2.50	0.50	1.45	0
TOTAL ONSITE:		96824	2.22					24,426

Drainage Area Name: Infiltration Bed - BMP 3

Cover Type/Condition	Soil Type	Area (sf)	Area (ac)	CN	S	Ia ((0.2*S)	Q Runoff ¹ (in)	Runoff Volume ² (ft ³)
Disturbed Area								
Paved/Impervious Areas	B	96824	2.22	98	0.20	0.04	3.03	24,426
Lawn (Good condition)	B			61	6.39	1.28	0.47	0
Lawn (Good condition)	D			80	2.50	0.50	1.45	0
TOTAL ONSITE:		96824	2.22					24,426
Volume Infiltrated (from DEP PCSM Spreadsheet)								24,357
Overflow volume to BMP 4								69

1. Runoff (in) = $Q = (P-0.2S)^2 / (P+0.8S)$ where
P = 2-Year Rainfall (in)
S=(1000 / CN) - 10

BMP Volume Calculation Worksheet

PROJECT: The Westtown School - Oak Lane Project
2-Year Rainfall: 3.26 in

Drainage Area Name: Infiltration Basin - BMP 4

Cover Type/Condition	Soil Type	Area (sf)	Area (ac)	CN	S	Ia ((0.2*S)	Q Runoff ¹ (in)	Runoff Volume ² (ft ³)
Disturbed Area								
Paved/Impervious Areas	B	12972	0.30	98	0.20	0.04	3.03	3,272
Lawn (Good condition)	B	222976	5.12	61	6.39	1.28	0.47	8,710
Lawn (Good condition)	D	23706	0.54	80	2.50	0.50	1.45	2,861
TOTAL ONSITE:		259654	5.96					14,843
							Additional Volume from BMP 3	69
							Volume Routed to BMP	14,912
Undisturbed Area								
Paved/Impervious Areas	B			98	0.20	0.04	3.03	0
Lawn (Good condition)	B	121339	2.79	61	6.39	1.28	0.47	4,740
Lawn (Good condition)	D	40248	0.92	80	2.50	0.50	1.45	4,857
TOTAL:		421241	9.67					24,440

1. Runoff (in) = $Q = (P - 0.2S)^2 / (P + 0.8S)$ where

P = 2-Year Rainfall (in)

S = (1000 / CN) - 10

2. Runoff Volume (CF) = $Q \times \text{Area} \times 1/12$

Q = Runoff (in)

Area = Land use area (sq. ft)

S = (1000 / CN) - 10

2. Runoff Volume (CF) = $Q \times \text{Area} \times 1/12$

Q = Runoff (in)

Area = Land use area (sq. ft)

Infiltration Bed - BMP 2 Calculations

Subsurface Infiltration Bed Volume

Inf Rate:	2.32 in/hr
Inf Area:	75,725 sf

Storage Volume = 23,035 cf at elev: 316.75

Infiltration Volume = Inf. Rate x Inf Area X Inf Period
 = 2.32 in/hr x 75,725 sf x 2 hr x (1ft/12in)
 = 29328 CF

Total Inf. Volume = Storage Volume + Infiltration Volume
 = 52,363 cf at elev: 316.75

Volume Captured = 24,426 cf

Volume Infiltrated = 24,426 cf

Test Pit	Infiltration Rate (in/hr)
TP-1A	1.80
TP-3B	12.00
Geomean	4.65
Safety Factor	2.00
Adjusted Rate	2.32

Loading Ratios

Total Drainage Area = 96824 sf
 Impervious Area = 96824 sf
 Infiltration Area = 75,725 sf
 Impervious Loading Ratio = 1.3:1
 Overall Loading Ratio = 1.3:1

Dewatering Time (After Rainfall Event)

$T = \frac{\text{Infiltration Volume}}{(\text{Inf. Rate}/12 \times \text{Inf. Area})}$
 = 1.7 hrs

Synthetic Turf Field Storage Calculations

BMP 2

WATER SURFACE ELEVATION (FEET)	SUBGRADE AREA (SQ.FT.)	AVERAGE AREA (SQ.FT.)	Δ ELEV. (FEET)	STORAGE VOLUME	x 0.40 (40% Void space)	Σ (CU.FT.)	(AC. FT.)
316	75725					0	0
		75725	0.67	50,736	20294		
316.67	75725					20,294	0.4659
		85638	0.08	6,851	2740		
316.75	95550					23,035	0.5288
		95550	0.75	71,663	28665		
317.5	95550					51,700	1.1869
		0	0.00	0	0		
						0	0.0000
		0	0.00	0	0		
						0	0.0000
		0	0.00	0	0		
						0	0.0000

Infiltration Bed - BMP 3 Calculations

Subsurface Infiltration Bed Volume

Inf Rate:	1.01 in/hr
Inf Area:	26,795 sf

Storage Volume = 21,916 cf at elev: 321.00

Infiltration Volume = Inf. Rate x Inf Area X Inf Period
 = 1.01 in/hr x 26,795 sf x 2 hr x (1ft/12in)
 = 4510 CF

Total Inf. Volume = Storage Volume + Infiltration Volume
 = 26,426 cf at elev: 321

Volume Captured = 24,426 cf

Volume Infiltrated = 24,357 cf

Test Pit	Infiltration Rate (in/hr)
TP-4A	1.20
TP-5A	3.40
Geomean	2.02
Safety Factor	2.00
Adjusted Rate	1.01

Loading Ratios

Total Drainage Area = 96824 sf
 Impervious Area = 96824 sf
 Infiltration Area = 26,795 sf
 Impervious Loading Ratio = 3.6:1
 Overall Loading Ratio = 3.6:1

Dewatering Time (After Rainfall Event)

$T = \frac{\text{Infiltration Volume}}{(\text{Inf. Rate}/12 \times \text{Inf. Area})}$
 = 10.8 hrs

Synthetic Turf Field Storage Calculations

BMP 3

WATER SURFACE ELEVATION (FEET)	SUBGRADE AREA (SQ.FT.)	AVERAGE AREA (SQ.FT.)	Δ ELEV. (FEET)	STORAGE VOLUME	x 0.40 (40% Void space)	Σ (CU.FT.)	(AC. FT.)
319	26795					0	0
		27195	1.00	27,195	10878		
320	27595					10,878	0.2497
		27595	1.00	27,595	11038		
321	27595					21,916	0.5031
		56028	0.65	36,418	14567		
321.65	84460					36,483	0.8375
		90005	0.10	9,001	3600		
321.75	95550					40,083	0.9202
		95550	0.75	71,663	28665		
322.5	95550					68,748	1.5782
		0	0.00	0	0		
						0	0.0000

Infiltration Basin - BMP 4 Calculations

Infiltration Volume

Inf Rate:	0.84 in/hr
Inf Area:	19,809 sf

Storage Volume = 22,478 cf at elev: 311.00

Infiltration Volume = Inf. Rate x Inf Area X Inf Period
 = 0.84 in/hr x 19,809 sf x 2 hr x (1ft/12in)
 = 2762 CF

Total Inf. Volume = Storage Volume + Infiltration Volume
 = 25,240 cf at elev: 311.00

Volume Captured = 14,843 cf

Overflow volume from BMP 3 = 69

Total Volume Captured¹ = 14,912

Volume Infiltrated¹ = 14,912 cf²

ET Credit¹ = 0 cf²

Total Credit = 14,912

Test Pit	Infiltration Rate (in/hr)
TP-6A	1.00
TP-7B	2.80
Geomean	1.67
Safety Factor	2.00
Adjusted Rate	0.84

Loading Ratios

Total Drainage Area = 421241 sf
 Impervious Area = 12972 sf
 Infiltration Area = 19,809 sf
 Impervious Loading Ratio = 0.7:1
 Overall Loading Ratio = 21.3:1

Dewatering Time (After Rainfall Event)

$T = \frac{\text{Storage Volume}}{(\text{Inf. Rate}/12 \times \text{Inf. Area})}$
 = 16.3 hrs

¹ See PADEP PCSM Volume Spreadsheet

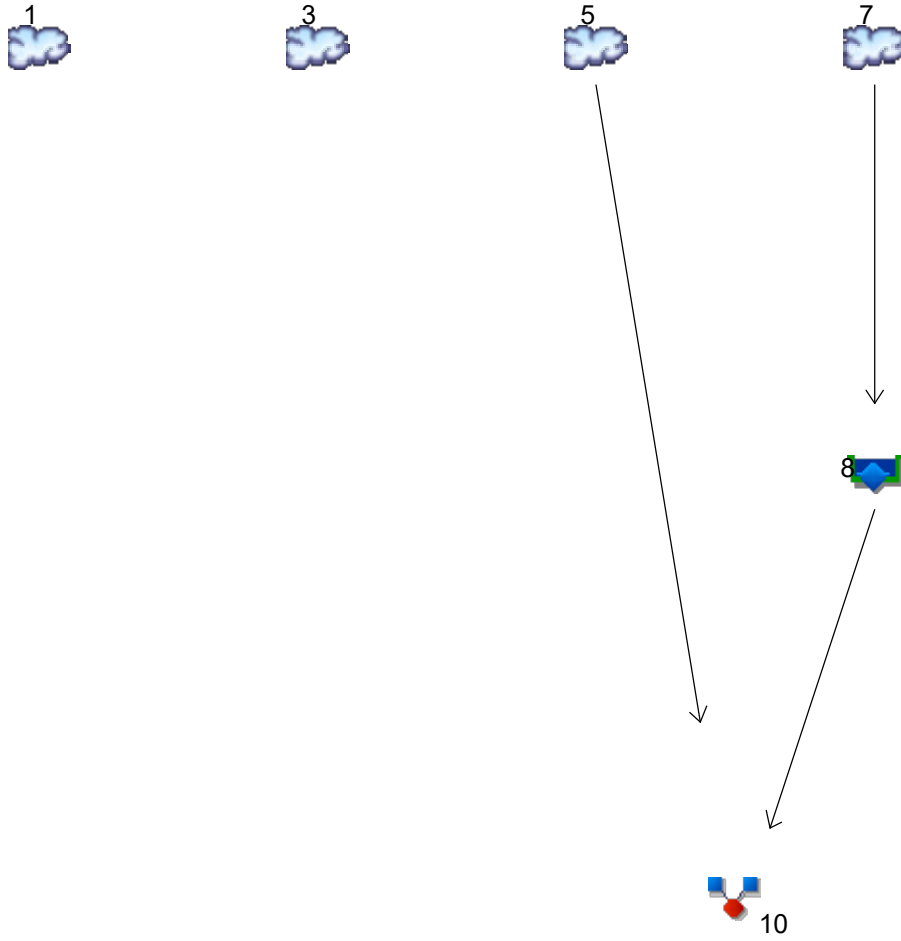
APPENDIX E

RATE CONTROL ANALYSIS

OVERALL HYDROLOGY

Watershed Model Schematic

Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2022



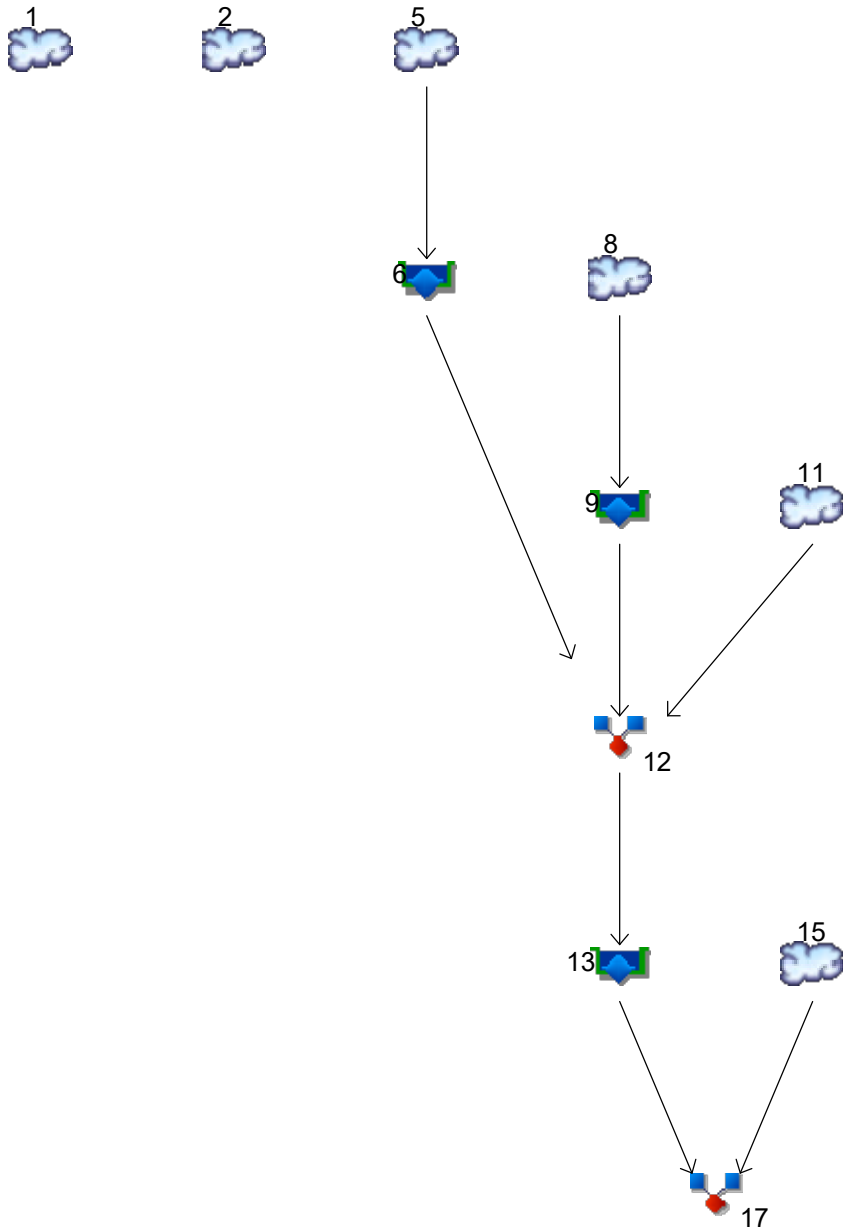
Hydrograph Return Period Recap

Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2022

Hyd. No.	Hydrograph type (origin)	Inflow hyd(s)	Peak Outflow (cfs)								Hydrograph Description
			1-yr	2-yr	3-yr	5-yr	10-yr	25-yr	50-yr	100-yr	
1	SCS Runoff	-----	0.857	2.379	-----	5.681	8.961	14.25	19.09	24.73	Pre-Dev. (E. Branch Chester Creek)
3	SCS Runoff	-----	0.498	1.525	-----	3.844	6.212	10.05	13.58	17.68	Pre-Dev. (EBCC) Onsite
5	SCS Runoff	-----	0.678	1.267	-----	2.311	3.279	4.785	6.123	7.622	EBCC-Undetained
7	SCS Runoff	-----	3.519	5.831	-----	9.819	13.44	19.04	24.03	29.58	BMP 1 IN
8	Reservoir	7	0.000	0.162	-----	0.667	1.829	5.137	8.706	13.69	BMP 1 Routed
10	Combine	5, 8,	0.678	1.267	-----	2.311	3.279	5.795	9.564	14.78	Post-Dev. E. Branch Chester (Combi

Watershed Model Schematic

Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2022



Hydrograph Return Period Recap

Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2022

Hyd. No.	Hydrograph type (origin)	Inflow hyd(s)	Peak Outflow (cfs)								Hydrograph Description
			1-yr	2-yr	3-yr	5-yr	10-yr	25-yr	50-yr	100-yr	
1	SCS Runoff	-----	1.827	5.020	-----	12.03	19.34	31.25	42.19	54.74	Pre-Dev. (Unt. to EBCC)
2	SCS Runoff	-----	1.333	3.664	-----	8.779	14.12	22.81	30.80	39.96	Pre-Dev. Unt. to EBCC Onsite (Redu
5	SCS Runoff	-----	8.084	9.771	-----	12.34	14.48	17.55	20.14	22.94	BMP 3 IN
6	Reservoir	5	0.000	0.006	-----	0.076	0.116	0.165	0.219	0.435	BMP 3 Routed
8	SCS Runoff	-----	8.084	9.771	-----	12.34	14.48	17.55	20.14	22.94	BMP 2 IN
9	Reservoir	8	0.000	0.000	-----	0.148	0.319	0.762	1.333	2.110	BMP 2 Routed
11	SCS Runoff	-----	2.564	5.132	-----	10.10	14.80	22.21	28.86	36.45	BMP 4 DA
12	Combine	6, 9, 11	2.564	5.132	-----	10.10	14.80	22.76	30.13	38.61	BMP 4 IN
13	Reservoir	12	0.000	0.019	-----	0.745	2.040	7.989	15.12	23.74	BMP 4 Routed
15	SCS Runoff	-----	1.201	2.510	-----	4.941	7.232	10.84	14.08	17.79	Unt. to EBCC Undetained
17	Combine	13, 15,	1.201	2.510	-----	4.941	7.232	10.84	17.45	26.78	Post-Dev. Unt. to EBCC (Combined)

PRE-DEVELOPMENT HYDROLOGY (EAST BRANCH CHESTER CREEK)



ELA SPORT

ATHLETIC FACILITIES DESIGN & CONSULTING

737 S. BROAD STREET
LITITZ, PA 17543
(717) 626-72713

PROJECT: The Westtown School - Oak Lane Project
LOCATION: Westtown Township
COUNTY: Chester

WATERSHED	LAND USE		Parking, Other Impervious (60% of total)		40% of Impervious Areas as Meadow		Meadow	Meadow	Total Area (ac.)	Composite 'CN' Value	Tc Min.
	HSG	"CN" Value	B	B	B	B	D				
Pre-Dev. EBCC		0.26	0.17	0.17	0.00	0.00	6.17	0.00	6.60	60	15
Pre-Dev. EBCC 'Onsite' (Reduction Factor)		0.14	0.09	0.09	0.00	0.00	4.68	0.00	4.91	59	15

ELA SPORT
ATHLETIC FACILITIES
DESIGN & CONSULTING

737 S. BROAD STREET
 LITITZ, PA 17543
 (717) 626-72713



SUMMARY - SUBAREAS TIME OF CONCENTRATION PRE-DEVELOPMENT CONDITIONS

PROJECT: The Westtown School - Oak Lane Project
 LOCATION: Westtown Township
 COUNTY: Chester

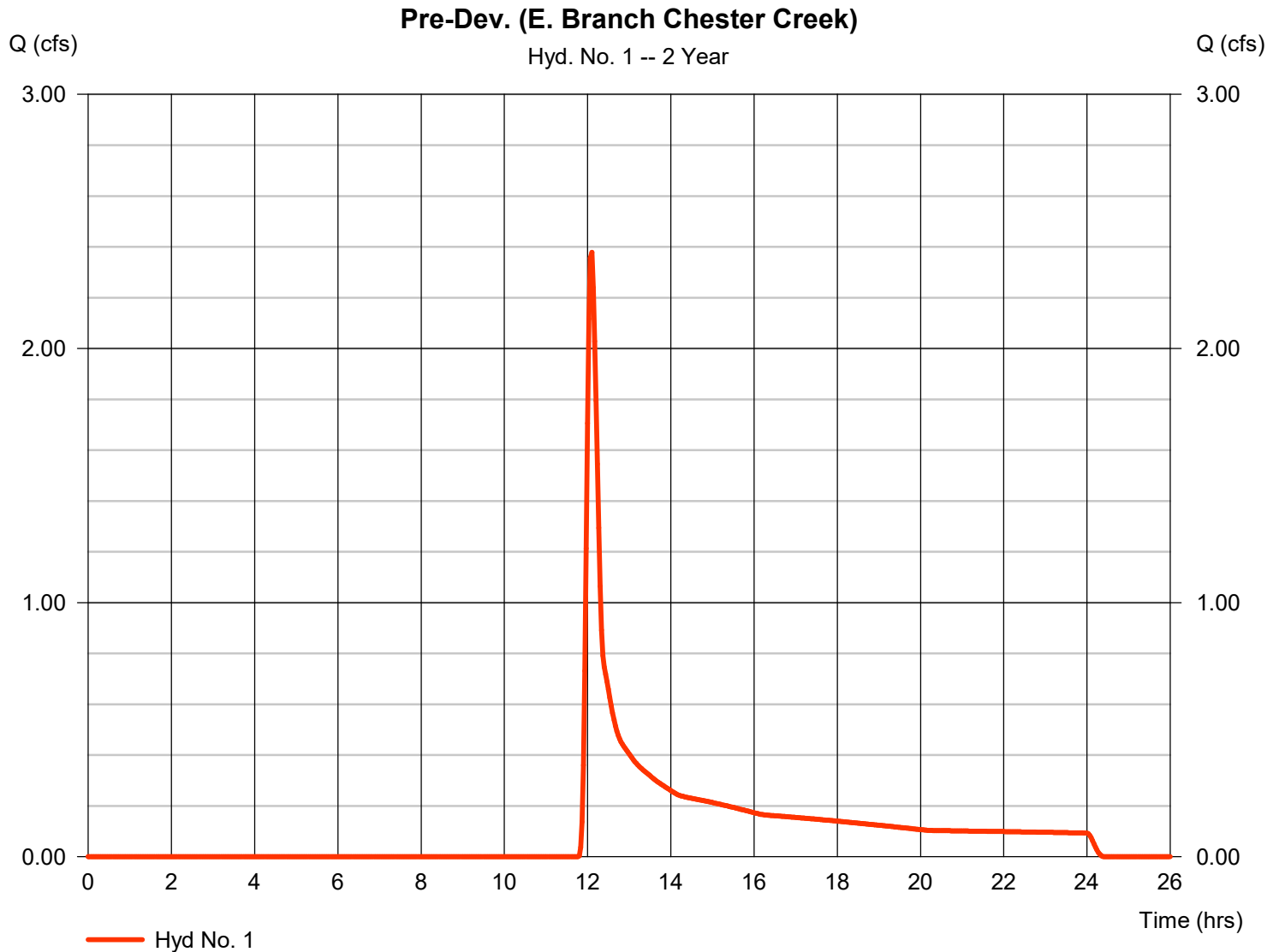
Time of concentration (Tc) or travel time (Tt)																				
Watershed	overland					Shallow Concentrated					Channel or Pipe							Total		
	Length L ₁ 100 ft. max. ft.	Slope S ₁ ft./ft.	Manning's n	2 yr rainfall in.	Tc Min.	Flow Path U/P	Length L ₂ ft.	Slope S ₂ ft./ft.	Average Velocity ft./s	Min. Tt	Channel or Pipe C/P	Flow Area sq.ft.	Wetted Perimeter ft.	Pipe Diameter in.	Slope S ₃ ft./ft.	Manning's n	Length L ₃ ft.	Tt Min.	Min. Hrs.	Total Hrs.
A	89	0.017	0.24	3.26	14	U	234	0.090	4.8	0.0	0.00	0.00	0.00					0		
					0				0	0.8	0.00	0.00	0.00					0		
					0				0	0	0.00	0.00	0.00					0		
					0				0	0	0.00	0.00	0.00					0		
					0				0	0	0.00	0.00	0.00					0.0		
					13.7					0.8								0.0		0.25
																		15		

Hydrograph Report

Hyd. No. 1

Pre-Dev. (E. Branch Chester Creek)

Hydrograph type	= SCS Runoff	Peak discharge	= 2.379 cfs
Storm frequency	= 2 yrs	Time to peak	= 12.10 hrs
Time interval	= 2 min	Hyd. volume	= 10,087 cuft
Drainage area	= 6.600 ac	Curve number	= 60
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 15.00 min
Total precip.	= 3.26 in	Distribution	= Type II
Storm duration	= 24 hrs	Shape factor	= 484

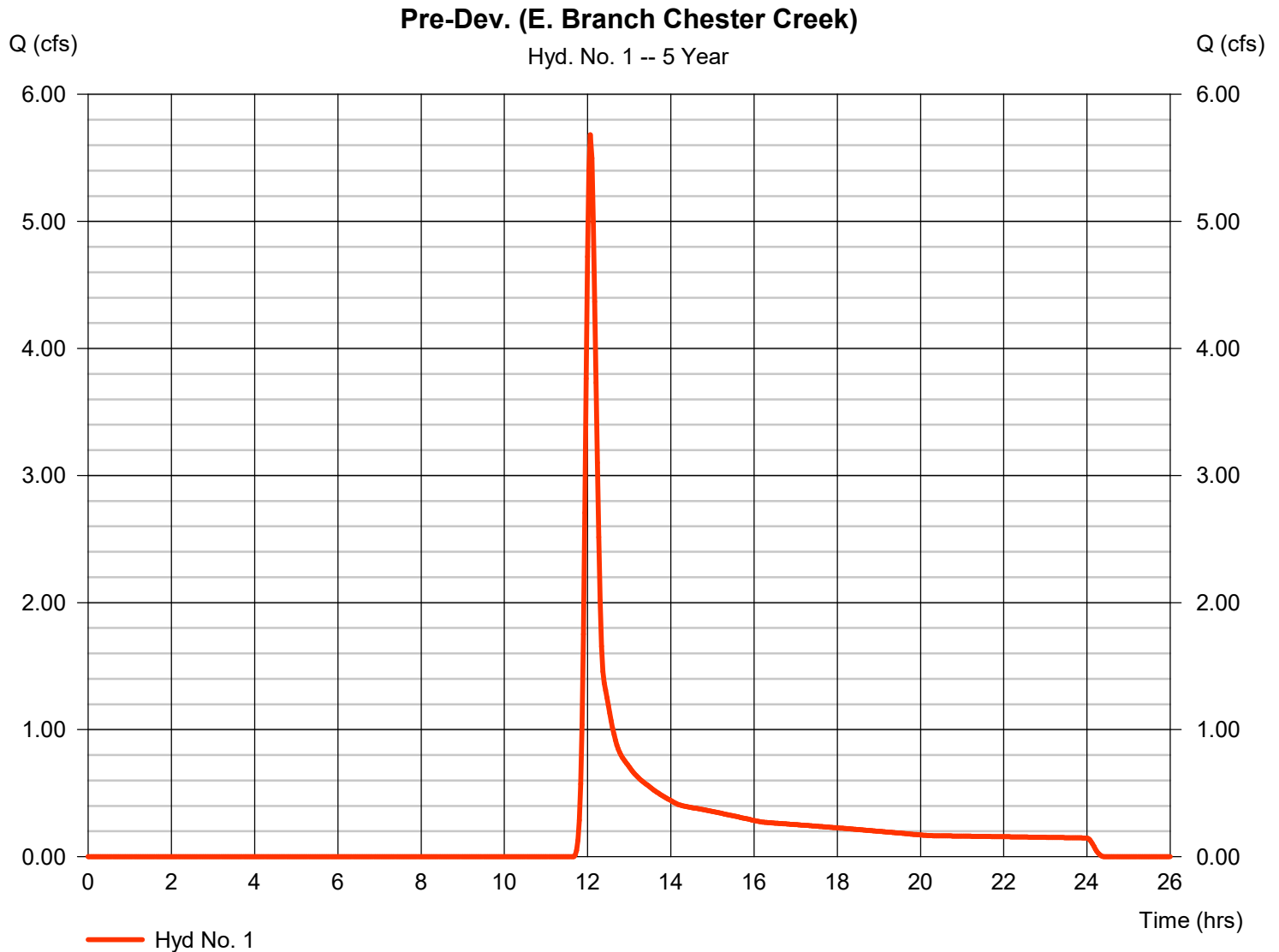


Hydrograph Report

Hyd. No. 1

Pre-Dev. (E. Branch Chester Creek)

Hydrograph type	= SCS Runoff	Peak discharge	= 5.681 cfs
Storm frequency	= 5 yrs	Time to peak	= 12.07 hrs
Time interval	= 2 min	Hyd. volume	= 18,953 cuft
Drainage area	= 6.600 ac	Curve number	= 60
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 15.00 min
Total precip.	= 4.10 in	Distribution	= Type II
Storm duration	= 24 hrs	Shape factor	= 484

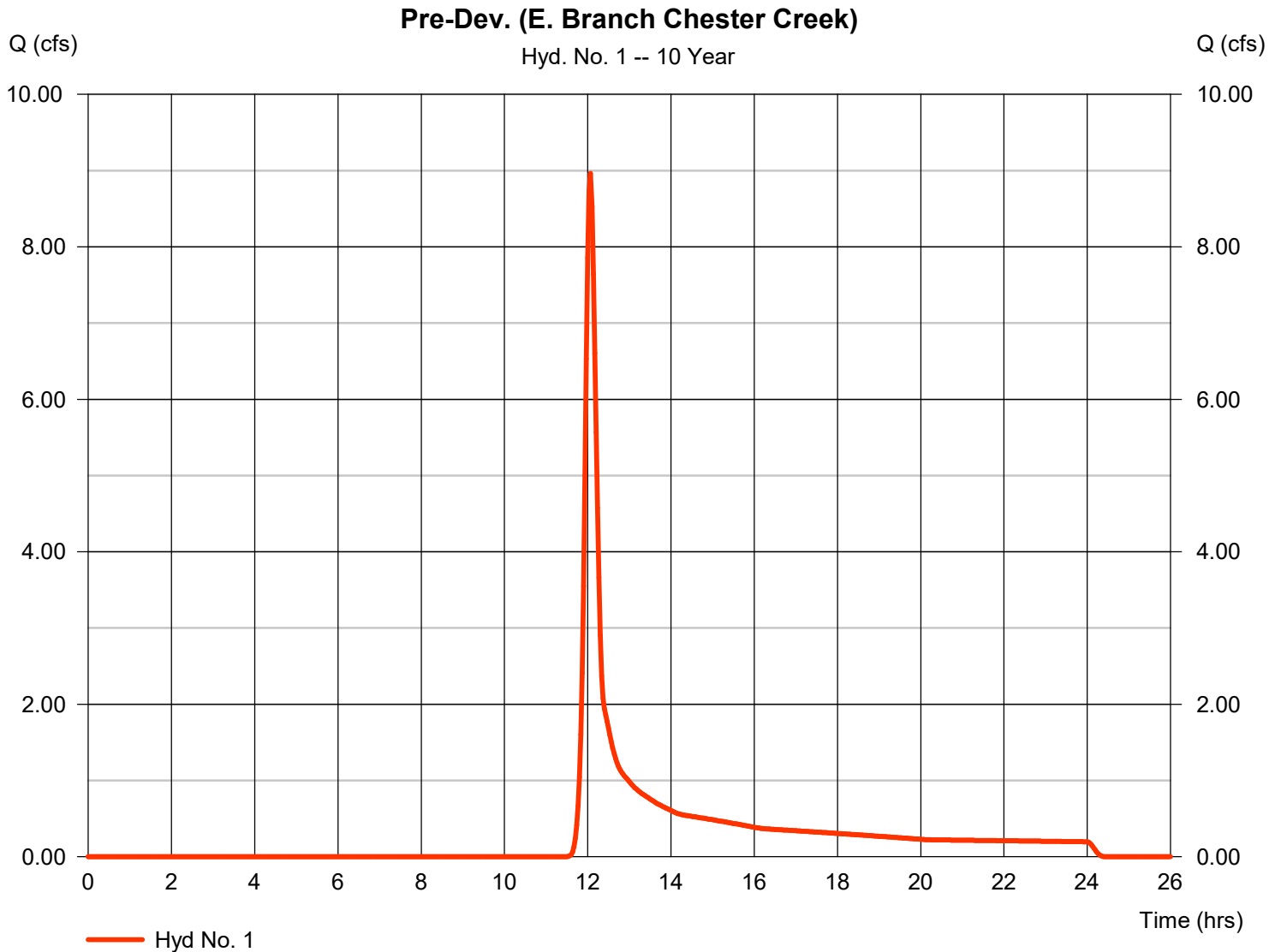


Hydrograph Report

Hyd. No. 1

Pre-Dev. (E. Branch Chester Creek)

Hydrograph type	= SCS Runoff	Peak discharge	= 8.961 cfs
Storm frequency	= 10 yrs	Time to peak	= 12.07 hrs
Time interval	= 2 min	Hyd. volume	= 27,703 cuft
Drainage area	= 6.600 ac	Curve number	= 60
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 15.00 min
Total precip.	= 4.80 in	Distribution	= Type II
Storm duration	= 24 hrs	Shape factor	= 484



Hydrograph Report

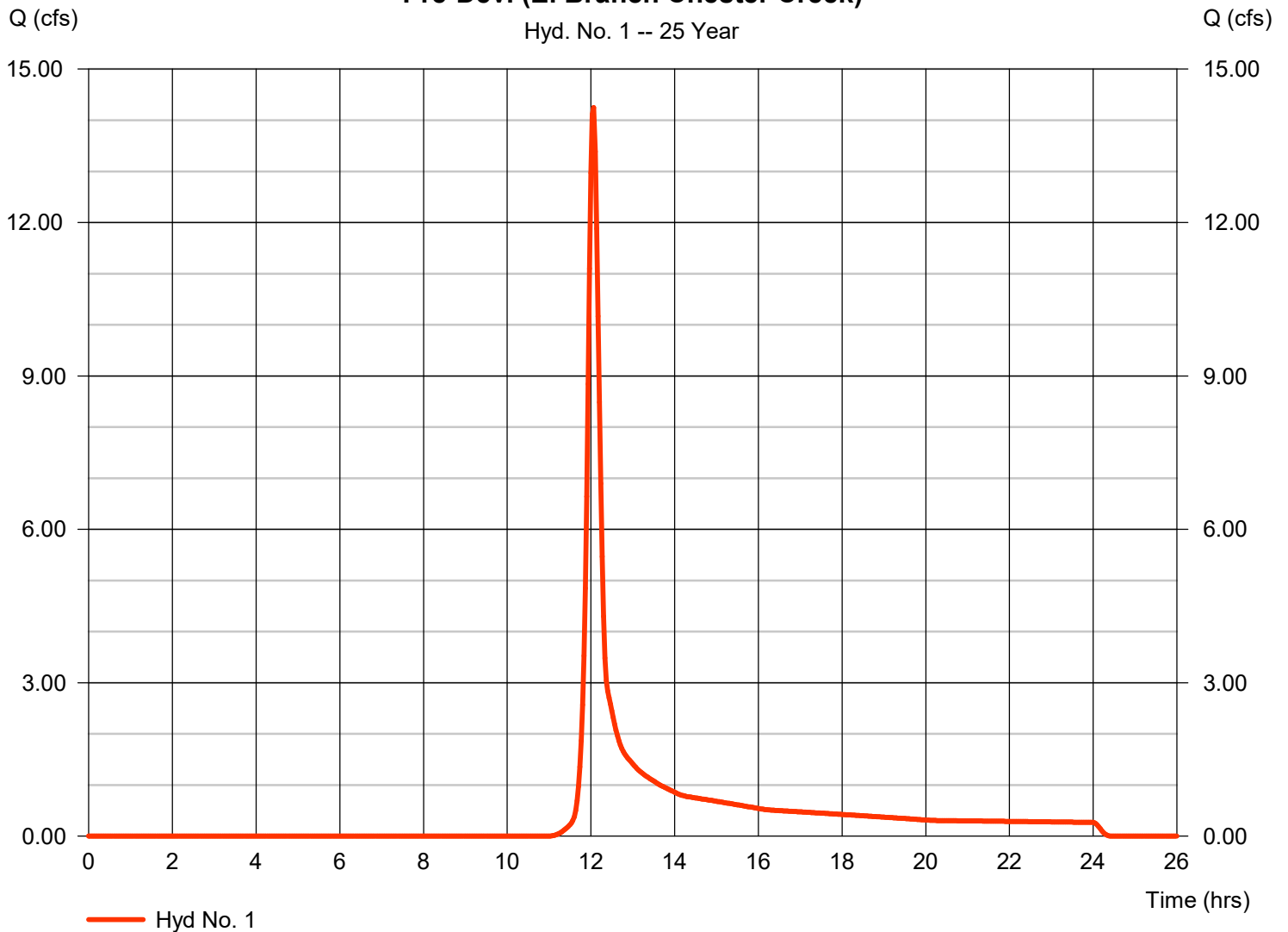
Hyd. No. 1

Pre-Dev. (E. Branch Chester Creek)

Hydrograph type	= SCS Runoff	Peak discharge	= 14.25 cfs
Storm frequency	= 25 yrs	Time to peak	= 12.07 hrs
Time interval	= 2 min	Hyd. volume	= 42,010 cuft
Drainage area	= 6.600 ac	Curve number	= 60
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 15.00 min
Total precip.	= 5.81 in	Distribution	= Type II
Storm duration	= 24 hrs	Shape factor	= 484

Pre-Dev. (E. Branch Chester Creek)

Hyd. No. 1 -- 25 Year

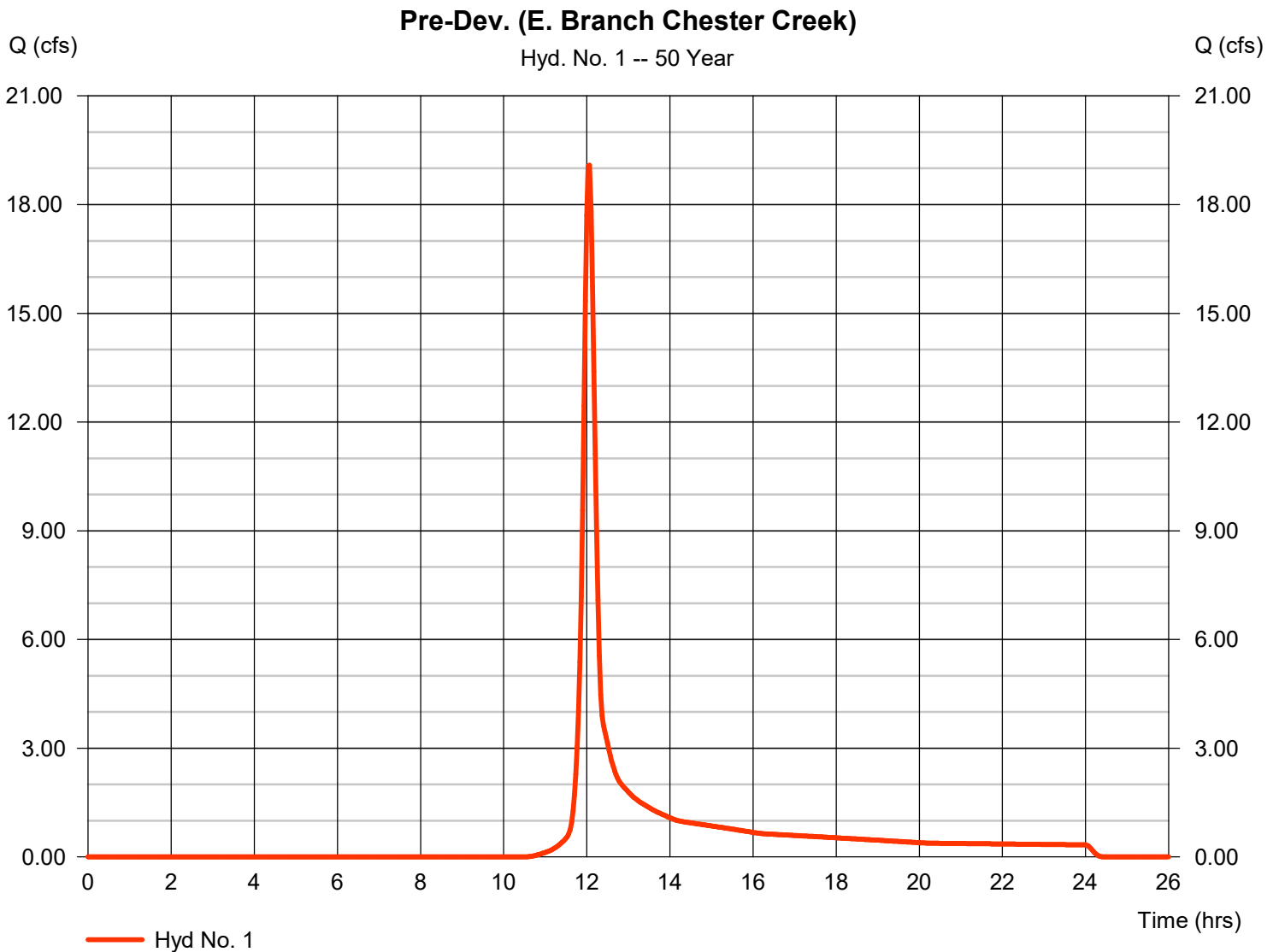


Hydrograph Report

Hyd. No. 1

Pre-Dev. (E. Branch Chester Creek)

Hydrograph type	= SCS Runoff	Peak discharge	= 19.09 cfs
Storm frequency	= 50 yrs	Time to peak	= 12.07 hrs
Time interval	= 2 min	Hyd. volume	= 55,262 cuft
Drainage area	= 6.600 ac	Curve number	= 60
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 15.00 min
Total precip.	= 6.66 in	Distribution	= Type II
Storm duration	= 24 hrs	Shape factor	= 484

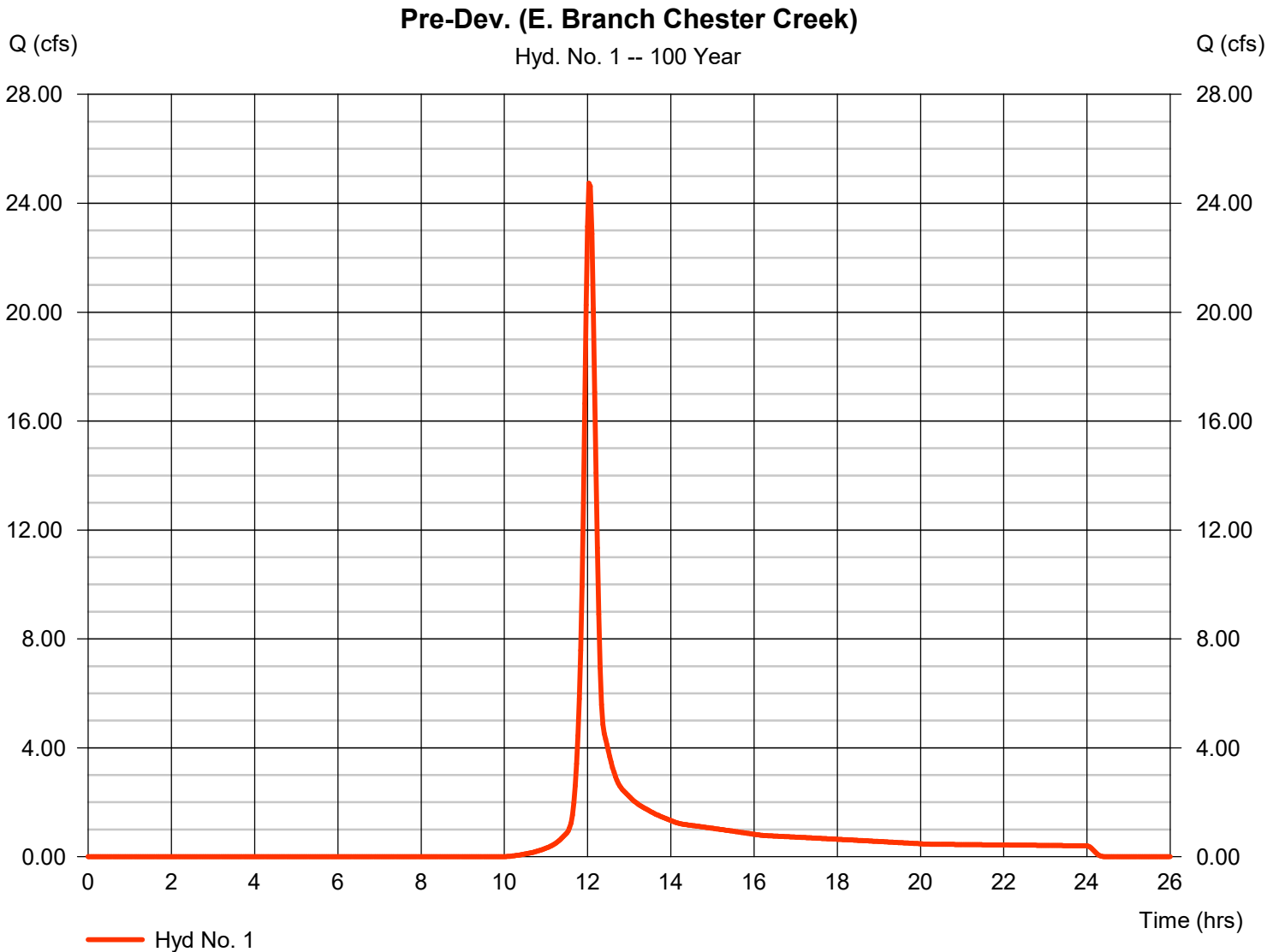


Hydrograph Report

Hyd. No. 1

Pre-Dev. (E. Branch Chester Creek)

Hydrograph type	= SCS Runoff	Peak discharge	= 24.73 cfs
Storm frequency	= 100 yrs	Time to peak	= 12.03 hrs
Time interval	= 2 min	Hyd. volume	= 70,585 cuft
Drainage area	= 6.600 ac	Curve number	= 60
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 15.00 min
Total precip.	= 7.58 in	Distribution	= Type II
Storm duration	= 24 hrs	Shape factor	= 484

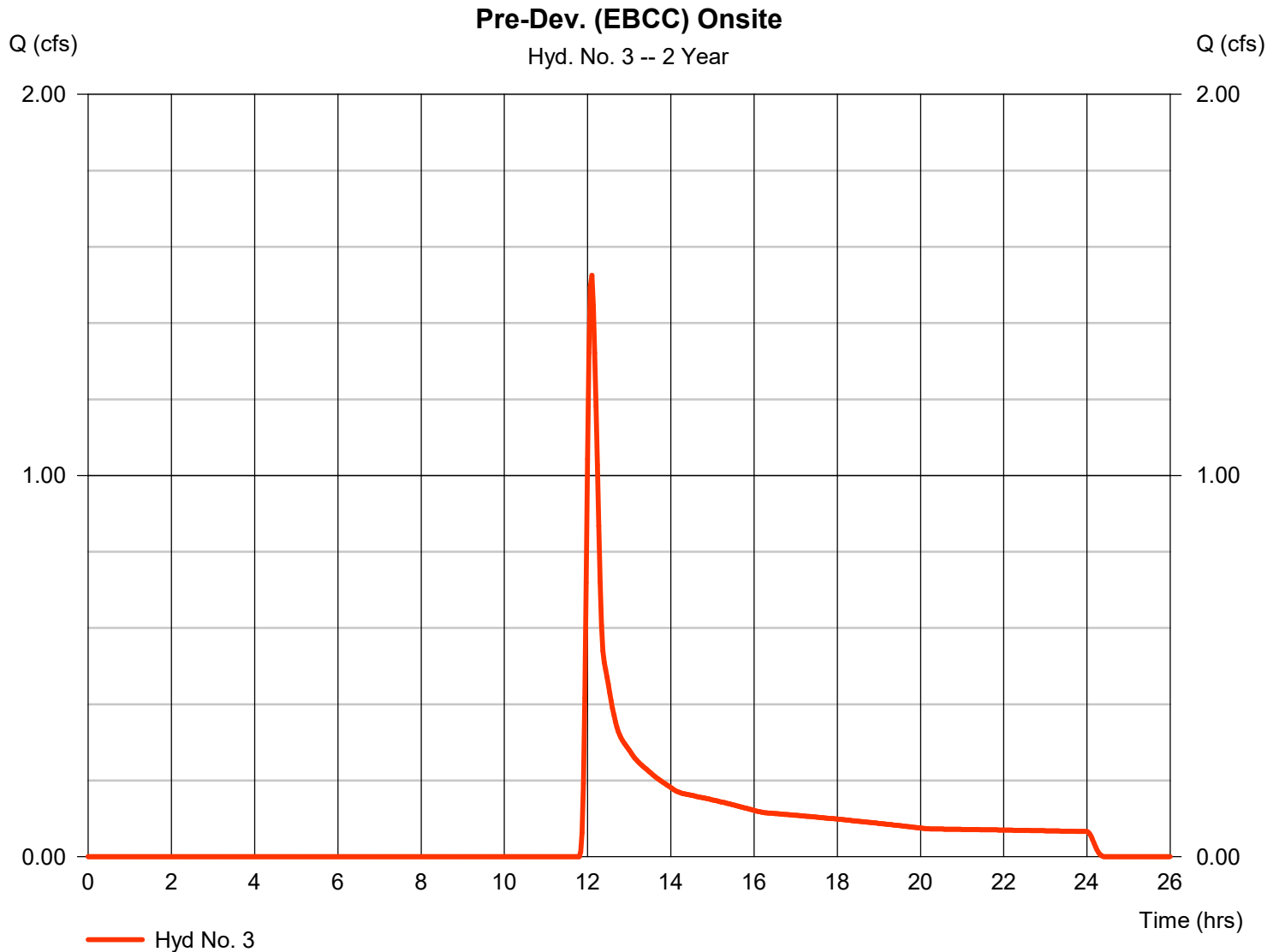


Hydrograph Report

Hyd. No. 3

Pre-Dev. (EBCC) Onsite

Hydrograph type	= SCS Runoff	Peak discharge	= 1.525 cfs
Storm frequency	= 2 yrs	Time to peak	= 12.10 hrs
Time interval	= 2 min	Hyd. volume	= 6,891 cuft
Drainage area	= 4.910 ac	Curve number	= 59
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 15.00 min
Total precip.	= 3.26 in	Distribution	= Type II
Storm duration	= 24 hrs	Shape factor	= 484

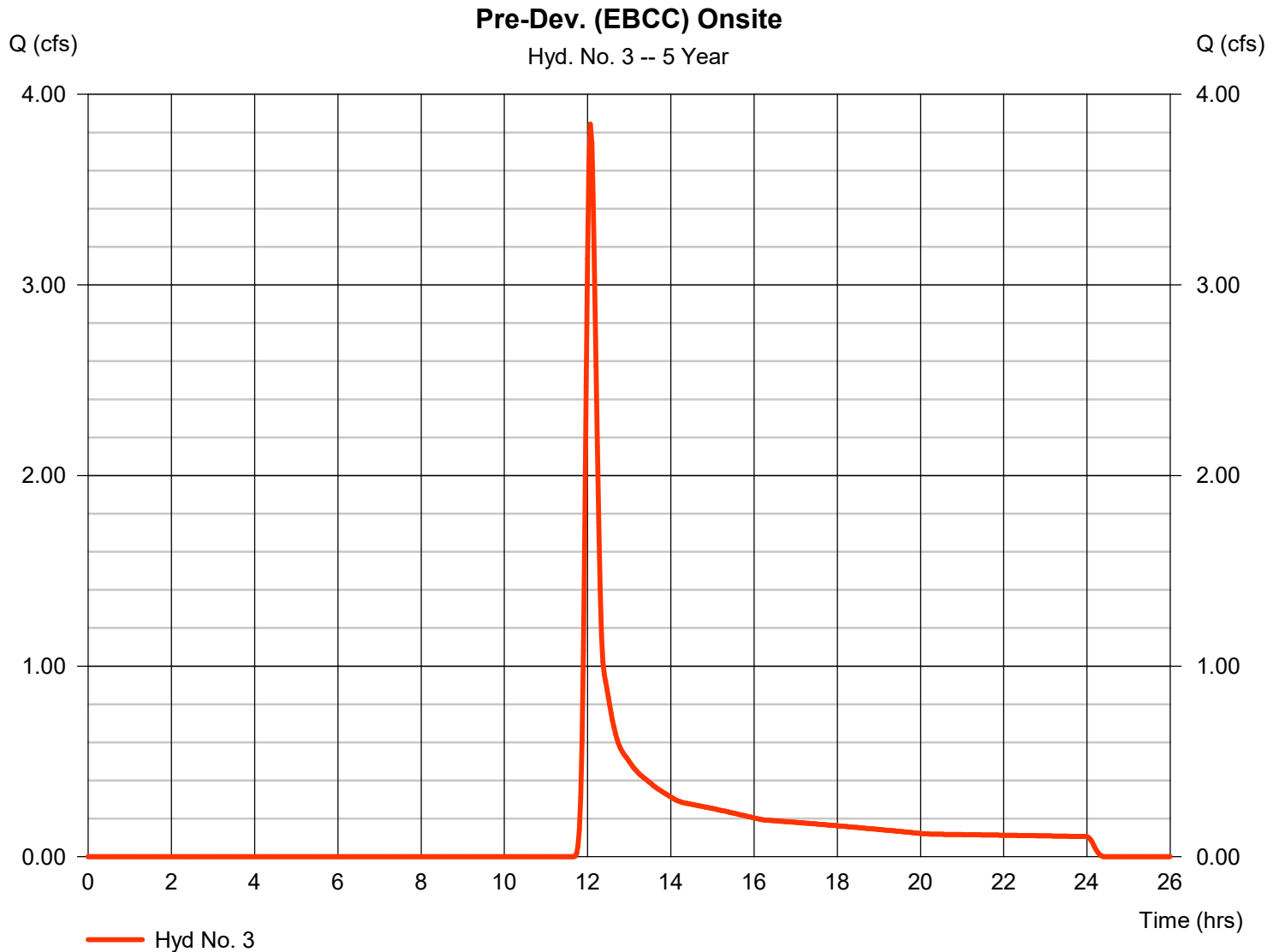


Hydrograph Report

Hyd. No. 3

Pre-Dev. (EBCC) Onsite

Hydrograph type	= SCS Runoff	Peak discharge	= 3.844 cfs
Storm frequency	= 5 yrs	Time to peak	= 12.07 hrs
Time interval	= 2 min	Hyd. volume	= 13,214 cuft
Drainage area	= 4.910 ac	Curve number	= 59
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 15.00 min
Total precip.	= 4.10 in	Distribution	= Type II
Storm duration	= 24 hrs	Shape factor	= 484

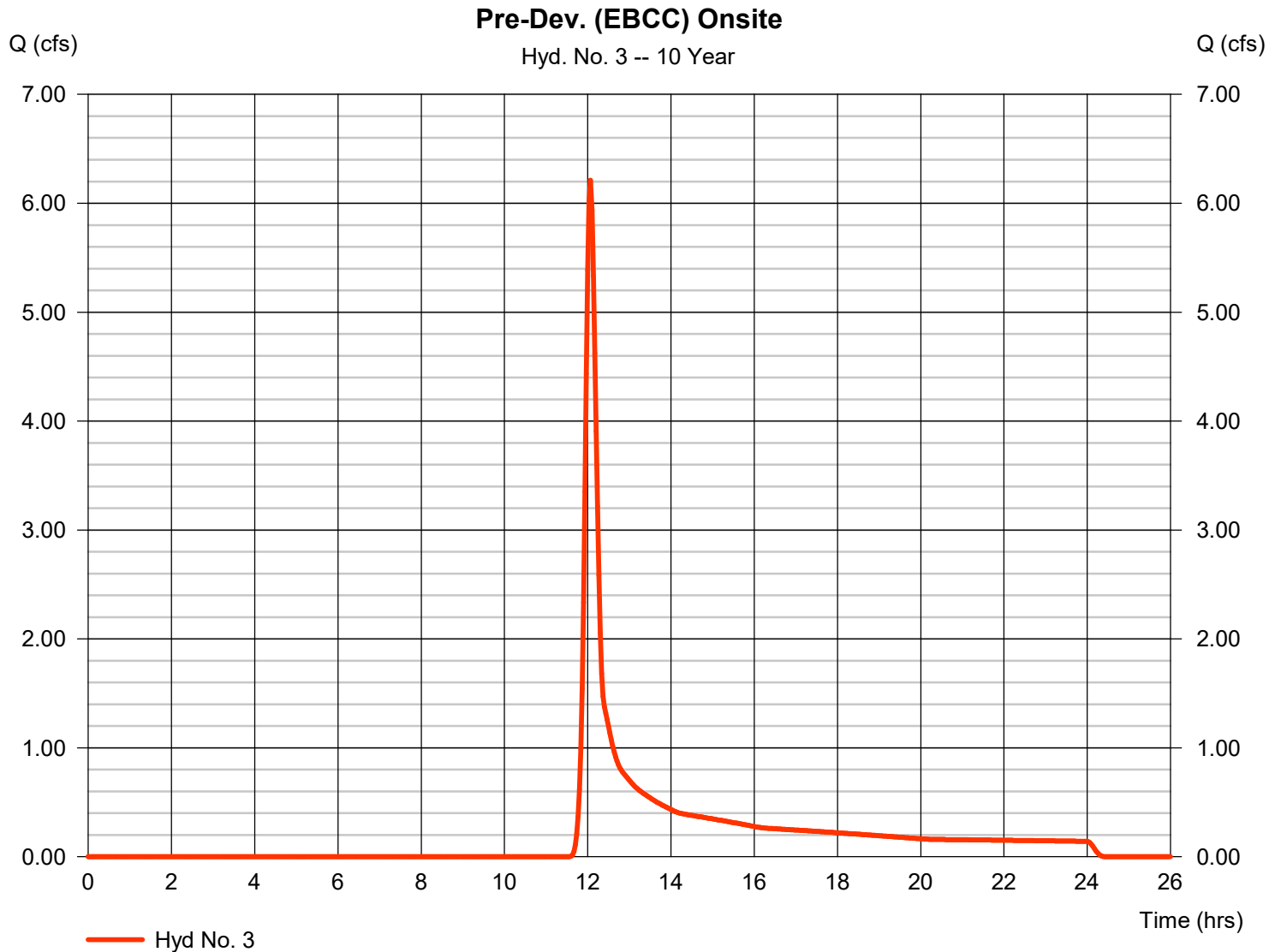


Hydrograph Report

Hyd. No. 3

Pre-Dev. (EBCC) Onsite

Hydrograph type	= SCS Runoff	Peak discharge	= 6.212 cfs
Storm frequency	= 10 yrs	Time to peak	= 12.07 hrs
Time interval	= 2 min	Hyd. volume	= 19,508 cuft
Drainage area	= 4.910 ac	Curve number	= 59
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 15.00 min
Total precip.	= 4.80 in	Distribution	= Type II
Storm duration	= 24 hrs	Shape factor	= 484

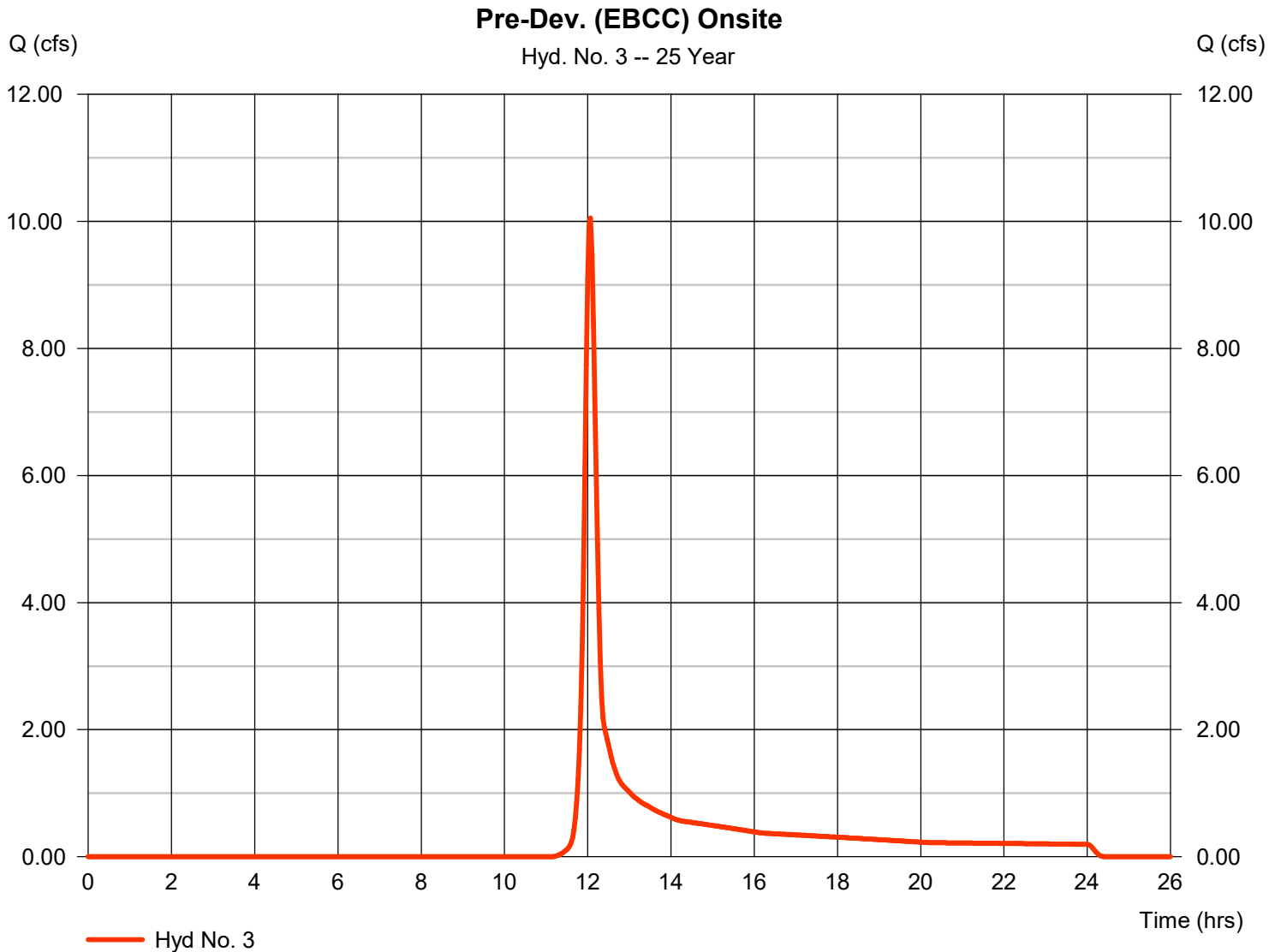


Hydrograph Report

Hyd. No. 3

Pre-Dev. (EBCC) Onsite

Hydrograph type	= SCS Runoff	Peak discharge	= 10.05 cfs
Storm frequency	= 25 yrs	Time to peak	= 12.07 hrs
Time interval	= 2 min	Hyd. volume	= 29,863 cuft
Drainage area	= 4.910 ac	Curve number	= 59
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 15.00 min
Total precip.	= 5.81 in	Distribution	= Type II
Storm duration	= 24 hrs	Shape factor	= 484

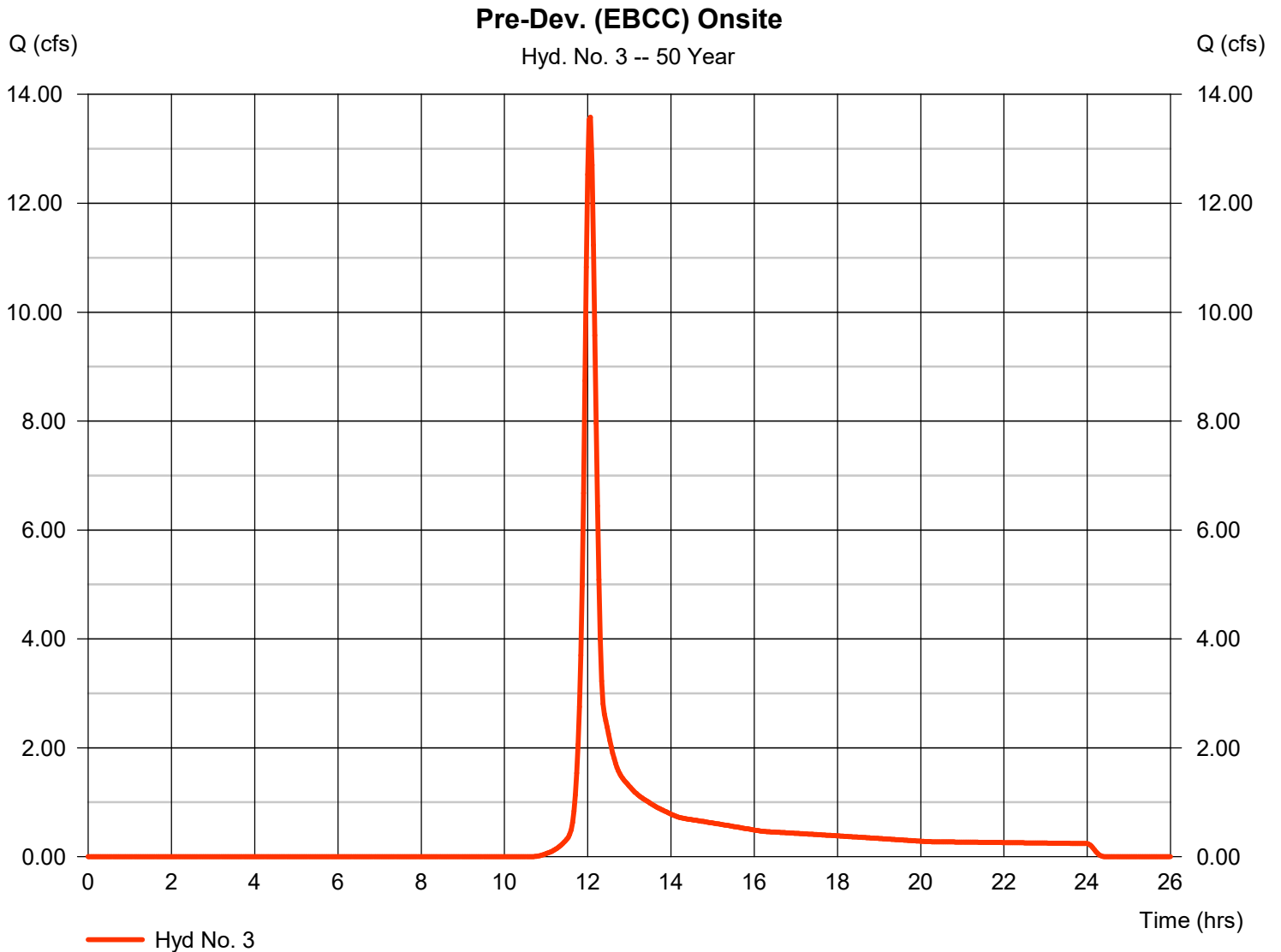


Hydrograph Report

Hyd. No. 3

Pre-Dev. (EBCC) Onsite

Hydrograph type	= SCS Runoff	Peak discharge	= 13.58 cfs
Storm frequency	= 50 yrs	Time to peak	= 12.07 hrs
Time interval	= 2 min	Hyd. volume	= 39,500 cuft
Drainage area	= 4.910 ac	Curve number	= 59
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 15.00 min
Total precip.	= 6.66 in	Distribution	= Type II
Storm duration	= 24 hrs	Shape factor	= 484

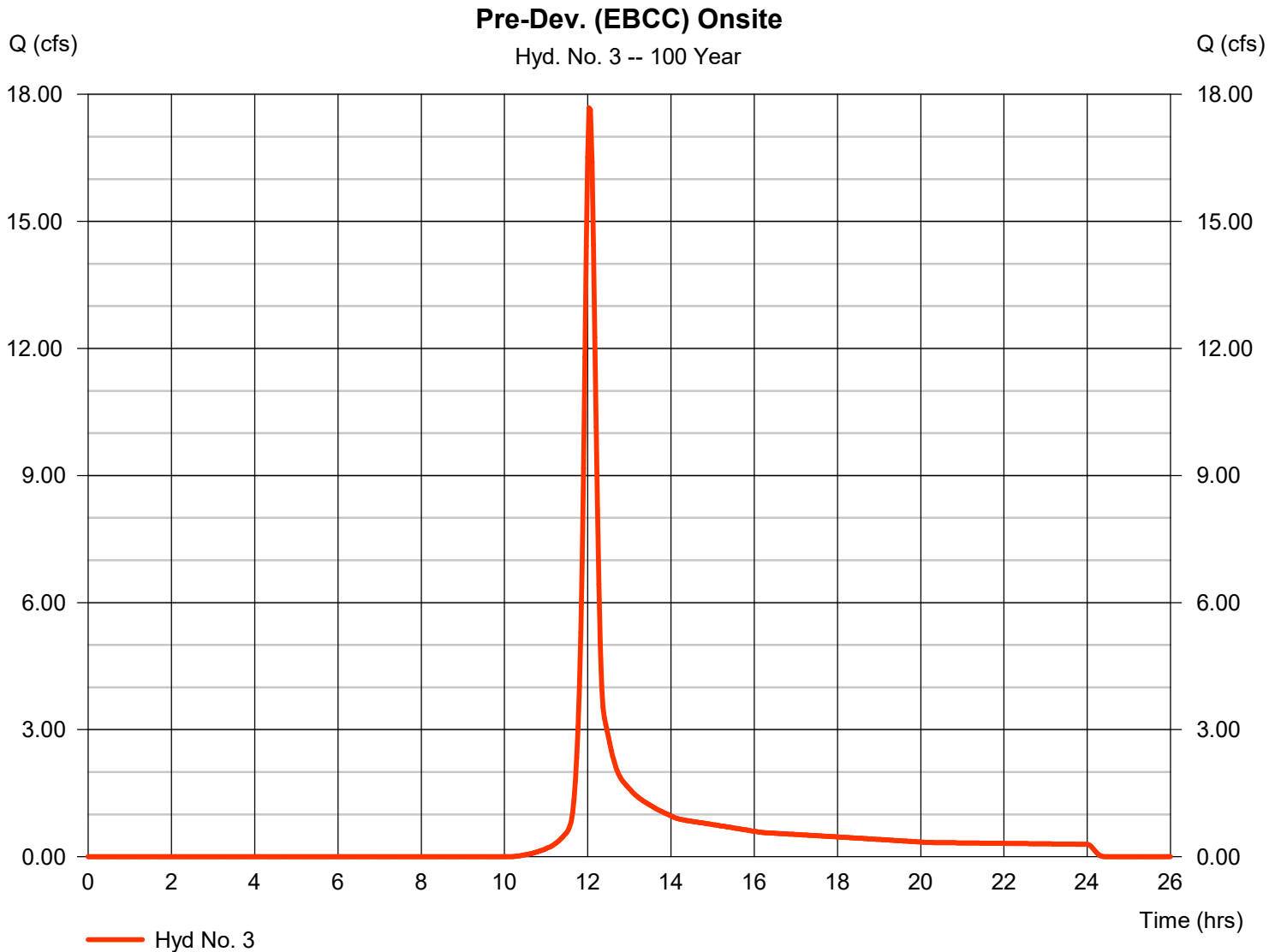


Hydrograph Report

Hyd. No. 3

Pre-Dev. (EBCC) Onsite

Hydrograph type	= SCS Runoff	Peak discharge	= 17.68 cfs
Storm frequency	= 100 yrs	Time to peak	= 12.03 hrs
Time interval	= 2 min	Hyd. volume	= 50,679 cuft
Drainage area	= 4.910 ac	Curve number	= 59
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 15.00 min
Total precip.	= 7.58 in	Distribution	= Type II
Storm duration	= 24 hrs	Shape factor	= 484



UNT. TO EAST BRANCH CHESTER CREEK



ELA SPORT
ATHLETIC FACILITIES DESIGN
& CONSULTING

737 S. BROAD STREET
 LITITZ, PA 17543
 (717) 626-72713

PROJECT: The Westtown School - Oak Lane Project
CATION: Westtown Township
COUNTY: Chester

LAND USE	Parking, Other Impervious (60% of total)			40% of Impervious Areas as Meadow			Meadow	Total Area (ac.)	Composite 'CN' Value	Tc Min.
	B	B	D	B	B	D	Meadow			
HSG	98	58	78	58	58	78				
"CN" Value	Area (ac)									
WATERSHED										
Unt. to East Branch Chester Creek										
	0.01	0.00	2.11	0.00	15.25	2.11	17.37	60	22	
Unt. to EBCC Onsite (Reduction Factor)										
	0.01	0.00	1.14	0.00	11.53	1.14	12.68	60	22	

ELA SPORT
ATHLETIC FACILITIES
DESIGN & CONSULTING

737 S. BROAD STREET
 LITITZ, PA 17543
 (717) 626-72713



SUMMARY - SUBAREAS TIME OF CONCENTRATION PRE-DEVELOPMENT CONDITIONS

PROJECT: The Westtown School - Oak Lane Project
 LOCATION: Westtown Township
 COUNTY: Chester

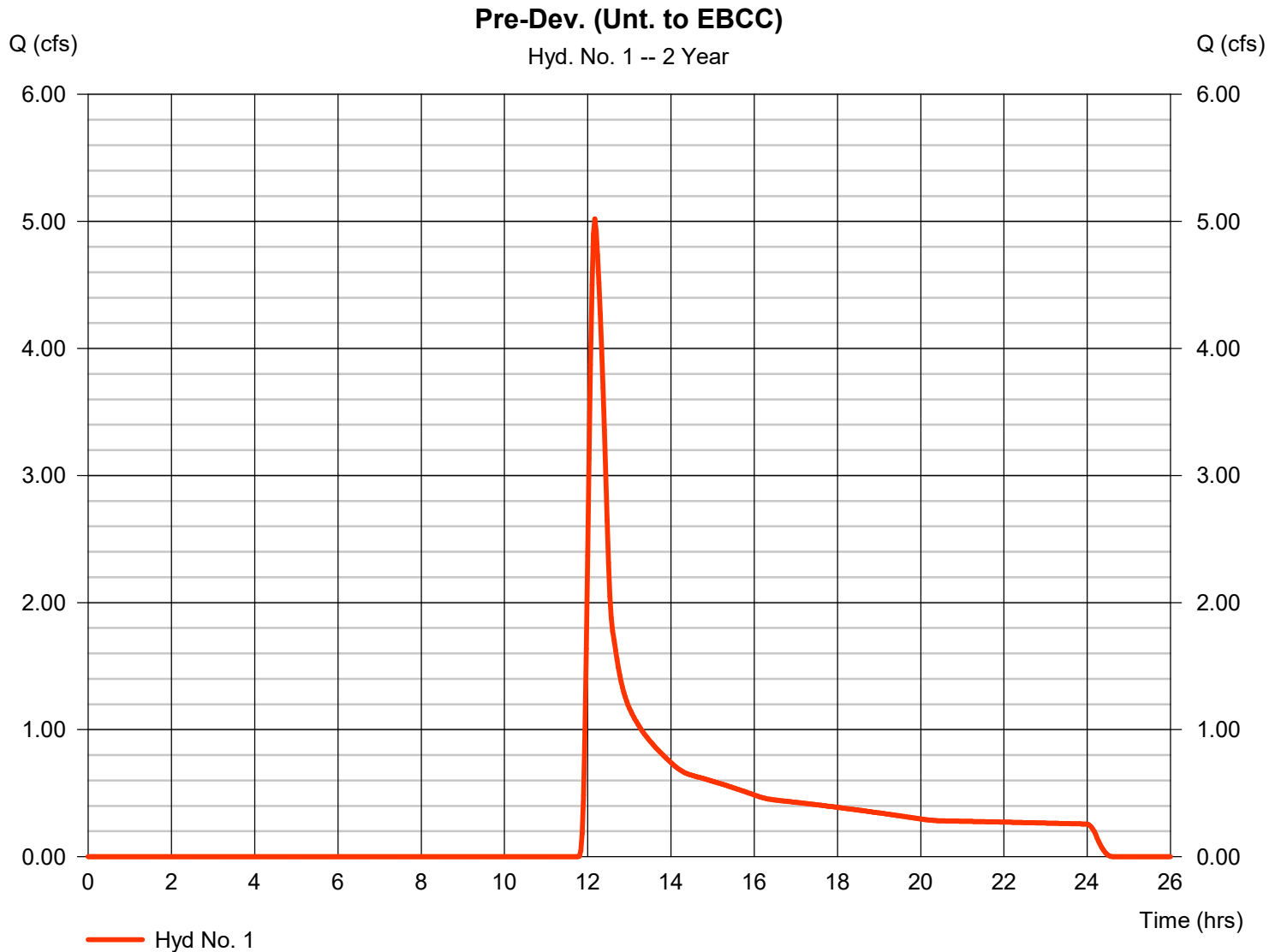
Time of concentration (Tc) or travel time (Tt)																						
overland					Shallow Concentrated					Channel or Pipe										Total		
Watershed	Length L ₁ ft.	Slope S ₁ ft./ft.	Manning's n	2 yr rainfall in.	Tc Min.	Flow Path U/P	Length L ₂ ft.	Slope S ₂ ft./ft.	Average Velocity ft./s	Velocity ft./s	Tt Min.	Channel or Pipe C/P	Flow Area sq.ft.	Wetted Perimeter ft.	Pipe Diameter in.	Slope S ₃ ft./ft.	Manning's n	Length L ₃ ft.	Tt Min.	Total Min.	Total Hrs.	
B	100	0.010	0.24	3.26	18.7	U	293	0.010	0	0	0.0		0.00	0.00						0.0		
					0	U	108	0.140	1.6	3.1	0.0		0.00	0.00						0.0		
					0	U			6	0.3	0.0		0.00	0.00						0.0		
					0				0	0	0.0		0.00	0.00						0.0		
					0				0	0	0.0		0.00	0.00						0.0		
					0				0	0	0.0		0.00	0.00						0.0		
					0				0	0	0.0		0.00	0.00						0.0		
					0				0	0	0.0		0.00	0.00						0.0		
					0				0	0	0.0		0.00	0.00						0.0		
					0				0	0	0.0		0.00	0.00						0.0		
					0				0	0	0.0		0.00	0.00						0.0		
					0				0	0	0.0		0.00	0.00						0.0		
					0				0	0	0.0		0.00	0.00						0.0		
					0				0	0	0.0		0.00	0.00						0.0		
					0				0	0	0.0		0.00	0.00						0.0		
					0				0	0	0.0		0.00	0.00						0.0		
					0				0	0	0.0		0.00	0.00						0.0		
					0				0	0	0.0		0.00	0.00						0.0		
					0				0	0	0.0		0.00	0.00						0.0		
					0				0	0	0.0		0.00	0.00						0.0		
					0				0	0	0.0		0.00	0.00						0.0		
					0				0	0	0.0		0.00	0.00						0.0		
					0				0	0	0.0		0.00	0.00						0.0		
					0				0	0	0.0		0.00	0.00						0.0		
					0				0	0	0.0		0.00	0.00						0.0		
					0				0	0	0.0		0.00	0.00						0.0		
					0				0	0	0.0		0.00	0.00						0.0		
					0				0	0	0.0		0.00	0.00						0.0		
					0				0	0	0.0		0.00	0.00						0.0		
					0				0	0	0.0		0.00	0.00						0.0		
					0				0	0	0.0		0.00	0.00						0.0		
					0				0	0	0.0		0.00	0.00						0.0		
					0				0	0	0.0		0.00	0.00						0.0		
					0				0	0	0.0		0.00	0.00						0.0		
					0				0	0	0.0		0.00	0.00						0.0		
					0				0	0	0.0		0.00	0.00						0.0		
					0				0	0	0.0		0.00	0.00						0.0		
					0				0	0	0.0		0.00	0.00						0.0		
					0				0	0	0.0		0.00	0.00						0.0		
					0				0	0	0.0		0.00	0.00						0.0		
					0				0	0	0.0		0.00	0.00						0.0		
					0				0	0	0.0		0.00	0.00						0.0		
					0				0	0	0.0		0.00	0.00						0.0		
					0				0	0	0.0		0.00	0.00						0.0		
					0				0	0	0.0		0.00	0.00						0.0		
					0				0	0	0.0		0.00	0.00						0.0		
					0				0	0	0.0		0.00	0.00						0.0		
					0				0	0	0.0		0.00	0.00						0.0		
					0				0	0	0.0		0.00	0.00						0.0		
					0				0	0	0.0		0.00	0.00						0.0		
					0				0	0	0.0		0.00	0.00						0.0		
					0				0	0	0.0		0.00	0.00						0.0		
					0				0	0	0.0		0.00	0.00						0.0		
					0				0	0	0.0		0.00	0.00						0.0		
					0				0	0	0.0		0.00	0.00						0.0		
					0				0	0	0.0		0.00	0.00						0.0		
					0				0	0	0.0		0.00	0.00						0.0		
					0				0	0	0.0		0.00	0.00						0.0		
					0				0	0	0.0		0.00	0.00						0.0		
					0				0	0	0.0		0.00	0.00						0.0		
					0				0	0	0.0		0.00	0.00						0.0		
					0				0	0	0.0		0.00	0.00						0.0		
					0				0	0	0.0		0.00	0.00						0.0		
					0				0	0	0.0		0.00	0.00						0.0		
					0				0	0	0.0		0.00	0.00						0.0		
					0				0	0	0.0		0.00	0.00						0.0		
					0				0	0	0.0		0.00	0.00						0.0		
					0				0	0	0.0		0.00	0.00						0.0		
					0				0	0	0.0		0.00	0.00						0.0		
					0				0	0	0.0		0.00	0.00						0.0		
					0				0	0	0.0		0.00	0.00						0.0		
					0				0	0	0.0		0.00	0.00						0.0		
					0				0	0	0.0		0.00	0.00						0.0		
					0				0	0	0.0		0.00	0.00						0.0		
					0				0	0	0.0		0.00	0.00						0.0		
					0				0	0	0.0		0.00	0.00						0.0		
					0				0	0	0.0		0.00	0.00						0.0		
					0				0	0	0.0		0.00	0.00						0.0		
					0				0	0	0.0		0.00	0.00						0.0		
					0																	

Hydrograph Report

Hyd. No. 1

Pre-Dev. (Unt. to EBCC)

Hydrograph type	= SCS Runoff	Peak discharge	= 5.020 cfs
Storm frequency	= 2 yrs	Time to peak	= 12.17 hrs
Time interval	= 2 min	Hyd. volume	= 27,714 cuft
Drainage area	= 17.370 ac	Curve number	= 60
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 22.00 min
Total precip.	= 3.26 in	Distribution	= Type II
Storm duration	= 24 hrs	Shape factor	= 484

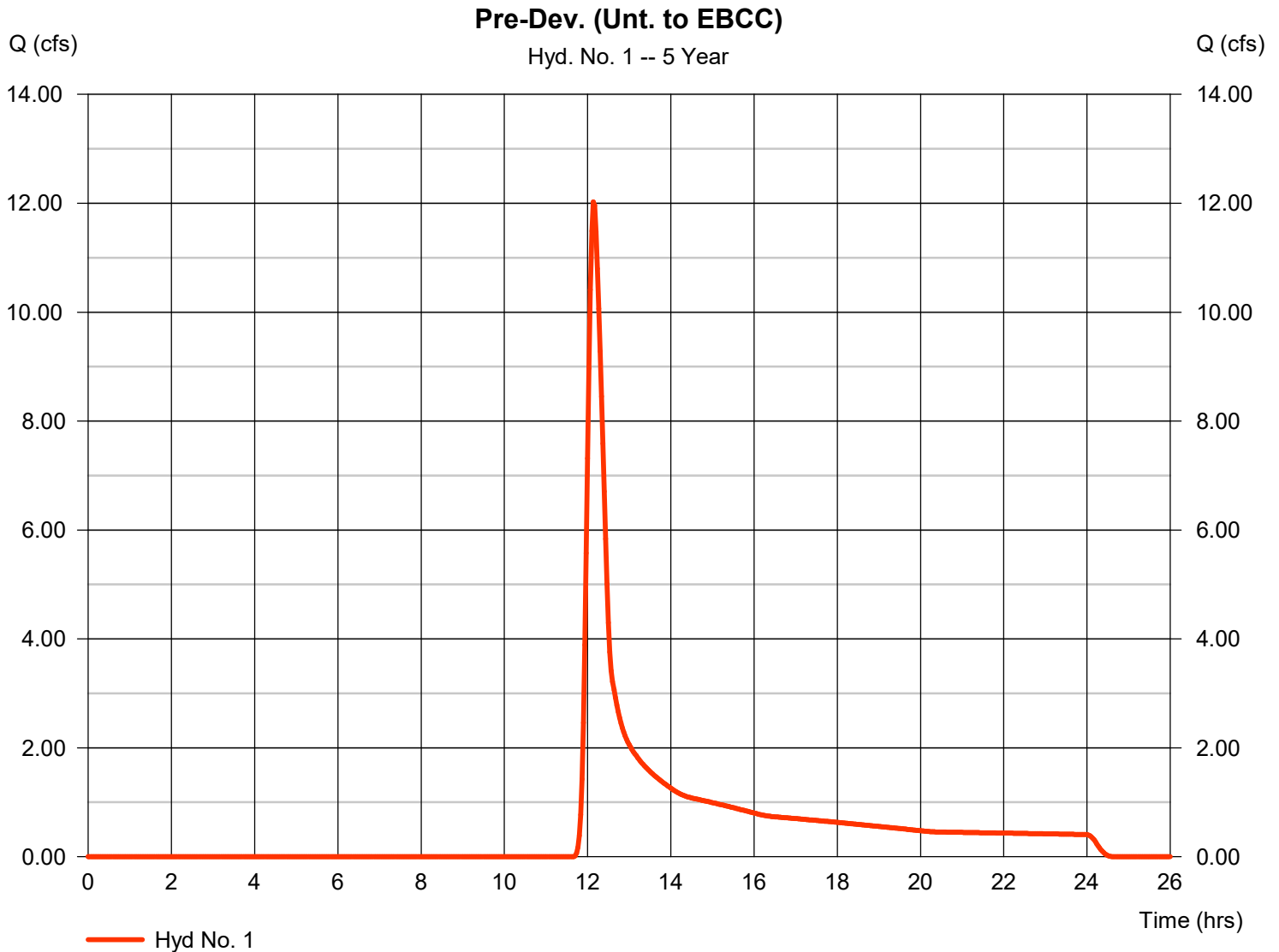


Hydrograph Report

Hyd. No. 1

Pre-Dev. (Unt. to EBCC)

Hydrograph type	= SCS Runoff	Peak discharge	= 12.03 cfs
Storm frequency	= 5 yrs	Time to peak	= 12.13 hrs
Time interval	= 2 min	Hyd. volume	= 52,072 cuft
Drainage area	= 17.370 ac	Curve number	= 60
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 22.00 min
Total precip.	= 4.10 in	Distribution	= Type II
Storm duration	= 24 hrs	Shape factor	= 484

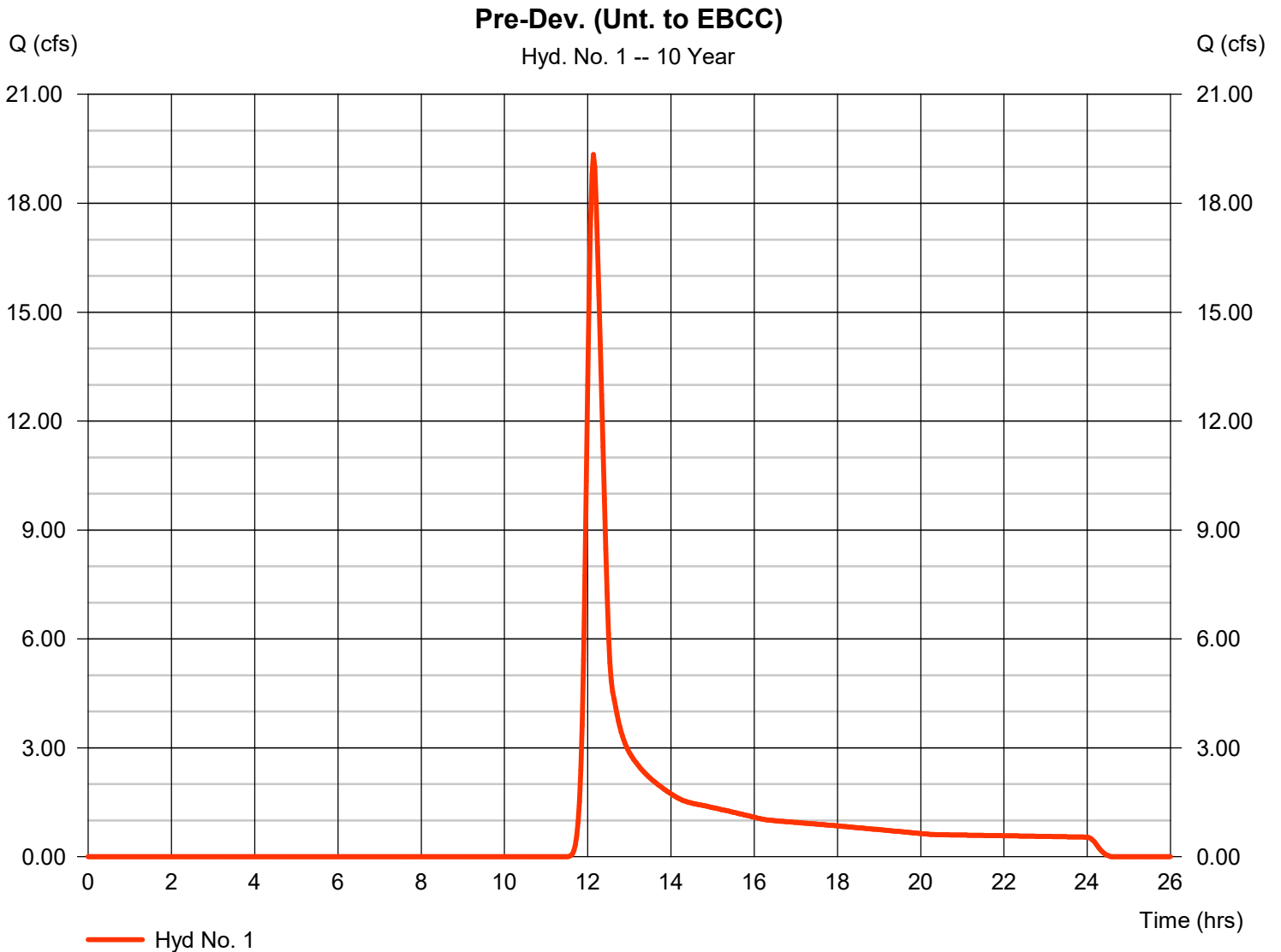


Hydrograph Report

Hyd. No. 1

Pre-Dev. (Unt. to EBCC)

Hydrograph type	= SCS Runoff	Peak discharge	= 19.34 cfs
Storm frequency	= 10 yrs	Time to peak	= 12.13 hrs
Time interval	= 2 min	Hyd. volume	= 76,114 cuft
Drainage area	= 17.370 ac	Curve number	= 60
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 22.00 min
Total precip.	= 4.80 in	Distribution	= Type II
Storm duration	= 24 hrs	Shape factor	= 484

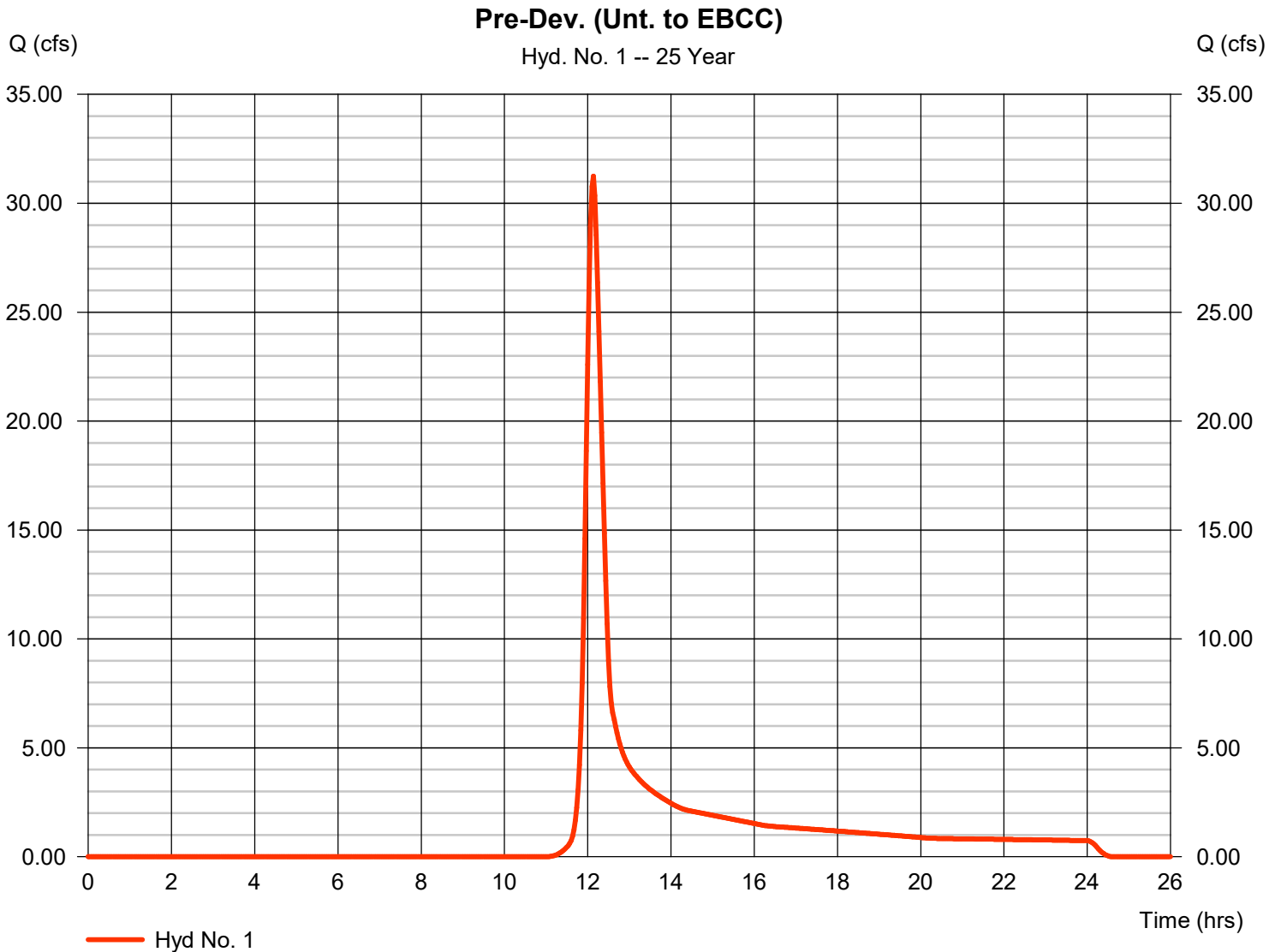


Hydrograph Report

Hyd. No. 1

Pre-Dev. (Unt. to EBCC)

Hydrograph type	= SCS Runoff	Peak discharge	= 31.25 cfs
Storm frequency	= 25 yrs	Time to peak	= 12.13 hrs
Time interval	= 2 min	Hyd. volume	= 115,422 cuft
Drainage area	= 17.370 ac	Curve number	= 60
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 22.00 min
Total precip.	= 5.81 in	Distribution	= Type II
Storm duration	= 24 hrs	Shape factor	= 484

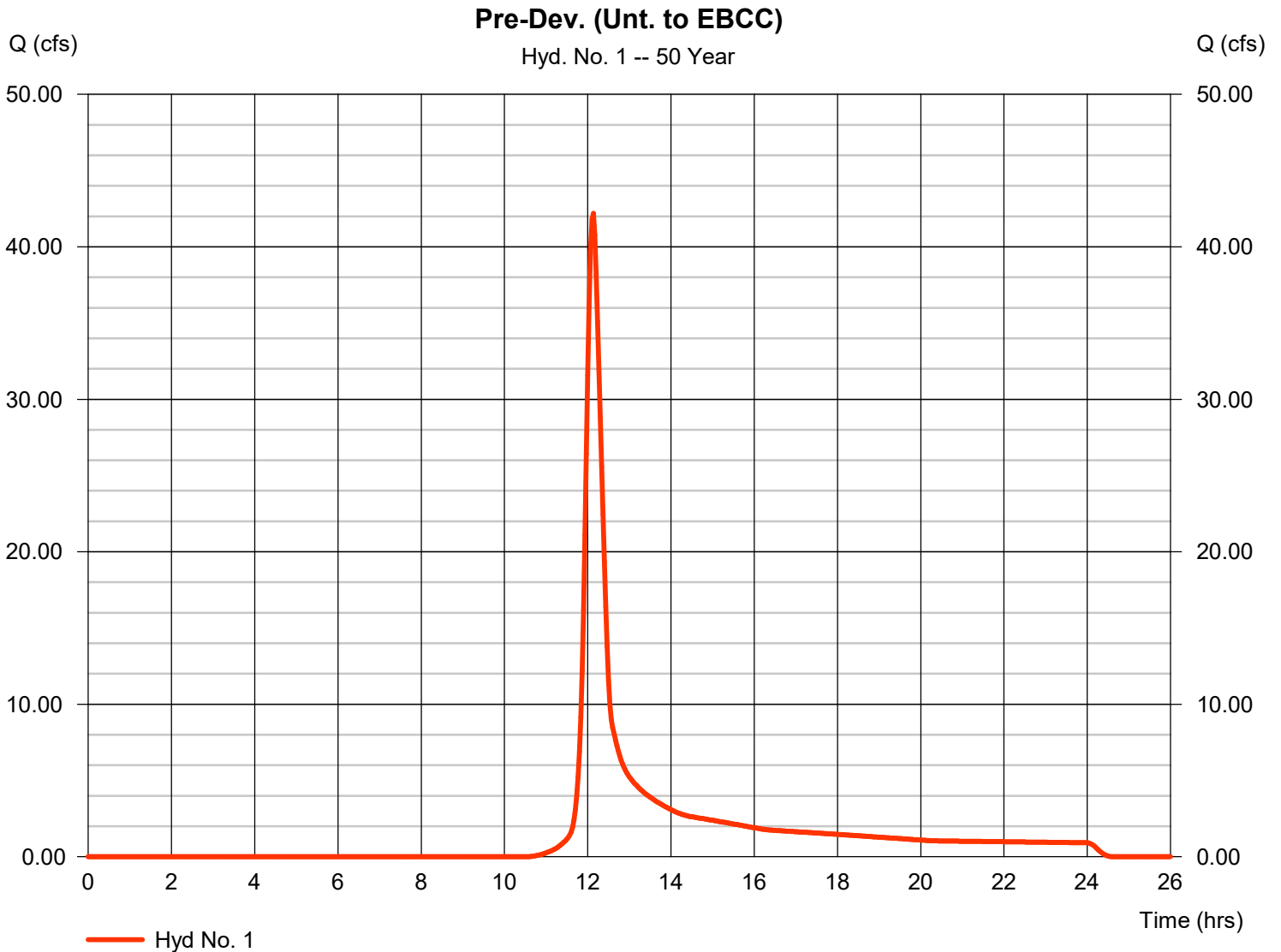


Hydrograph Report

Hyd. No. 1

Pre-Dev. (Unt. to EBCC)

Hydrograph type	= SCS Runoff	Peak discharge	= 42.19 cfs
Storm frequency	= 50 yrs	Time to peak	= 12.13 hrs
Time interval	= 2 min	Hyd. volume	= 151,832 cuft
Drainage area	= 17.370 ac	Curve number	= 60
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 22.00 min
Total precip.	= 6.66 in	Distribution	= Type II
Storm duration	= 24 hrs	Shape factor	= 484

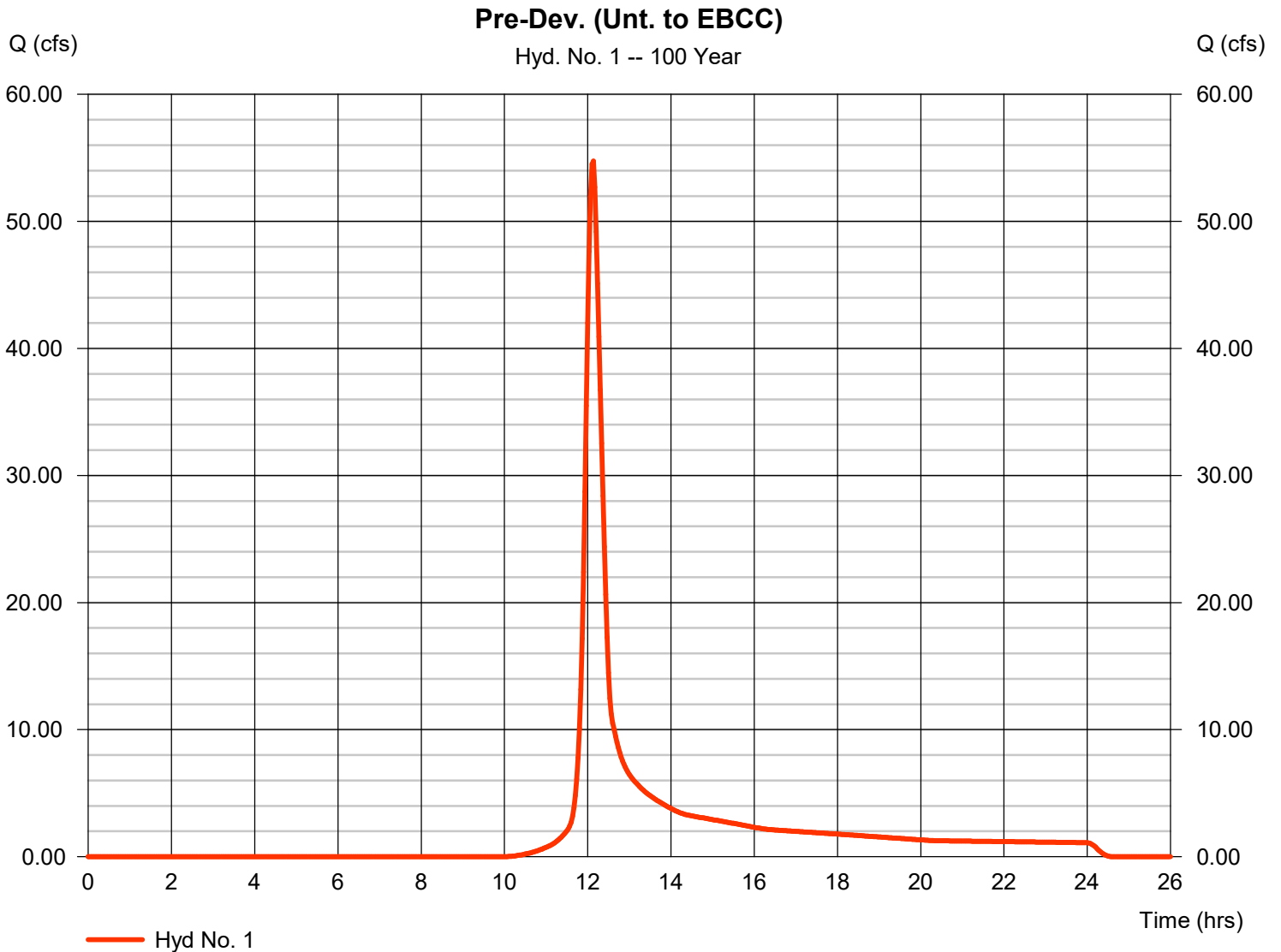


Hydrograph Report

Hyd. No. 1

Pre-Dev. (Unt. to EBCC)

Hydrograph type	= SCS Runoff	Peak discharge	= 54.74 cfs
Storm frequency	= 100 yrs	Time to peak	= 12.13 hrs
Time interval	= 2 min	Hyd. volume	= 193,933 cuft
Drainage area	= 17.370 ac	Curve number	= 60
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 22.00 min
Total precip.	= 7.58 in	Distribution	= Type II
Storm duration	= 24 hrs	Shape factor	= 484

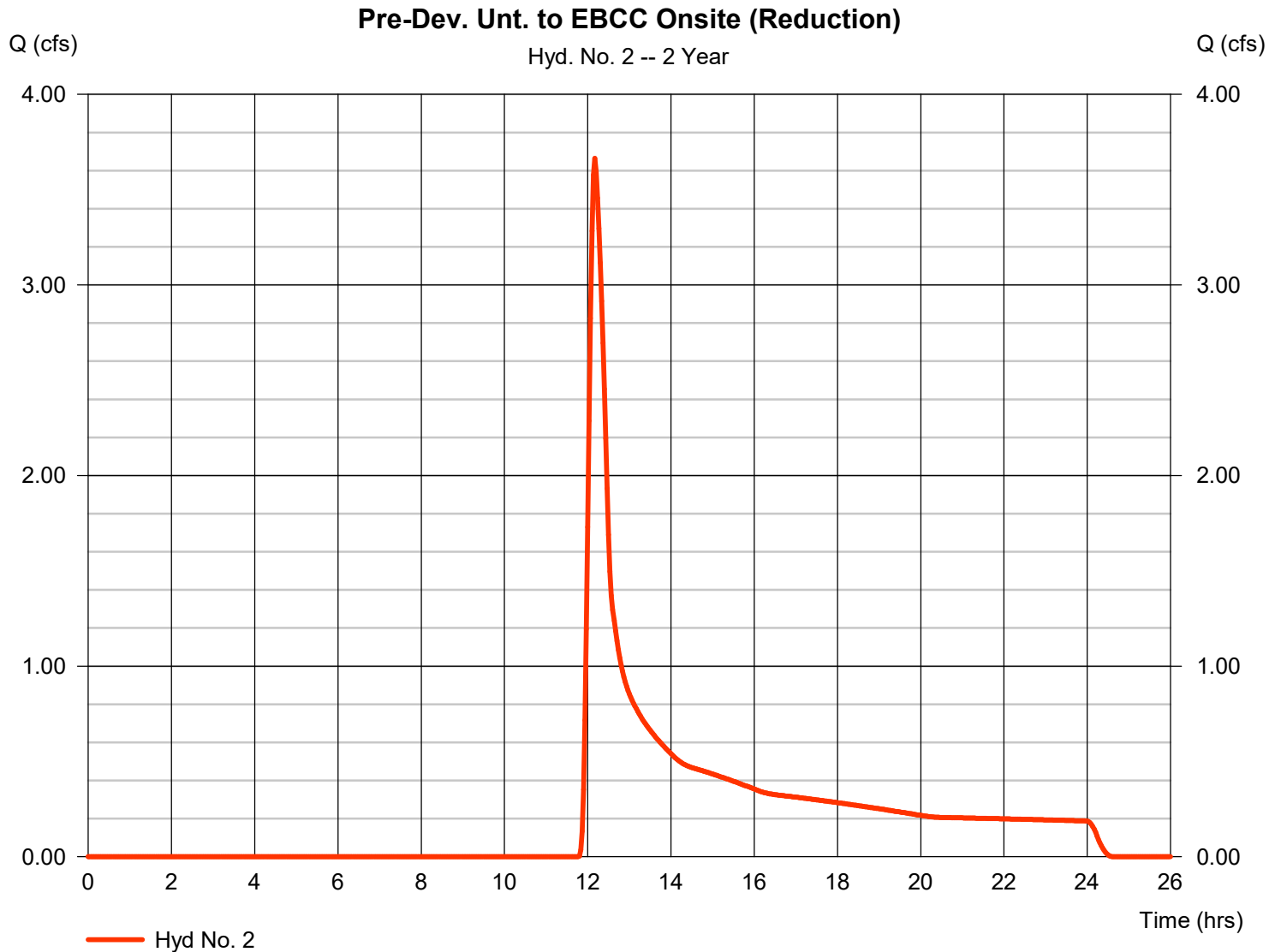


Hydrograph Report

Hyd. No. 2

Pre-Dev. Unt. to EBCC Onsite (Reduction)

Hydrograph type	= SCS Runoff	Peak discharge	= 3.664 cfs
Storm frequency	= 2 yrs	Time to peak	= 12.17 hrs
Time interval	= 2 min	Hyd. volume	= 20,231 cuft
Drainage area	= 12.680 ac	Curve number	= 60
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 22.00 min
Total precip.	= 3.26 in	Distribution	= Type II
Storm duration	= 24 hrs	Shape factor	= 484

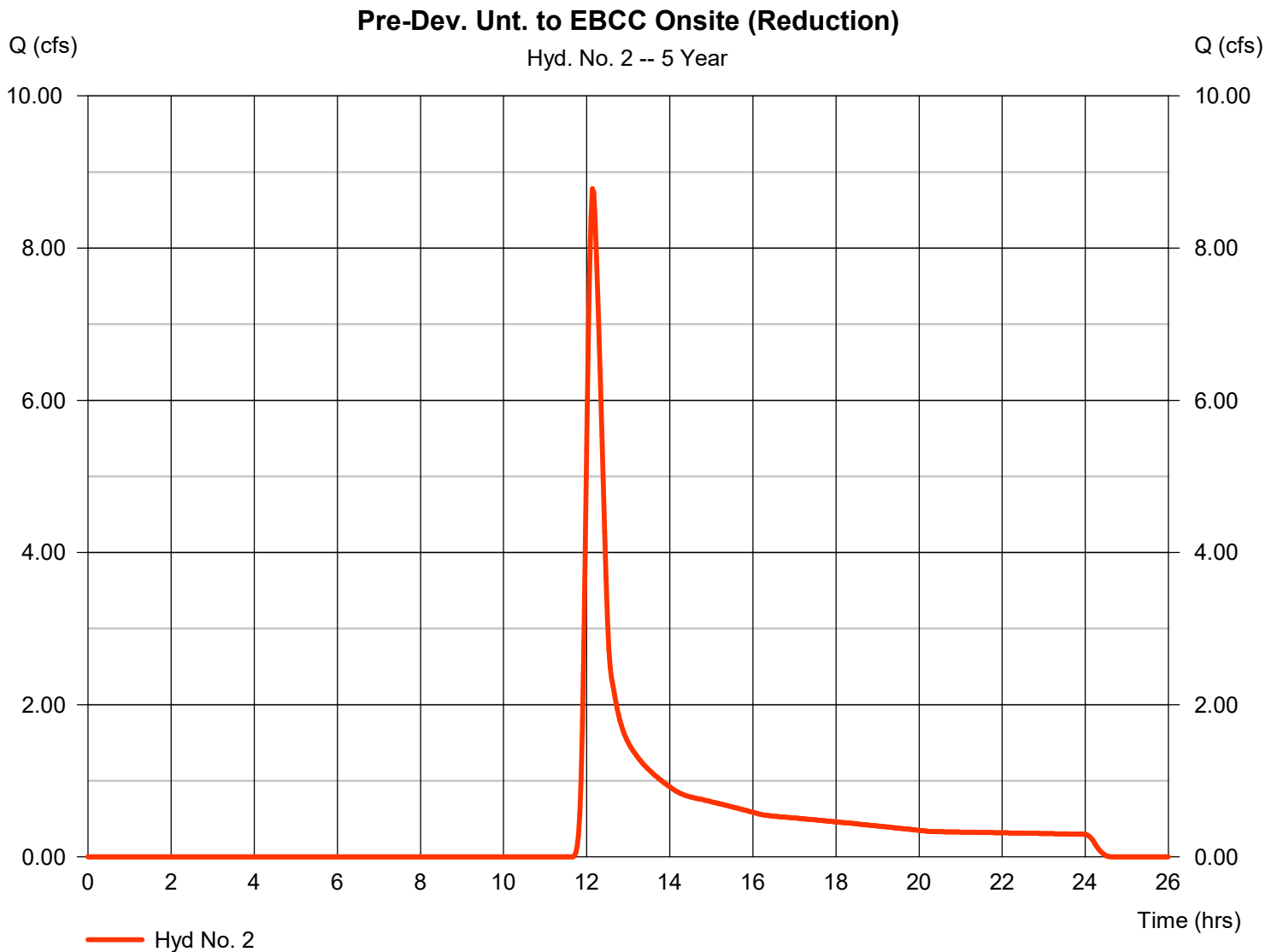


Hydrograph Report

Hyd. No. 2

Pre-Dev. Unt. to EBCC Onsite (Reduction)

Hydrograph type	= SCS Runoff	Peak discharge	= 8.779 cfs
Storm frequency	= 5 yrs	Time to peak	= 12.13 hrs
Time interval	= 2 min	Hyd. volume	= 38,012 cuft
Drainage area	= 12.680 ac	Curve number	= 60
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 22.00 min
Total precip.	= 4.10 in	Distribution	= Type II
Storm duration	= 24 hrs	Shape factor	= 484

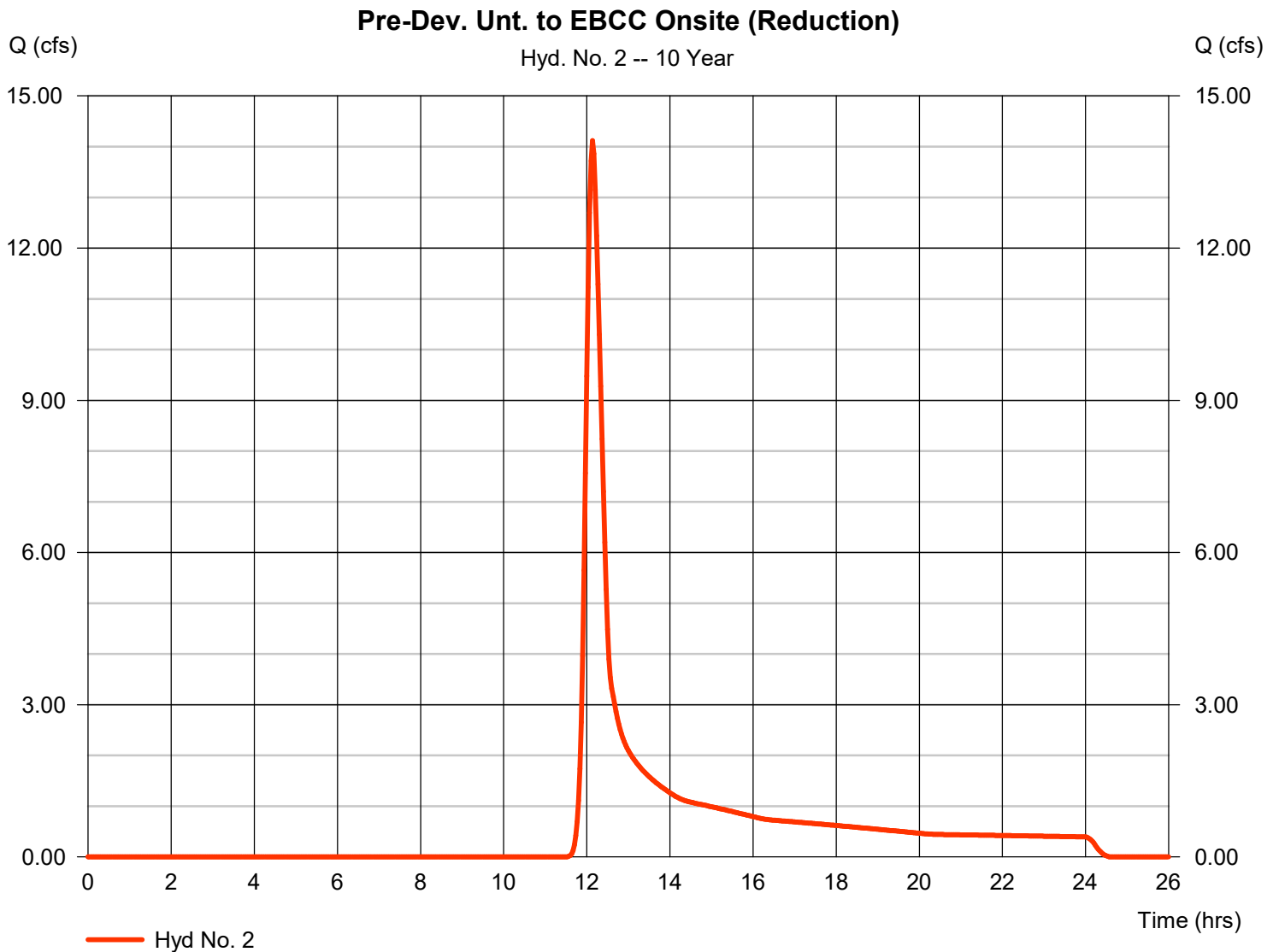


Hydrograph Report

Hyd. No. 2

Pre-Dev. Unt. to EBCC Onsite (Reduction)

Hydrograph type	= SCS Runoff	Peak discharge	= 14.12 cfs
Storm frequency	= 10 yrs	Time to peak	= 12.13 hrs
Time interval	= 2 min	Hyd. volume	= 55,563 cuft
Drainage area	= 12.680 ac	Curve number	= 60
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 22.00 min
Total precip.	= 4.80 in	Distribution	= Type II
Storm duration	= 24 hrs	Shape factor	= 484

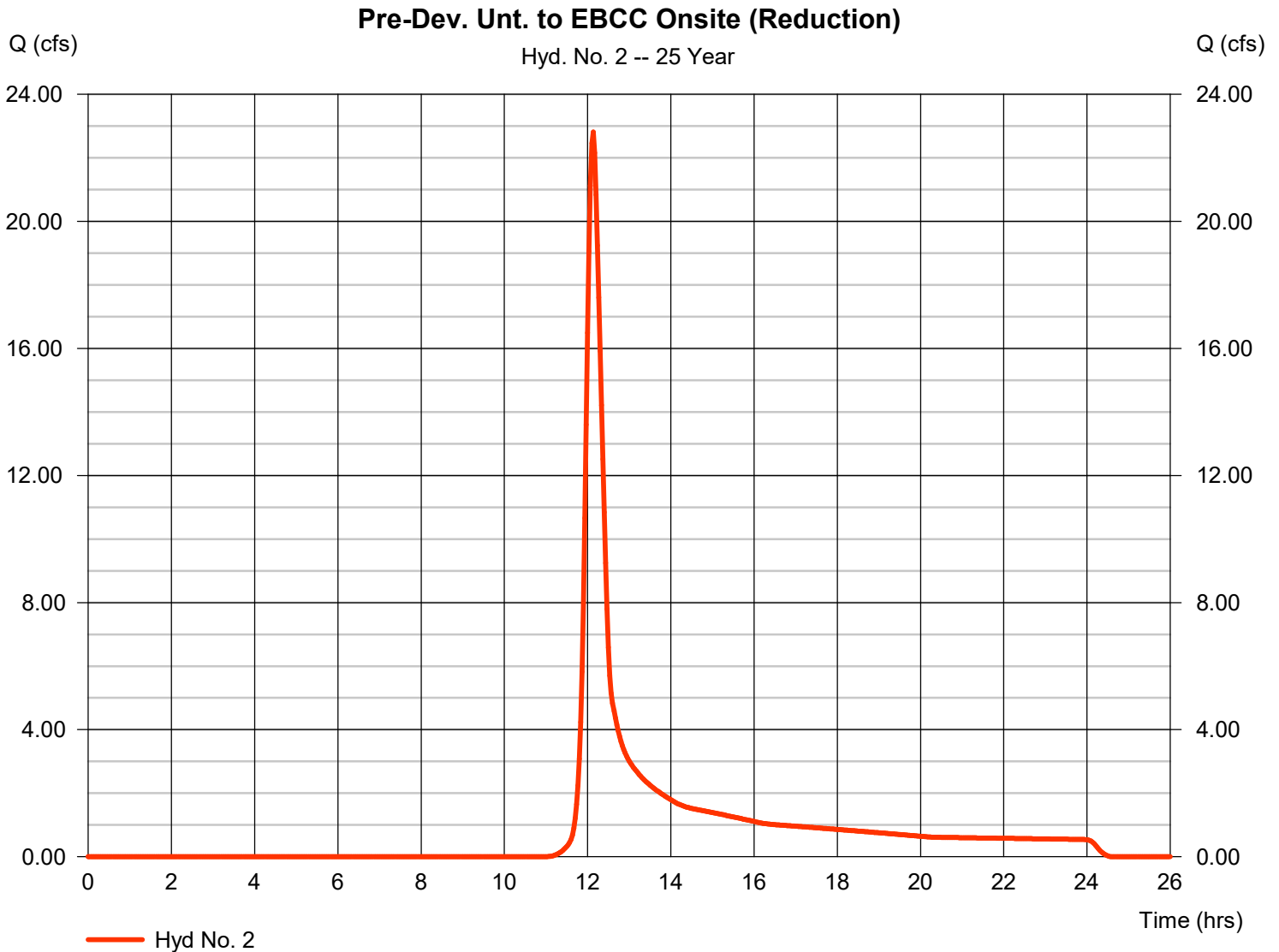


Hydrograph Report

Hyd. No. 2

Pre-Dev. Unt. to EBCC Onsite (Reduction)

Hydrograph type	= SCS Runoff	Peak discharge	= 22.81 cfs
Storm frequency	= 25 yrs	Time to peak	= 12.13 hrs
Time interval	= 2 min	Hyd. volume	= 84,257 cuft
Drainage area	= 12.680 ac	Curve number	= 60
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 22.00 min
Total precip.	= 5.81 in	Distribution	= Type II
Storm duration	= 24 hrs	Shape factor	= 484

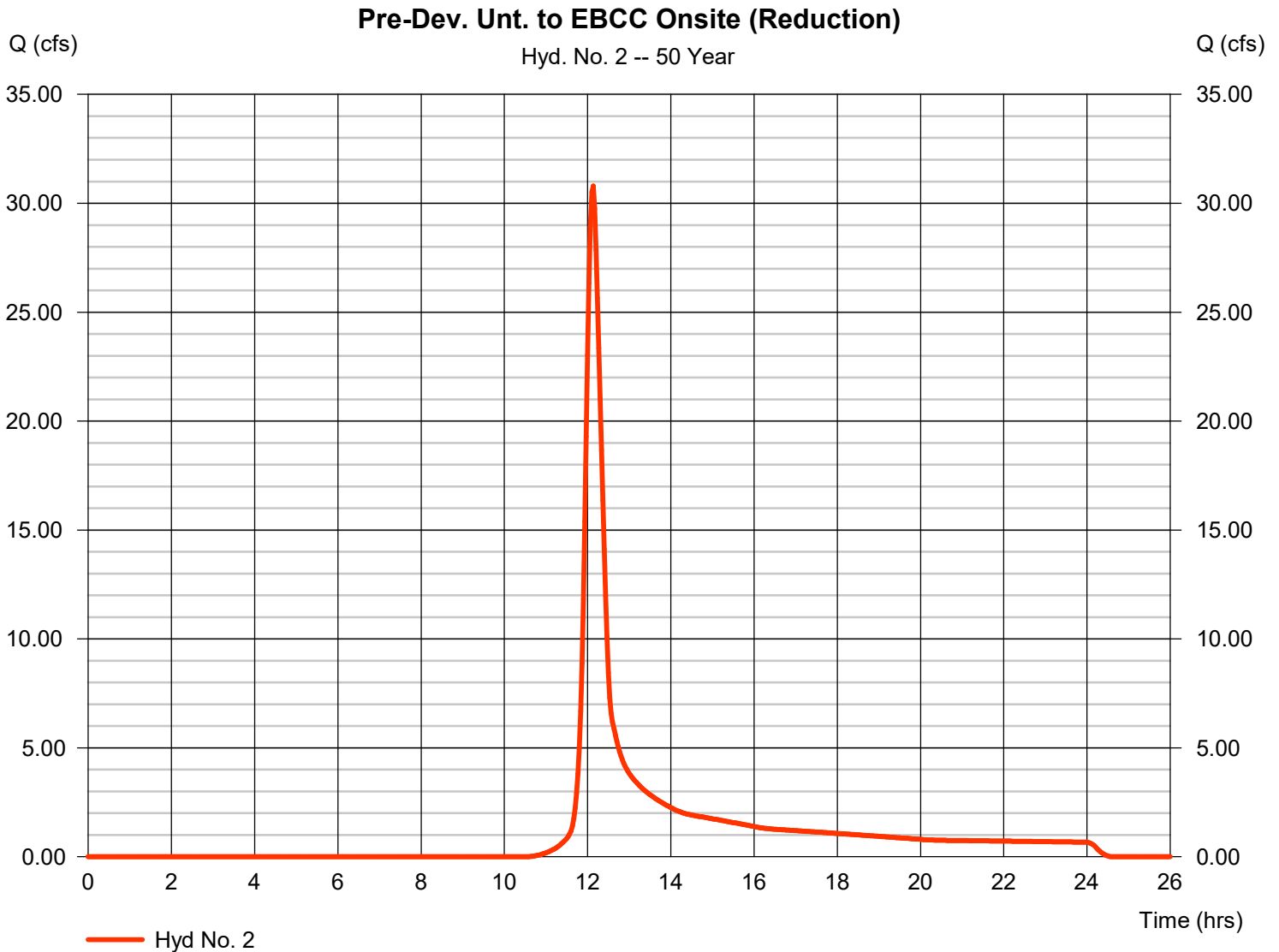


Hydrograph Report

Hyd. No. 2

Pre-Dev. Unt. to EBCC Onsite (Reduction)

Hydrograph type	= SCS Runoff	Peak discharge	= 30.80 cfs
Storm frequency	= 50 yrs	Time to peak	= 12.13 hrs
Time interval	= 2 min	Hyd. volume	= 110,837 cuft
Drainage area	= 12.680 ac	Curve number	= 60
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 22.00 min
Total precip.	= 6.66 in	Distribution	= Type II
Storm duration	= 24 hrs	Shape factor	= 484

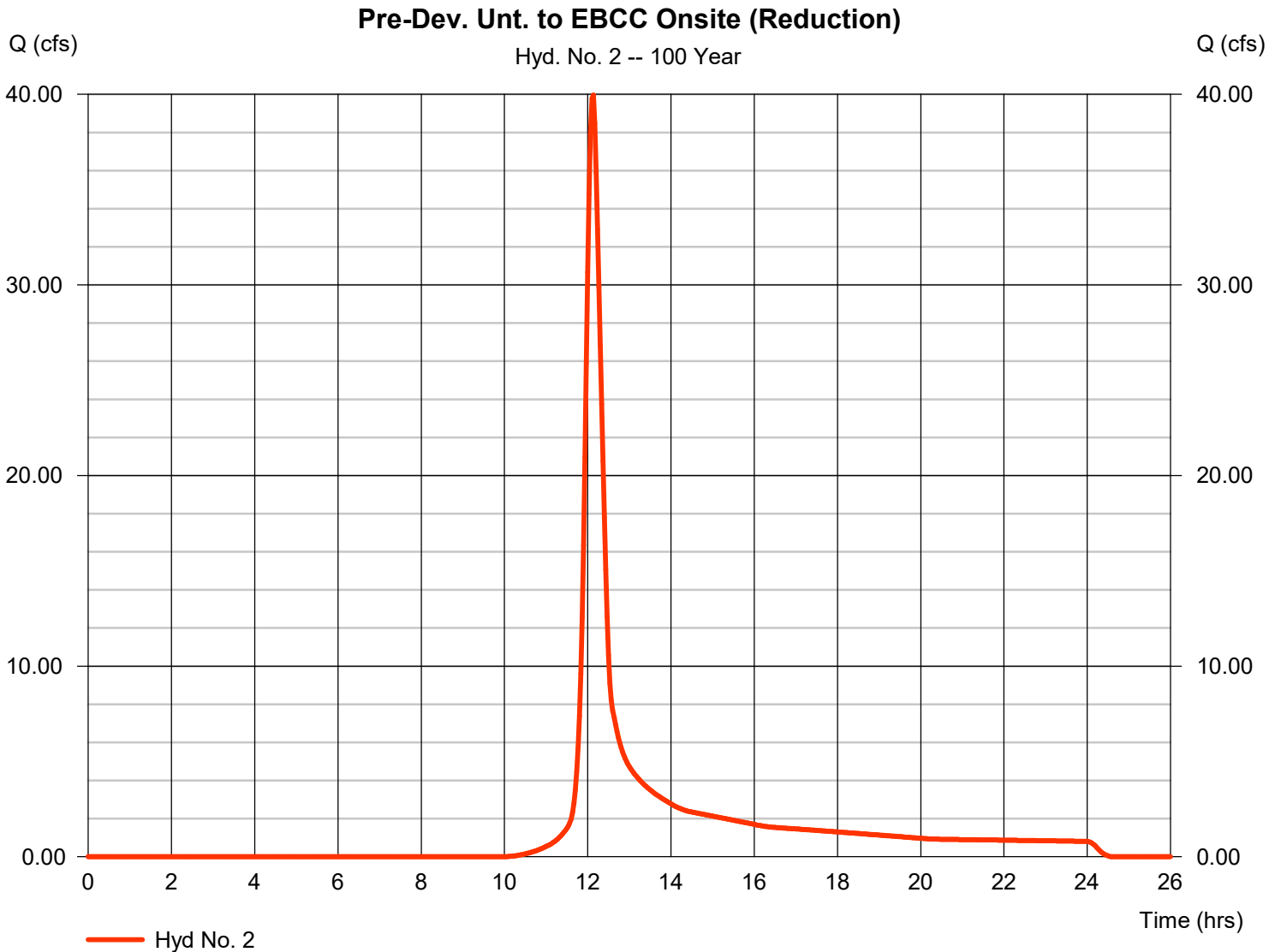


Hydrograph Report

Hyd. No. 2

Pre-Dev. Unt. to EBCC Onsite (Reduction)

Hydrograph type	= SCS Runoff	Peak discharge	= 39.96 cfs
Storm frequency	= 100 yrs	Time to peak	= 12.13 hrs
Time interval	= 2 min	Hyd. volume	= 141,570 cuft
Drainage area	= 12.680 ac	Curve number	= 60
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 22.00 min
Total precip.	= 7.58 in	Distribution	= Type II
Storm duration	= 24 hrs	Shape factor	= 484



POST-DEVELOPMENT HYDROLOGY (EAST BRANCH CHESTER CREEK)



ELA SPORT
 ATHLETIC FACILITIES DESIGN &
 CONSULTING

737 S. BROAD STREET
 LITITZ, PA 17543
 (717) 626-72713

**NRCS (SCS) TR-55- WATERSHED WEIGHTED
 CURVE NUMBER
 POST-DEVELOPMENT SUMMARY**

PROJECT: The Westtown School - Oak Lane Project
 LOCATION: Westtown Township
 COUNTY: Chester

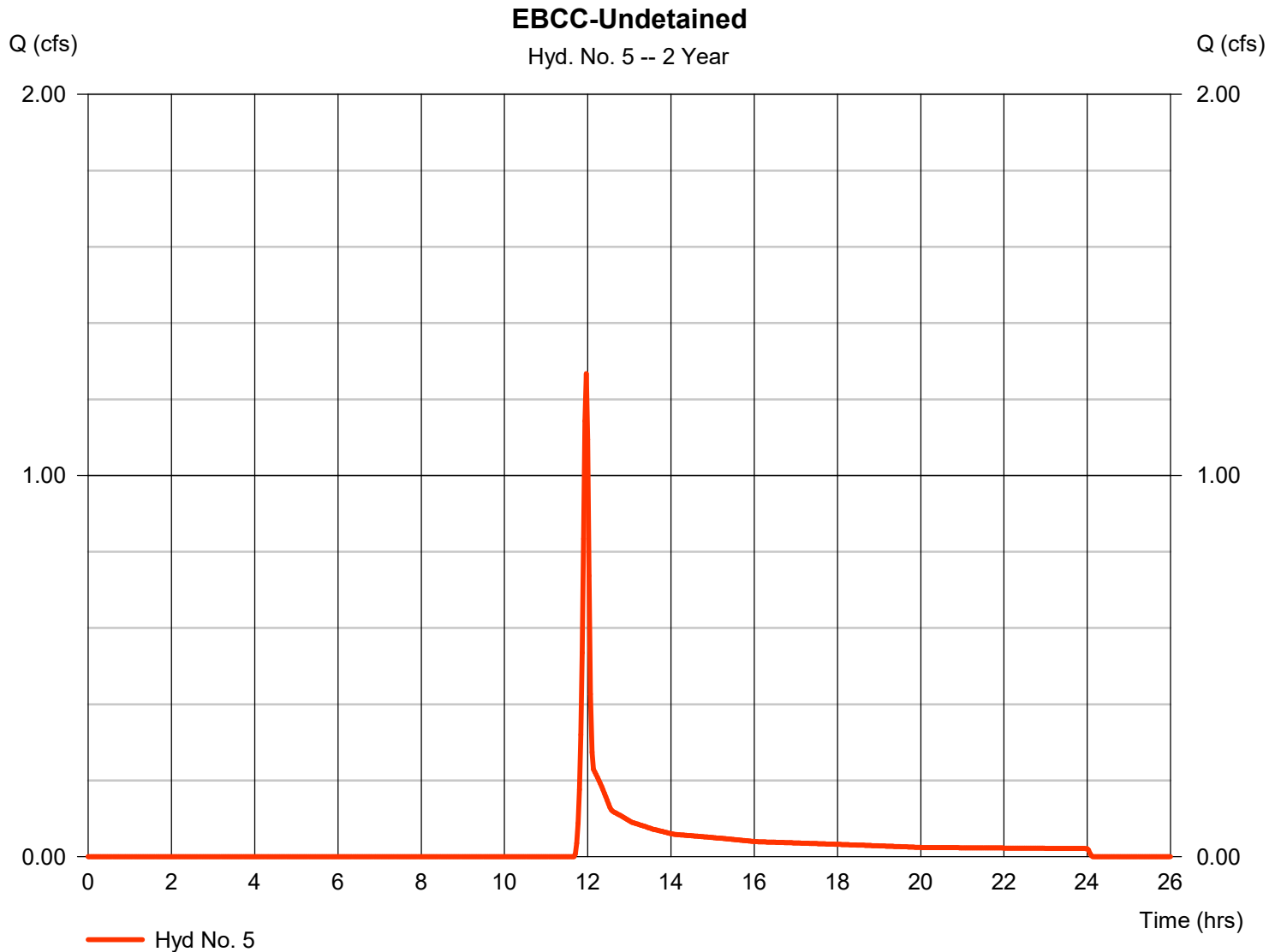
WATERSHED	LAND USE	Area (ac)						Total Area (ac.)	Composite 'CN' Value	Tc Min.	
		Parking, Other Impervious (Disturbed Area)	Parking, Other Impervious (Undisturbed Area)	Open Space (Disturbed Area)	Open Space (Undisturbed Area)	Open Space (Disturbed Area)	Open Space (Undisturbed Area)				
East Branch Chester Creek Undetained	HSG	B	B	B	B	B	D	1.27	65	5	
	"CN" Value	98	98	61	61	61	80				
BMP 1	1.07		0.16	0.03	1.10	0.03	0.00	0.00	4.99	70	13
	1.07		0.16	0.03	1.10	0.03	0.00	0.00	4.99	70	13

Hydrograph Report

Hyd. No. 5

EBCC-Undetained

Hydrograph type	= SCS Runoff	Peak discharge	= 1.267 cfs
Storm frequency	= 2 yrs	Time to peak	= 11.97 hrs
Time interval	= 2 min	Hyd. volume	= 2,722 cuft
Drainage area	= 1.270 ac	Curve number	= 65
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 5.00 min
Total precip.	= 3.26 in	Distribution	= Type II
Storm duration	= 24 hrs	Shape factor	= 484

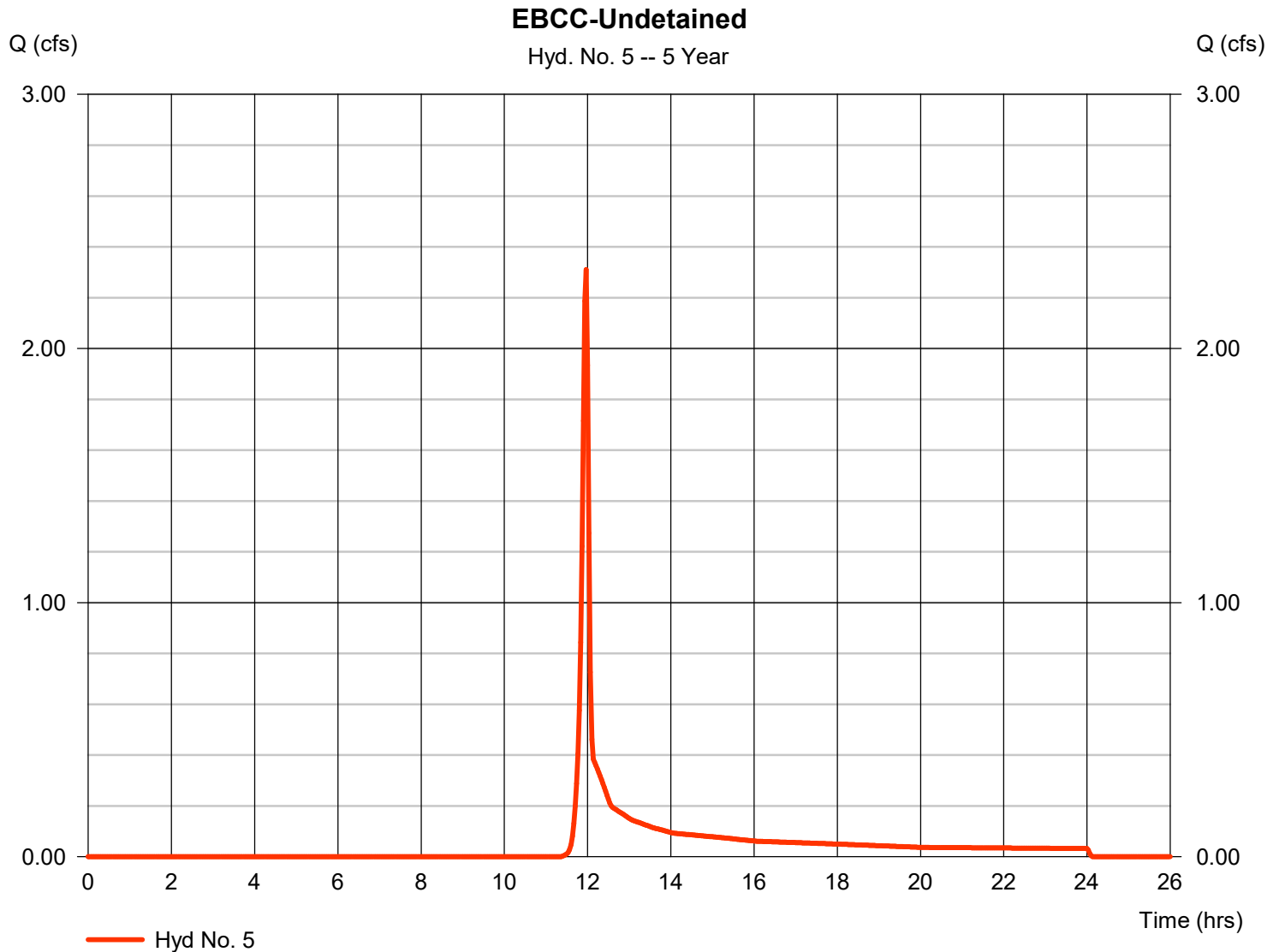


Hydrograph Report

Hyd. No. 5

EBCC-Undetained

Hydrograph type	= SCS Runoff	Peak discharge	= 2.311 cfs
Storm frequency	= 5 yrs	Time to peak	= 11.97 hrs
Time interval	= 2 min	Hyd. volume	= 4,698 cuft
Drainage area	= 1.270 ac	Curve number	= 65
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 5.00 min
Total precip.	= 4.10 in	Distribution	= Type II
Storm duration	= 24 hrs	Shape factor	= 484

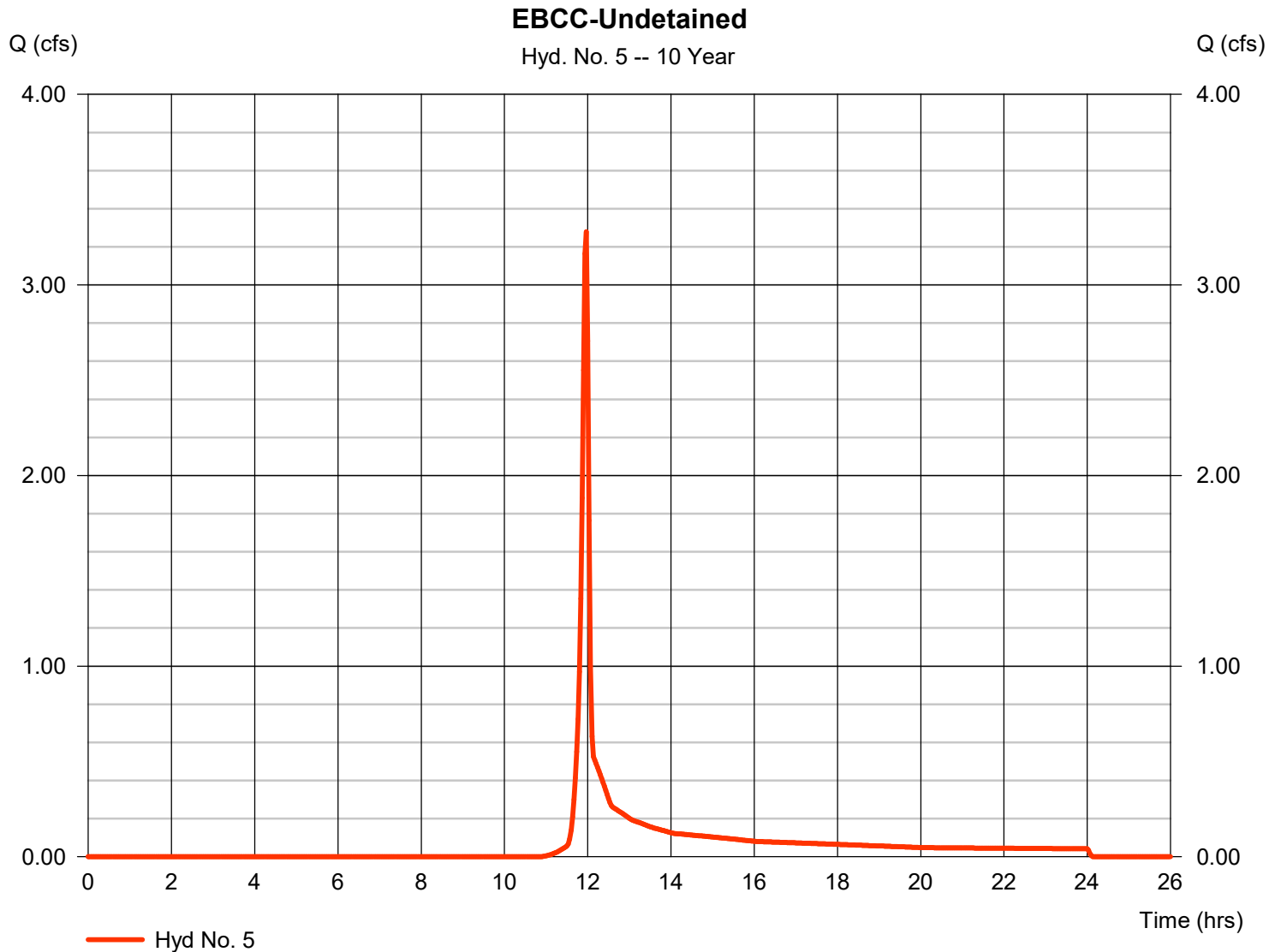


Hydrograph Report

Hyd. No. 5

EBCC-Undetained

Hydrograph type	= SCS Runoff	Peak discharge	= 3.279 cfs
Storm frequency	= 10 yrs	Time to peak	= 11.97 hrs
Time interval	= 2 min	Hyd. volume	= 6,578 cuft
Drainage area	= 1.270 ac	Curve number	= 65
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 5.00 min
Total precip.	= 4.80 in	Distribution	= Type II
Storm duration	= 24 hrs	Shape factor	= 484

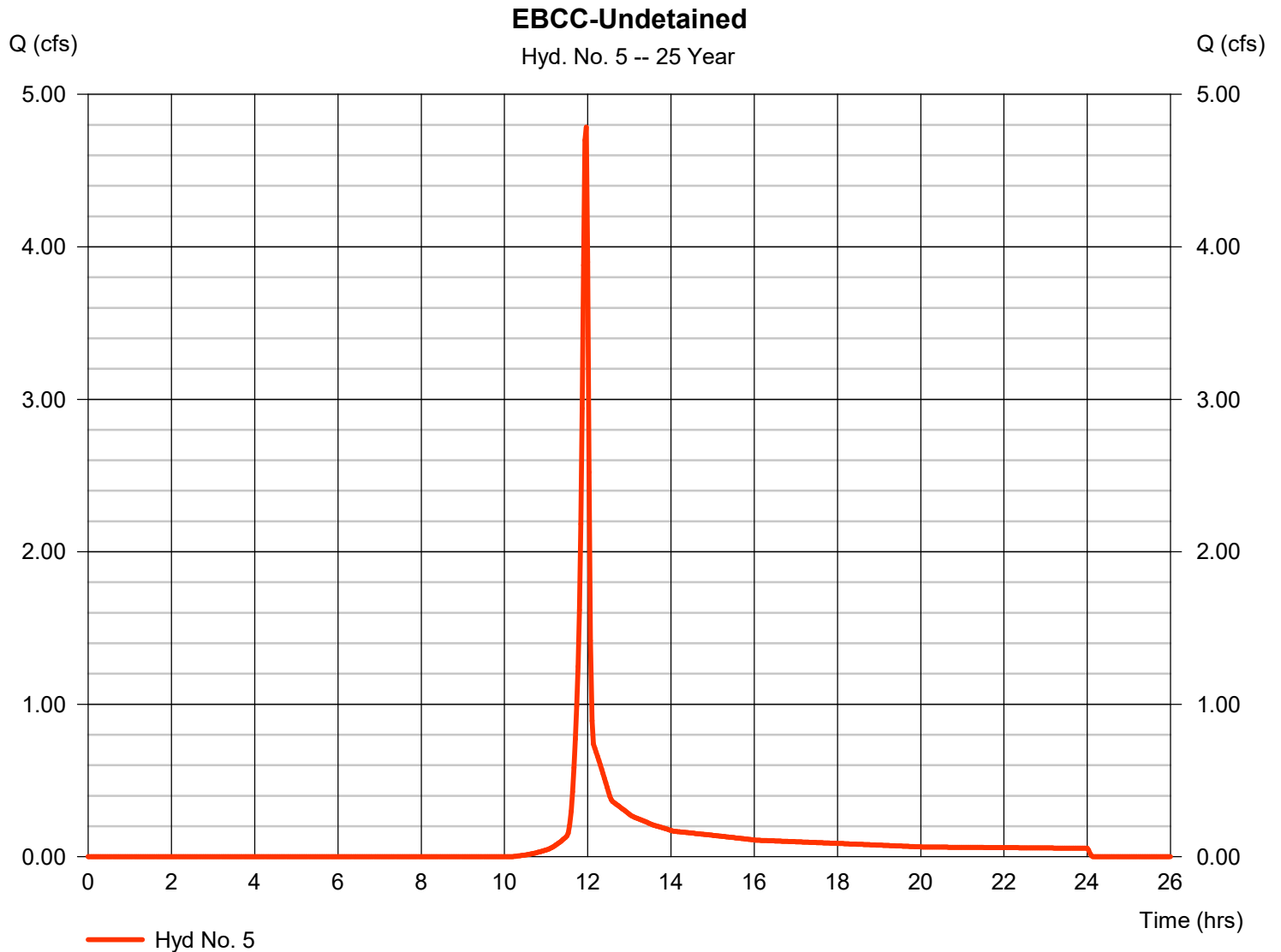


Hydrograph Report

Hyd. No. 5

EBCC-Undetained

Hydrograph type	= SCS Runoff	Peak discharge	= 4.785 cfs
Storm frequency	= 25 yrs	Time to peak	= 11.97 hrs
Time interval	= 2 min	Hyd. volume	= 9,569 cuft
Drainage area	= 1.270 ac	Curve number	= 65
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 5.00 min
Total precip.	= 5.81 in	Distribution	= Type II
Storm duration	= 24 hrs	Shape factor	= 484

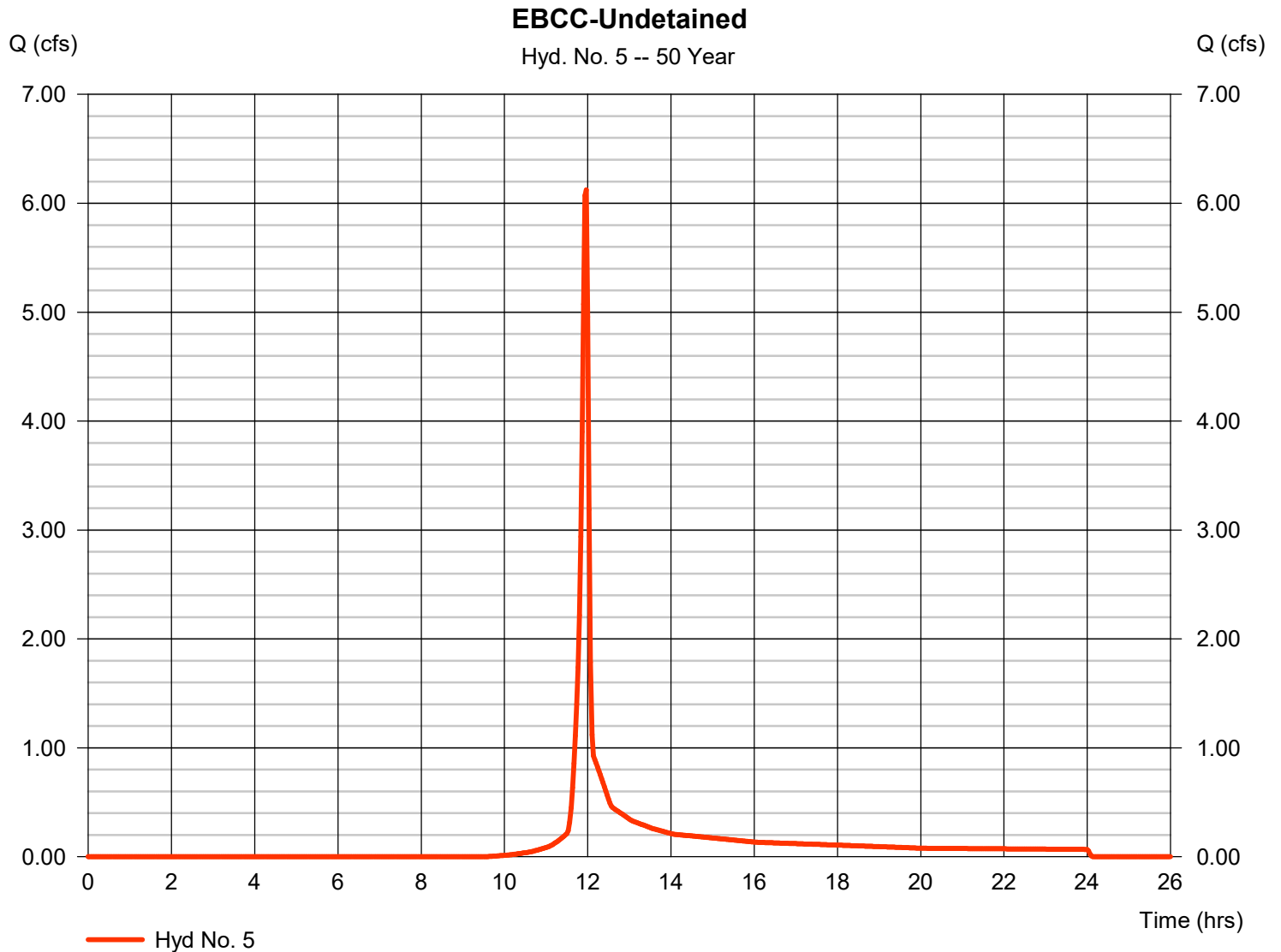


Hydrograph Report

Hyd. No. 5

EBCC-Undetained

Hydrograph type	= SCS Runoff	Peak discharge	= 6.123 cfs
Storm frequency	= 50 yrs	Time to peak	= 11.97 hrs
Time interval	= 2 min	Hyd. volume	= 12,283 cuft
Drainage area	= 1.270 ac	Curve number	= 65
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 5.00 min
Total precip.	= 6.66 in	Distribution	= Type II
Storm duration	= 24 hrs	Shape factor	= 484

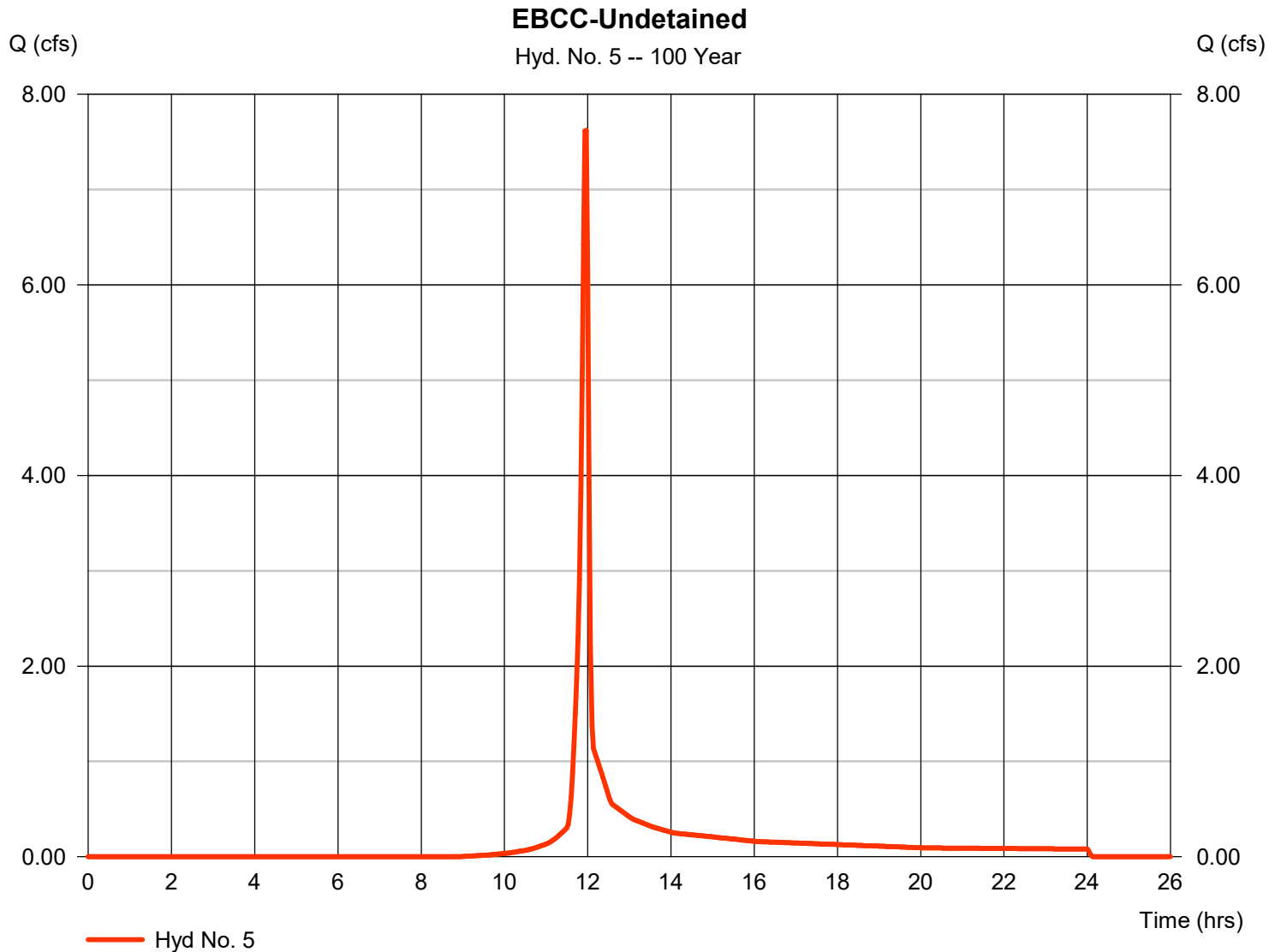


Hydrograph Report

Hyd. No. 5

EBCC-Undetained

Hydrograph type	= SCS Runoff	Peak discharge	= 7.622 cfs
Storm frequency	= 100 yrs	Time to peak	= 11.97 hrs
Time interval	= 2 min	Hyd. volume	= 15,375 cuft
Drainage area	= 1.270 ac	Curve number	= 65
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 5.00 min
Total precip.	= 7.58 in	Distribution	= Type II
Storm duration	= 24 hrs	Shape factor	= 484

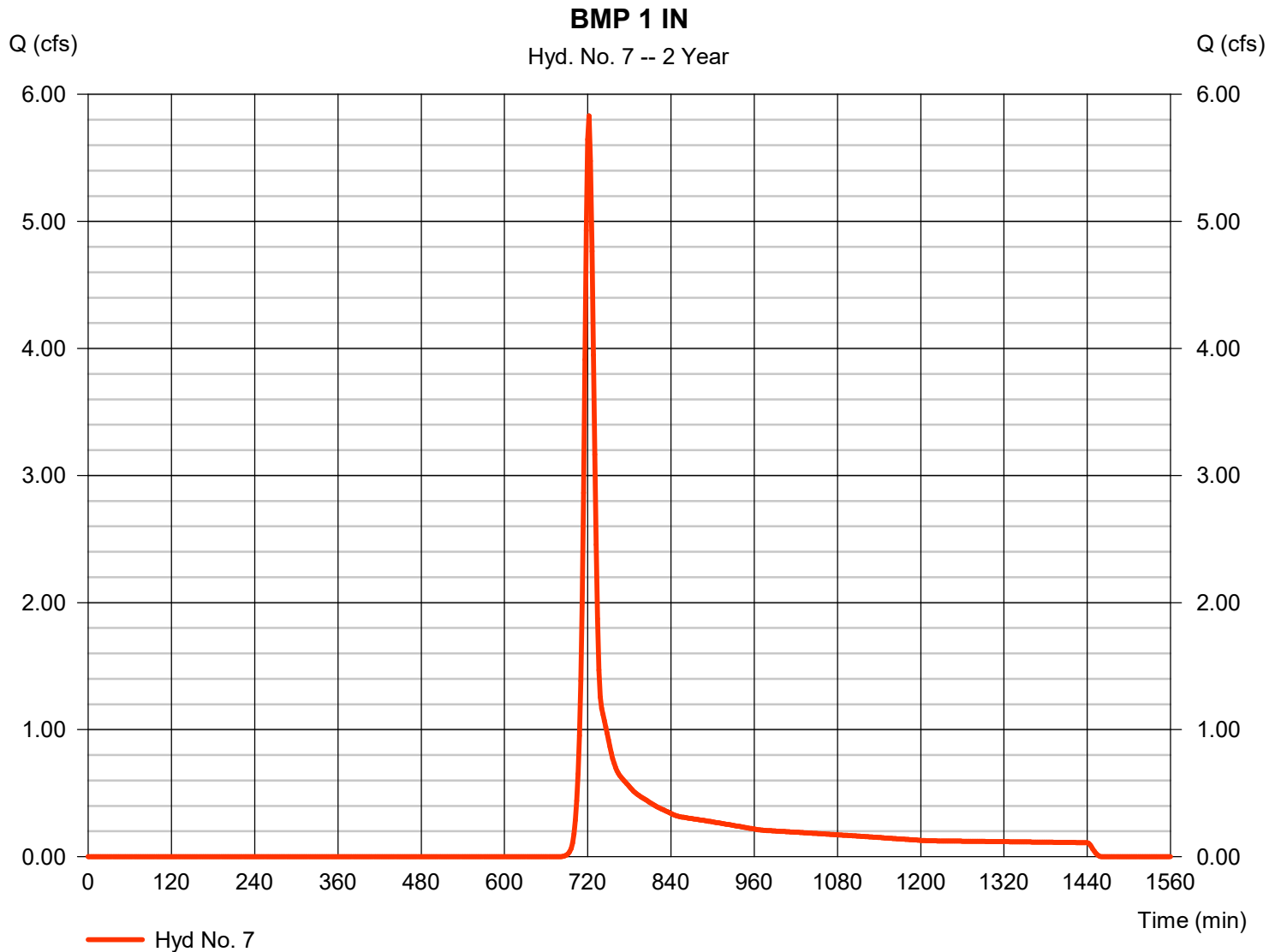


Hydrograph Report

Hyd. No. 7

BMP 1 IN

Hydrograph type	= SCS Runoff	Peak discharge	= 5.831 cfs
Storm frequency	= 2 yrs	Time to peak	= 722 min
Time interval	= 2 min	Hyd. volume	= 16,125 cuft
Drainage area	= 4.990 ac	Curve number	= 70
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 13.00 min
Total precip.	= 3.26 in	Distribution	= Type II
Storm duration	= 24 hrs	Shape factor	= 484



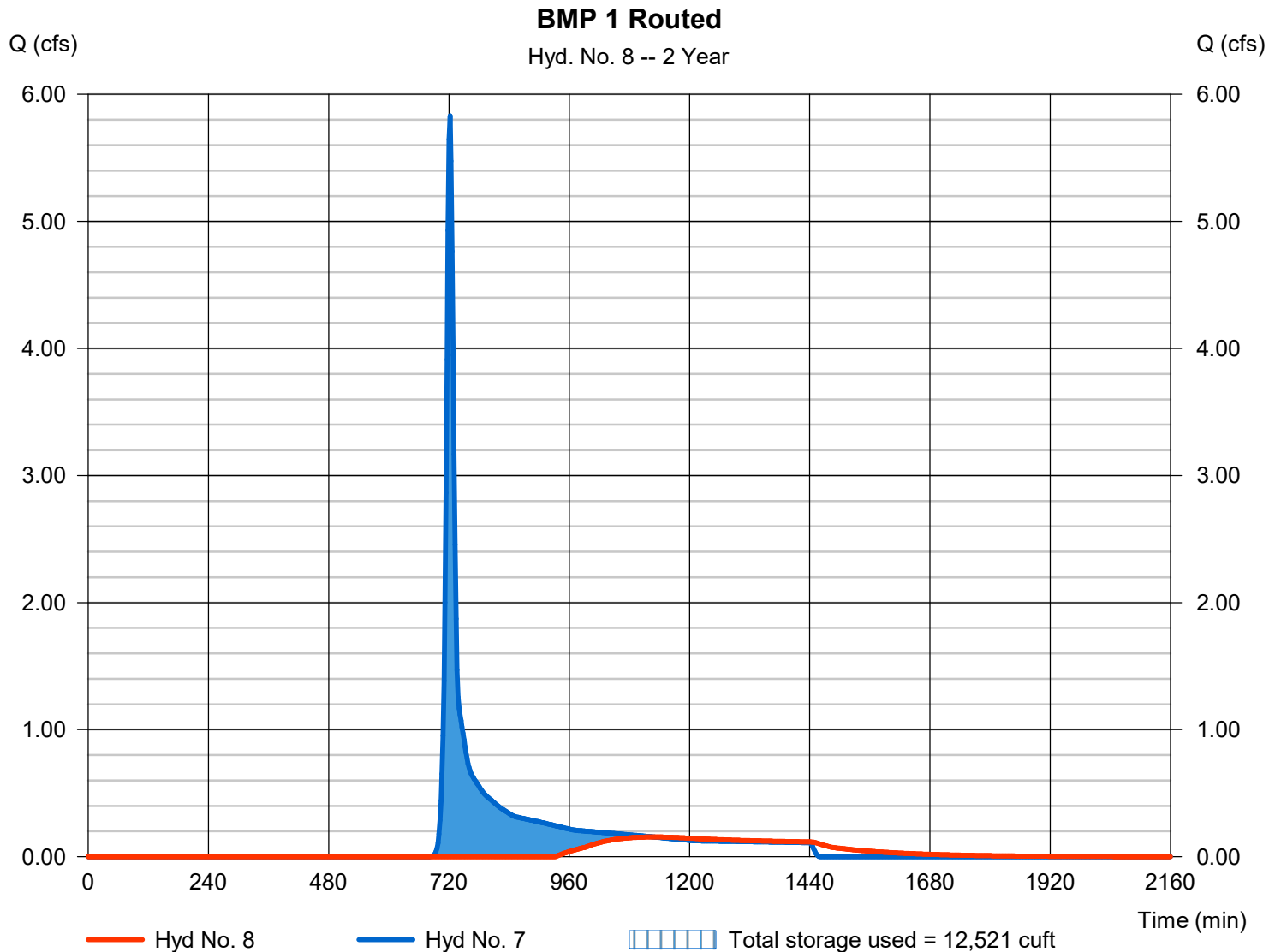
Hydrograph Report

Hyd. No. 8

BMP 1 Routed

Hydrograph type	= Reservoir	Peak discharge	= 0.155 cfs
Storm frequency	= 2 yrs	Time to peak	= 1128 min
Time interval	= 2 min	Hyd. volume	= 4,613 cuft
Inflow hyd. No.	= 7 - BMP 1 IN	Max. Elevation	= 289.58 ft
Reservoir name	= BMP 1	Max. Storage	= 12,521 cuft

Storage Indication method used.



Pond Report

Pond No. 7 - BMP 1

Pond Data

Contours -User-defined contour areas. Conic method used for volume calculation. Begining Elevation = 288.50 ft

Stage / Storage Table

Stage (ft)	Elevation (ft)	Contour area (sqft)	Incr. Storage (cuft)	Total storage (cuft)
0.00	288.50	10,675	0	0
0.50	289.00	11,498	5,541	5,541
1.00	289.50	12,356	5,962	11,503
1.50	290.00	13,211	6,390	17,893
2.50	291.00	15,025	14,107	32,000
3.50	292.00	16,928	15,965	47,965
4.50	293.00	19,112	18,007	65,972

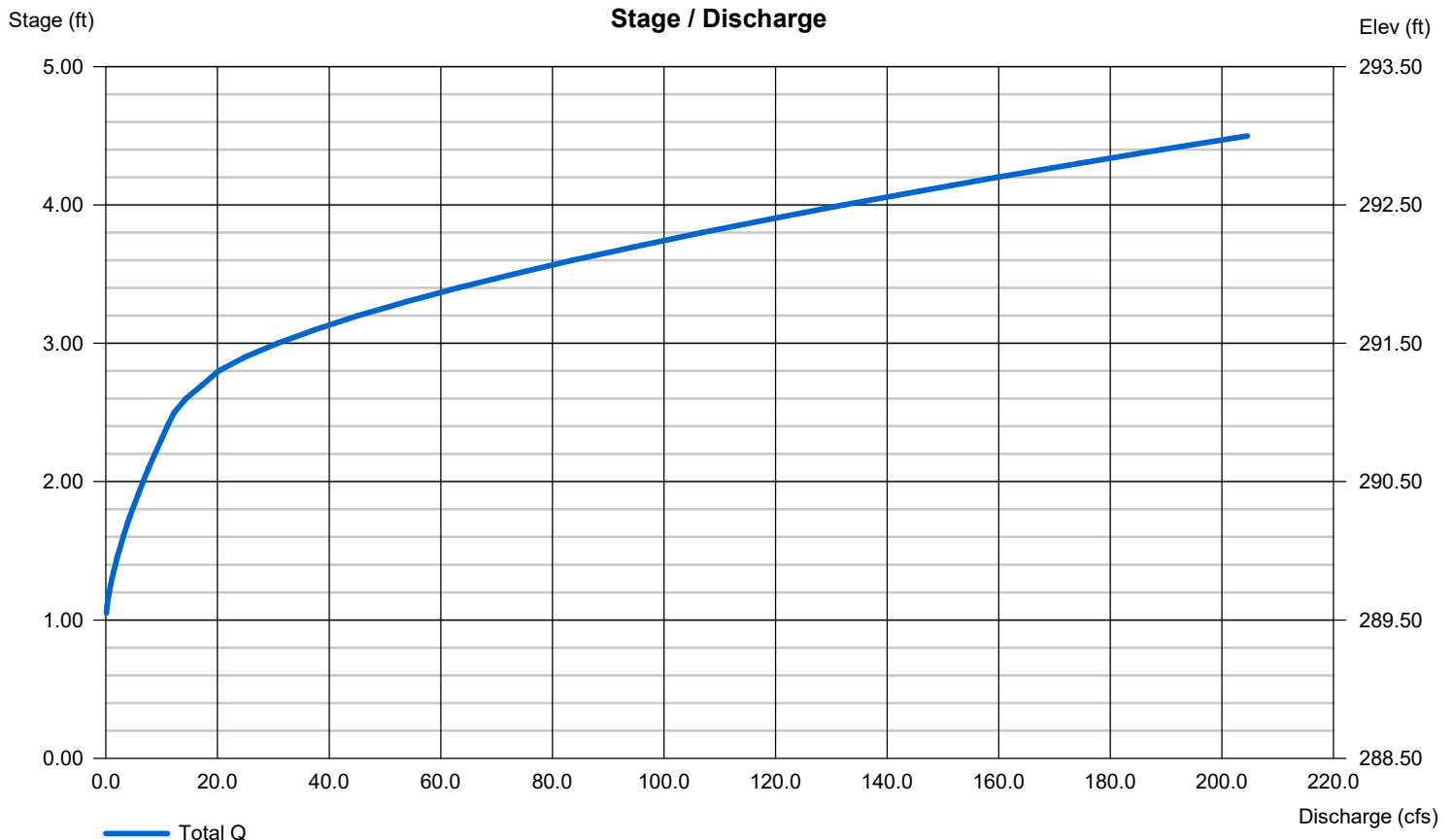
Culvert / Orifice Structures

	[A]	[B]	[C]	[PrfRsr]
Rise (in)	= 18.00	Inactive	0.00	0.00
Span (in)	= 18.00	0.00	0.00	0.00
No. Barrels	= 1	1	0	0
Invert El. (ft)	= 284.25	0.00	0.00	0.00
Length (ft)	= 28.47	0.10	0.00	0.00
Slope (%)	= 0.53	0.00	0.00	n/a
N-Value	= .013	.013	.013	n/a
Orifice Coeff.	= 0.60	0.60	0.60	0.60
Multi-Stage	= n/a	Yes	No	No

Weir Structures

	[A]	[B]	[C]	[D]
Crest Len (ft)	= 8.50	2.00	30.00	0.00
Crest El. (ft)	= 291.00	289.50	291.25	0.00
Weir Coeff.	= 3.33	3.33	2.60	3.33
Weir Type	= 1	Rect	Broad	---
Multi-Stage	= Yes	Yes	No	No
Exfil.(in/hr)	= 0.000 (by Wet area)			
TW Elev. (ft)	= 0.00			

Note: Culvert/Orifice outflows are analyzed under inlet (ic) and outlet (oc) control. Weir risers checked for orifice conditions (ic) and submergence (s).

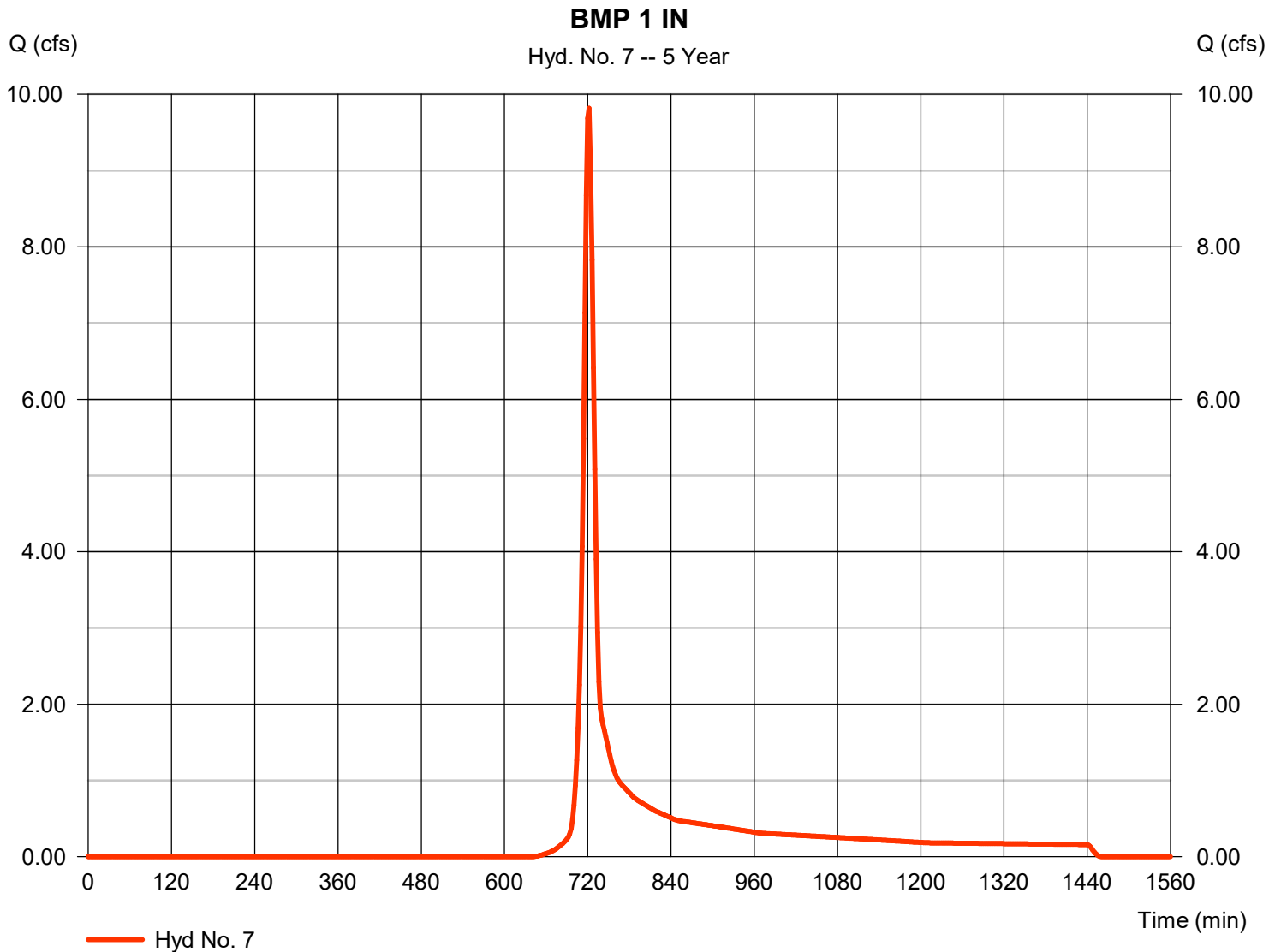


Hydrograph Report

Hyd. No. 7

BMP 1 IN

Hydrograph type	= SCS Runoff	Peak discharge	= 9.819 cfs
Storm frequency	= 5 yrs	Time to peak	= 722 min
Time interval	= 2 min	Hyd. volume	= 26,092 cuft
Drainage area	= 4.990 ac	Curve number	= 70
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 13.00 min
Total precip.	= 4.10 in	Distribution	= Type II
Storm duration	= 24 hrs	Shape factor	= 484



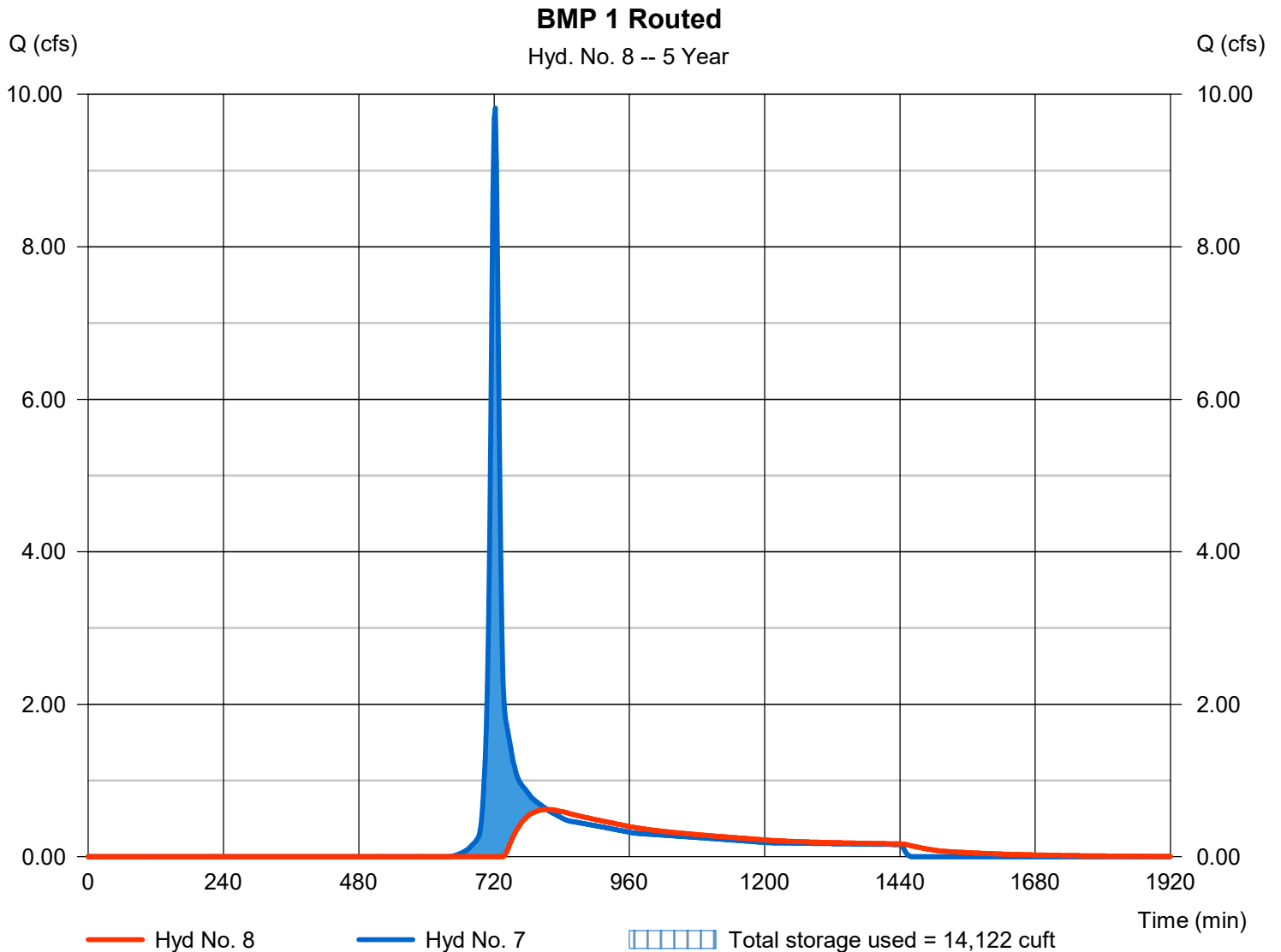
Hydrograph Report

Hyd. No. 8

BMP 1 Routed

Hydrograph type	= Reservoir	Peak discharge	= 0.619 cfs
Storm frequency	= 5 yrs	Time to peak	= 814 min
Time interval	= 2 min	Hyd. volume	= 14,581 cuft
Inflow hyd. No.	= 7 - BMP 1 IN	Max. Elevation	= 289.70 ft
Reservoir name	= BMP 1	Max. Storage	= 14,122 cuft

Storage Indication method used.

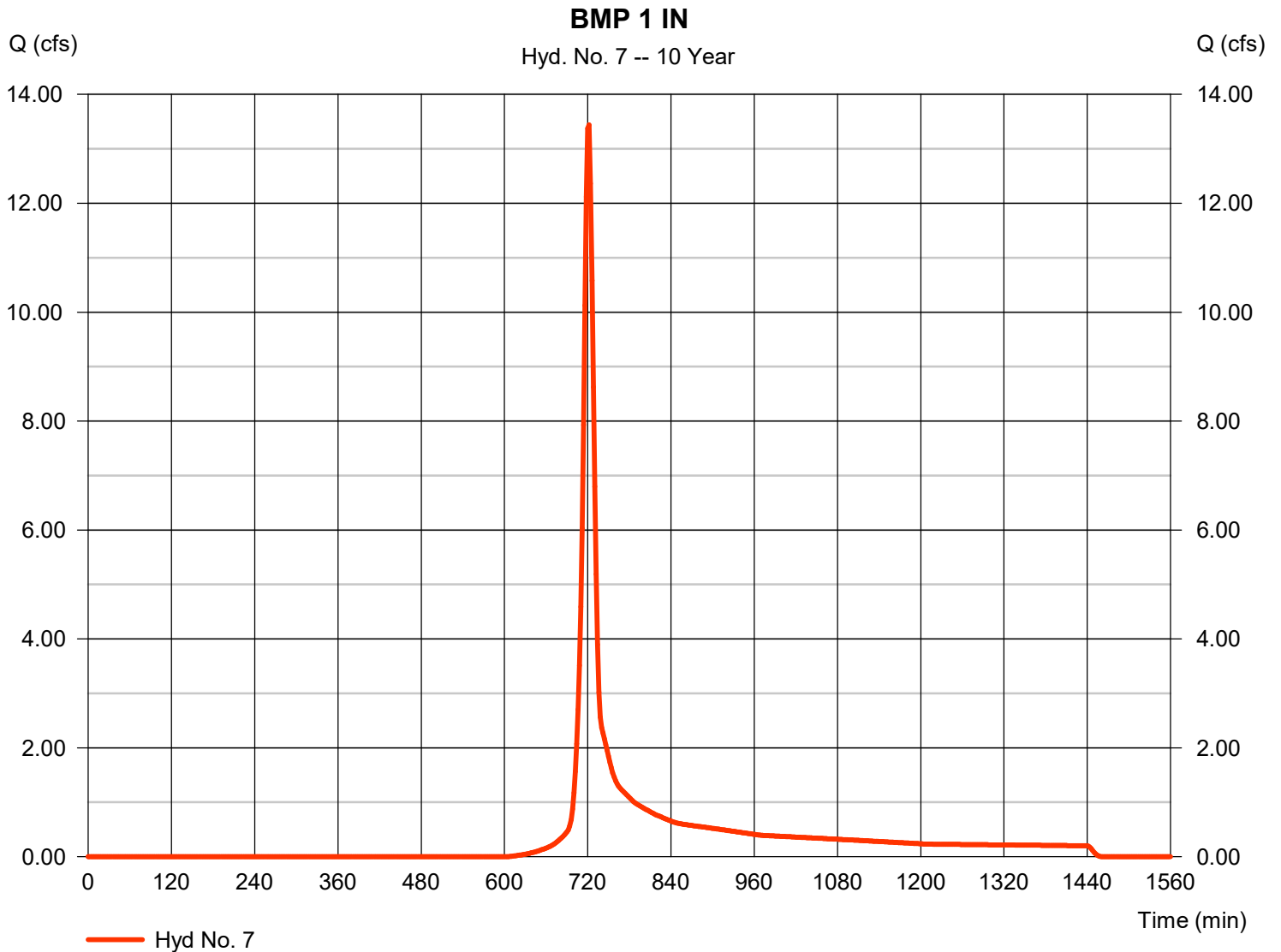


Hydrograph Report

Hyd. No. 7

BMP 1 IN

Hydrograph type	= SCS Runoff	Peak discharge	= 13.44 cfs
Storm frequency	= 10 yrs	Time to peak	= 722 min
Time interval	= 2 min	Hyd. volume	= 35,291 cuft
Drainage area	= 4.990 ac	Curve number	= 70
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 13.00 min
Total precip.	= 4.80 in	Distribution	= Type II
Storm duration	= 24 hrs	Shape factor	= 484



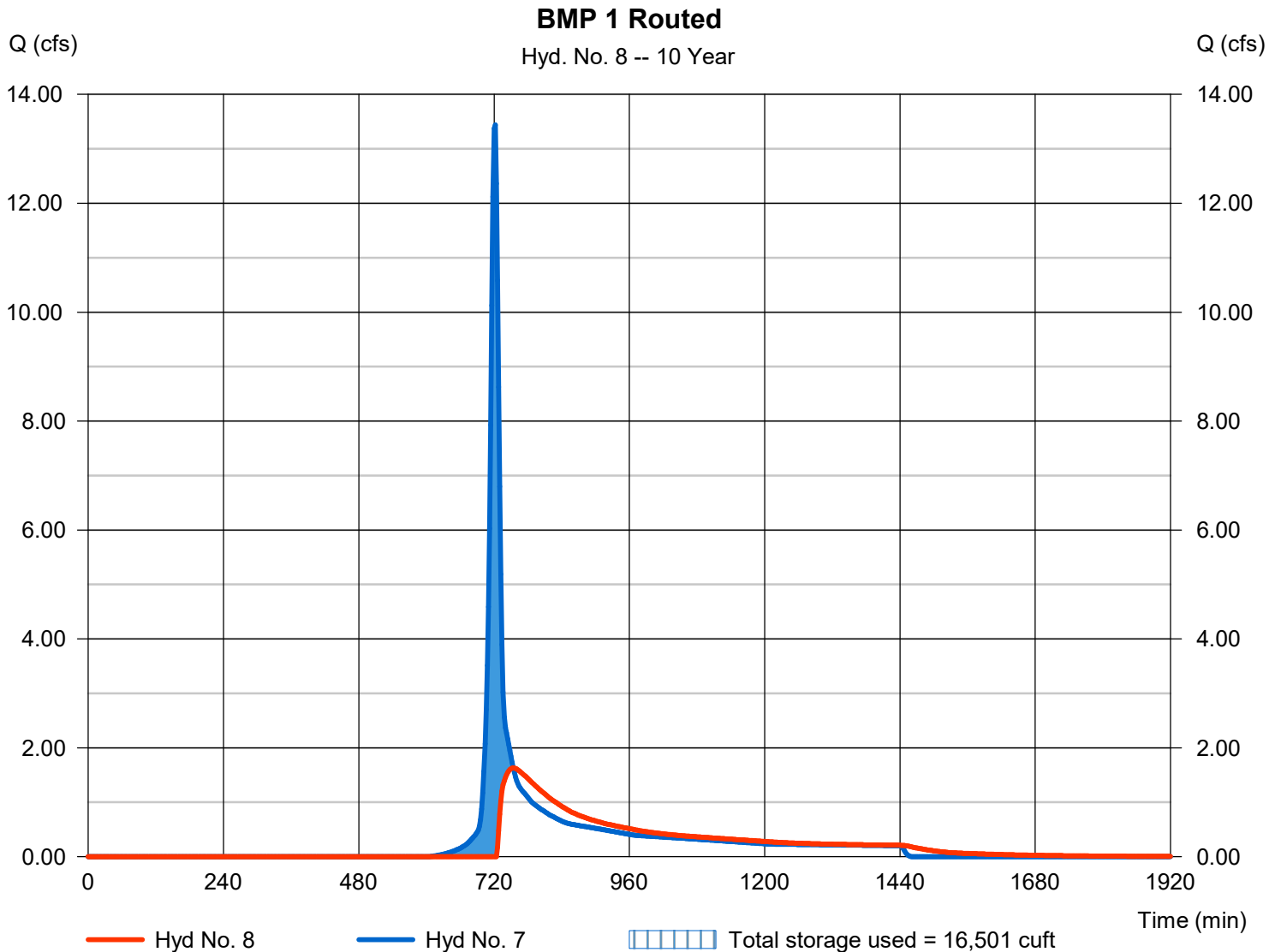
Hydrograph Report

Hyd. No. 8

BMP 1 Routed

Hydrograph type	= Reservoir	Peak discharge	= 1.630 cfs
Storm frequency	= 10 yrs	Time to peak	= 754 min
Time interval	= 2 min	Hyd. volume	= 23,780 cuft
Inflow hyd. No.	= 7 - BMP 1 IN	Max. Elevation	= 289.89 ft
Reservoir name	= BMP 1	Max. Storage	= 16,501 cuft

Storage Indication method used.

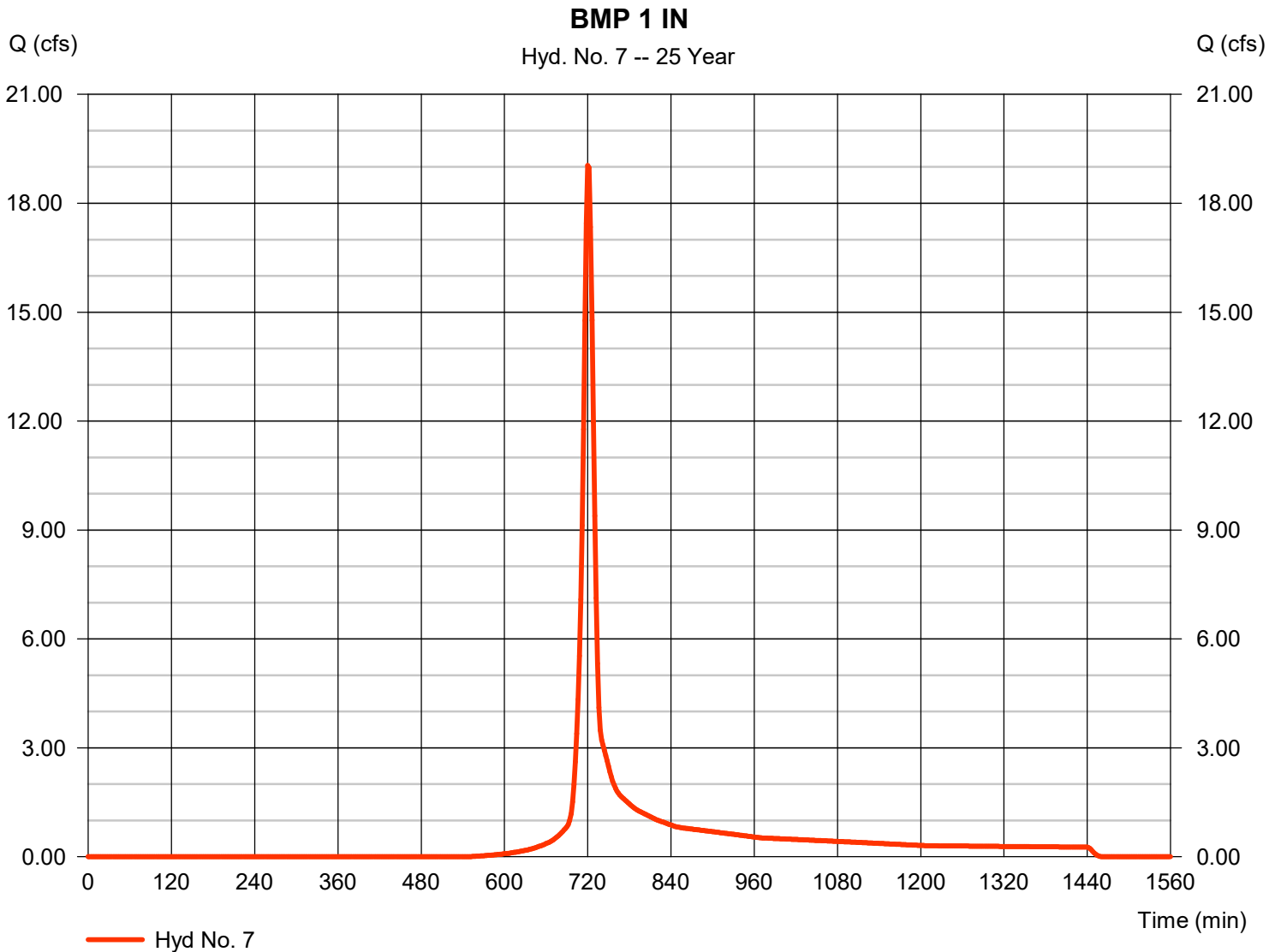


Hydrograph Report

Hyd. No. 7

BMP 1 IN

Hydrograph type	= SCS Runoff	Peak discharge	= 19.04 cfs
Storm frequency	= 25 yrs	Time to peak	= 720 min
Time interval	= 2 min	Hyd. volume	= 49,600 cuft
Drainage area	= 4.990 ac	Curve number	= 70
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 13.00 min
Total precip.	= 5.81 in	Distribution	= Type II
Storm duration	= 24 hrs	Shape factor	= 484



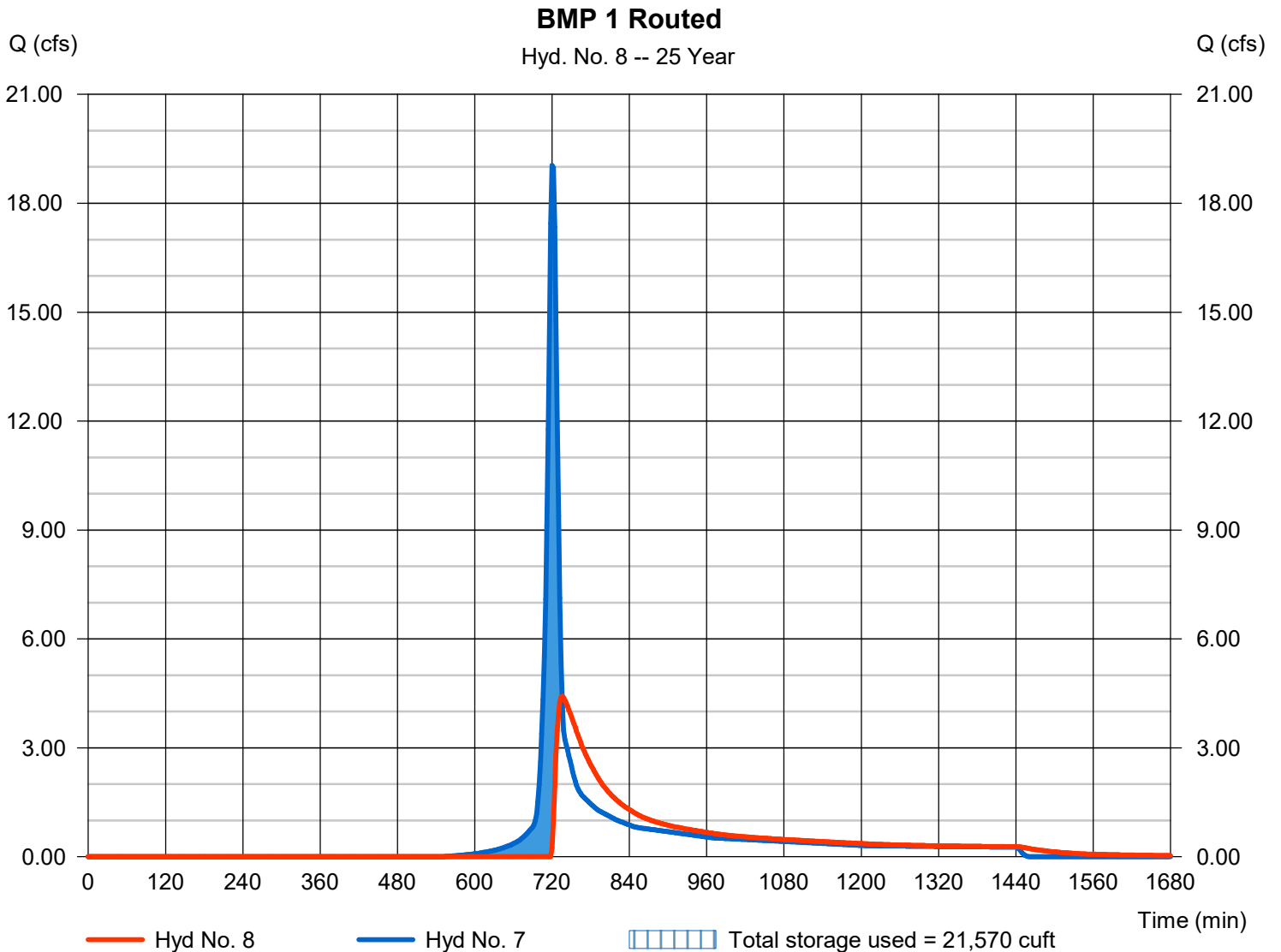
Hydrograph Report

Hyd. No. 8

BMP 1 Routed

Hydrograph type	= Reservoir	Peak discharge	= 4.425 cfs
Storm frequency	= 25 yrs	Time to peak	= 736 min
Time interval	= 2 min	Hyd. volume	= 38,088 cuft
Inflow hyd. No.	= 7 - BMP 1 IN	Max. Elevation	= 290.26 ft
Reservoir name	= BMP 1	Max. Storage	= 21,570 cuft

Storage Indication method used.

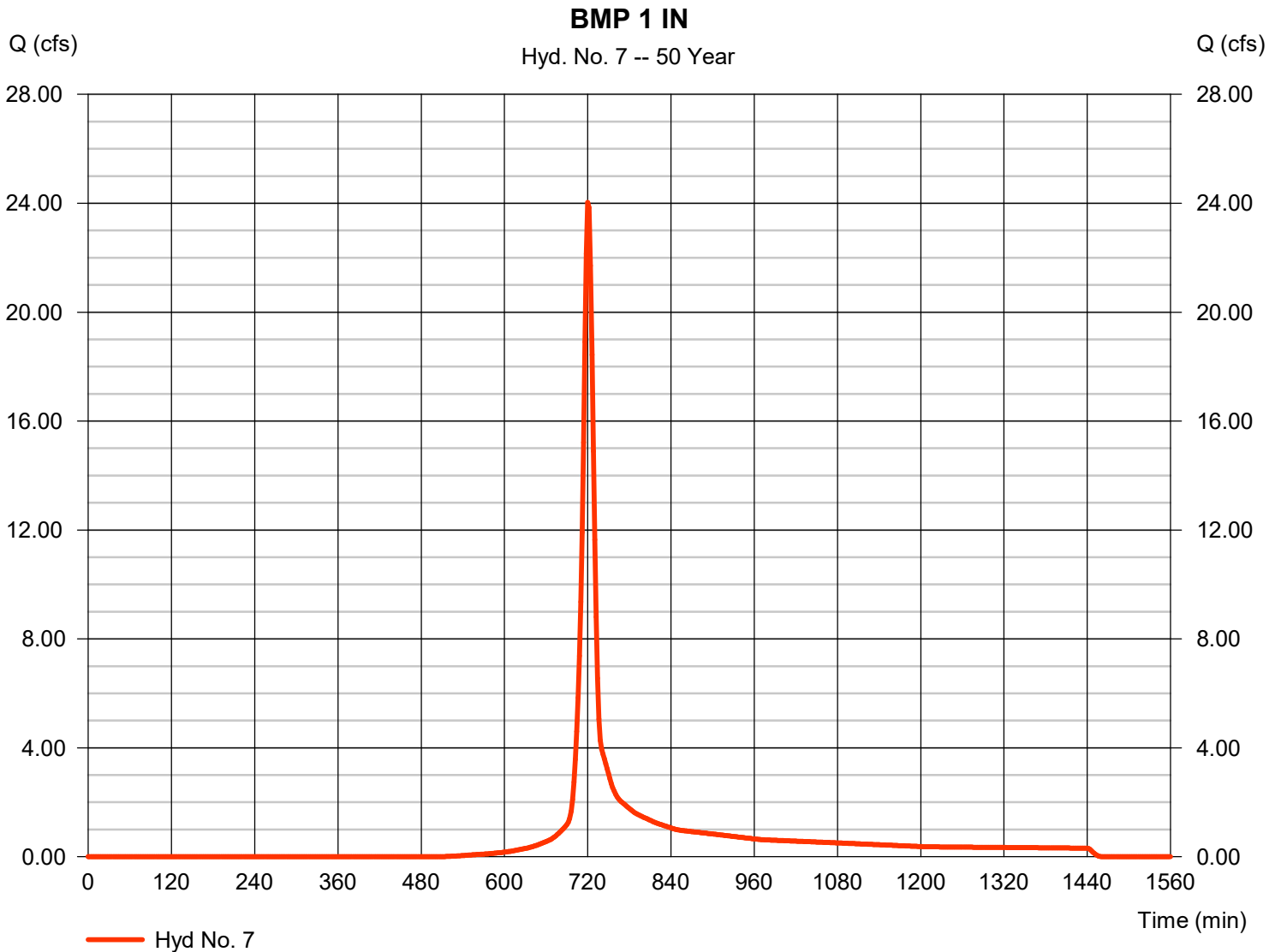


Hydrograph Report

Hyd. No. 7

BMP 1 IN

Hydrograph type	= SCS Runoff	Peak discharge	= 24.03 cfs
Storm frequency	= 50 yrs	Time to peak	= 720 min
Time interval	= 2 min	Hyd. volume	= 62,348 cuft
Drainage area	= 4.990 ac	Curve number	= 70
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 13.00 min
Total precip.	= 6.66 in	Distribution	= Type II
Storm duration	= 24 hrs	Shape factor	= 484



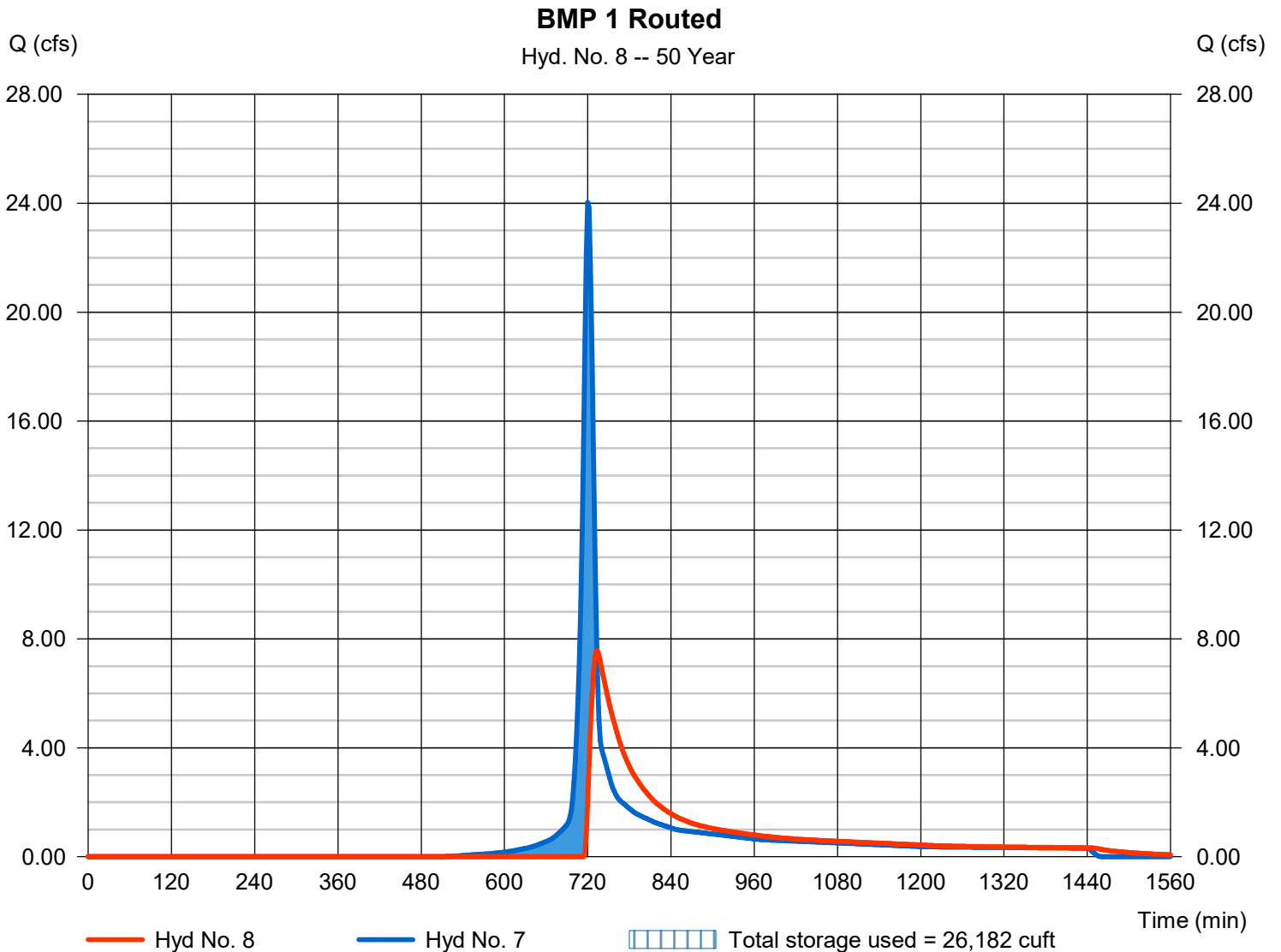
Hydrograph Report

Hyd. No. 8

BMP 1 Routed

Hydrograph type	= Reservoir	Peak discharge	= 7.557 cfs
Storm frequency	= 50 yrs	Time to peak	= 734 min
Time interval	= 2 min	Hyd. volume	= 50,837 cuft
Inflow hyd. No.	= 7 - BMP 1 IN	Max. Elevation	= 290.59 ft
Reservoir name	= BMP 1	Max. Storage	= 26,182 cuft

Storage Indication method used.

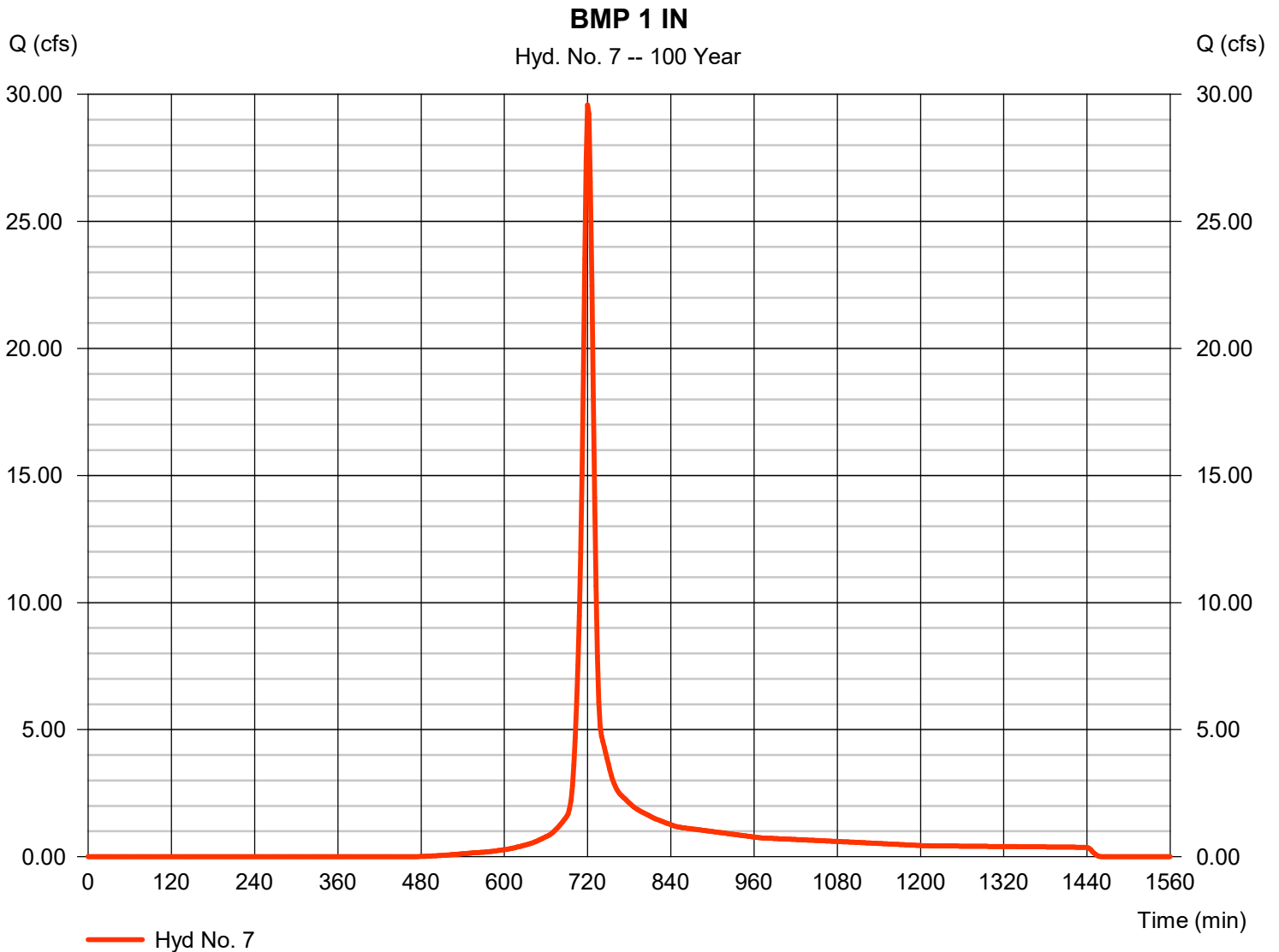


Hydrograph Report

Hyd. No. 7

BMP 1 IN

Hydrograph type	= SCS Runoff	Peak discharge	= 29.58 cfs
Storm frequency	= 100 yrs	Time to peak	= 720 min
Time interval	= 2 min	Hyd. volume	= 76,692 cuft
Drainage area	= 4.990 ac	Curve number	= 70
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 13.00 min
Total precip.	= 7.58 in	Distribution	= Type II
Storm duration	= 24 hrs	Shape factor	= 484



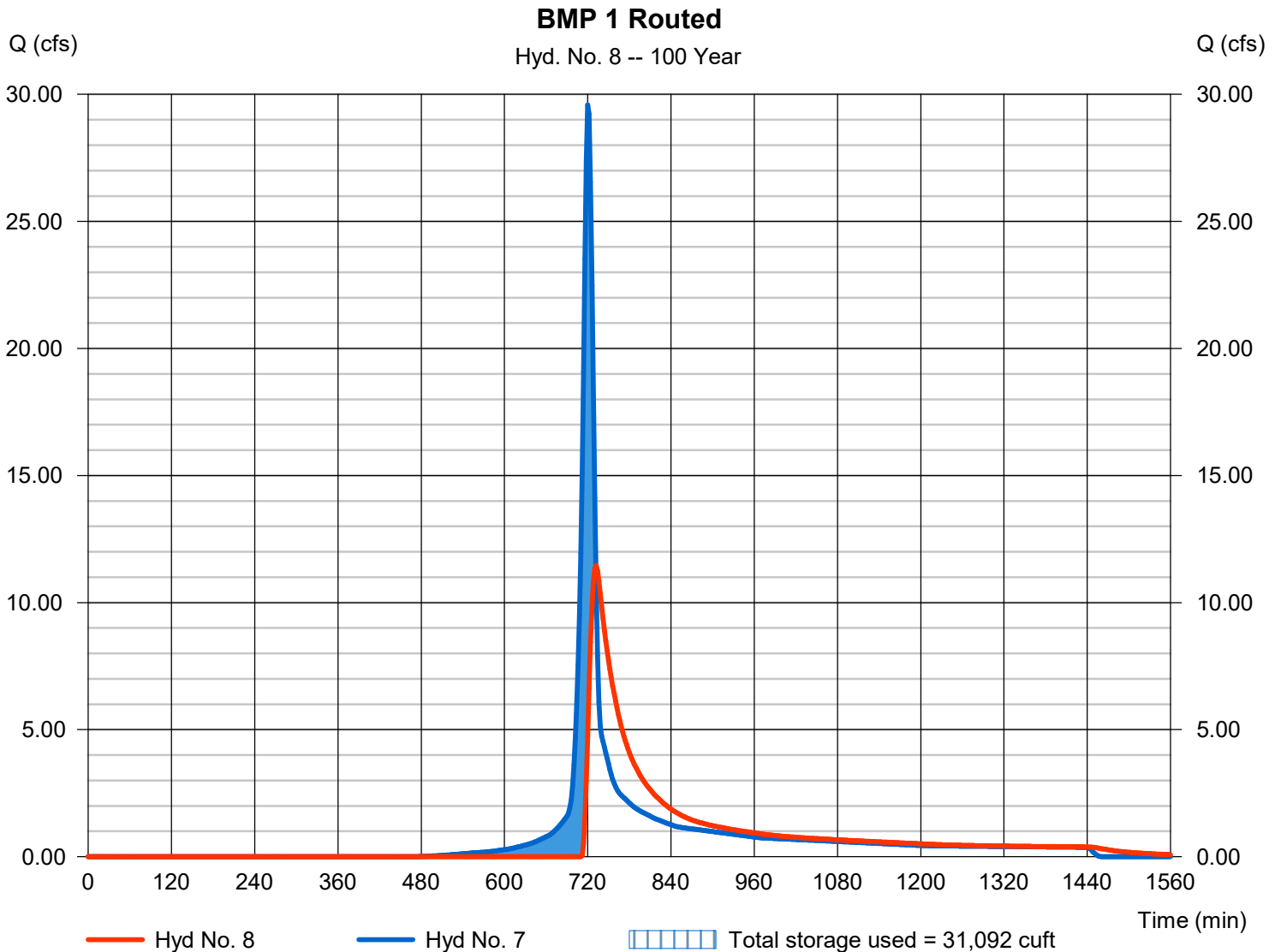
Hydrograph Report

Hyd. No. 8

BMP 1 Routed

Hydrograph type	= Reservoir	Peak discharge	= 11.46 cfs
Storm frequency	= 100 yrs	Time to peak	= 732 min
Time interval	= 2 min	Hyd. volume	= 65,180 cuft
Inflow hyd. No.	= 7 - BMP 1 IN	Max. Elevation	= 290.94 ft
Reservoir name	= BMP 1	Max. Storage	= 31,092 cuft

Storage Indication method used.

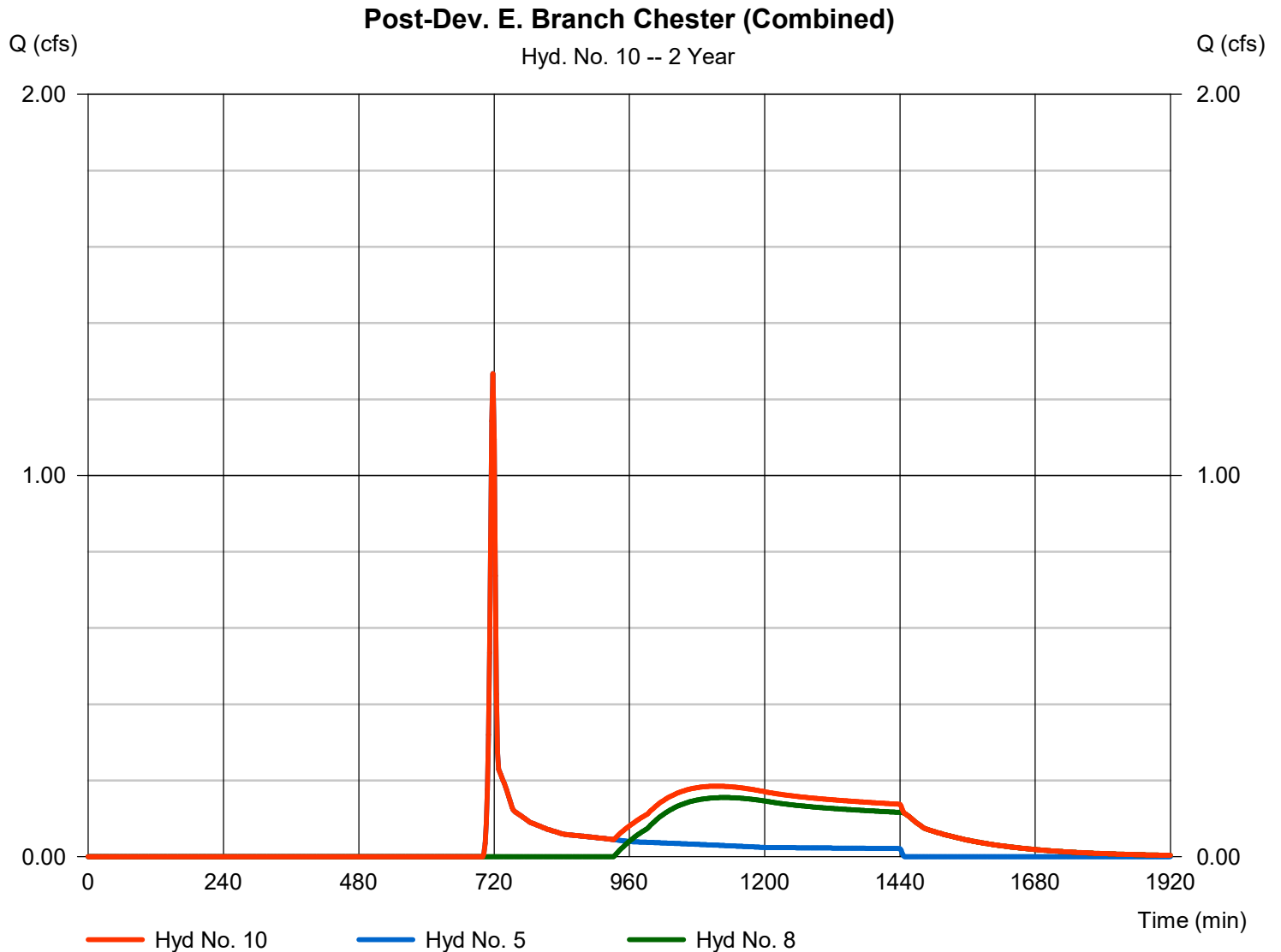


Hydrograph Report

Hyd. No. 10

Post-Dev. E. Branch Chester (Combined)

Hydrograph type	= Combine	Peak discharge	= 1.267 cfs
Storm frequency	= 2 yrs	Time to peak	= 718 min
Time interval	= 2 min	Hyd. volume	= 7,335 cuft
Inflow hyds.	= 5, 8	Contrib. drain. area	= 1.270 ac



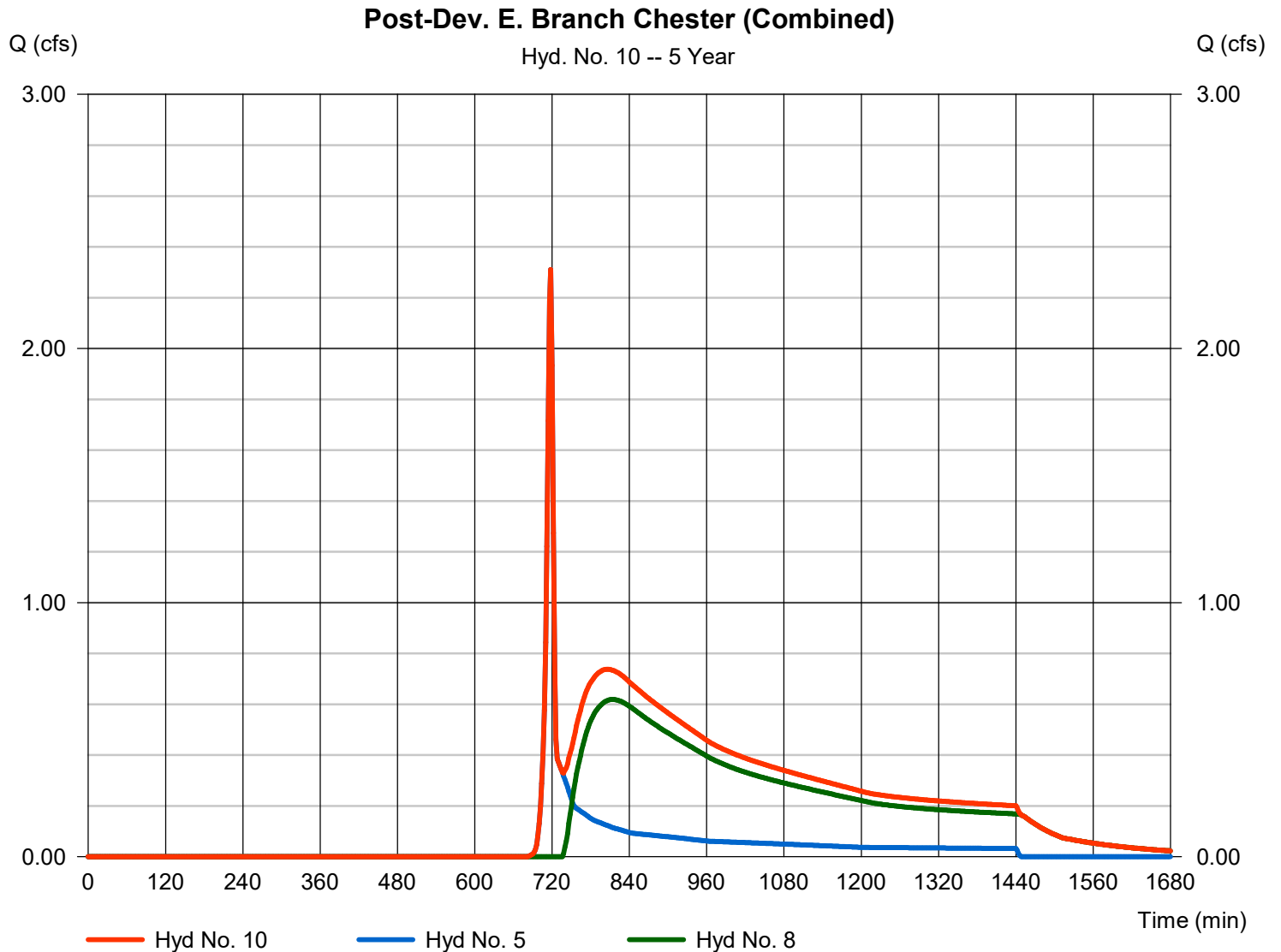
Hydrograph Report

Hyd. No. 10

Post-Dev. E. Branch Chester (Combined)

Hydrograph type = Combine
Storm frequency = 5 yrs
Time interval = 2 min
Inflow hyds. = 5, 8

Peak discharge = 2.311 cfs
Time to peak = 718 min
Hyd. volume = 19,279 cuft
Contrib. drain. area = 1.270 ac



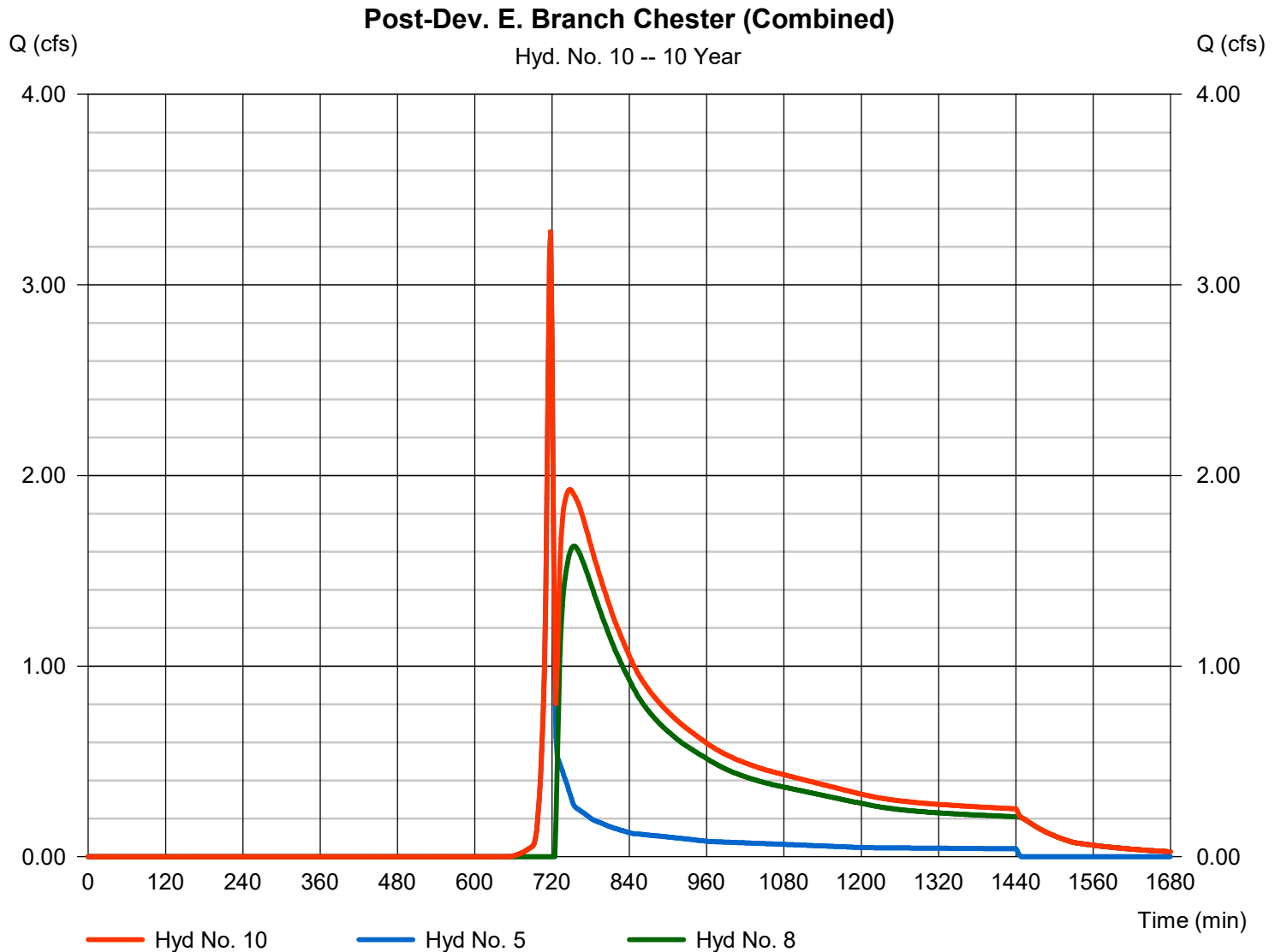
Hydrograph Report

Hyd. No. 10

Post-Dev. E. Branch Chester (Combined)

Hydrograph type = Combine
Storm frequency = 10 yrs
Time interval = 2 min
Inflow hyds. = 5, 8

Peak discharge = 3.279 cfs
Time to peak = 718 min
Hyd. volume = 30,358 cuft
Contrib. drain. area = 1.270 ac

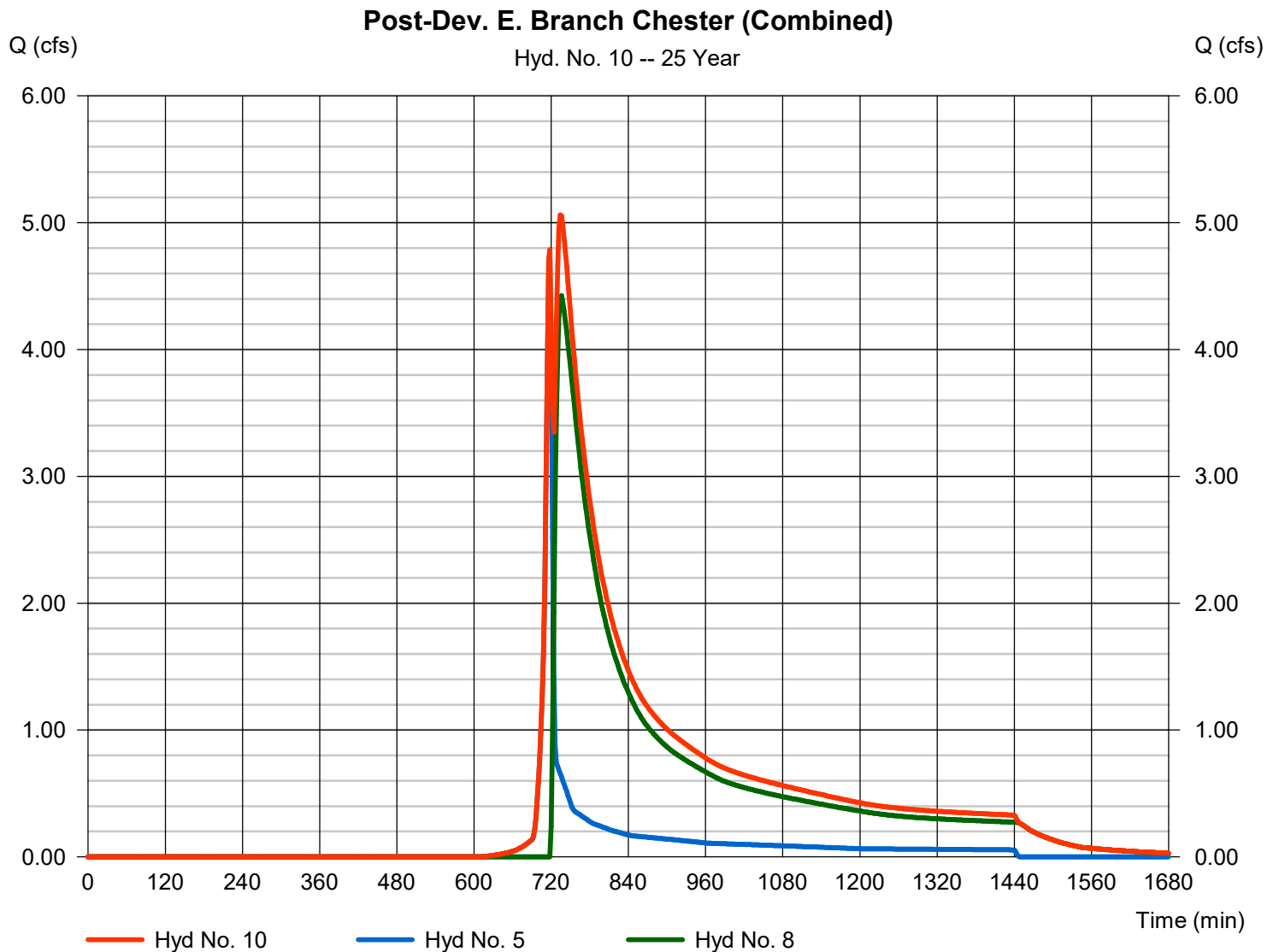


Hydrograph Report

Hyd. No. 10

Post-Dev. E. Branch Chester (Combined)

Hydrograph type	= Combine	Peak discharge	= 5.061 cfs
Storm frequency	= 25 yrs	Time to peak	= 734 min
Time interval	= 2 min	Hyd. volume	= 47,657 cuft
Inflow hyds.	= 5, 8	Contrib. drain. area	= 1.270 ac



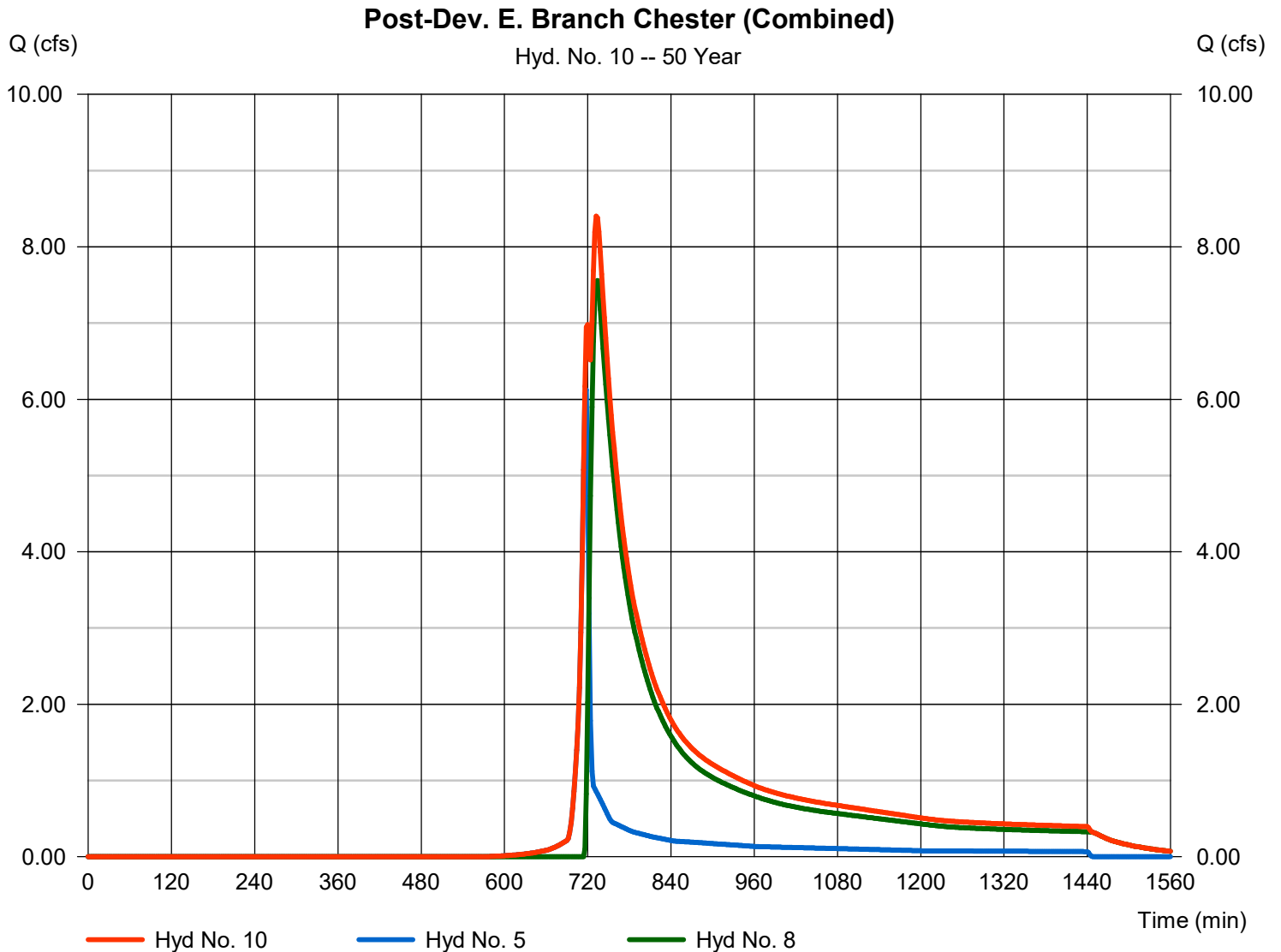
Hydrograph Report

Hyd. No. 10

Post-Dev. E. Branch Chester (Combined)

Hydrograph type = Combine
Storm frequency = 50 yrs
Time interval = 2 min
Inflow hyds. = 5, 8

Peak discharge = 8.403 cfs
Time to peak = 732 min
Hyd. volume = 63,120 cuft
Contrib. drain. area = 1.270 ac



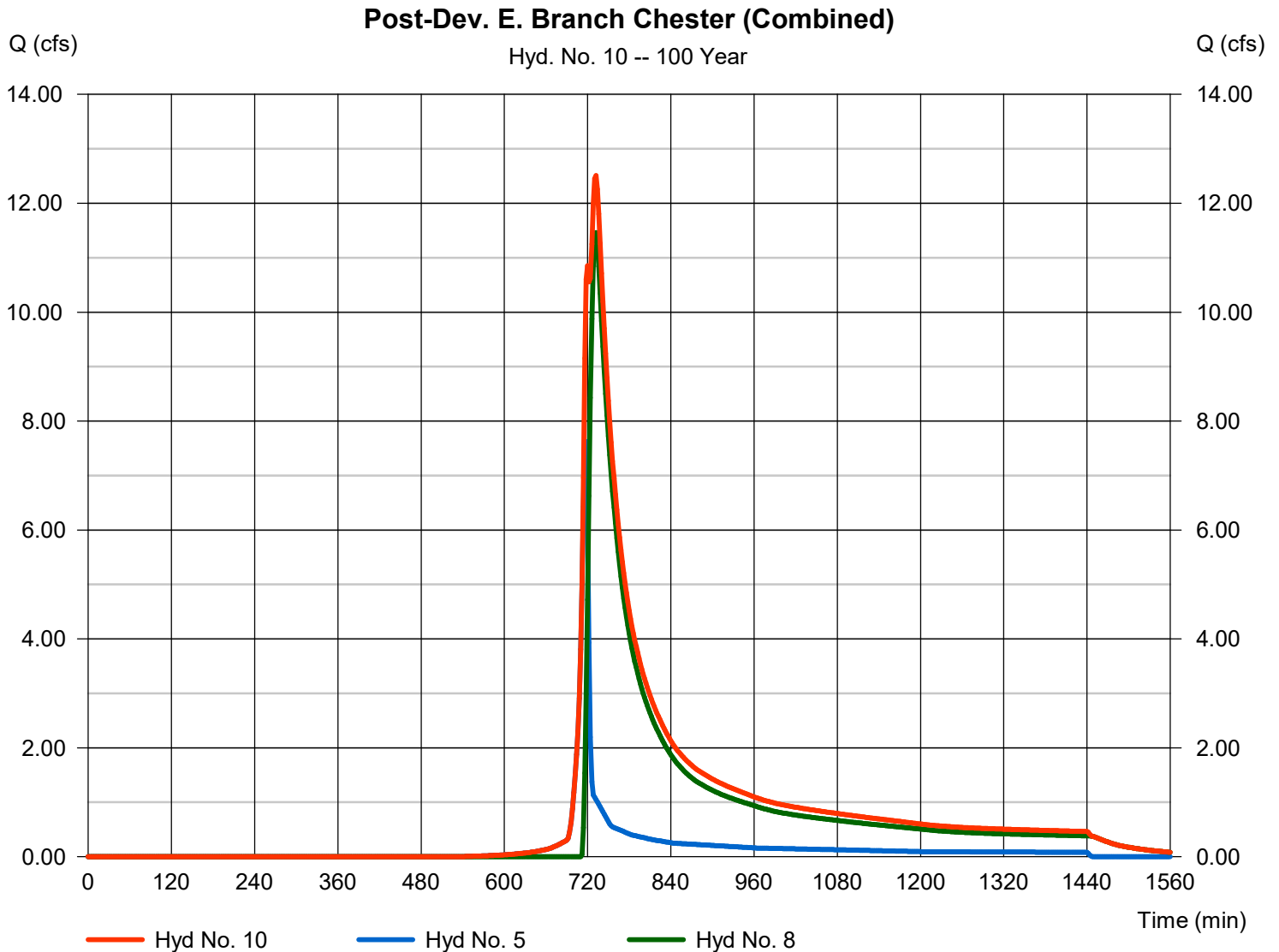
Hydrograph Report

Hyd. No. 10

Post-Dev. E. Branch Chester (Combined)

Hydrograph type = Combine
Storm frequency = 100 yrs
Time interval = 2 min
Inflow hyds. = 5, 8

Peak discharge = 12.51 cfs
Time to peak = 732 min
Hyd. volume = 80,555 cuft
Contrib. drain. area = 1.270 ac



UNT. TO EAST BRANCH CHESTER CREEK

ELA SPORT

ATHLETIC FACILITIES
DESIGN & CONSULTING

737 S. BROAD STREET
LITITZ, PA 17543
(717) 626-72713

NRCS (SCS) TR-55- WATERSHED WEIGHTED CURVE NUMBER POST-DEVELOPMENT SUMMARY

PROJECT: The Westtown School - Oak Lane Project
LOCATION: Westtown Township
COUNTY: Chester



LAND USE	Area (ac)						Total Area (ac.)	Composite 'CN' Value	Tc Min.
	Parking, Other Impervious (Disturbed Area)	Parking, Other Impervious (Undisturbed Area)	Open Space (Disturbed Area)	Open Space (Undisturbed Area)	Open Space (Disturbed Area)	Open Space (Undisturbed Area)			
HSG	B	B	B	B	D	D			
"CN" Value	98	98	61	61	80	80			
WATERSHED									
Infiltration Basin - BMP 4	0.30	0.00	5.12	2.79	0.54	0.92	9.67	65	22
Infiltration Bed - BMP 2	2.22	0.00	0.00	0.00	0.00	0.00	2.22	98	5
Infiltration Bed - BMP 3	2.22	0.00	0.00	0.00	0.00	0.00	2.22	98	5
Undetained	0.00	0.00	2.01	0.93	0.60	0.04	3.59	64	12



ELA SPORT
ATHLETIC FACILITIES
DESIGN & CONSULTING

737 S. BROAD STREET
 LITITZ, PA 17543
 (717) 626-72713

SUMMARY - SUBAREAS TIME OF CONCENTRATION PRE-DEVELOPMENT CONDITIONS

PROJECT: The Westtown School - Oak Lane Project
 LOCATION: Westtown Township
 COUNTY: Chester

Time of concentration (Tc) or travel time (Tt)
NRCS Velocity(Segmental) Method

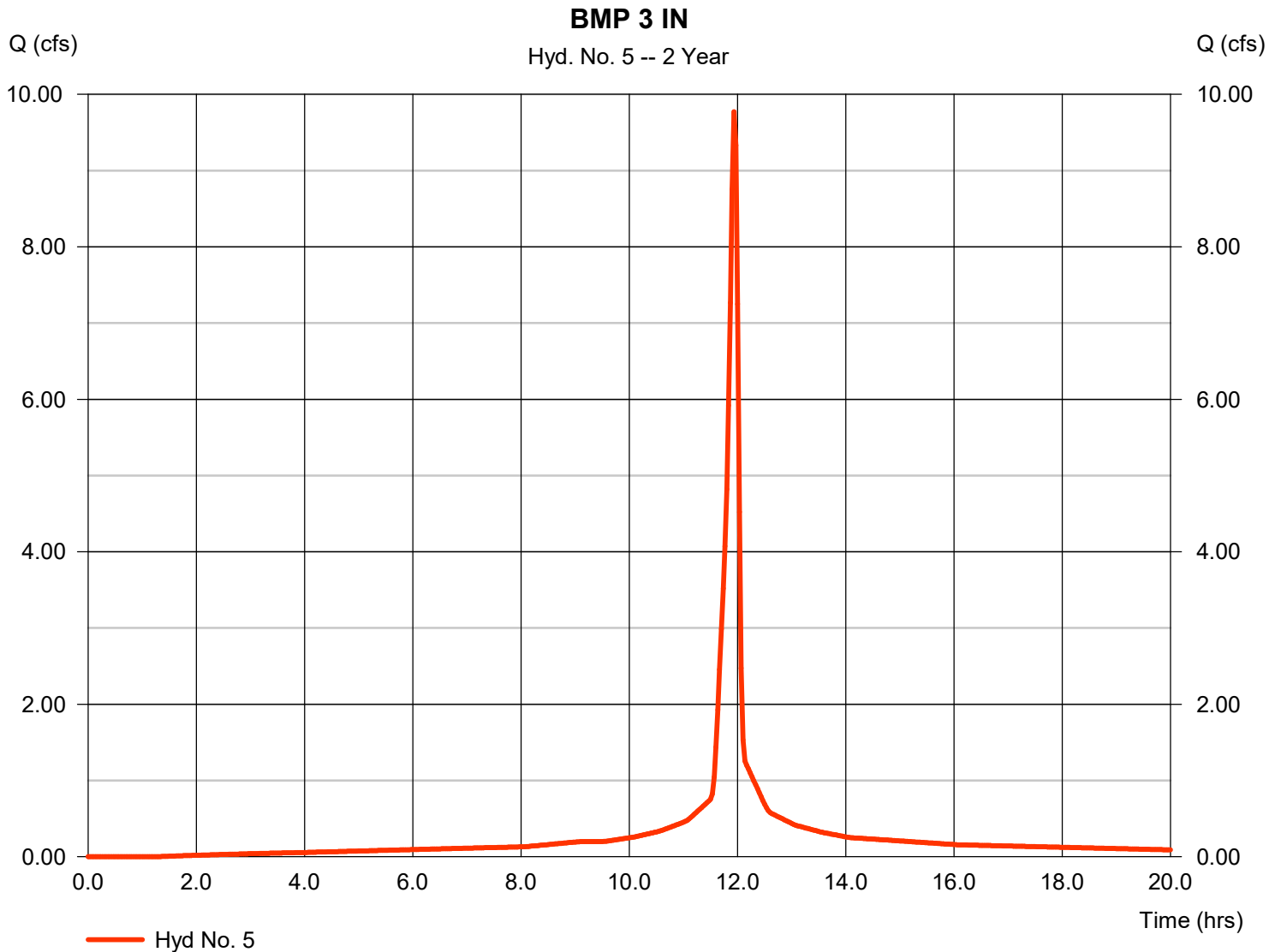
Sub area	overland						Shallow Concentrated							Channel or Pipe							Total	
	Length L ₁ 100 ft. max.	Slope S ₁	Manning's n	2 yr rainfall in.	Tc Min.	Flow Path Cover	Length L ₂ ft.	Slope S ₂ ft./ft.	Average Velocity ft./s	Tt Min.	Channel or Pipe C/P	Flow Area sq.ft.	Wetted Perimeter ft.	Pipe Diameter in.	Slope S ₃ ft./ft.	Manning's n	Length L ₃ ft.	Tt Min.	Tc Hrs.			
BMP 1	100	0.011	0.24	3.26	18			0	0.0	0.0	0.00	0.00						0				
				3.26	0	U	350	0.011	1.7	3.4	0.00	0.00						0				
				3.26	0	U	62	0.167	6.6	0.2	0.00	0.00						0				
					0				0	0	0.00	0.00						0				
					0				0	0	0.00	0.00						0.0				
					18					3.6								0.0	0.37			
Unt. to EBCC	100	0.040	0.24	3.26	10.7			0	0	0.0	0.00	0.00						0.0				
Undetained					0	U	313	0.048	3.5	1.5	0.00	0.00						0.0				
					0				0	0	0.00	0.00						0.0				
					0				0	0	0.00	0.00						0.0				
					0				0	0	0.00	0.00						0.0				
					0				0	0	0.00	0.00						0.0				
					0				0	0	0.00	0.00						0.0				
					0				0	0	0.00	0.00						0.0				
					10.7					1.5								0	0.20			

Hydrograph Report

Hyd. No. 5

BMP 3 IN

Hydrograph type	= SCS Runoff	Peak discharge	= 9.771 cfs
Storm frequency	= 2 yrs	Time to peak	= 11.93 hrs
Time interval	= 2 min	Hyd. volume	= 22,871 cuft
Drainage area	= 2.220 ac	Curve number	= 98
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 5.00 min
Total precip.	= 3.26 in	Distribution	= Type II
Storm duration	= 24 hrs	Shape factor	= 484



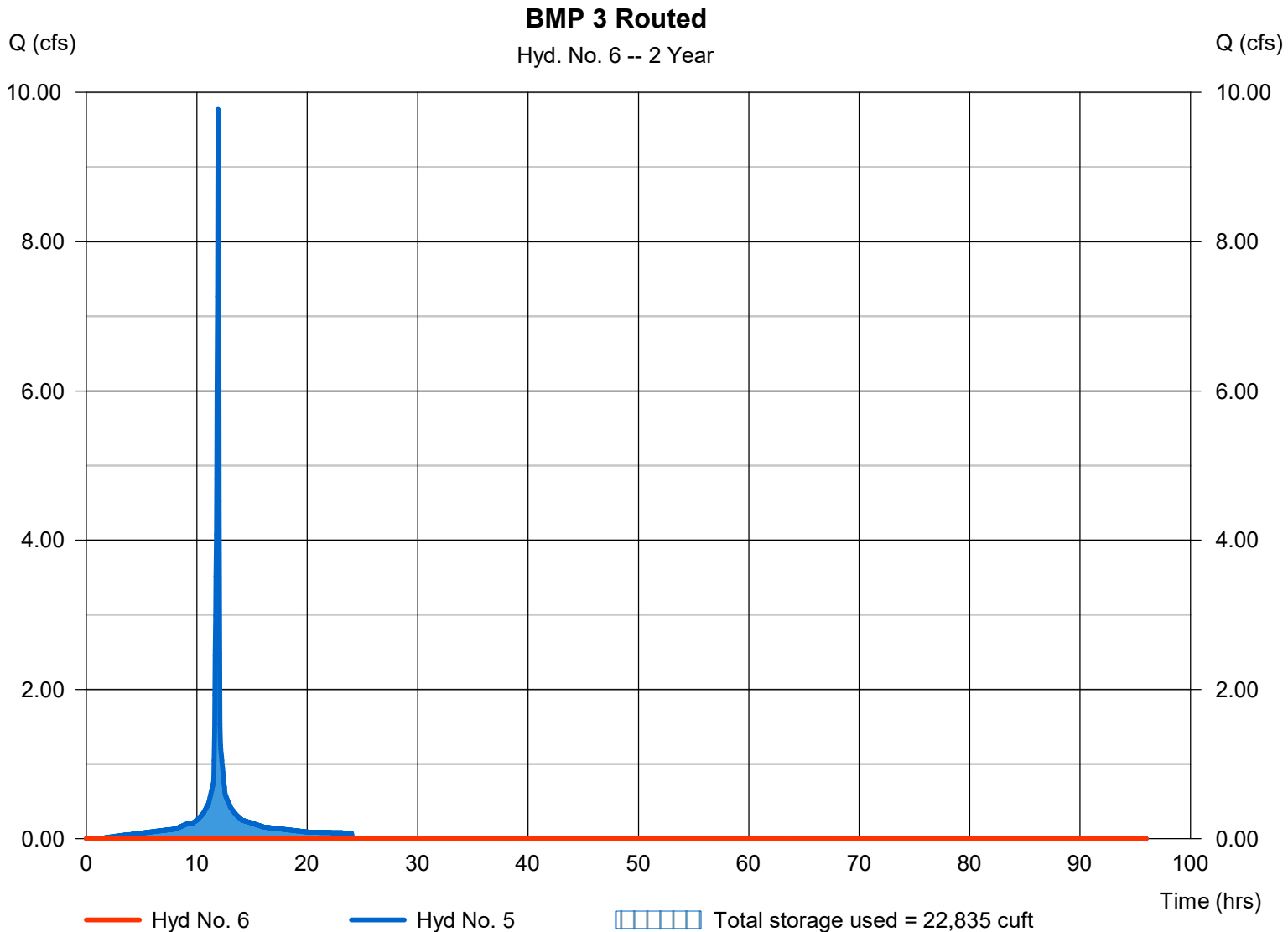
Hydrograph Report

Hyd. No. 6

BMP 3 Routed

Hydrograph type	= Reservoir	Peak discharge	= 0.006 cfs
Storm frequency	= 2 yrs	Time to peak	= 24.10 hrs
Time interval	= 2 min	Hyd. volume	= 772 cuft
Inflow hyd. No.	= 5 - BMP 3 IN	Max. Elevation	= 321.04 ft
Reservoir name	= BMP 3	Max. Storage	= 22,835 cuft

Storage Indication method used.



Pond Report

Pond No. 7 - BMP 3

Pond Data

Pond storage is based on user-defined values.

Stage / Storage Table

Stage (ft)	Elevation (ft)	Contour area (sqft)	Incr. Storage (cuft)	Total storage (cuft)
0.00	319.00	n/a	0	0
1.00	320.00	n/a	10,878	10,878
2.00	321.00	n/a	11,038	21,916
2.65	321.65	n/a	14,567	36,483
2.75	321.75	n/a	3,600	40,083
3.50	322.50	n/a	28,665	68,748

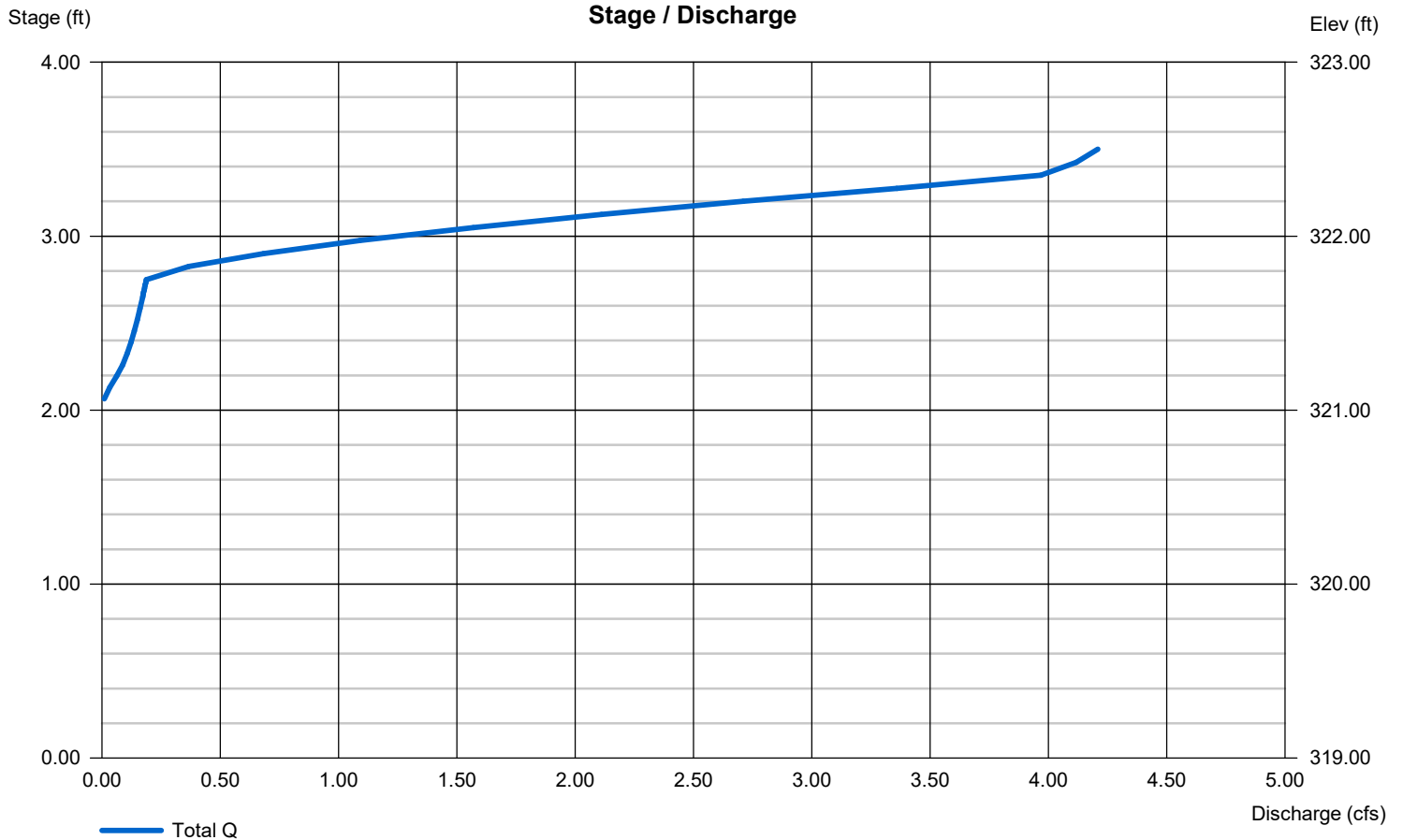
Culvert / Orifice Structures

	[A]	[B]	[C]	[PrfRsr]
Rise (in)	= 12.00	3.00	0.00	0.00
Span (in)	= 12.00	3.00	0.00	0.00
No. Barrels	= 1	1	0	0
Invert El. (ft)	= 319.00	321.00	0.00	0.00
Length (ft)	= 245.00	0.10	0.00	0.00
Slope (%)	= 0.75	0.00	0.00	n/a
N-Value	= .013	.013	.013	n/a
Orifice Coeff.	= 0.60	0.60	0.60	0.60
Multi-Stage	= n/a	Yes	No	No

Weir Structures

	[A]	[B]	[C]	[D]
Crest Len (ft)	= 3.14	0.00	0.00	0.00
Crest El. (ft)	= 321.75	0.00	0.00	0.00
Weir Coeff.	= 2.60	3.33	3.33	3.33
Weir Type	= Broad	---	---	---
Multi-Stage	= Yes	No	No	No
Exfil.(in/hr)	= 0.000 (by Wet area)			
TW Elev. (ft)	= 0.00			

Note: Culvert/Orifice outflows are analyzed under inlet (ic) and outlet (oc) control. Weir risers checked for orifice conditions (ic) and submergence (s).

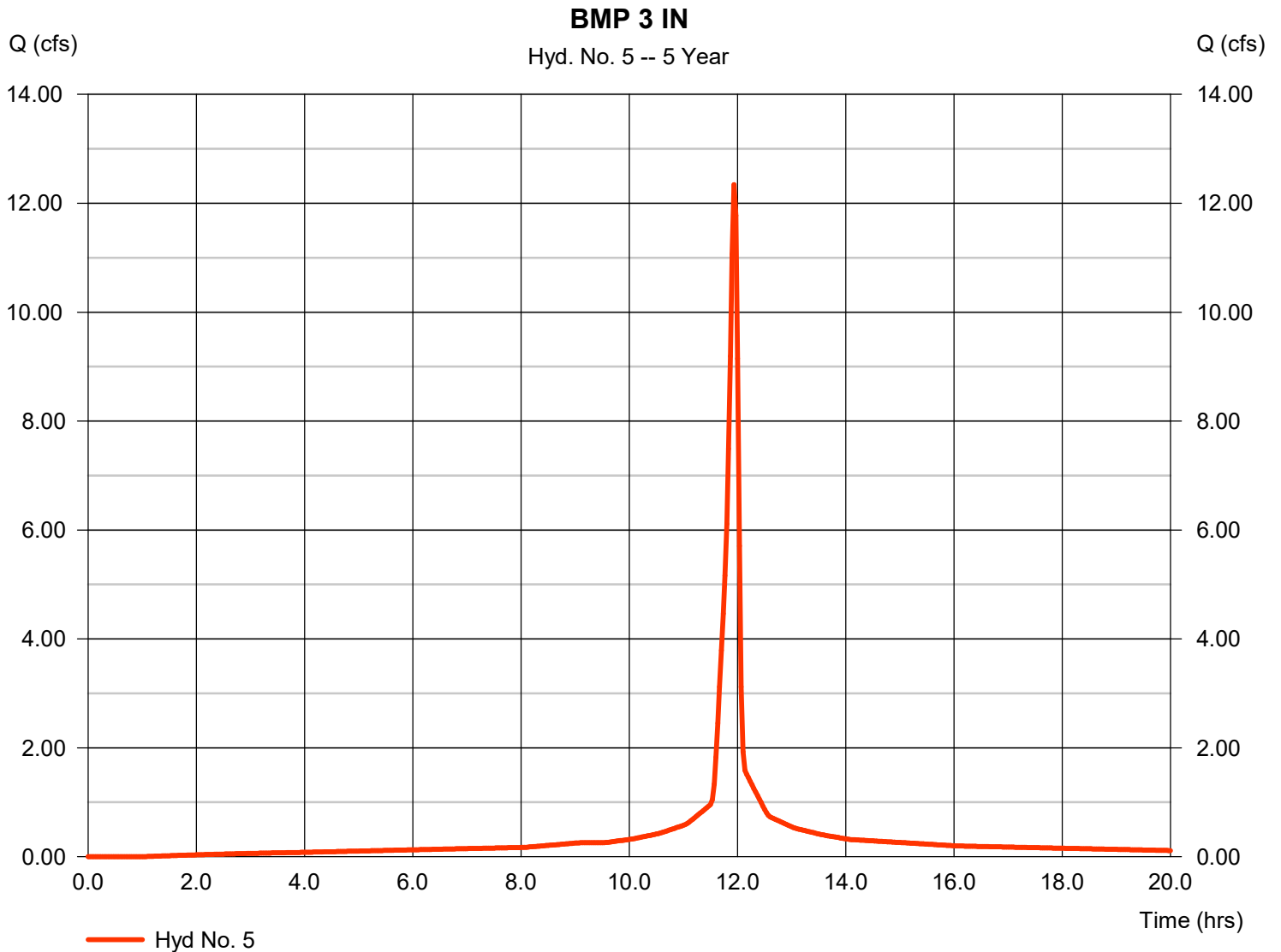


Hydrograph Report

Hyd. No. 5

BMP 3 IN

Hydrograph type	= SCS Runoff	Peak discharge	= 12.34 cfs
Storm frequency	= 5 yrs	Time to peak	= 11.93 hrs
Time interval	= 2 min	Hyd. volume	= 29,199 cuft
Drainage area	= 2.220 ac	Curve number	= 98
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 5.00 min
Total precip.	= 4.10 in	Distribution	= Type II
Storm duration	= 24 hrs	Shape factor	= 484



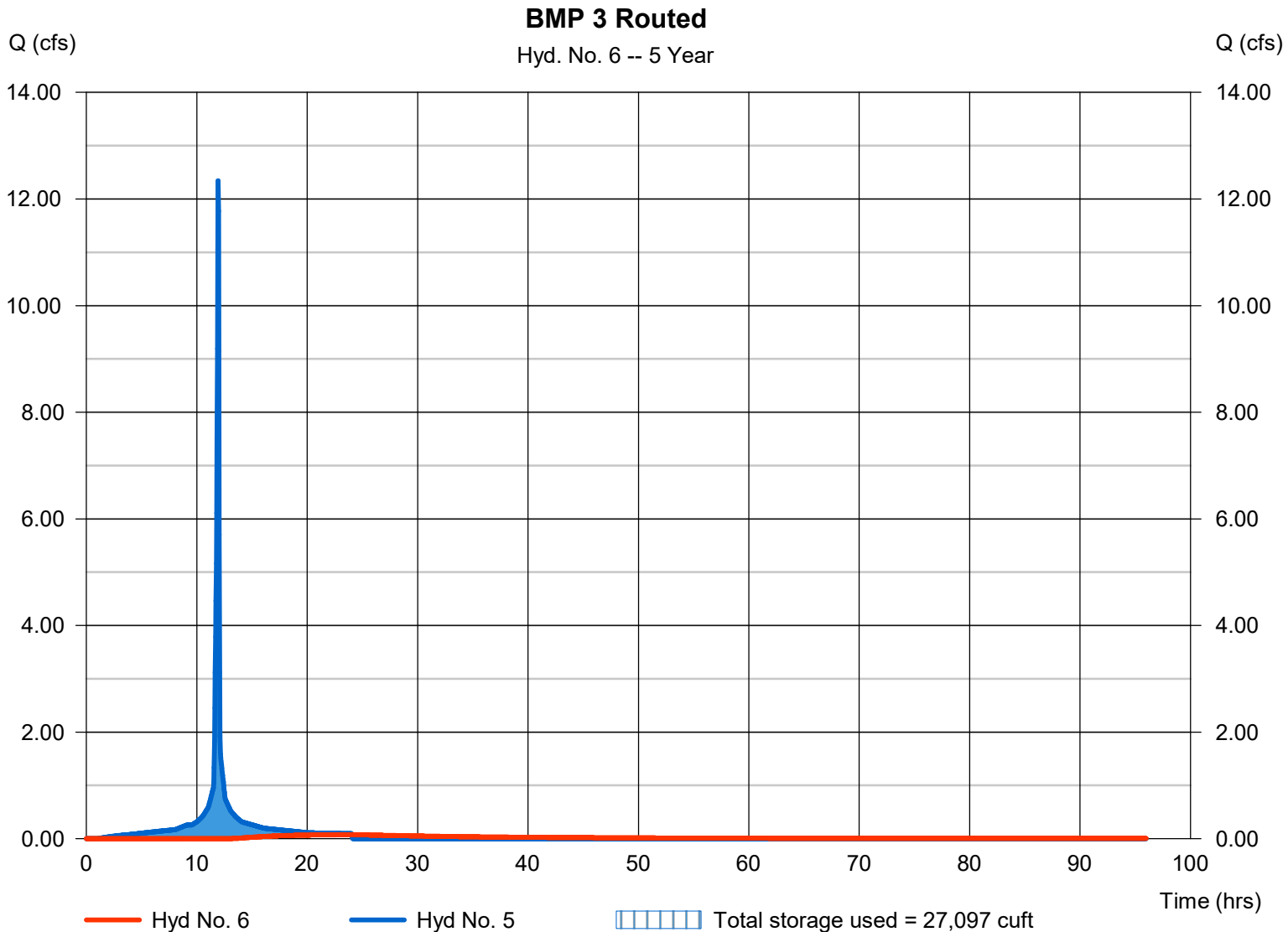
Hydrograph Report

Hyd. No. 6

BMP 3 Routed

Hydrograph type	= Reservoir	Peak discharge	= 0.076 cfs
Storm frequency	= 5 yrs	Time to peak	= 24.03 hrs
Time interval	= 2 min	Hyd. volume	= 6,655 cuft
Inflow hyd. No.	= 5 - BMP 3 IN	Max. Elevation	= 321.23 ft
Reservoir name	= BMP 3	Max. Storage	= 27,097 cuft

Storage Indication method used.

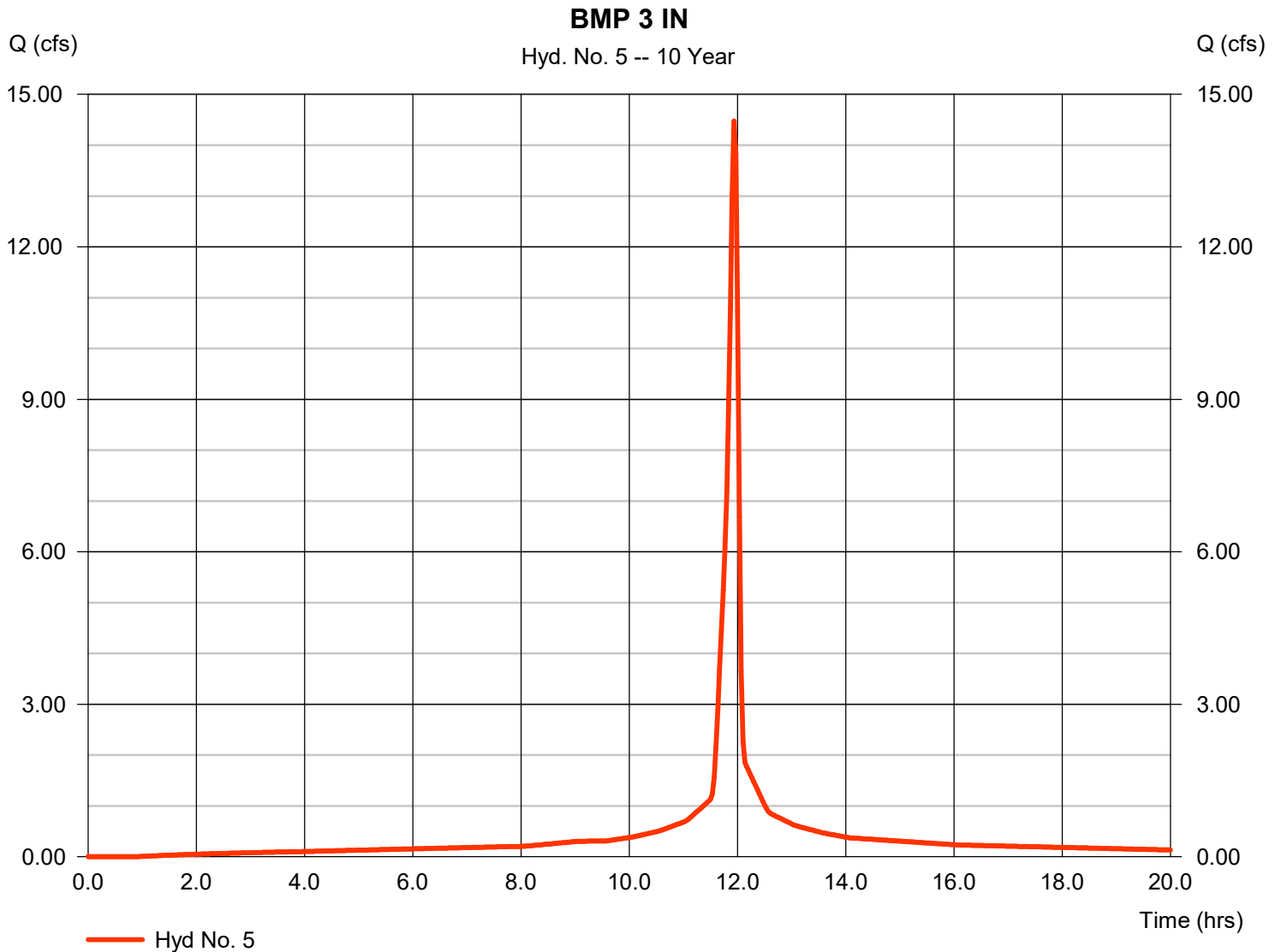


Hydrograph Report

Hyd. No. 5

BMP 3 IN

Hydrograph type	= SCS Runoff	Peak discharge	= 14.48 cfs
Storm frequency	= 10 yrs	Time to peak	= 11.93 hrs
Time interval	= 2 min	Hyd. volume	= 34,477 cuft
Drainage area	= 2.220 ac	Curve number	= 98
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 5.00 min
Total precip.	= 4.80 in	Distribution	= Type II
Storm duration	= 24 hrs	Shape factor	= 484



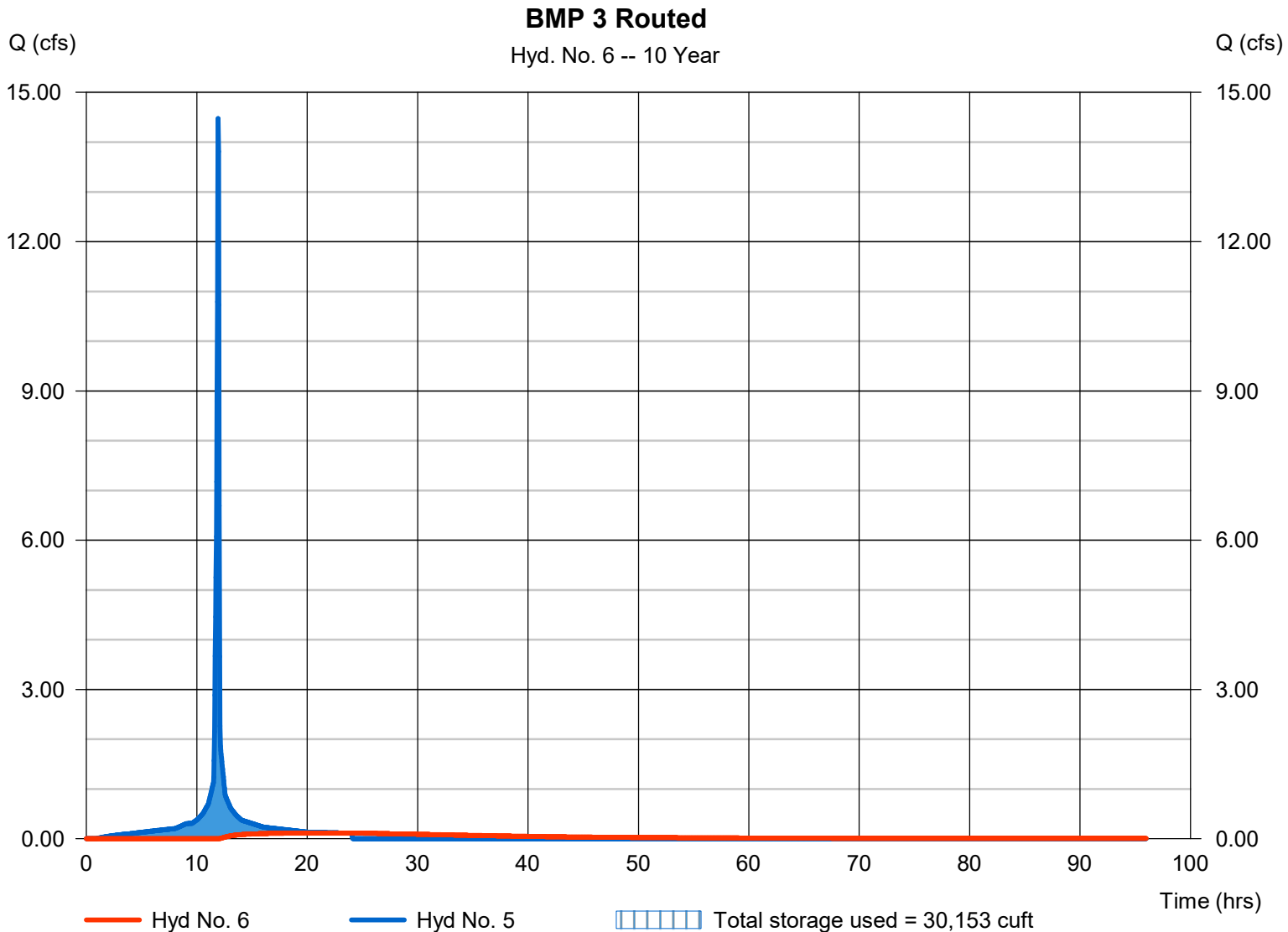
Hydrograph Report

Hyd. No. 6

BMP 3 Routed

Hydrograph type	= Reservoir	Peak discharge	= 0.116 cfs
Storm frequency	= 10 yrs	Time to peak	= 22.97 hrs
Time interval	= 2 min	Hyd. volume	= 11,796 cuft
Inflow hyd. No.	= 5 - BMP 3 IN	Max. Elevation	= 321.37 ft
Reservoir name	= BMP 3	Max. Storage	= 30,153 cuft

Storage Indication method used.

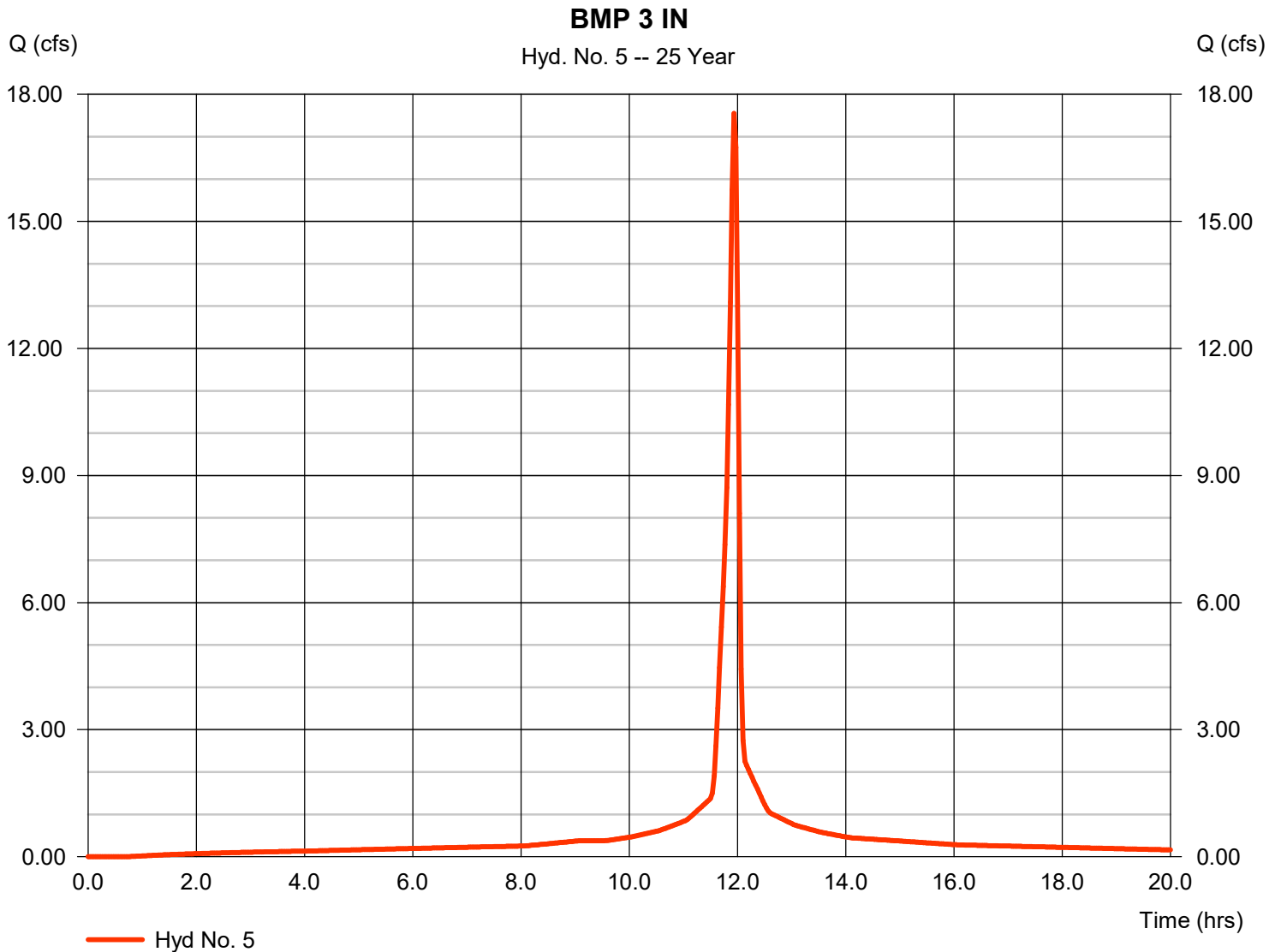


Hydrograph Report

Hyd. No. 5

BMP 3 IN

Hydrograph type	= SCS Runoff	Peak discharge	= 17.55 cfs
Storm frequency	= 25 yrs	Time to peak	= 11.93 hrs
Time interval	= 2 min	Hyd. volume	= 42,097 cuft
Drainage area	= 2.220 ac	Curve number	= 98
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 5.00 min
Total precip.	= 5.81 in	Distribution	= Type II
Storm duration	= 24 hrs	Shape factor	= 484



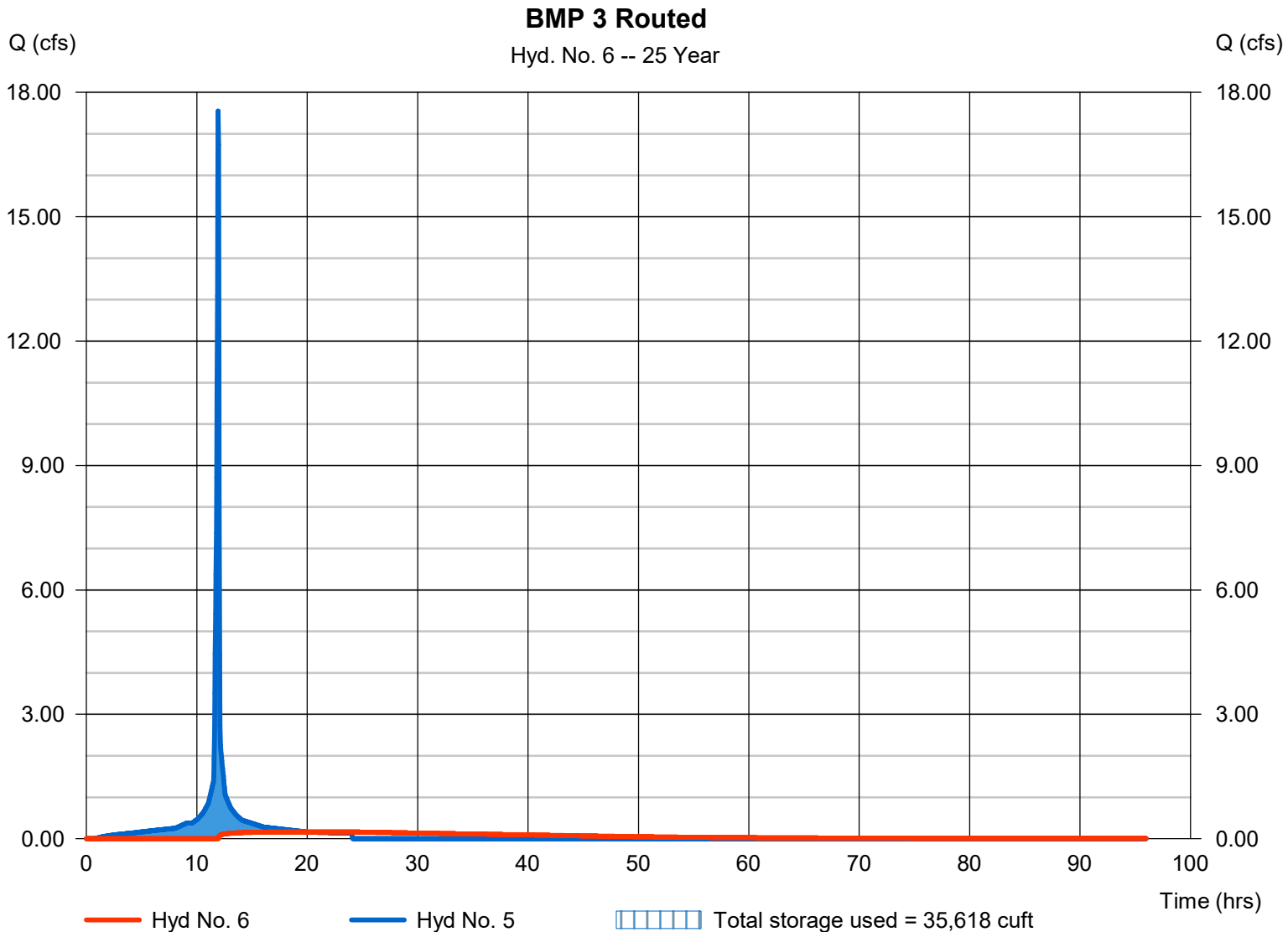
Hydrograph Report

Hyd. No. 6

BMP 3 Routed

Hydrograph type	= Reservoir	Peak discharge	= 0.165 cfs
Storm frequency	= 25 yrs	Time to peak	= 19.83 hrs
Time interval	= 2 min	Hyd. volume	= 19,215 cuft
Inflow hyd. No.	= 5 - BMP 3 IN	Max. Elevation	= 321.61 ft
Reservoir name	= BMP 3	Max. Storage	= 35,618 cuft

Storage Indication method used.

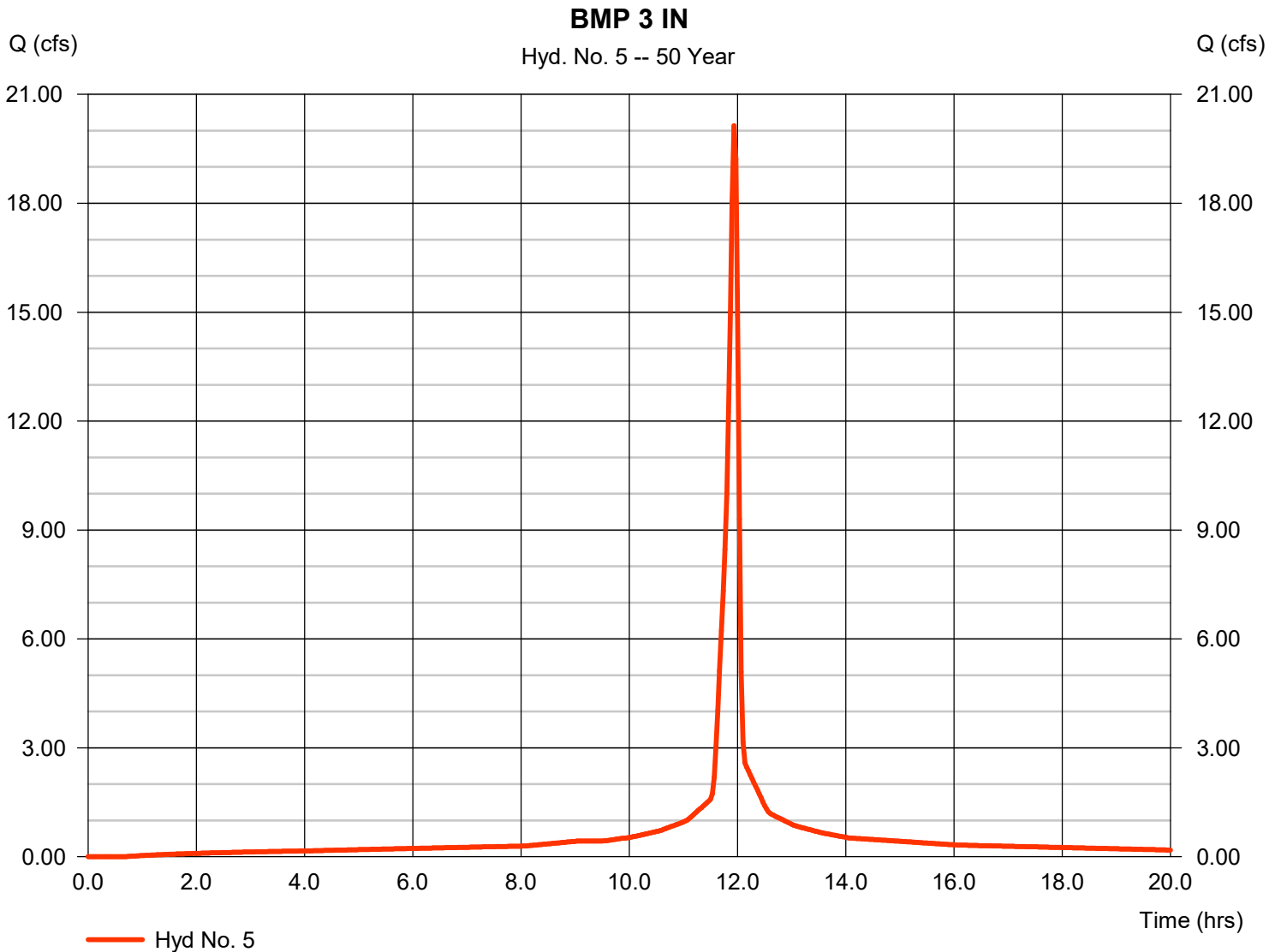


Hydrograph Report

Hyd. No. 5

BMP 3 IN

Hydrograph type	= SCS Runoff	Peak discharge	= 20.14 cfs
Storm frequency	= 50 yrs	Time to peak	= 11.93 hrs
Time interval	= 2 min	Hyd. volume	= 48,512 cuft
Drainage area	= 2.220 ac	Curve number	= 98
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 5.00 min
Total precip.	= 6.66 in	Distribution	= Type II
Storm duration	= 24 hrs	Shape factor	= 484



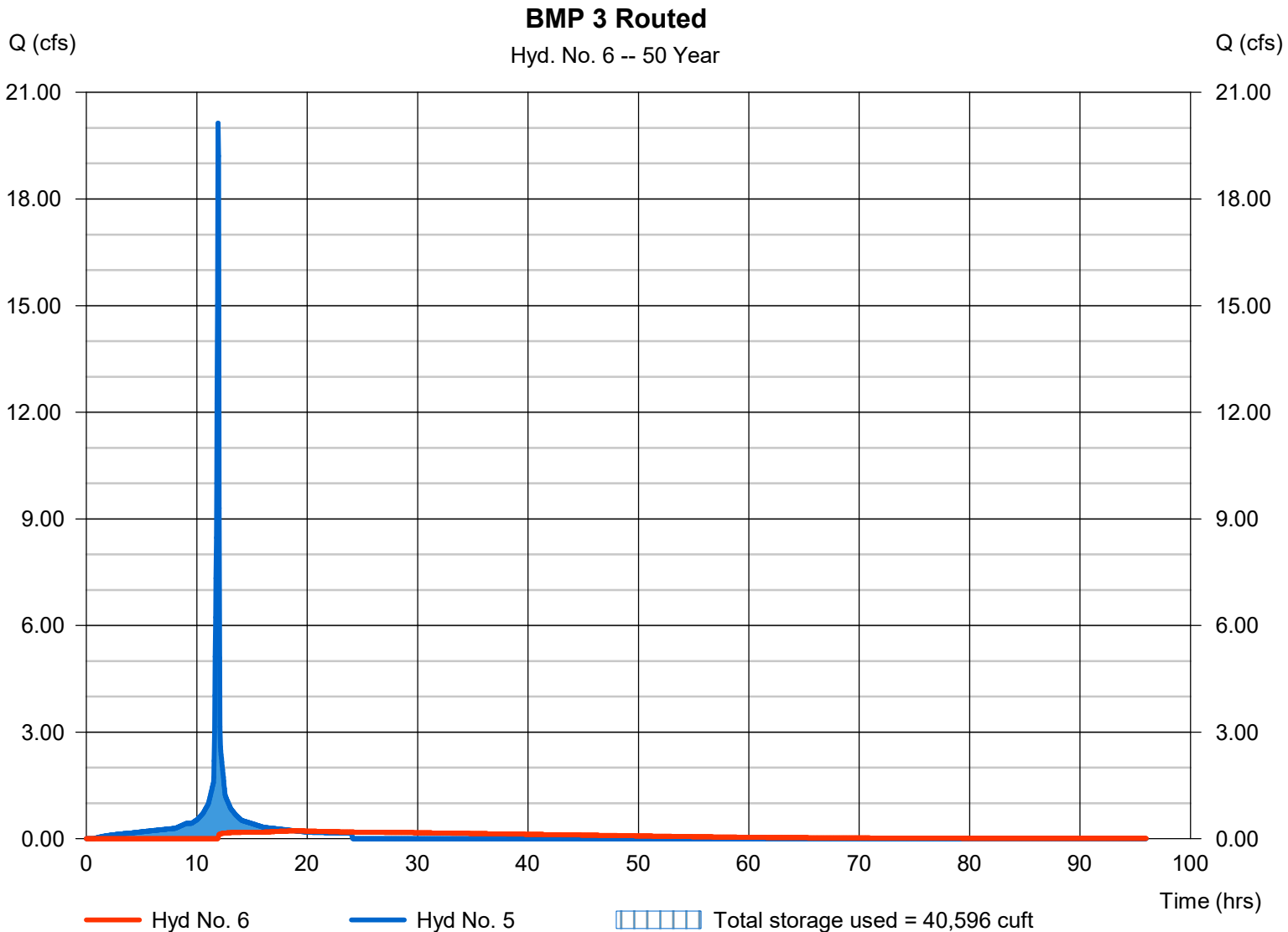
Hydrograph Report

Hyd. No. 6

BMP 3 Routed

Hydrograph type	= Reservoir	Peak discharge	= 0.219 cfs
Storm frequency	= 50 yrs	Time to peak	= 19.00 hrs
Time interval	= 2 min	Hyd. volume	= 25,455 cuft
Inflow hyd. No.	= 5 - BMP 3 IN	Max. Elevation	= 321.76 ft
Reservoir name	= BMP 3	Max. Storage	= 40,596 cuft

Storage Indication method used.

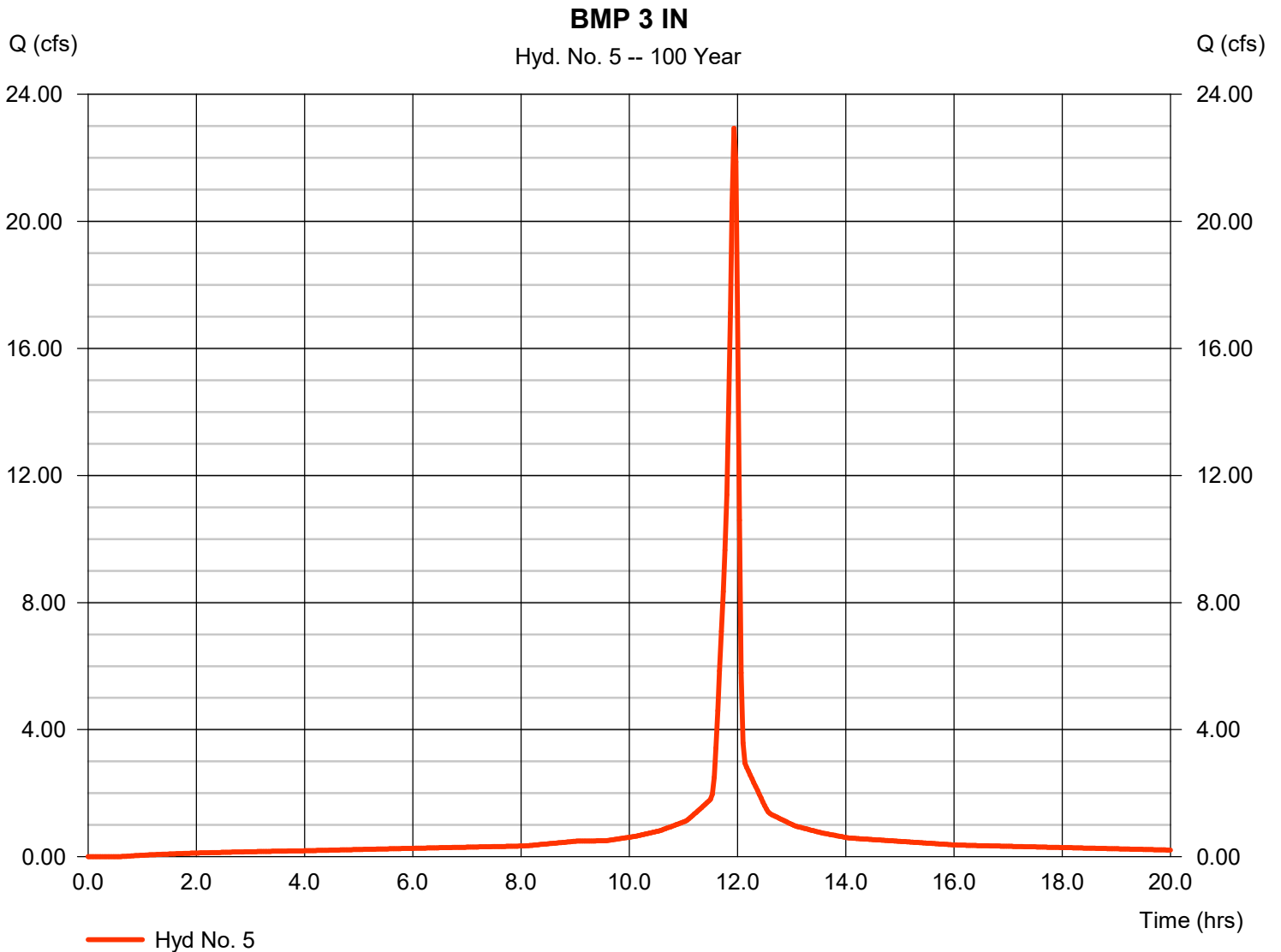


Hydrograph Report

Hyd. No. 5

BMP 3 IN

Hydrograph type	= SCS Runoff	Peak discharge	= 22.94 cfs
Storm frequency	= 100 yrs	Time to peak	= 11.93 hrs
Time interval	= 2 min	Hyd. volume	= 55,457 cuft
Drainage area	= 2.220 ac	Curve number	= 98
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 5.00 min
Total precip.	= 7.58 in	Distribution	= Type II
Storm duration	= 24 hrs	Shape factor	= 484



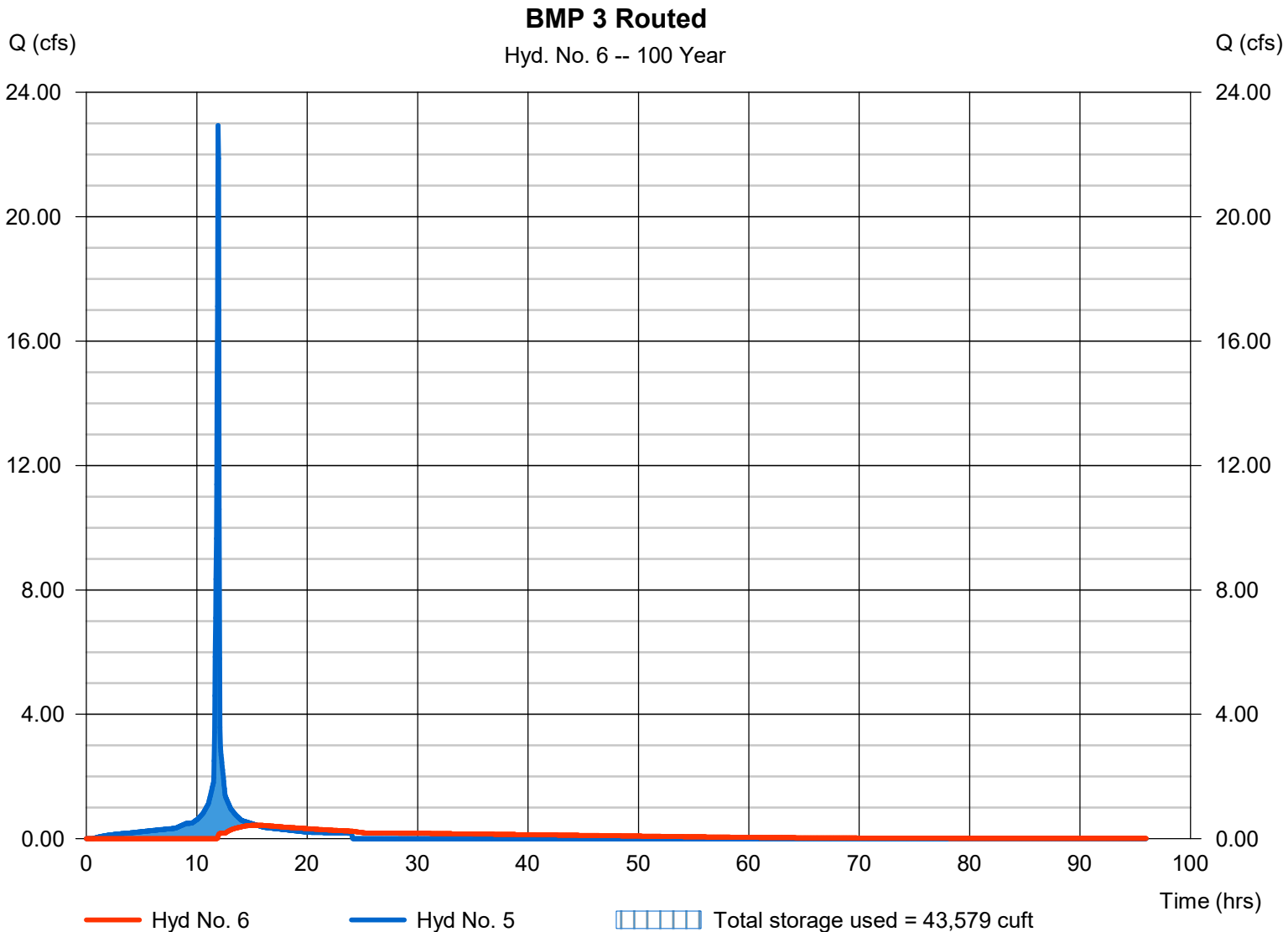
Hydrograph Report

Hyd. No. 6

BMP 3 Routed

Hydrograph type	= Reservoir	Peak discharge	= 0.435 cfs
Storm frequency	= 100 yrs	Time to peak	= 15.43 hrs
Time interval	= 2 min	Hyd. volume	= 32,369 cuft
Inflow hyd. No.	= 5 - BMP 3 IN	Max. Elevation	= 321.84 ft
Reservoir name	= BMP 3	Max. Storage	= 43,579 cuft

Storage Indication method used.

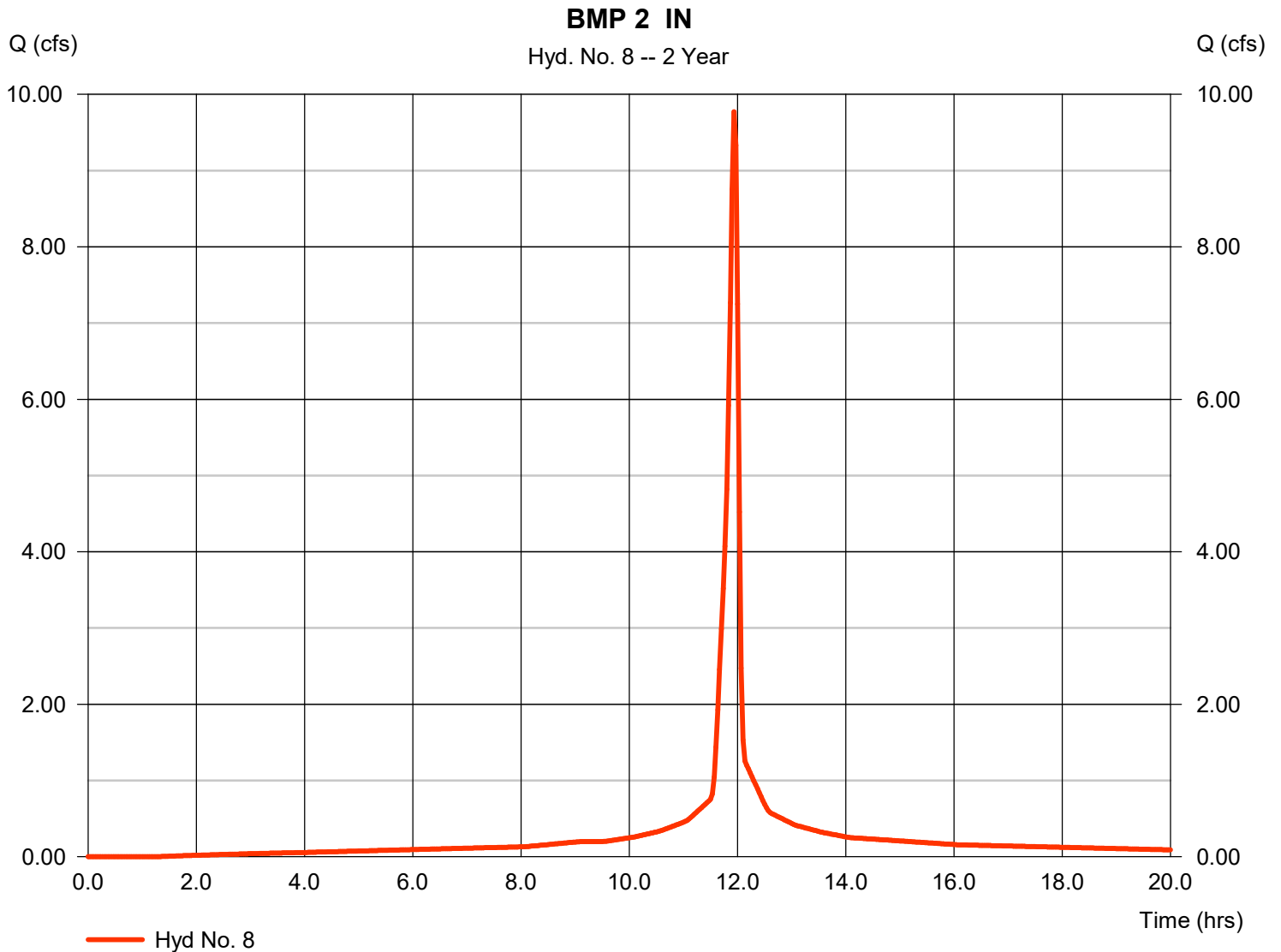


Hydrograph Report

Hyd. No. 8

BMP 2 IN

Hydrograph type	= SCS Runoff	Peak discharge	= 9.771 cfs
Storm frequency	= 2 yrs	Time to peak	= 11.93 hrs
Time interval	= 2 min	Hyd. volume	= 22,871 cuft
Drainage area	= 2.220 ac	Curve number	= 98
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 5.00 min
Total precip.	= 3.26 in	Distribution	= Type II
Storm duration	= 24 hrs	Shape factor	= 484



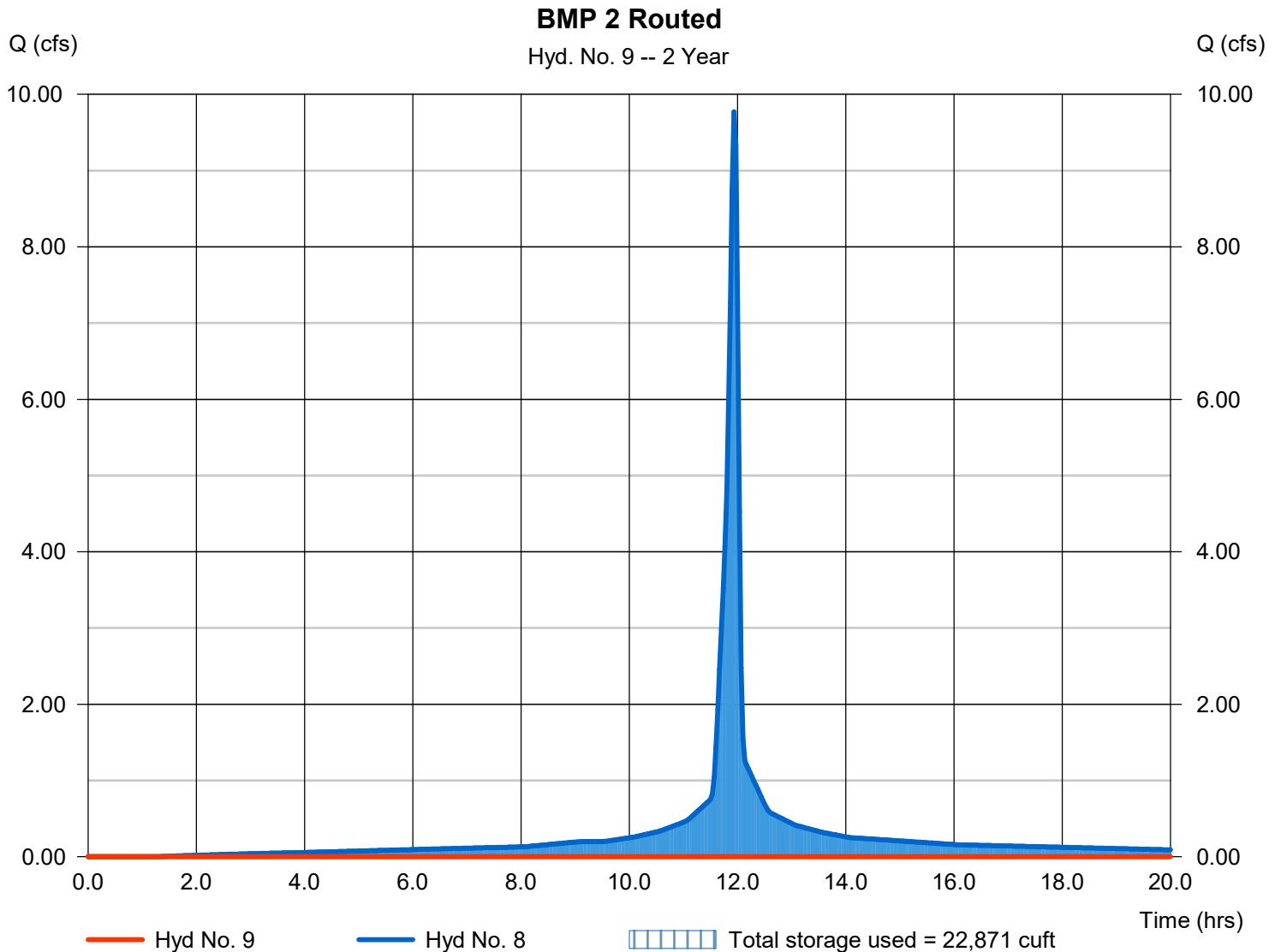
Hydrograph Report

Hyd. No. 9

BMP 2 Routed

Hydrograph type	= Reservoir	Peak discharge	= 0.000 cfs
Storm frequency	= 2 yrs	Time to peak	= n/a
Time interval	= 2 min	Hyd. volume	= 0 cuft
Inflow hyd. No.	= 8 - BMP 2 IN	Max. Elevation	= 316.75 ft
Reservoir name	= BMP 2	Max. Storage	= 22,871 cuft

Storage Indication method used.



Pond Report

Pond No. 6 - BMP 2

Pond Data

Pond storage is based on user-defined values.

Stage / Storage Table

Stage (ft)	Elevation (ft)	Contour area (sqft)	Incr. Storage (cuft)	Total storage (cuft)
0.00	316.00	n/a	0	0
0.67	316.67	n/a	20,294	20,294
0.75	316.75	n/a	2,741	23,035
1.50	317.50	n/a	28,665	51,700

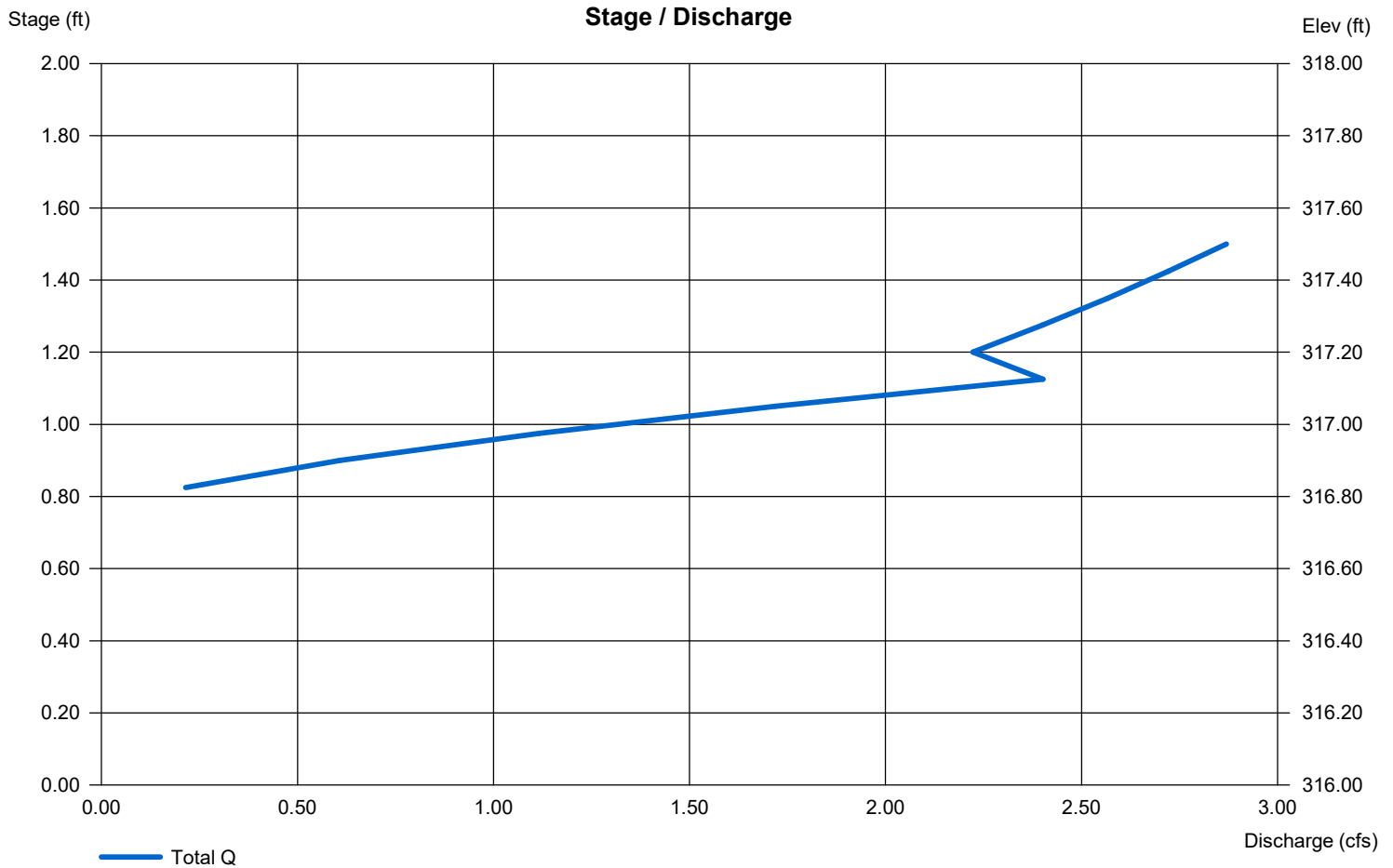
Culvert / Orifice Structures

	[A]	[B]	[C]	[PrfRsr]
Rise (in)	= 15.00	0.00	0.00	0.00
Span (in)	= 15.00	0.00	0.00	0.00
No. Barrels	= 1	0	0	0
Invert El. (ft)	= 312.50	0.00	0.00	0.00
Length (ft)	= 84.00	0.00	0.00	0.00
Slope (%)	= 0.53	0.00	0.00	n/a
N-Value	= .013	.013	.013	n/a
Orifice Coeff.	= 0.60	0.60	0.60	0.60
Multi-Stage	= n/a	No	No	No

Weir Structures

	[A]	[B]	[C]	[D]
Crest Len (ft)	= 3.14	0.00	0.00	0.00
Crest El. (ft)	= 316.75	0.00	0.00	0.00
Weir Coeff.	= 3.33	3.33	3.33	3.33
Weir Type	= 1	---	---	---
Multi-Stage	= Yes	No	No	No
Exfil.(in/hr)	= 0.000 (by Wet area)			
TW Elev. (ft)	= 0.00			

Note: Culvert/Orifice outflows are analyzed under inlet (ic) and outlet (oc) control. Weir risers checked for orifice conditions (ic) and submergence (s).

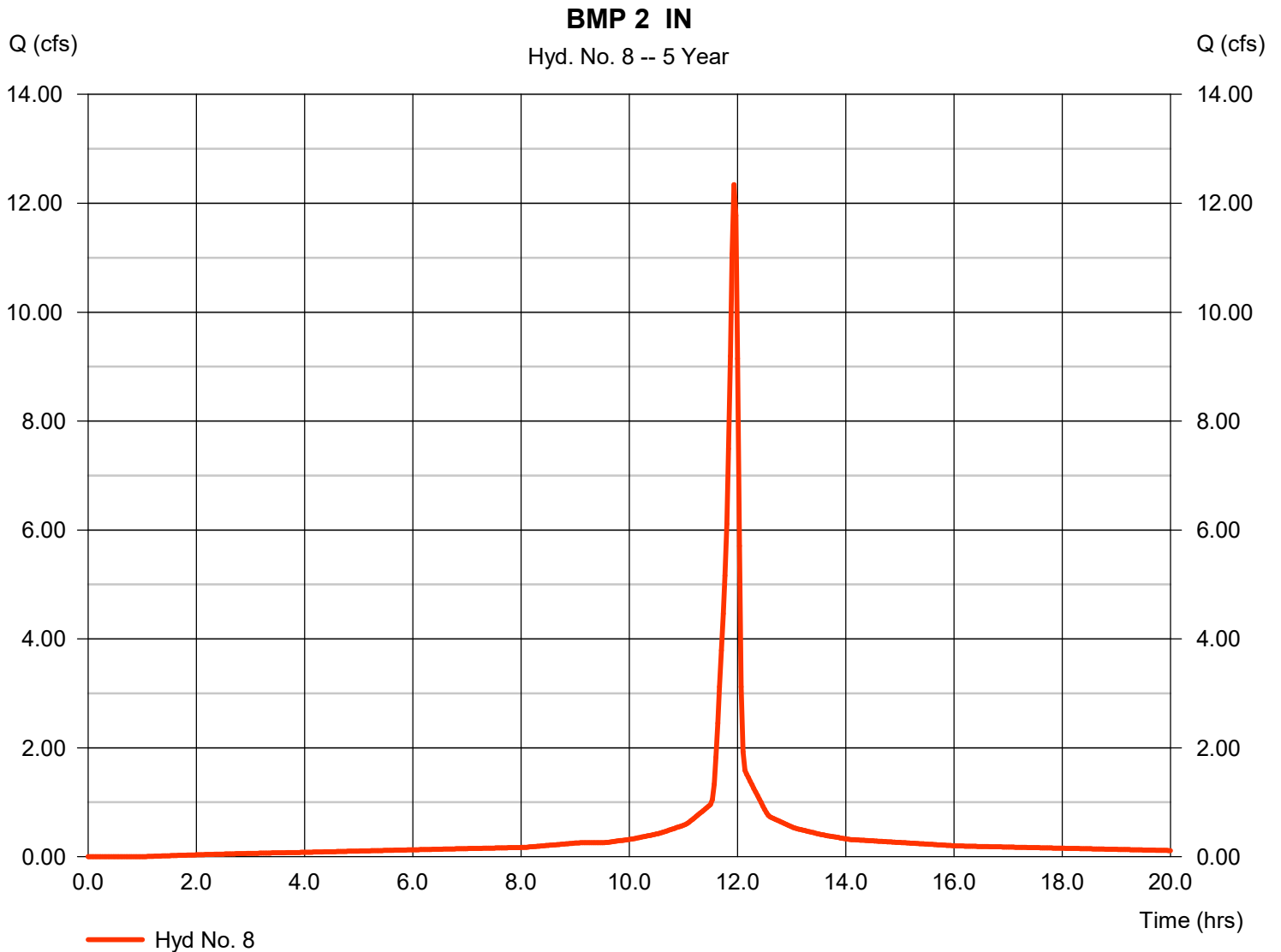


Hydrograph Report

Hyd. No. 8

BMP 2 IN

Hydrograph type	= SCS Runoff	Peak discharge	= 12.34 cfs
Storm frequency	= 5 yrs	Time to peak	= 11.93 hrs
Time interval	= 2 min	Hyd. volume	= 29,199 cuft
Drainage area	= 2.220 ac	Curve number	= 98
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 5.00 min
Total precip.	= 4.10 in	Distribution	= Type II
Storm duration	= 24 hrs	Shape factor	= 484



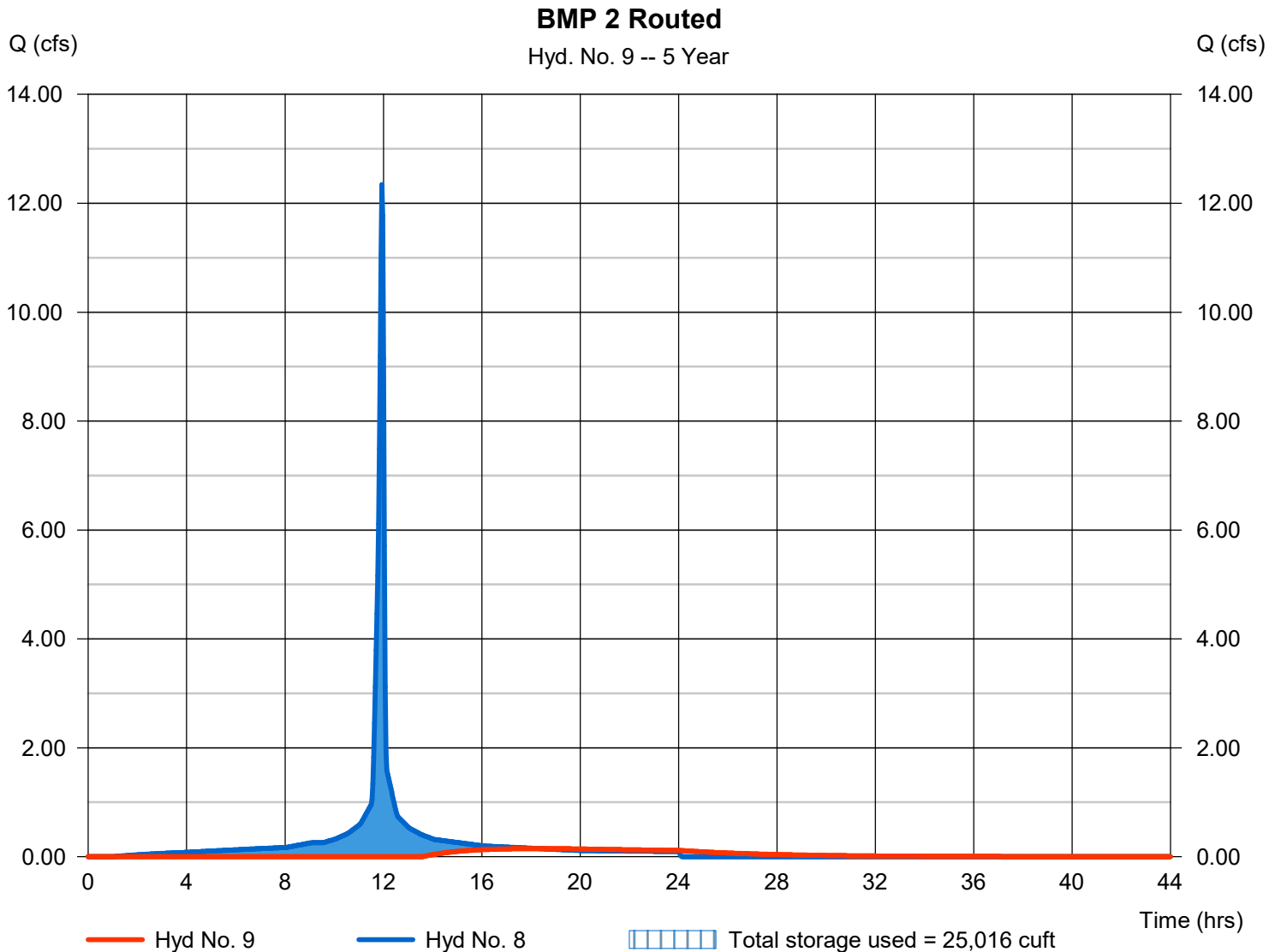
Hydrograph Report

Hyd. No. 9

BMP 2 Routed

Hydrograph type	= Reservoir	Peak discharge	= 0.148 cfs
Storm frequency	= 5 yrs	Time to peak	= 18.33 hrs
Time interval	= 2 min	Hyd. volume	= 6,151 cuft
Inflow hyd. No.	= 8 - BMP 2 IN	Max. Elevation	= 316.80 ft
Reservoir name	= BMP 2	Max. Storage	= 25,016 cuft

Storage Indication method used.

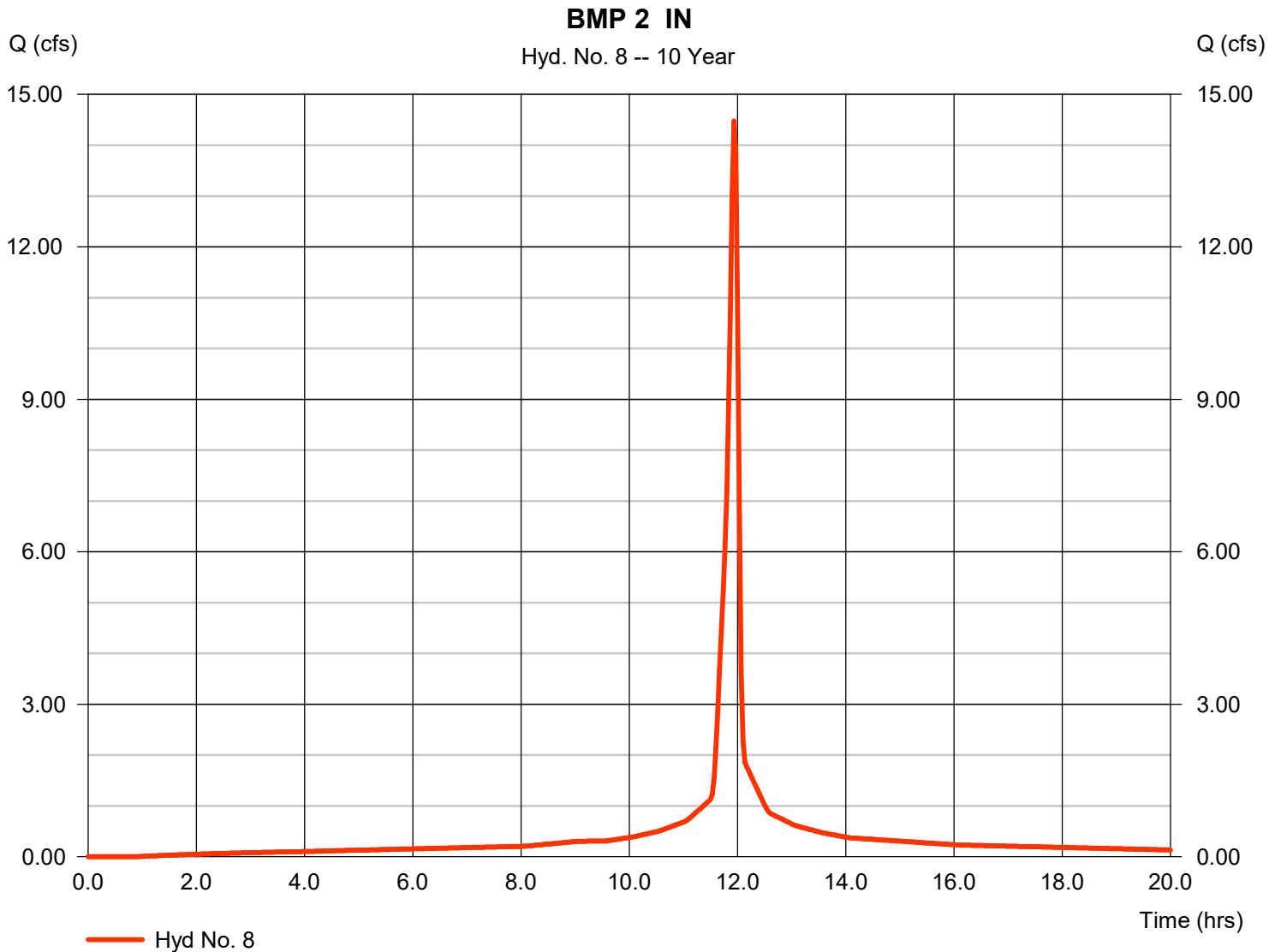


Hydrograph Report

Hyd. No. 8

BMP 2 IN

Hydrograph type	= SCS Runoff	Peak discharge	= 14.48 cfs
Storm frequency	= 10 yrs	Time to peak	= 11.93 hrs
Time interval	= 2 min	Hyd. volume	= 34,477 cuft
Drainage area	= 2.220 ac	Curve number	= 98
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 5.00 min
Total precip.	= 4.80 in	Distribution	= Type II
Storm duration	= 24 hrs	Shape factor	= 484



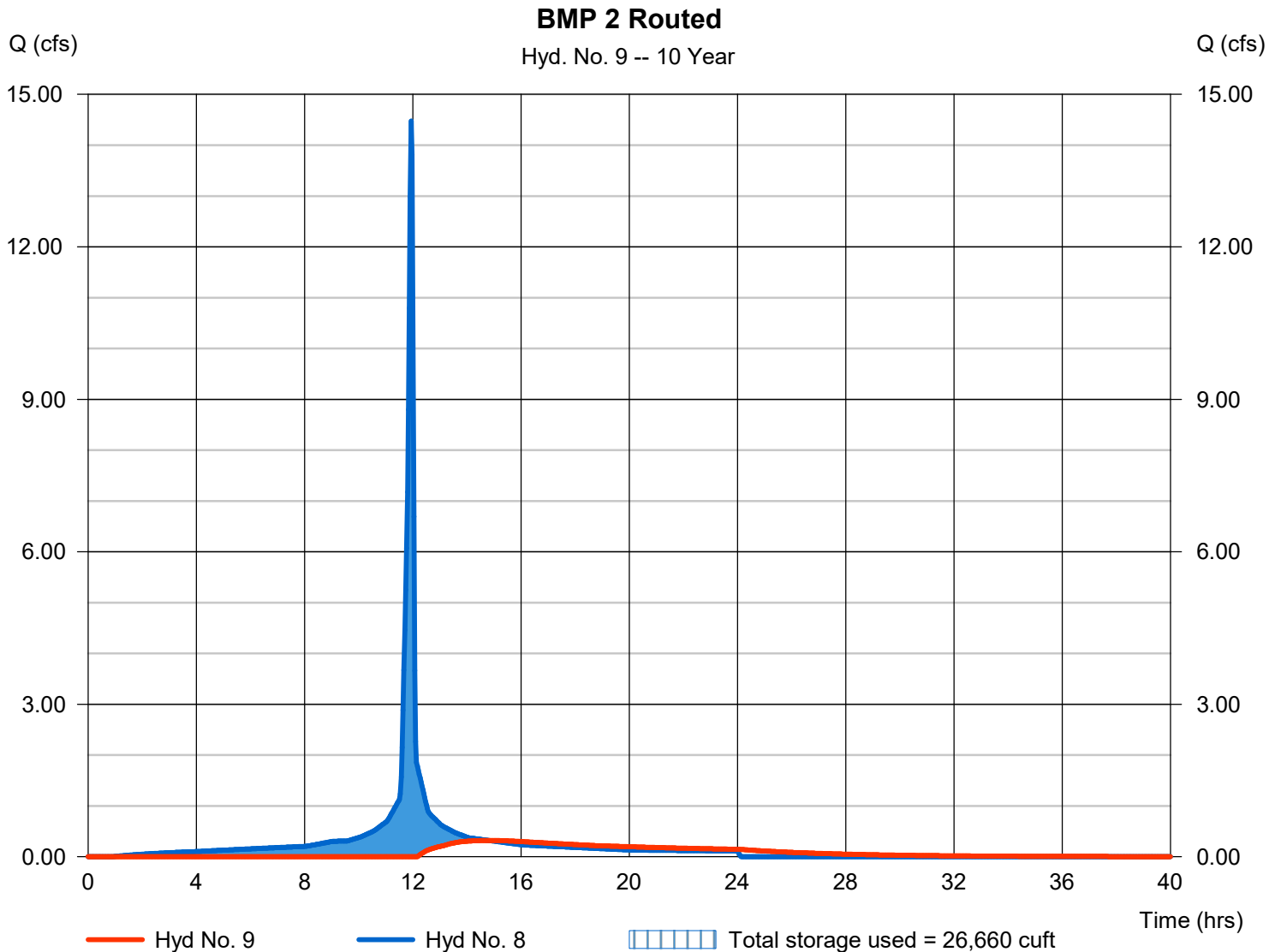
Hydrograph Report

Hyd. No. 9

BMP 2 Routed

Hydrograph type	= Reservoir	Peak discharge	= 0.319 cfs
Storm frequency	= 10 yrs	Time to peak	= 14.80 hrs
Time interval	= 2 min	Hyd. volume	= 11,429 cuft
Inflow hyd. No.	= 8 - BMP 2 IN	Max. Elevation	= 316.84 ft
Reservoir name	= BMP 2	Max. Storage	= 26,660 cuft

Storage Indication method used.

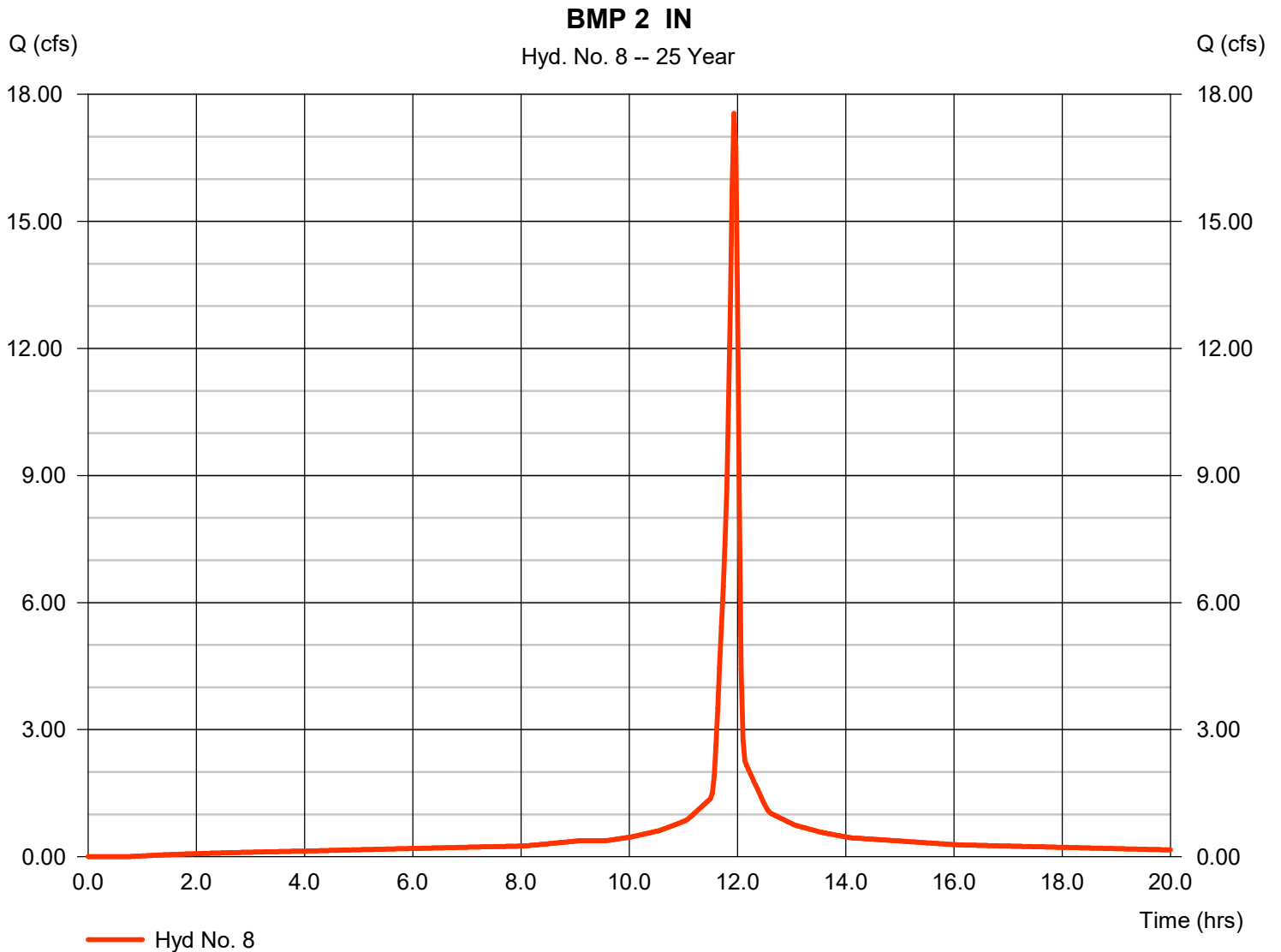


Hydrograph Report

Hyd. No. 8

BMP 2 IN

Hydrograph type	= SCS Runoff	Peak discharge	= 17.55 cfs
Storm frequency	= 25 yrs	Time to peak	= 11.93 hrs
Time interval	= 2 min	Hyd. volume	= 42,097 cuft
Drainage area	= 2.220 ac	Curve number	= 98
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 5.00 min
Total precip.	= 5.81 in	Distribution	= Type II
Storm duration	= 24 hrs	Shape factor	= 484



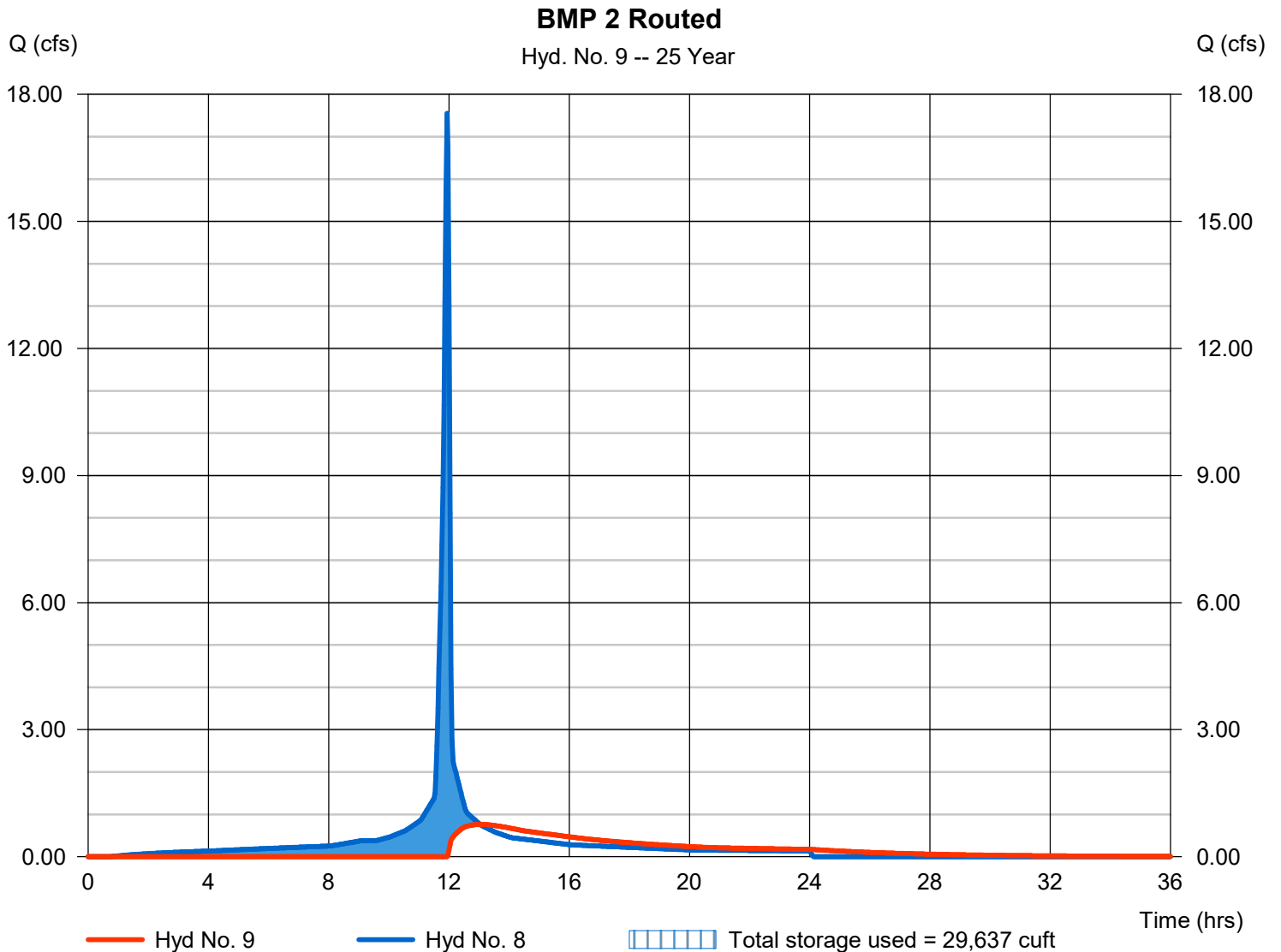
Hydrograph Report

Hyd. No. 9

BMP 2 Routed

Hydrograph type	= Reservoir	Peak discharge	= 0.762 cfs
Storm frequency	= 25 yrs	Time to peak	= 13.03 hrs
Time interval	= 2 min	Hyd. volume	= 19,048 cuft
Inflow hyd. No.	= 8 - BMP 2 IN	Max. Elevation	= 316.92 ft
Reservoir name	= BMP 2	Max. Storage	= 29,637 cuft

Storage Indication method used.

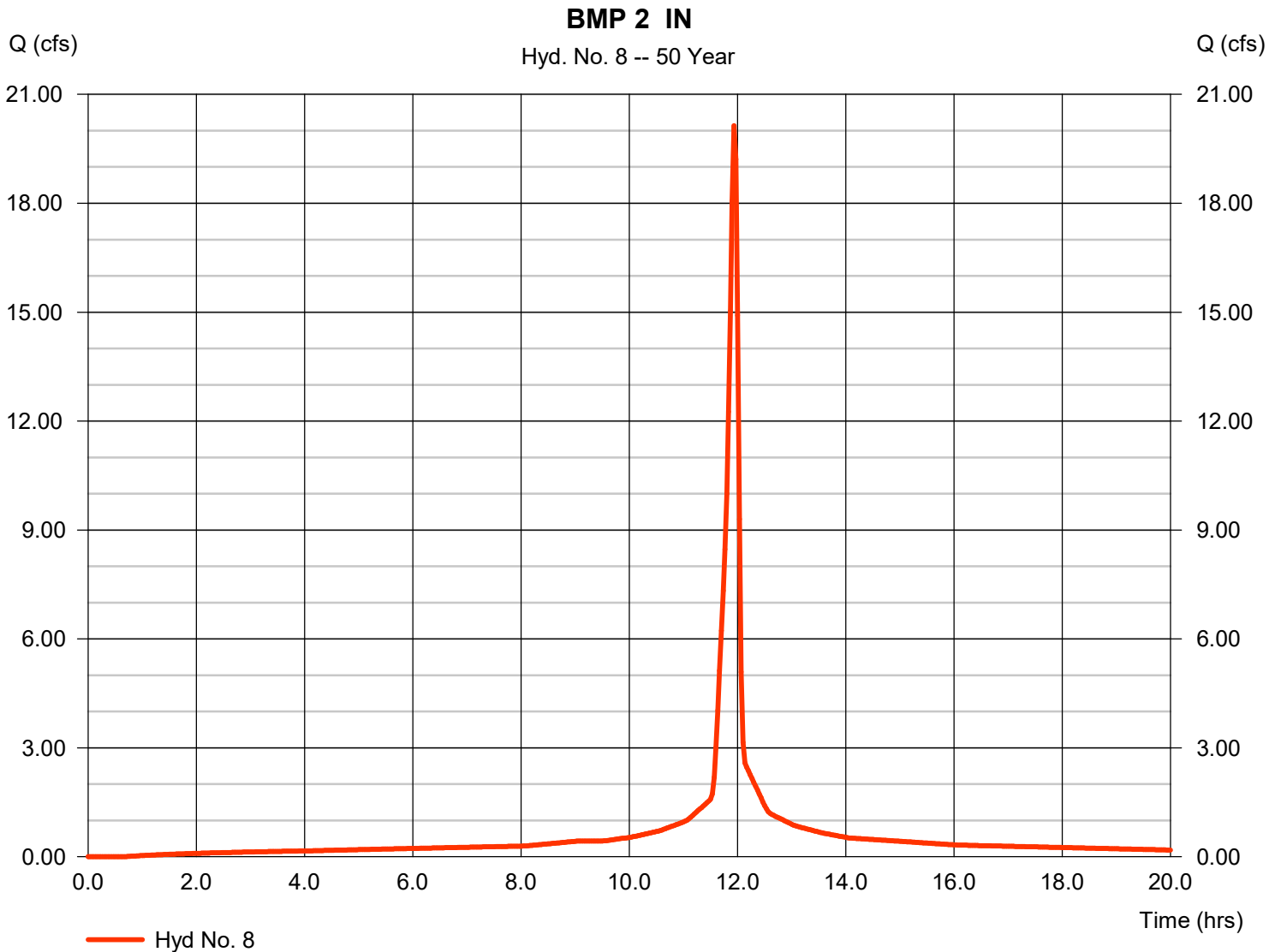


Hydrograph Report

Hyd. No. 8

BMP 2 IN

Hydrograph type	= SCS Runoff	Peak discharge	= 20.14 cfs
Storm frequency	= 50 yrs	Time to peak	= 11.93 hrs
Time interval	= 2 min	Hyd. volume	= 48,512 cuft
Drainage area	= 2.220 ac	Curve number	= 98
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 5.00 min
Total precip.	= 6.66 in	Distribution	= Type II
Storm duration	= 24 hrs	Shape factor	= 484



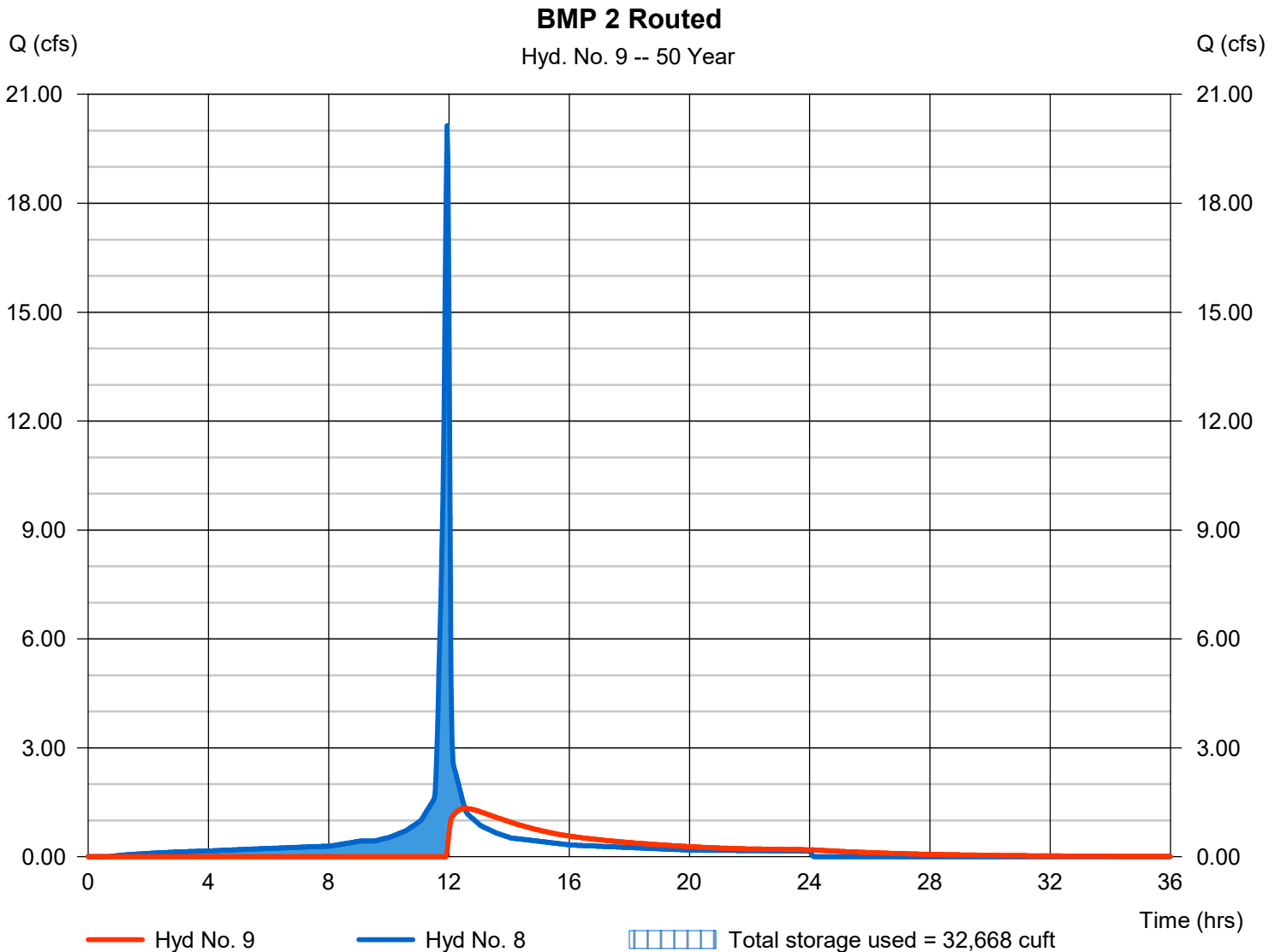
Hydrograph Report

Hyd. No. 9

BMP 2 Routed

Hydrograph type	= Reservoir	Peak discharge	= 1.333 cfs
Storm frequency	= 50 yrs	Time to peak	= 12.53 hrs
Time interval	= 2 min	Hyd. volume	= 25,463 cuft
Inflow hyd. No.	= 8 - BMP 2 IN	Max. Elevation	= 317.00 ft
Reservoir name	= BMP 2	Max. Storage	= 32,668 cuft

Storage Indication method used.

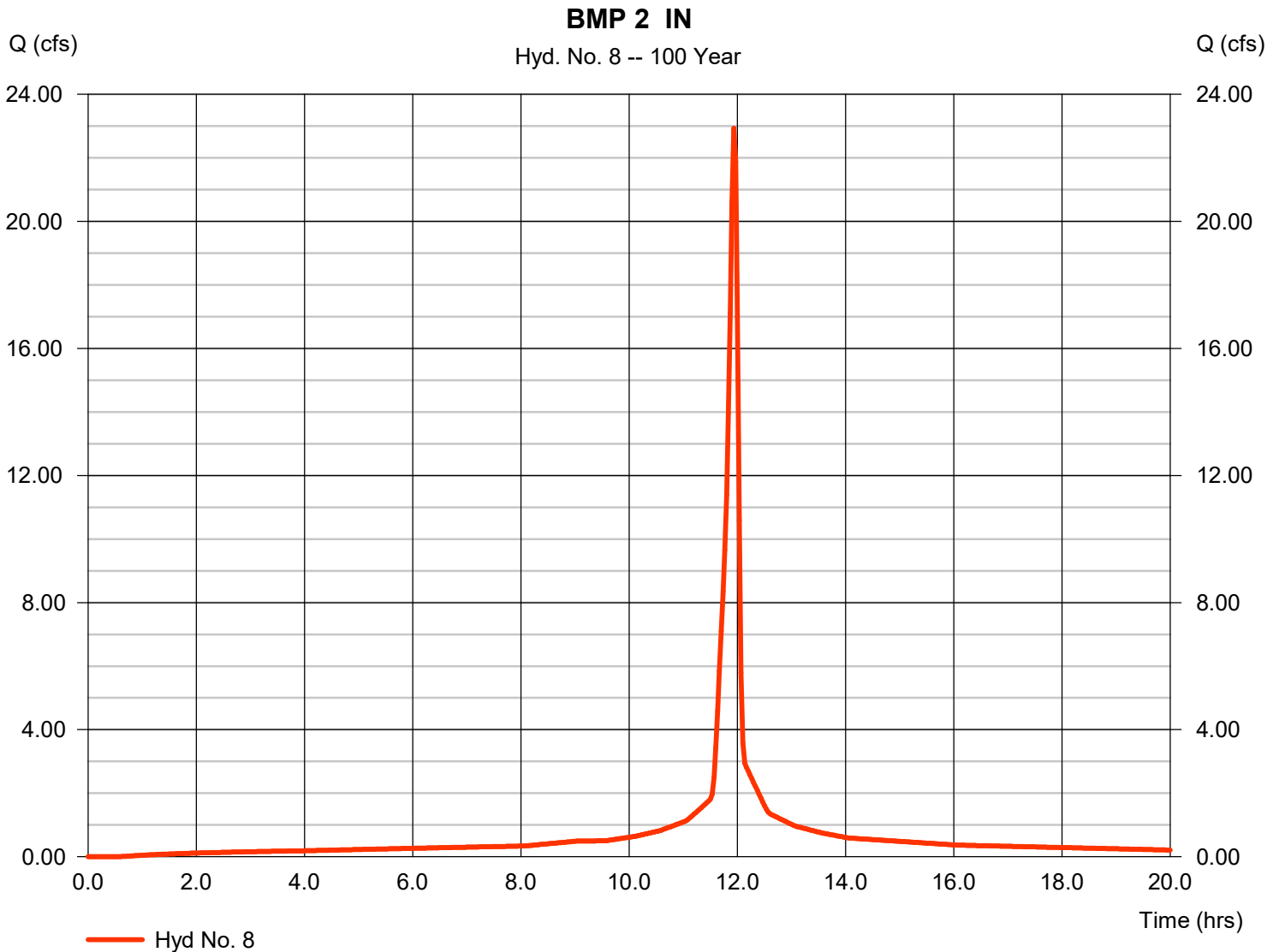


Hydrograph Report

Hyd. No. 8

BMP 2 IN

Hydrograph type	= SCS Runoff	Peak discharge	= 22.94 cfs
Storm frequency	= 100 yrs	Time to peak	= 11.93 hrs
Time interval	= 2 min	Hyd. volume	= 55,457 cuft
Drainage area	= 2.220 ac	Curve number	= 98
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 5.00 min
Total precip.	= 7.58 in	Distribution	= Type II
Storm duration	= 24 hrs	Shape factor	= 484



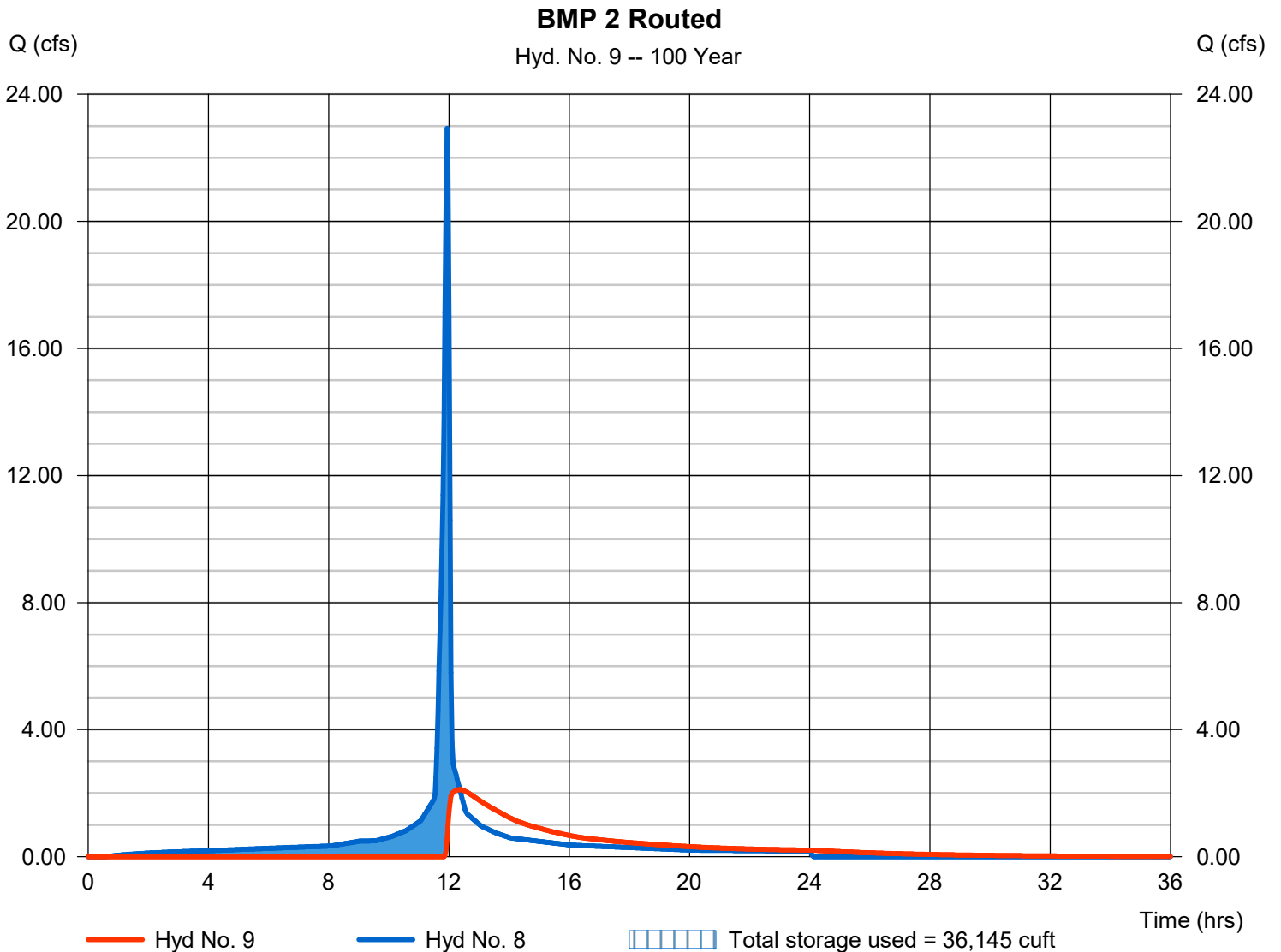
Hydrograph Report

Hyd. No. 9

BMP 2 Routed

Hydrograph type	= Reservoir	Peak discharge	= 2.110 cfs
Storm frequency	= 100 yrs	Time to peak	= 12.37 hrs
Time interval	= 2 min	Hyd. volume	= 32,409 cuft
Inflow hyd. No.	= 8 - BMP 2 IN	Max. Elevation	= 317.09 ft
Reservoir name	= BMP 2	Max. Storage	= 36,145 cuft

Storage Indication method used.

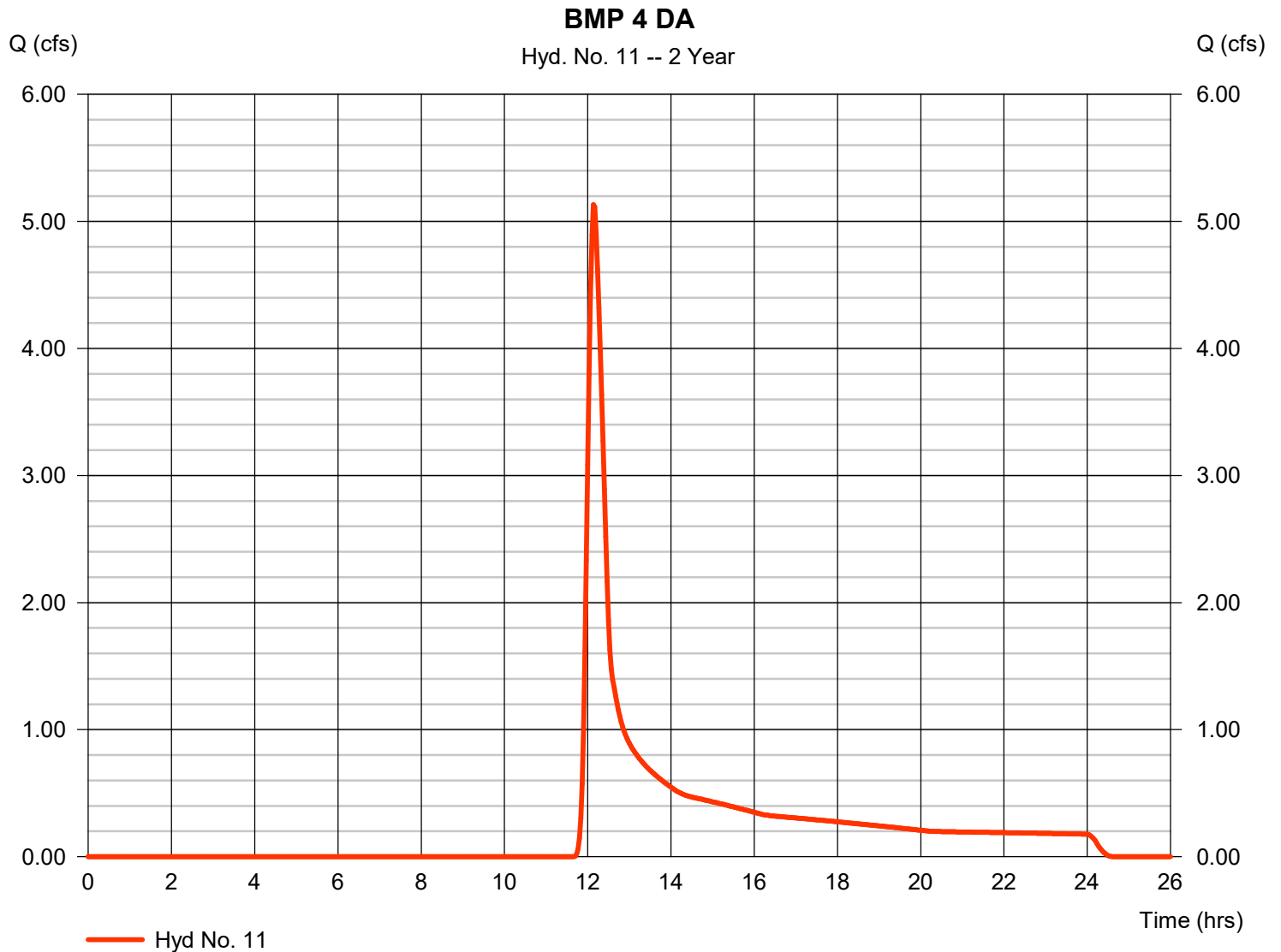


Hydrograph Report

Hyd. No. 11

BMP 4 DA

Hydrograph type	= SCS Runoff	Peak discharge	= 5.132 cfs
Storm frequency	= 2 yrs	Time to peak	= 12.13 hrs
Time interval	= 2 min	Hyd. volume	= 22,498 cuft
Drainage area	= 9.670 ac	Curve number	= 65
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 22.00 min
Total precip.	= 3.26 in	Distribution	= Type II
Storm duration	= 24 hrs	Shape factor	= 484



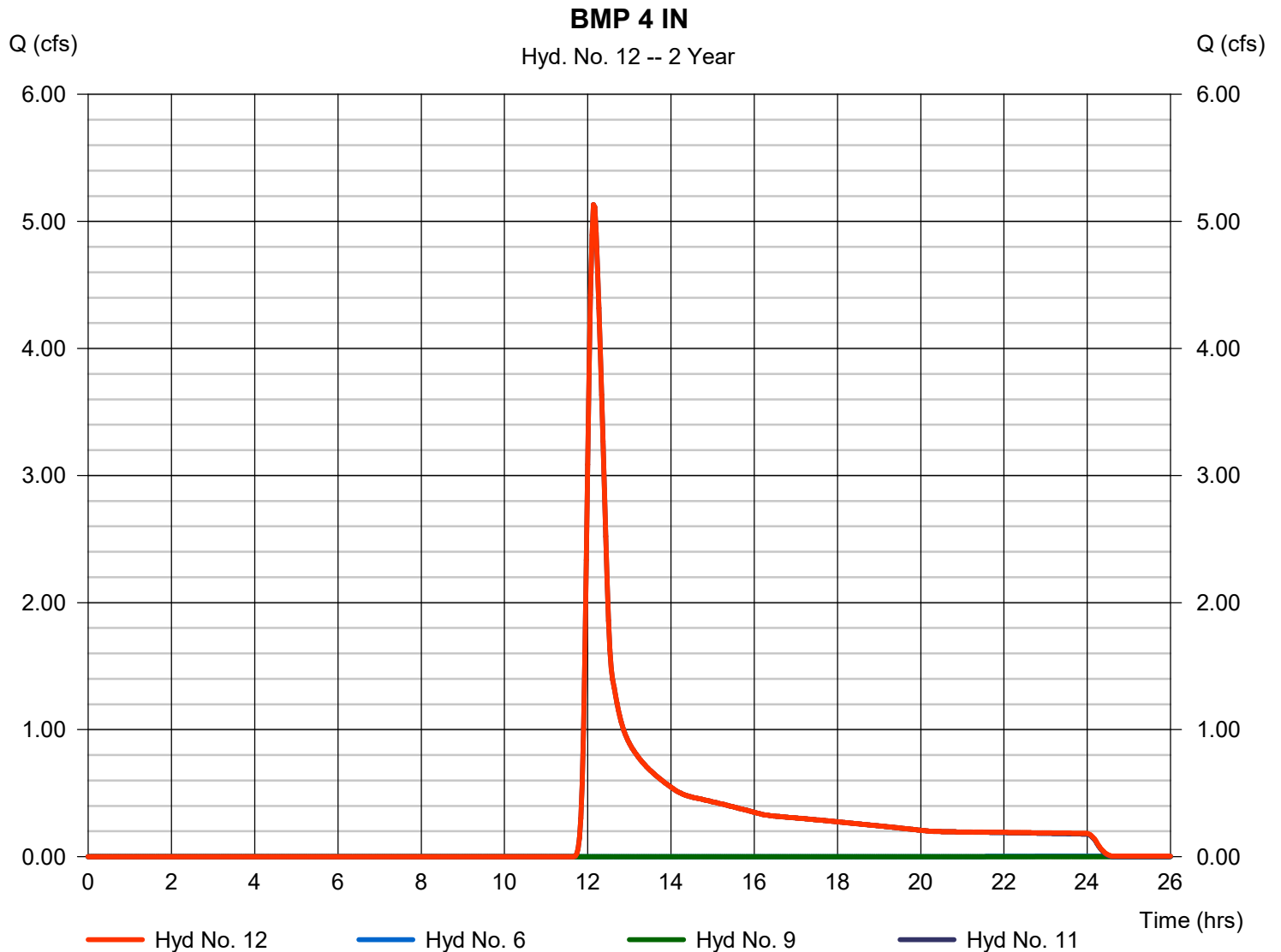
Hydrograph Report

Hyd. No. 12

BMP 4 IN

Hydrograph type = Combine
Storm frequency = 2 yrs
Time interval = 2 min
Inflow hyds. = 6, 9, 11

Peak discharge = 5.132 cfs
Time to peak = 12.13 hrs
Hyd. volume = 23,271 cuft
Contrib. drain. area = 9.670 ac



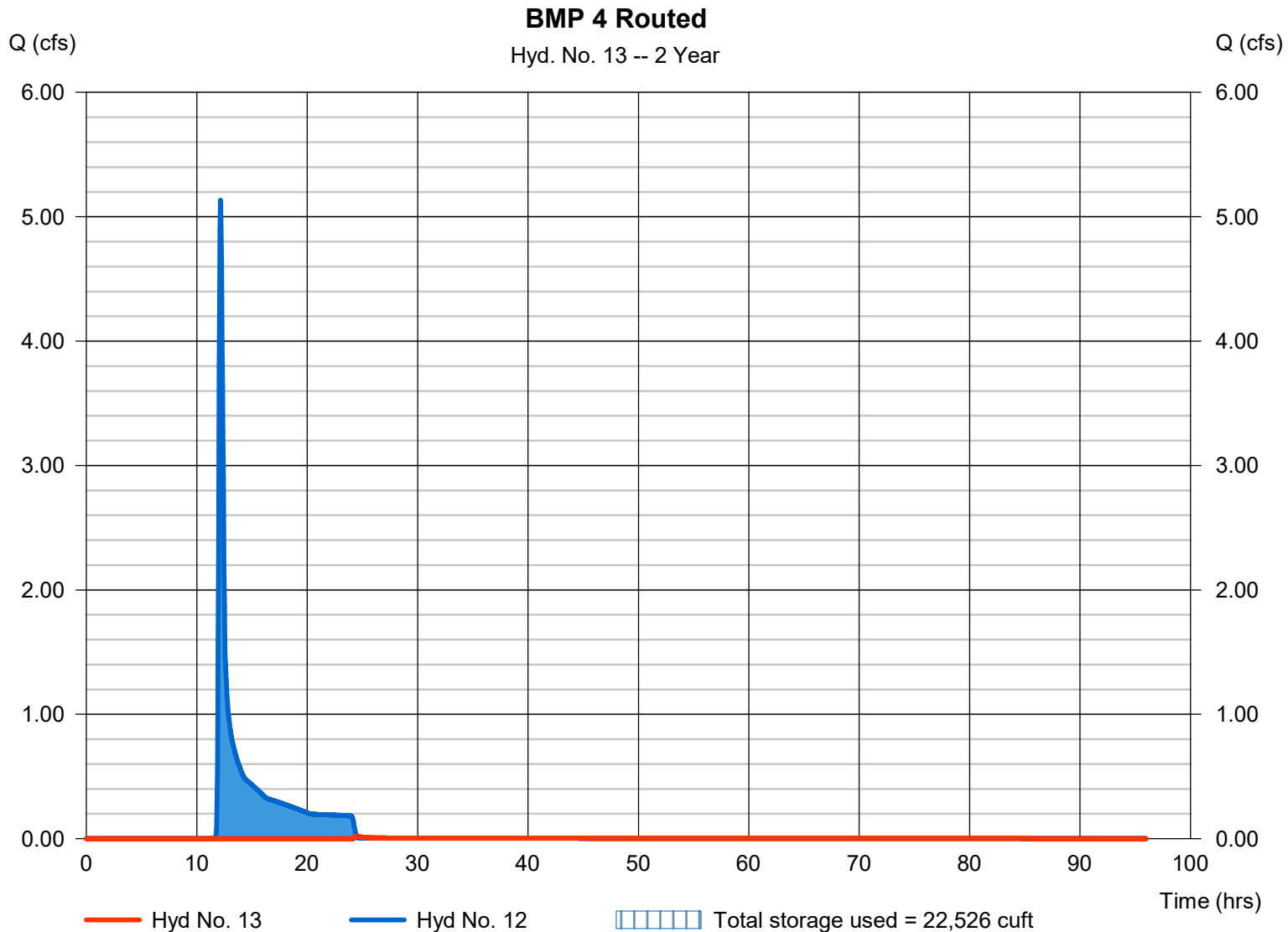
Hydrograph Report

Hyd. No. 13

BMP 4 Routed

Hydrograph type	= Reservoir	Peak discharge	= 0.019 cfs
Storm frequency	= 2 yrs	Time to peak	= 24.47 hrs
Time interval	= 2 min	Hyd. volume	= 790 cuft
Inflow hyd. No.	= 12 - BMP 4 IN	Max. Elevation	= 311.00 ft
Reservoir name	= BMP 4	Max. Storage	= 22,526 cuft

Storage Indication method used.



Pond Report

Pond No. 5 - BMP 4

Pond Data

Contours -User-defined contour areas. Conic method used for volume calculation. Begining Elevation = 310.00 ft

Stage / Storage Table

Stage (ft)	Elevation (ft)	Contour area (sqft)	Incr. Storage (cuft)	Total storage (cuft)
0.00	310.00	19,809	0	0
1.00	311.00	25,262	22,478	22,478
2.00	312.00	31,631	28,384	50,862
3.00	313.00	39,183	35,336	86,198
4.00	314.00	46,661	42,863	129,062
4.50	314.50	49,481	24,030	153,091
5.00	315.00	52,258	25,429	178,520

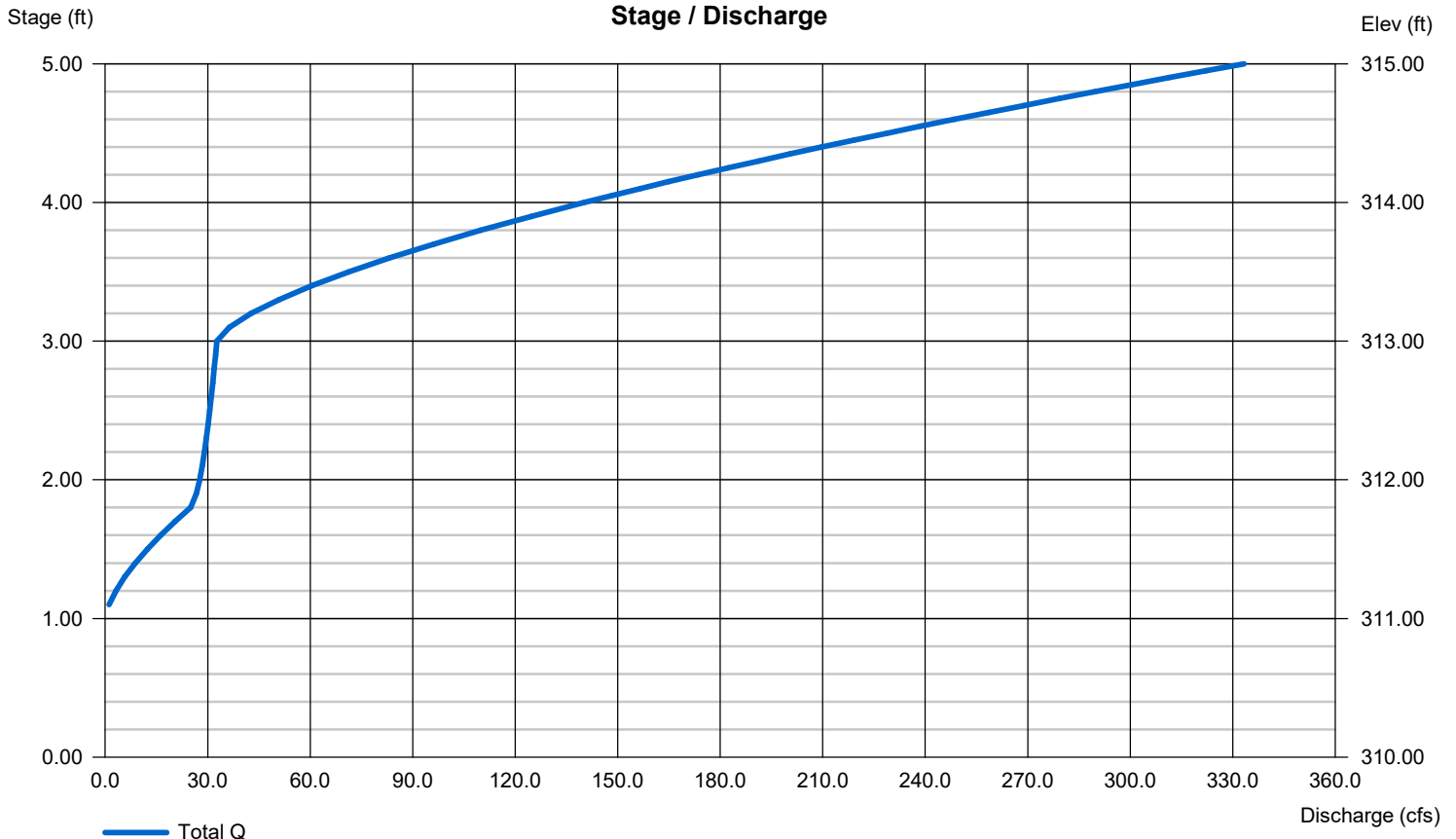
Culvert / Orifice Structures

	[A]	[B]	[C]	[PrfRsr]
Rise (in)	= 24.00	0.00	0.00	0.00
Span (in)	= 24.00	0.00	0.00	0.00
No. Barrels	= 1	0	0	0
Invert El. (ft)	= 307.25	0.00	0.00	0.00
Length (ft)	= 36.00	0.00	0.00	0.00
Slope (%)	= 0.69	0.00	0.00	n/a
N-Value	= .013	.013	.013	n/a
Orifice Coeff.	= 0.60	0.60	0.60	0.60
Multi-Stage	= n/a	No	No	No

Weir Structures

	[A]	[B]	[C]	[D]
Crest Len (ft)	= 10.50	Inactive	40.00	0.00
Crest El. (ft)	= 311.00	311.00	313.00	0.00
Weir Coeff.	= 3.33	3.33	2.60	3.33
Weir Type	= 1	Rect	Broad	---
Multi-Stage	= Yes	Yes	No	No
Exfil.(in/hr)	= 0.000 (by Contour)			
TW Elev. (ft)	= 0.00			

Note: Culvert/Orifice outflows are analyzed under inlet (ic) and outlet (oc) control. Weir risers checked for orifice conditions (ic) and submergence (s).

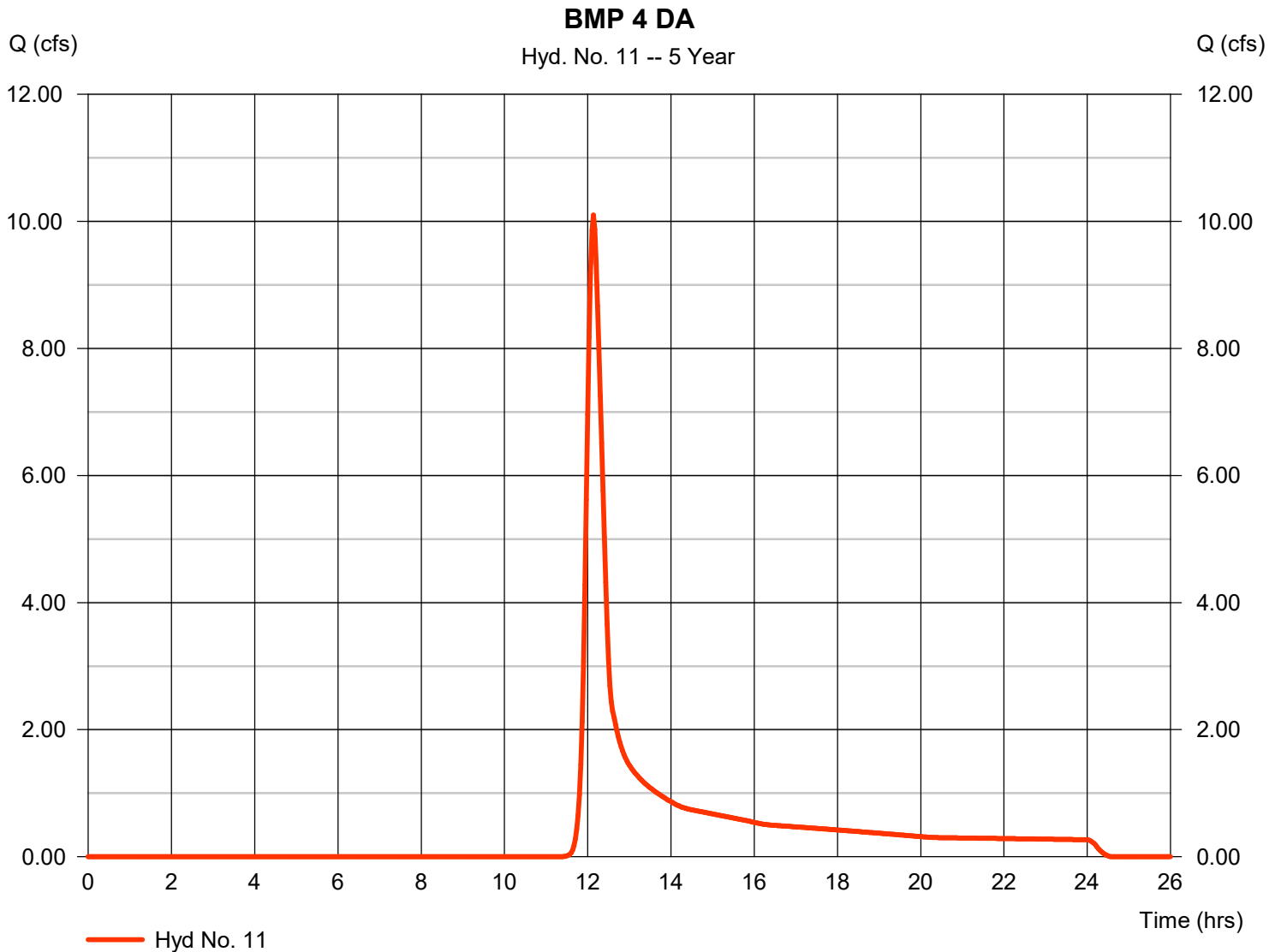


Hydrograph Report

Hyd. No. 11

BMP 4 DA

Hydrograph type	= SCS Runoff	Peak discharge	= 10.10 cfs
Storm frequency	= 5 yrs	Time to peak	= 12.13 hrs
Time interval	= 2 min	Hyd. volume	= 38,836 cuft
Drainage area	= 9.670 ac	Curve number	= 65
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 22.00 min
Total precip.	= 4.10 in	Distribution	= Type II
Storm duration	= 24 hrs	Shape factor	= 484



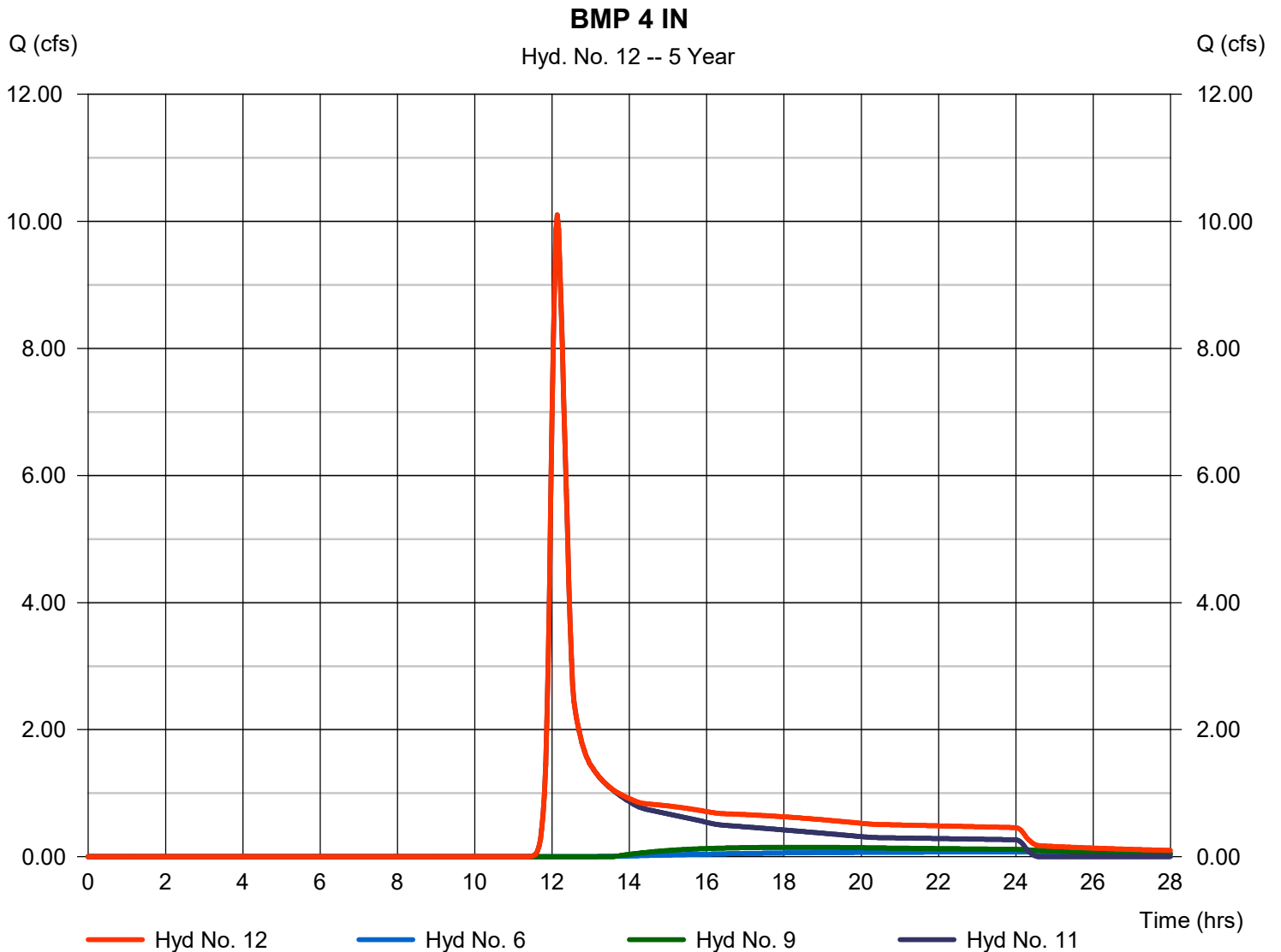
Hydrograph Report

Hyd. No. 12

BMP 4 IN

Hydrograph type = Combine
Storm frequency = 5 yrs
Time interval = 2 min
Inflow hyds. = 6, 9, 11

Peak discharge = 10.10 cfs
Time to peak = 12.13 hrs
Hyd. volume = 51,642 cuft
Contrib. drain. area = 9.670 ac



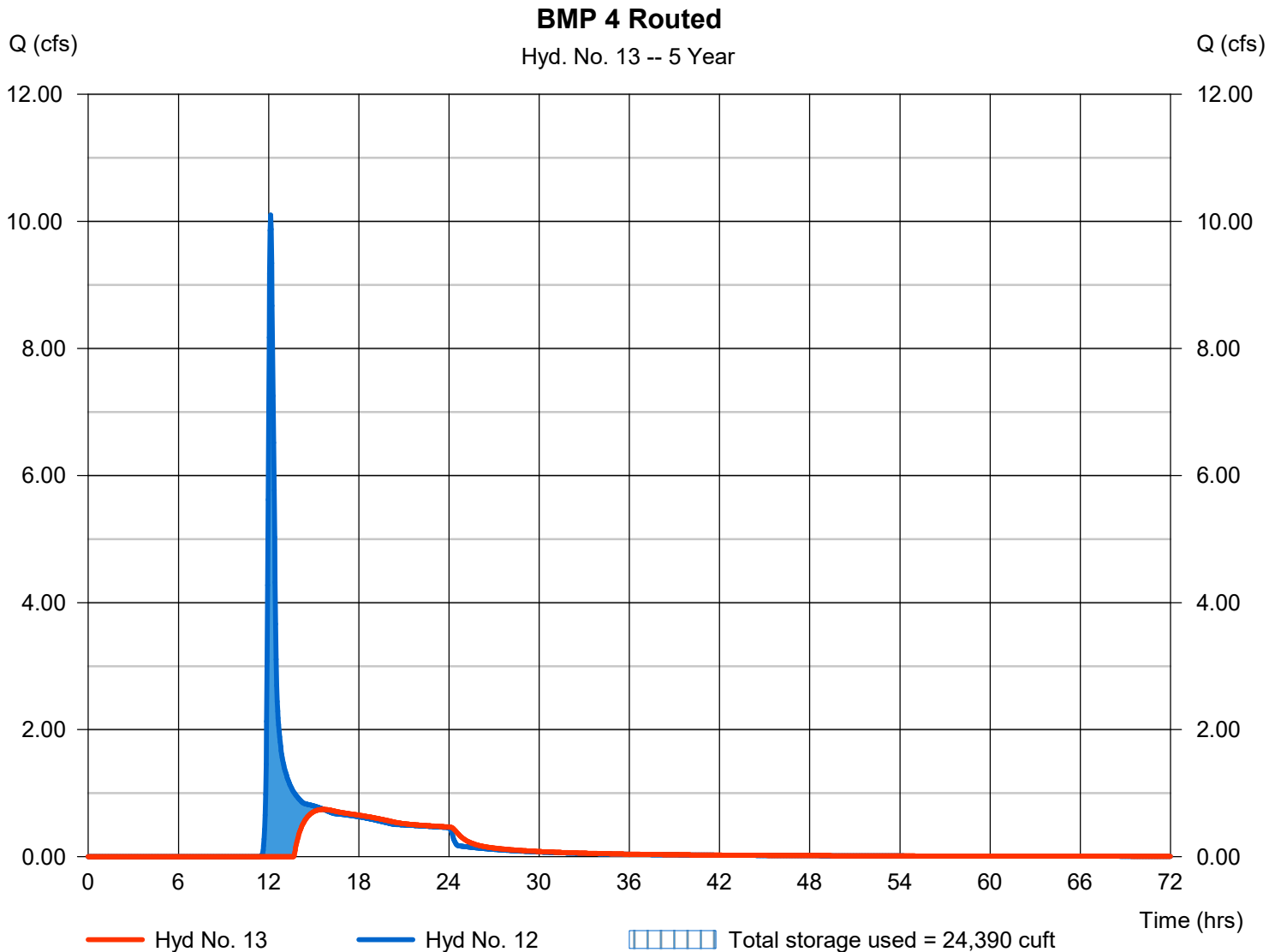
Hydrograph Report

Hyd. No. 13

BMP 4 Routed

Hydrograph type	= Reservoir	Peak discharge	= 0.745 cfs
Storm frequency	= 5 yrs	Time to peak	= 15.67 hrs
Time interval	= 2 min	Hyd. volume	= 29,154 cuft
Inflow hyd. No.	= 12 - BMP 4 IN	Max. Elevation	= 311.07 ft
Reservoir name	= BMP 4	Max. Storage	= 24,390 cuft

Storage Indication method used.

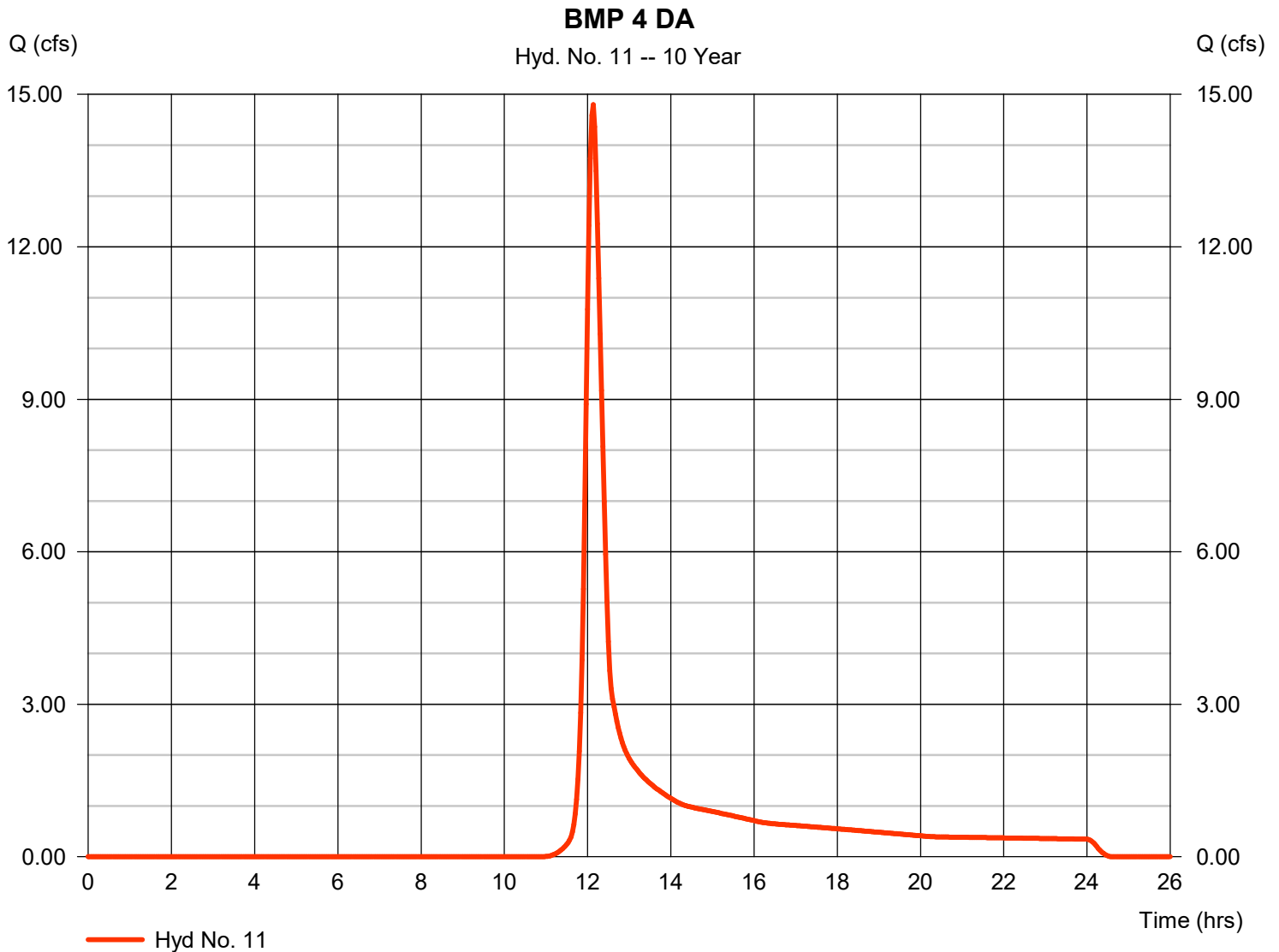


Hydrograph Report

Hyd. No. 11

BMP 4 DA

Hydrograph type	= SCS Runoff	Peak discharge	= 14.80 cfs
Storm frequency	= 10 yrs	Time to peak	= 12.13 hrs
Time interval	= 2 min	Hyd. volume	= 54,377 cuft
Drainage area	= 9.670 ac	Curve number	= 65
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 22.00 min
Total precip.	= 4.80 in	Distribution	= Type II
Storm duration	= 24 hrs	Shape factor	= 484



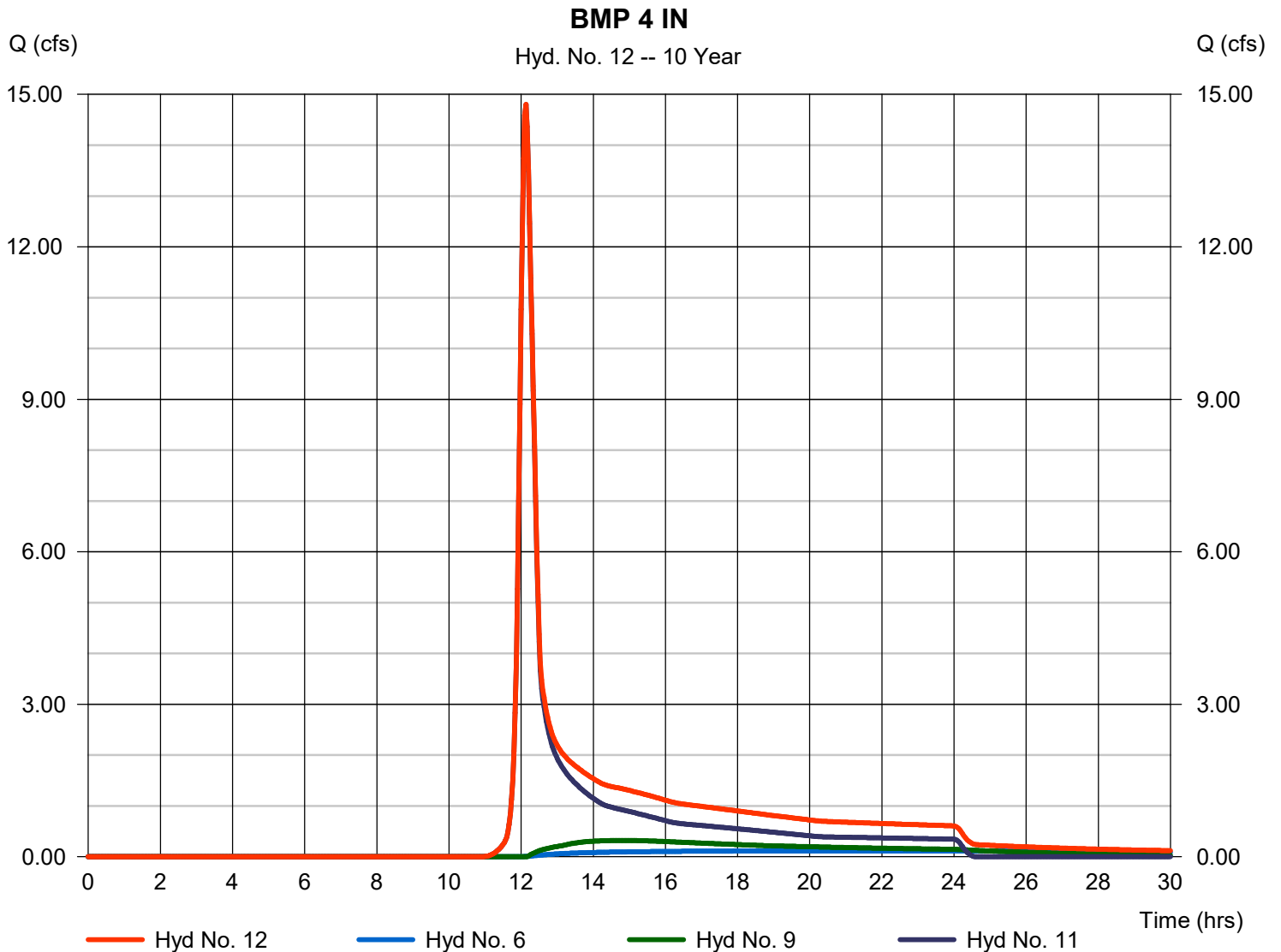
Hydrograph Report

Hyd. No. 12

BMP 4 IN

Hydrograph type = Combine
Storm frequency = 10 yrs
Time interval = 2 min
Inflow hyds. = 6, 9, 11

Peak discharge = 14.80 cfs
Time to peak = 12.13 hrs
Hyd. volume = 77,602 cuft
Contrib. drain. area = 9.670 ac



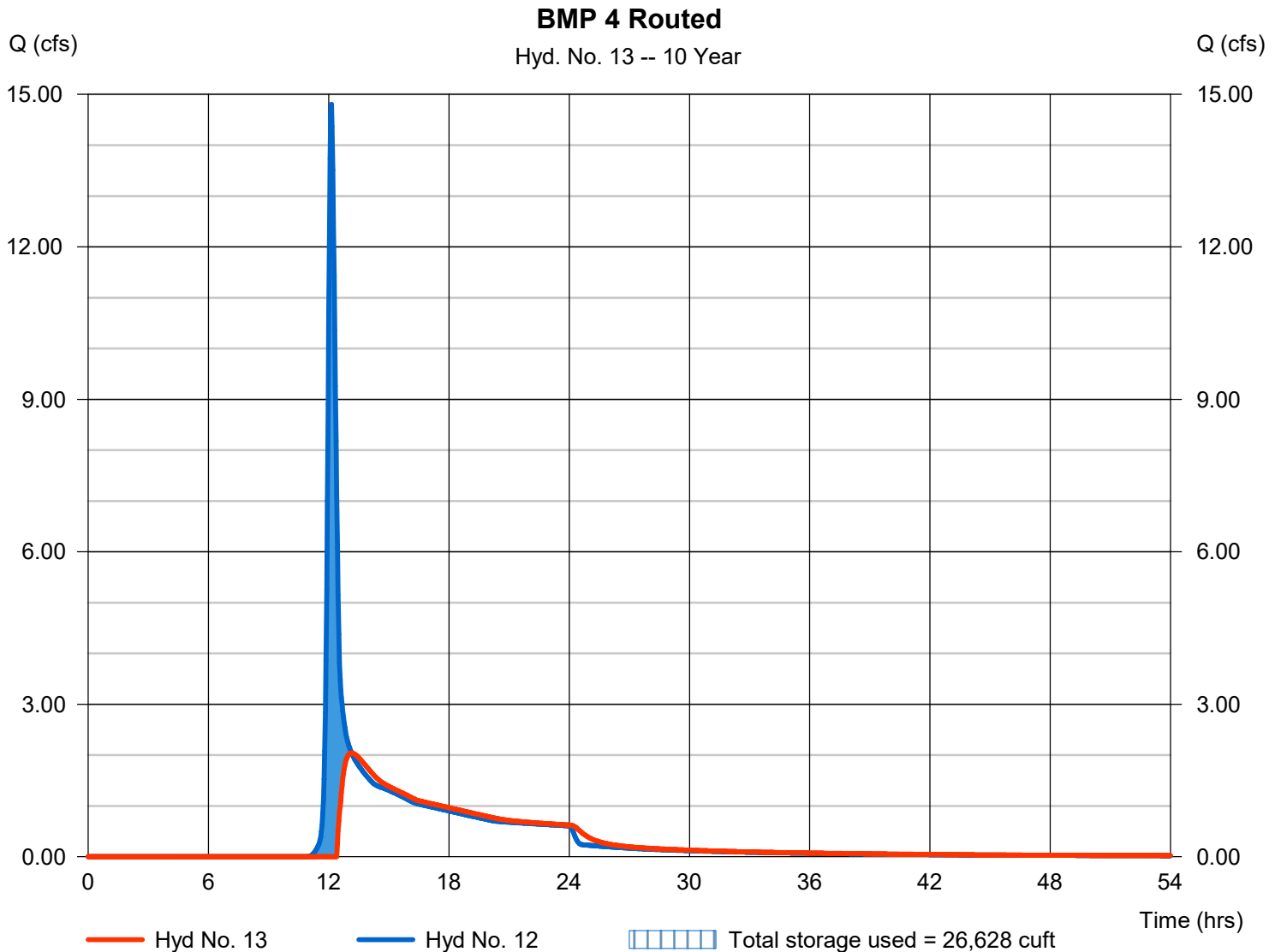
Hydrograph Report

Hyd. No. 13

BMP 4 Routed

Hydrograph type	= Reservoir	Peak discharge	= 2.040 cfs
Storm frequency	= 10 yrs	Time to peak	= 13.13 hrs
Time interval	= 2 min	Hyd. volume	= 55,111 cuft
Inflow hyd. No.	= 12 - BMP 4 IN	Max. Elevation	= 311.15 ft
Reservoir name	= BMP 4	Max. Storage	= 26,628 cuft

Storage Indication method used.

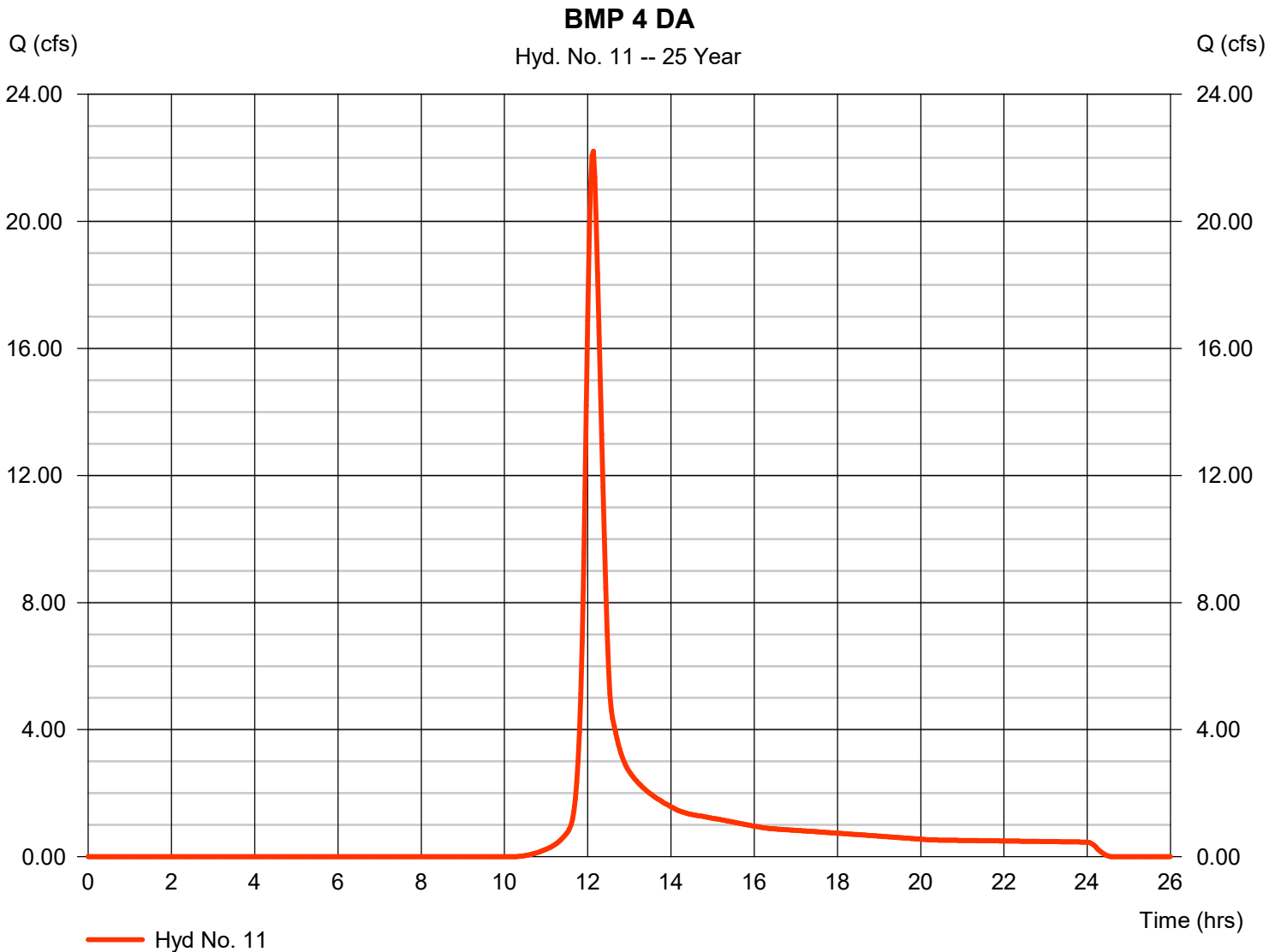


Hydrograph Report

Hyd. No. 11

BMP 4 DA

Hydrograph type	= SCS Runoff	Peak discharge	= 22.21 cfs
Storm frequency	= 25 yrs	Time to peak	= 12.13 hrs
Time interval	= 2 min	Hyd. volume	= 79,109 cuft
Drainage area	= 9.670 ac	Curve number	= 65
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 22.00 min
Total precip.	= 5.81 in	Distribution	= Type II
Storm duration	= 24 hrs	Shape factor	= 484



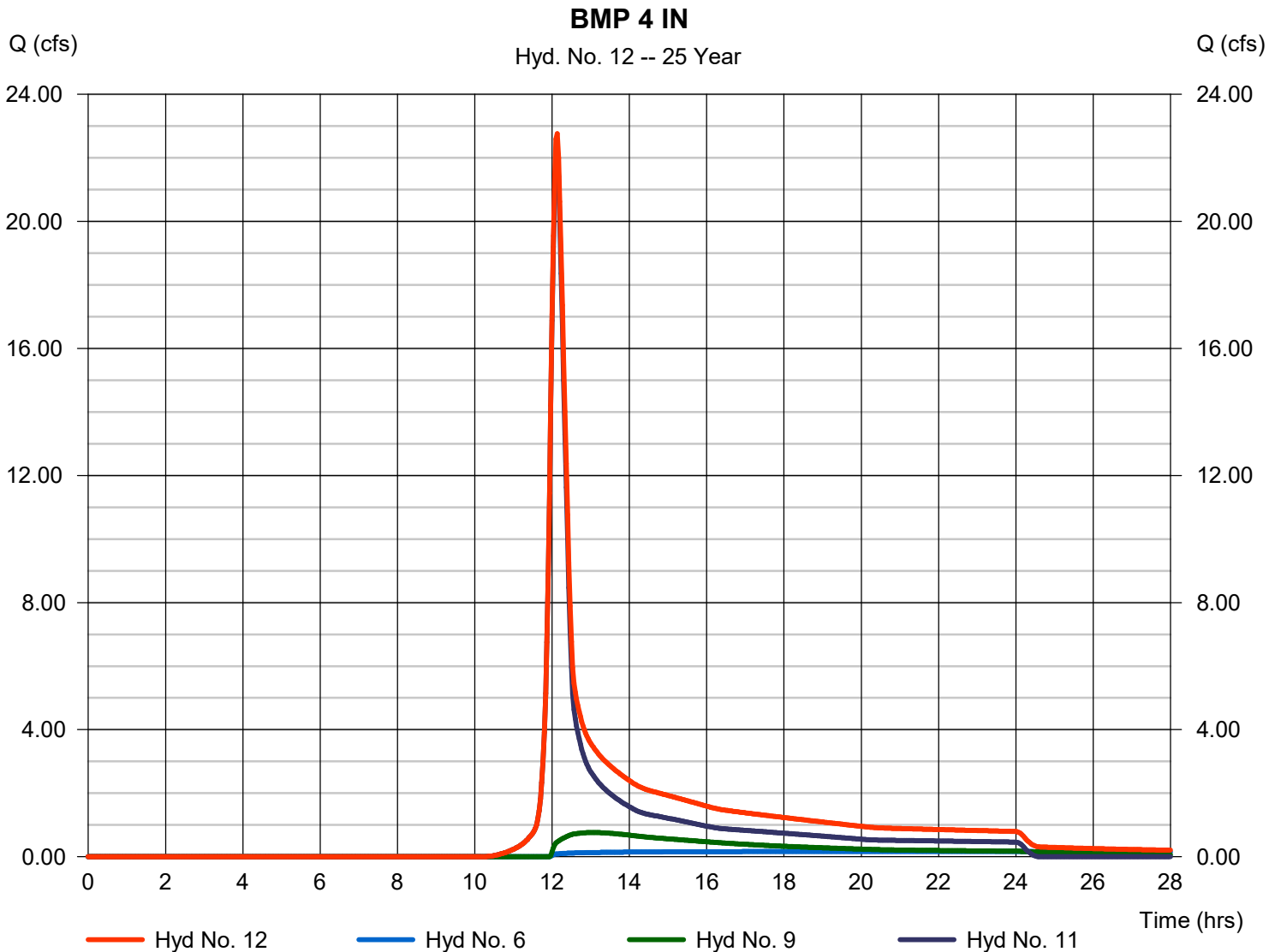
Hydrograph Report

Hyd. No. 12

BMP 4 IN

Hydrograph type = Combine
Storm frequency = 25 yrs
Time interval = 2 min
Inflow hyds. = 6, 9, 11

Peak discharge = 22.76 cfs
Time to peak = 12.13 hrs
Hyd. volume = 117,372 cuft
Contrib. drain. area = 9.670 ac



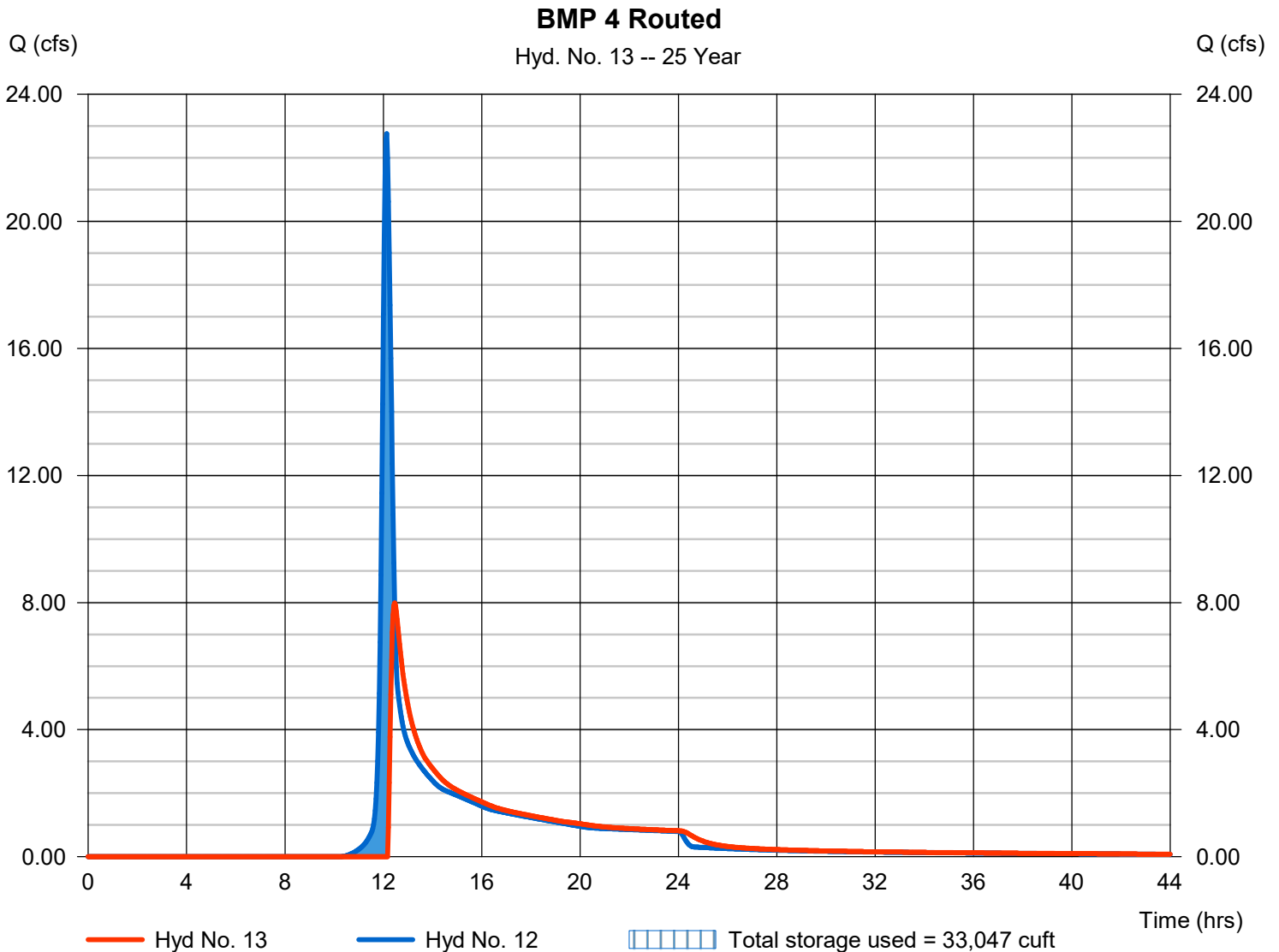
Hydrograph Report

Hyd. No. 13

BMP 4 Routed

Hydrograph type	= Reservoir	Peak discharge	= 7.989 cfs
Storm frequency	= 25 yrs	Time to peak	= 12.47 hrs
Time interval	= 2 min	Hyd. volume	= 94,878 cuft
Inflow hyd. No.	= 12 - BMP 4 IN	Max. Elevation	= 311.37 ft
Reservoir name	= BMP 4	Max. Storage	= 33,047 cuft

Storage Indication method used.

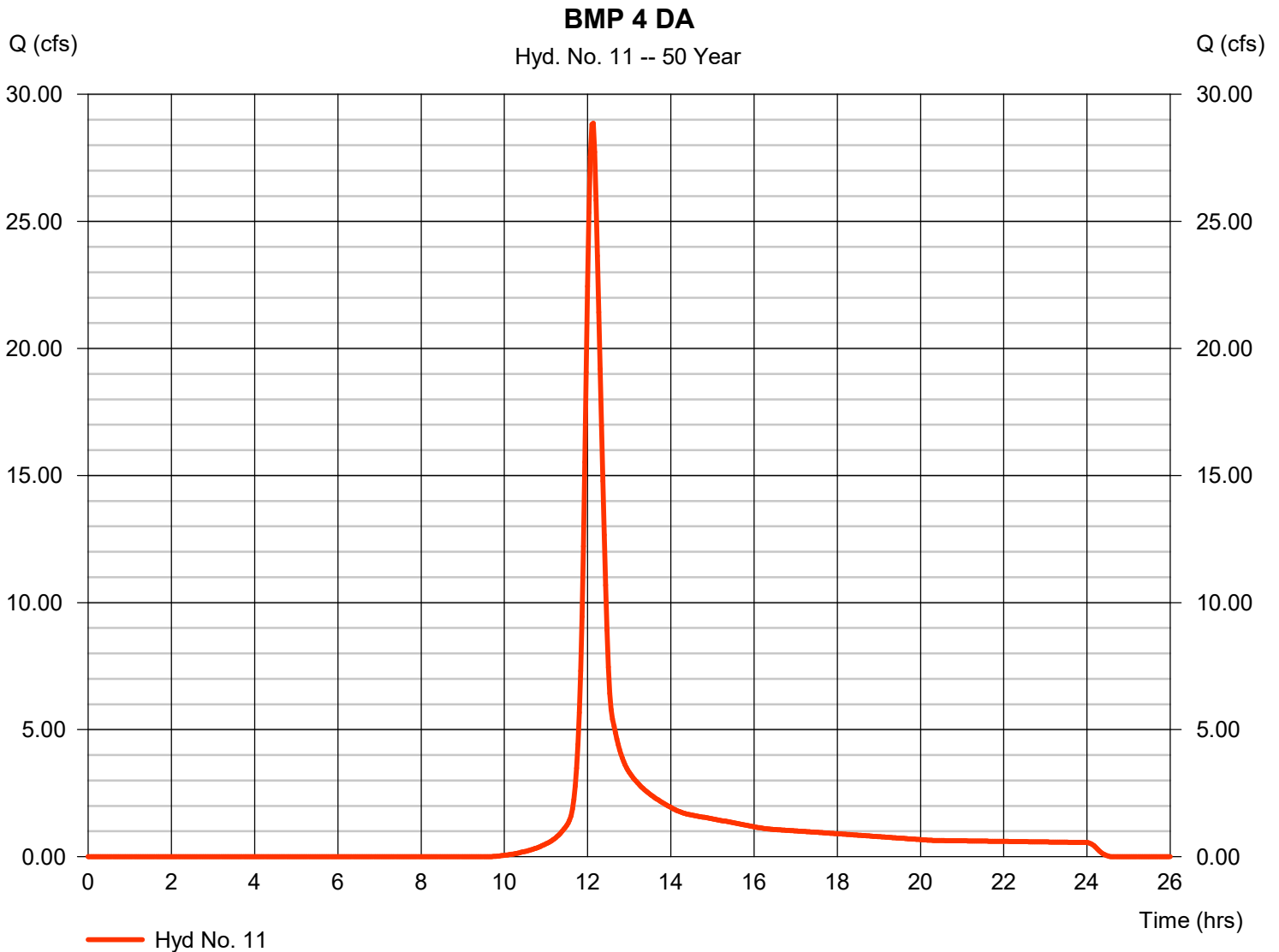


Hydrograph Report

Hyd. No. 11

BMP 4 DA

Hydrograph type	= SCS Runoff	Peak discharge	= 28.86 cfs
Storm frequency	= 50 yrs	Time to peak	= 12.13 hrs
Time interval	= 2 min	Hyd. volume	= 101,543 cuft
Drainage area	= 9.670 ac	Curve number	= 65
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 22.00 min
Total precip.	= 6.66 in	Distribution	= Type II
Storm duration	= 24 hrs	Shape factor	= 484



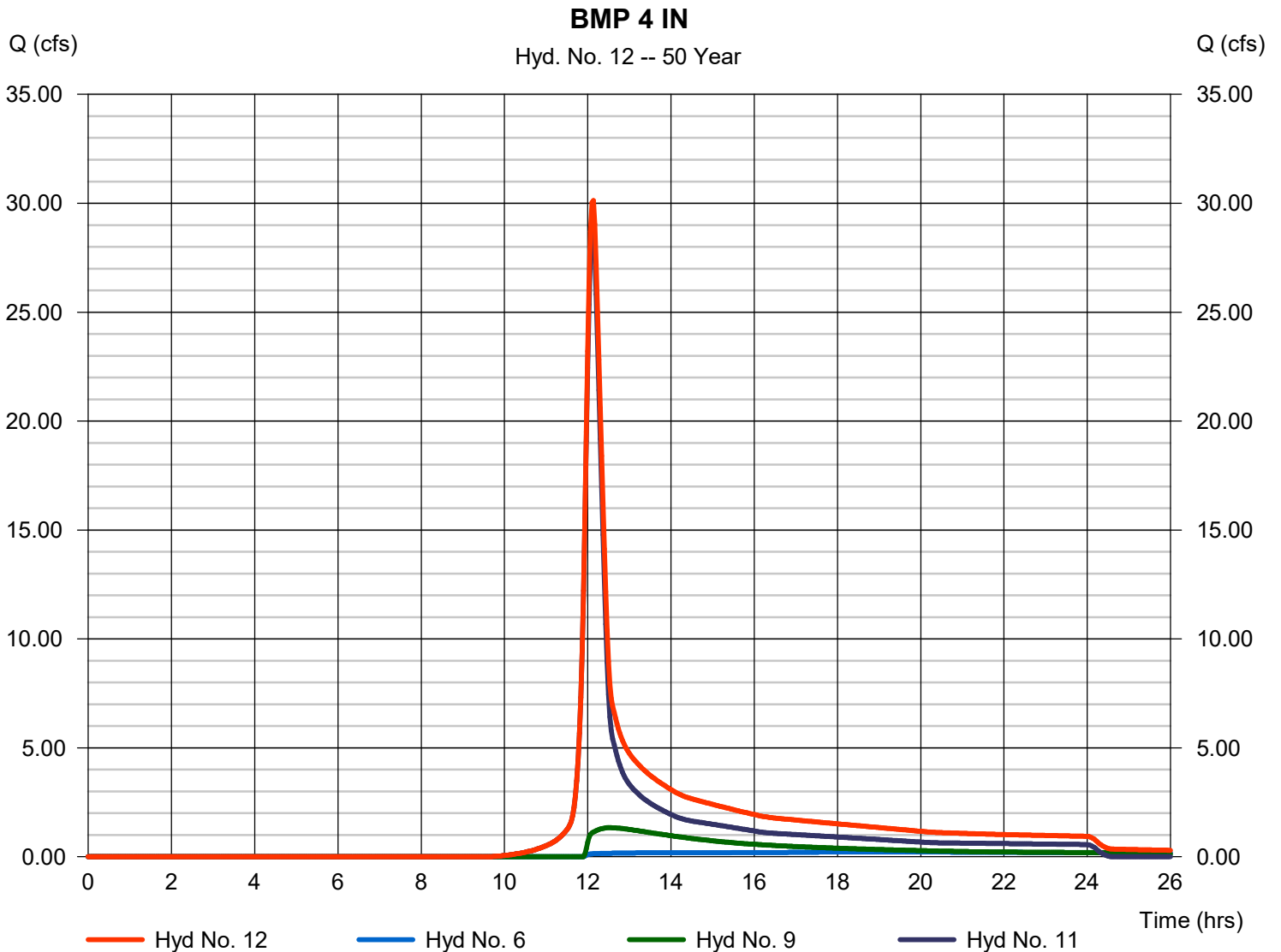
Hydrograph Report

Hyd. No. 12

BMP 4 IN

Hydrograph type = Combine
Storm frequency = 50 yrs
Time interval = 2 min
Inflow hyds. = 6, 9, 11

Peak discharge = 30.13 cfs
Time to peak = 12.13 hrs
Hyd. volume = 152,462 cuft
Contrib. drain. area = 9.670 ac



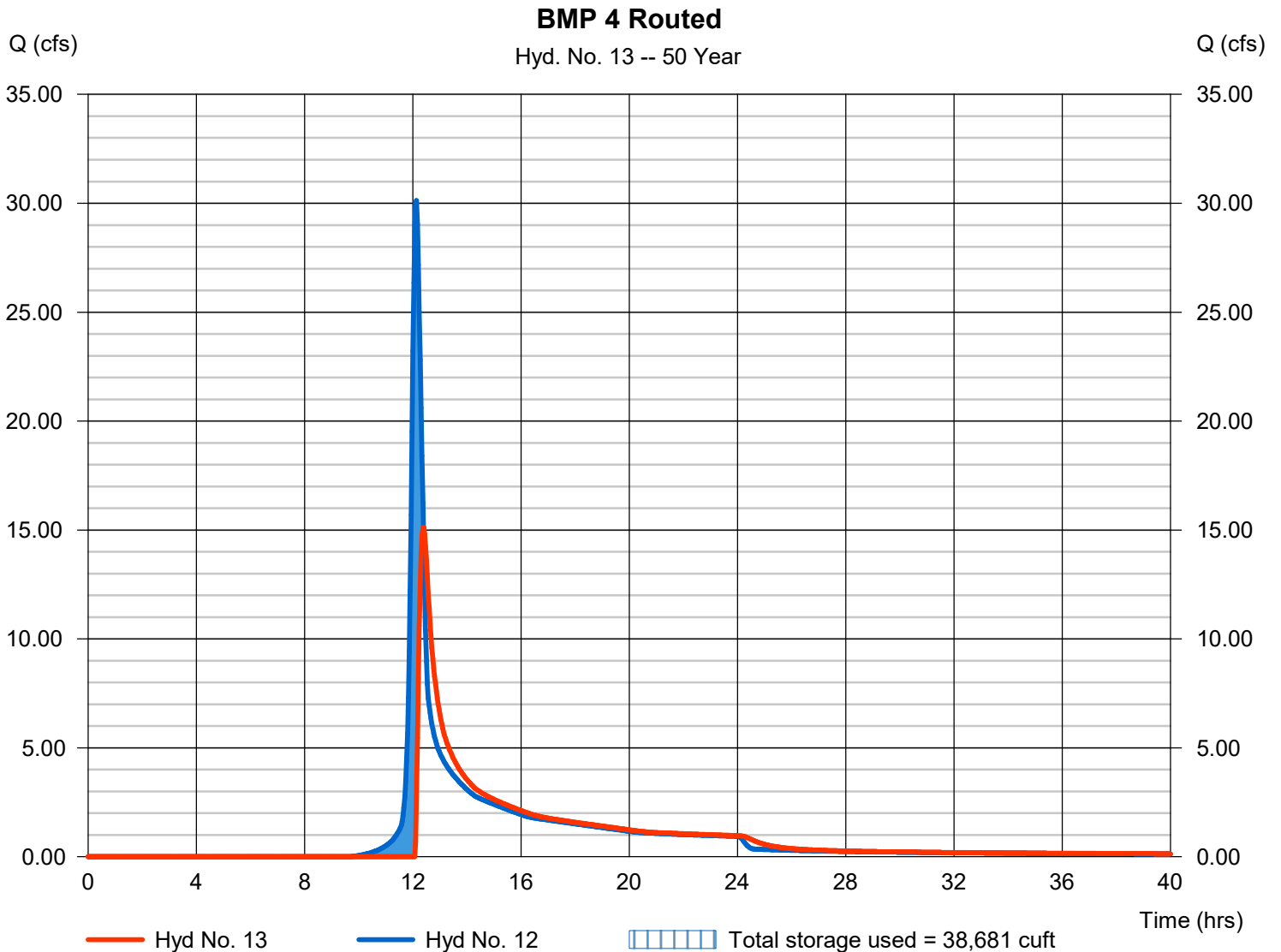
Hydrograph Report

Hyd. No. 13

BMP 4 Routed

Hydrograph type	= Reservoir	Peak discharge	= 15.12 cfs
Storm frequency	= 50 yrs	Time to peak	= 12.40 hrs
Time interval	= 2 min	Hyd. volume	= 129,965 cuft
Inflow hyd. No.	= 12 - BMP 4 IN	Max. Elevation	= 311.57 ft
Reservoir name	= BMP 4	Max. Storage	= 38,681 cuft

Storage Indication method used.

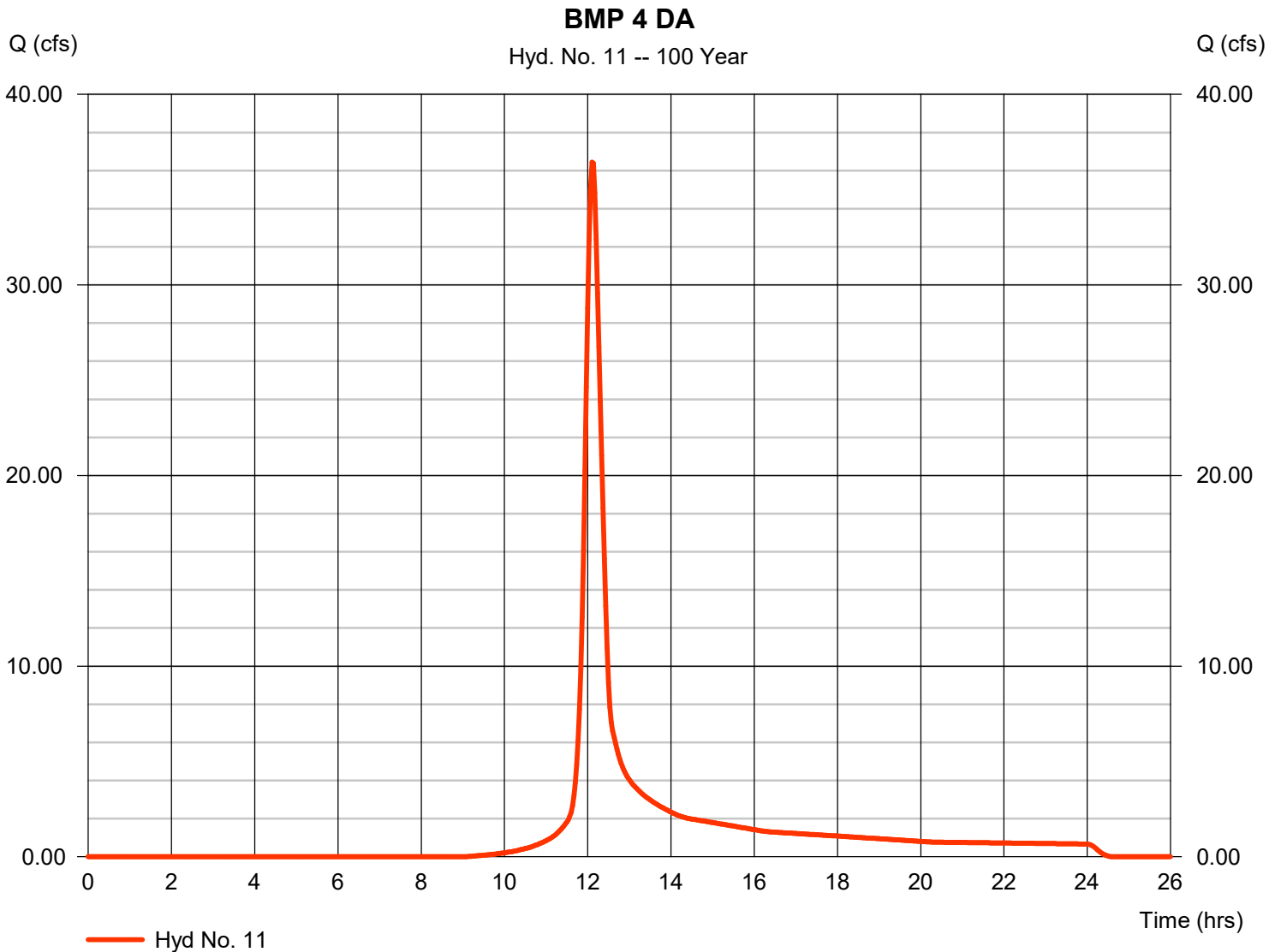


Hydrograph Report

Hyd. No. 11

BMP 4 DA

Hydrograph type	= SCS Runoff	Peak discharge	= 36.45 cfs
Storm frequency	= 100 yrs	Time to peak	= 12.10 hrs
Time interval	= 2 min	Hyd. volume	= 127,104 cuft
Drainage area	= 9.670 ac	Curve number	= 65
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 22.00 min
Total precip.	= 7.58 in	Distribution	= Type II
Storm duration	= 24 hrs	Shape factor	= 484



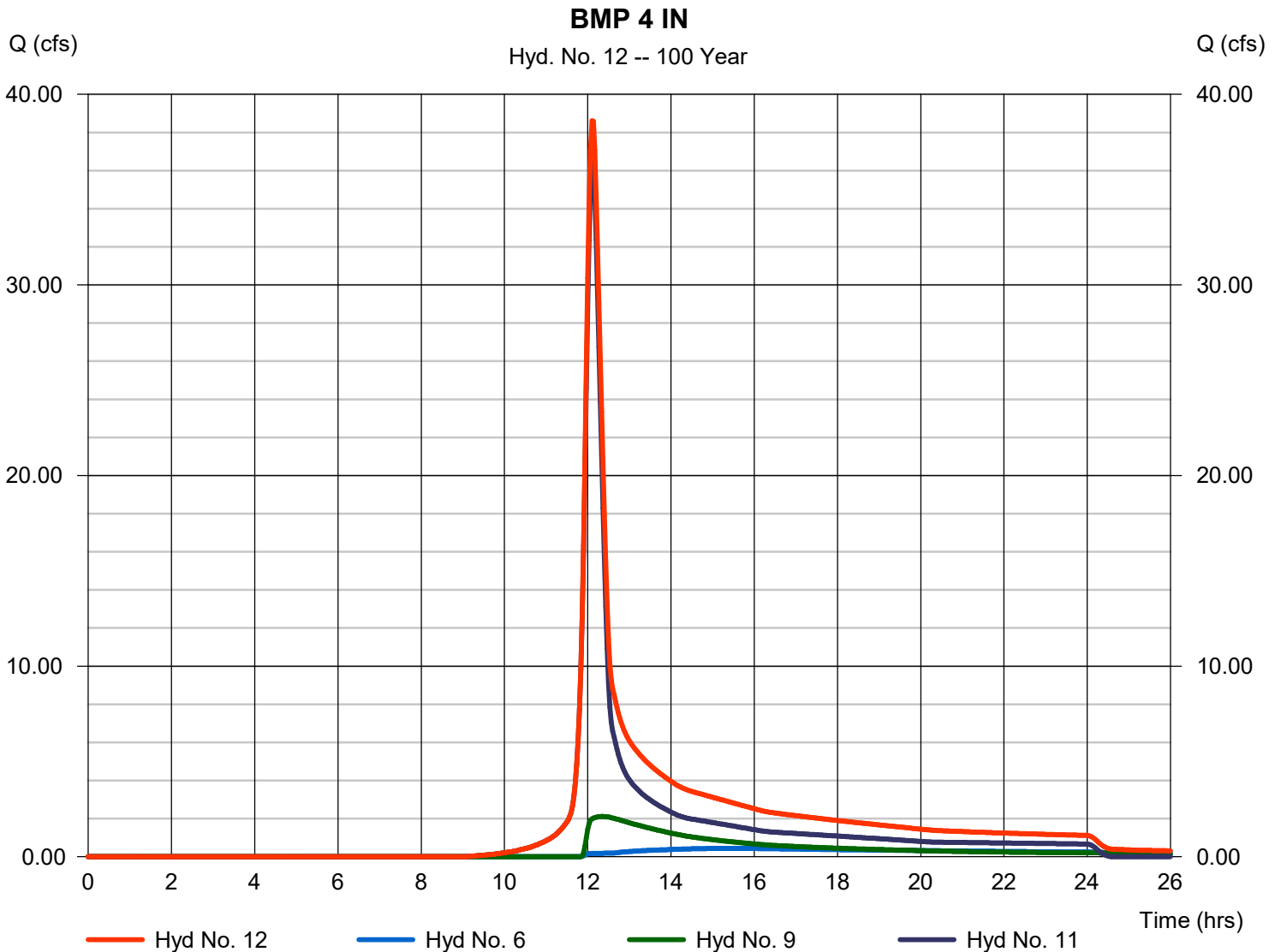
Hydrograph Report

Hyd. No. 12

BMP 4 IN

Hydrograph type = Combine
Storm frequency = 100 yrs
Time interval = 2 min
Inflow hyds. = 6, 9, 11

Peak discharge = 38.61 cfs
Time to peak = 12.10 hrs
Hyd. volume = 191,882 cuft
Contrib. drain. area = 9.670 ac



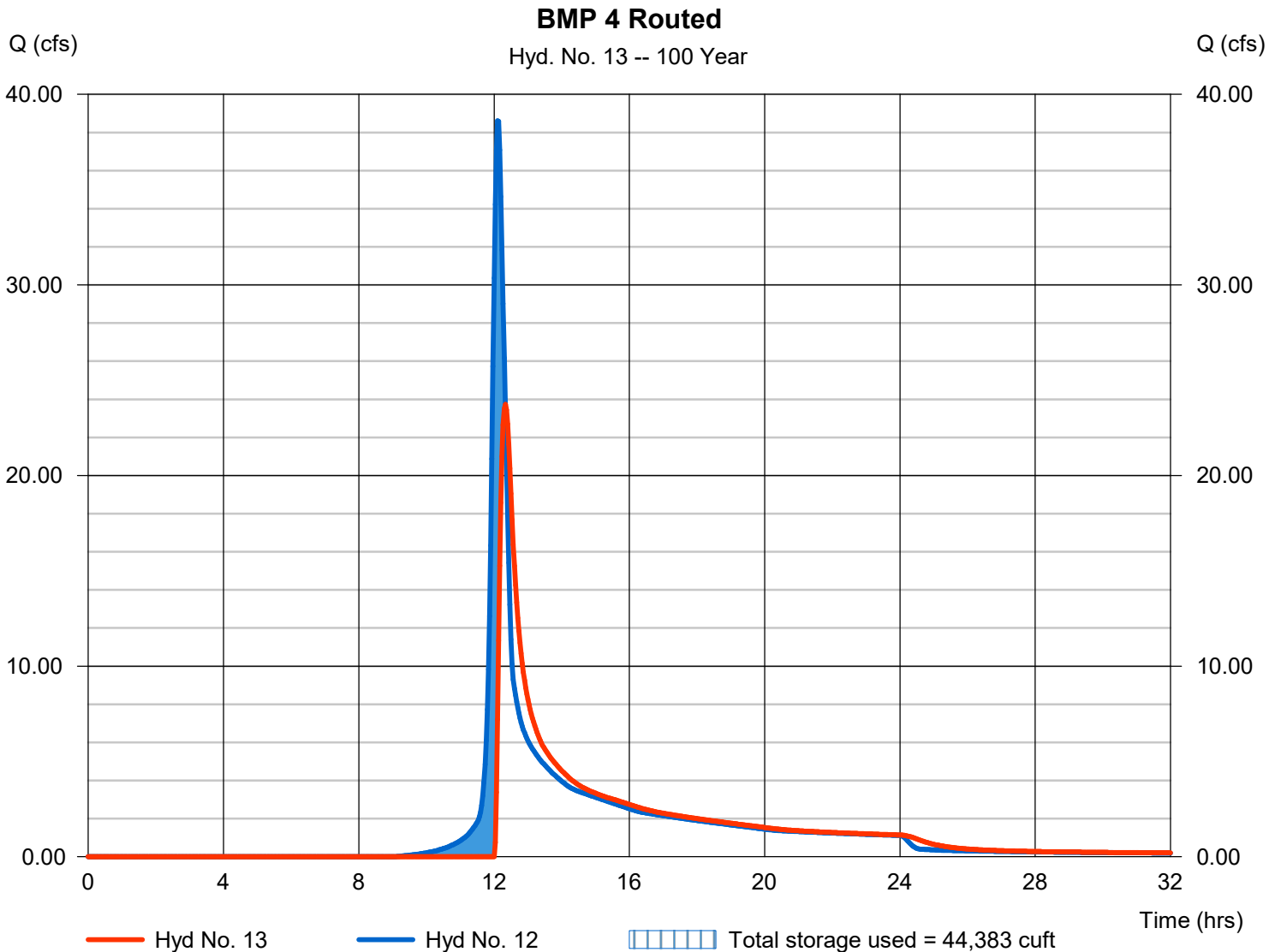
Hydrograph Report

Hyd. No. 13

BMP 4 Routed

Hydrograph type	= Reservoir	Peak discharge	= 23.74 cfs
Storm frequency	= 100 yrs	Time to peak	= 12.33 hrs
Time interval	= 2 min	Hyd. volume	= 169,384 cuft
Inflow hyd. No.	= 12 - BMP 4 IN	Max. Elevation	= 311.77 ft
Reservoir name	= BMP 4	Max. Storage	= 44,383 cuft

Storage Indication method used.

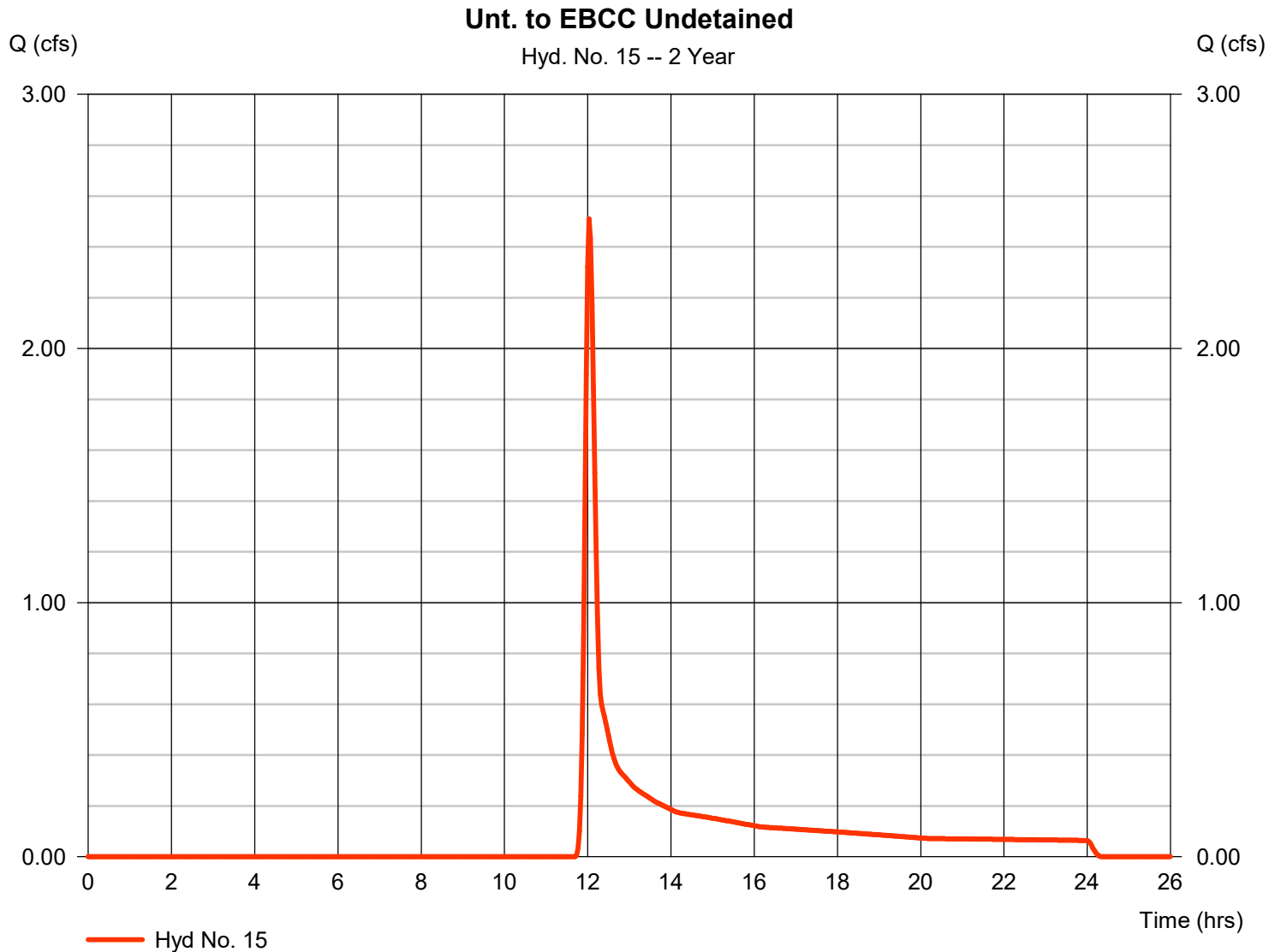


Hydrograph Report

Hyd. No. 15

Unt. to EBCC Undetained

Hydrograph type	= SCS Runoff	Peak discharge	= 2.510 cfs
Storm frequency	= 2 yrs	Time to peak	= 12.03 hrs
Time interval	= 2 min	Hyd. volume	= 7,892 cuft
Drainage area	= 3.590 ac	Curve number	= 64
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 12.00 min
Total precip.	= 3.26 in	Distribution	= Type II
Storm duration	= 24 hrs	Shape factor	= 484

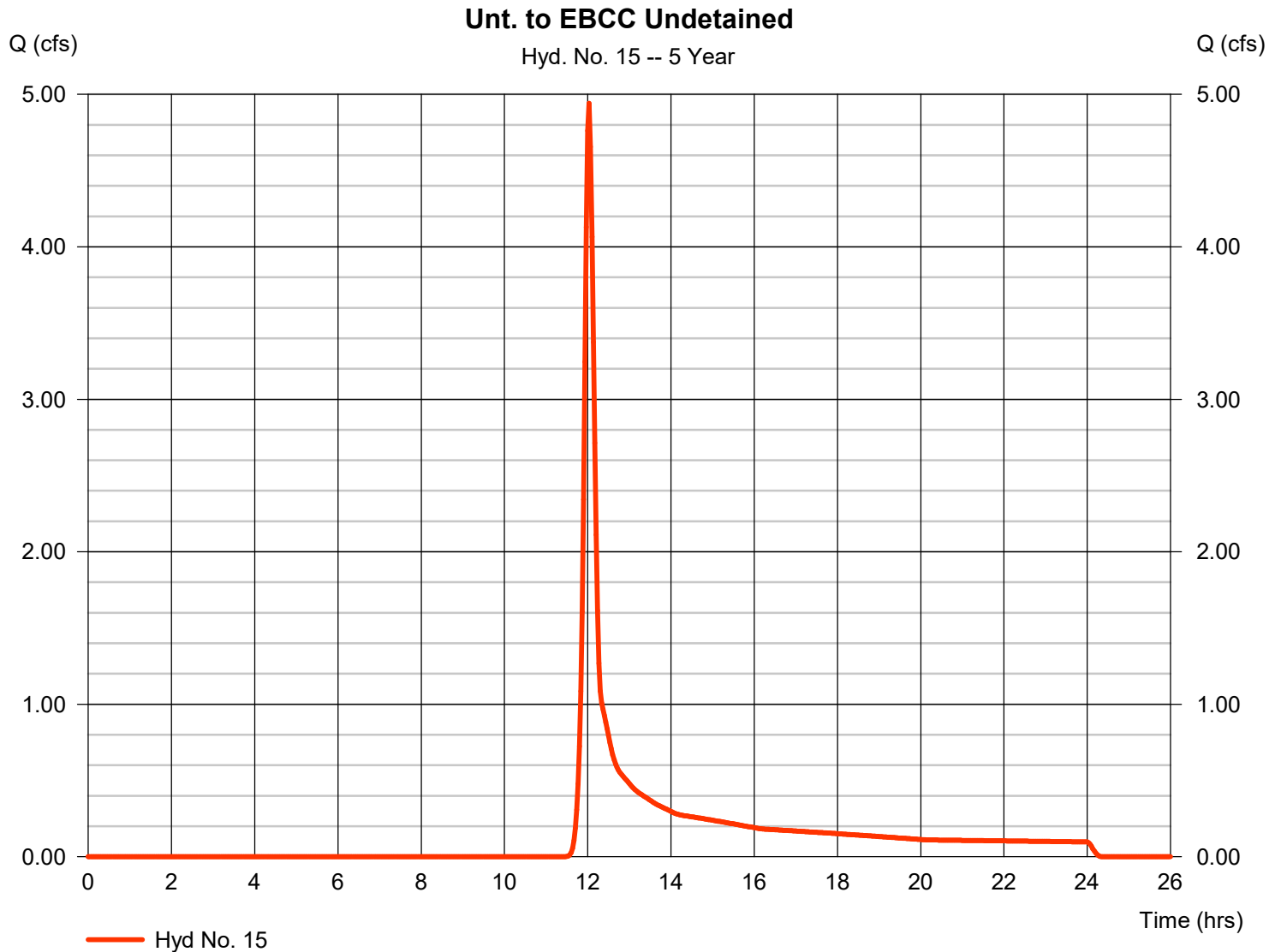


Hydrograph Report

Hyd. No. 15

Unt. to EBCC Undetained

Hydrograph type	= SCS Runoff	Peak discharge	= 4.941 cfs
Storm frequency	= 5 yrs	Time to peak	= 12.03 hrs
Time interval	= 2 min	Hyd. volume	= 13,831 cuft
Drainage area	= 3.590 ac	Curve number	= 64
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 12.00 min
Total precip.	= 4.10 in	Distribution	= Type II
Storm duration	= 24 hrs	Shape factor	= 484

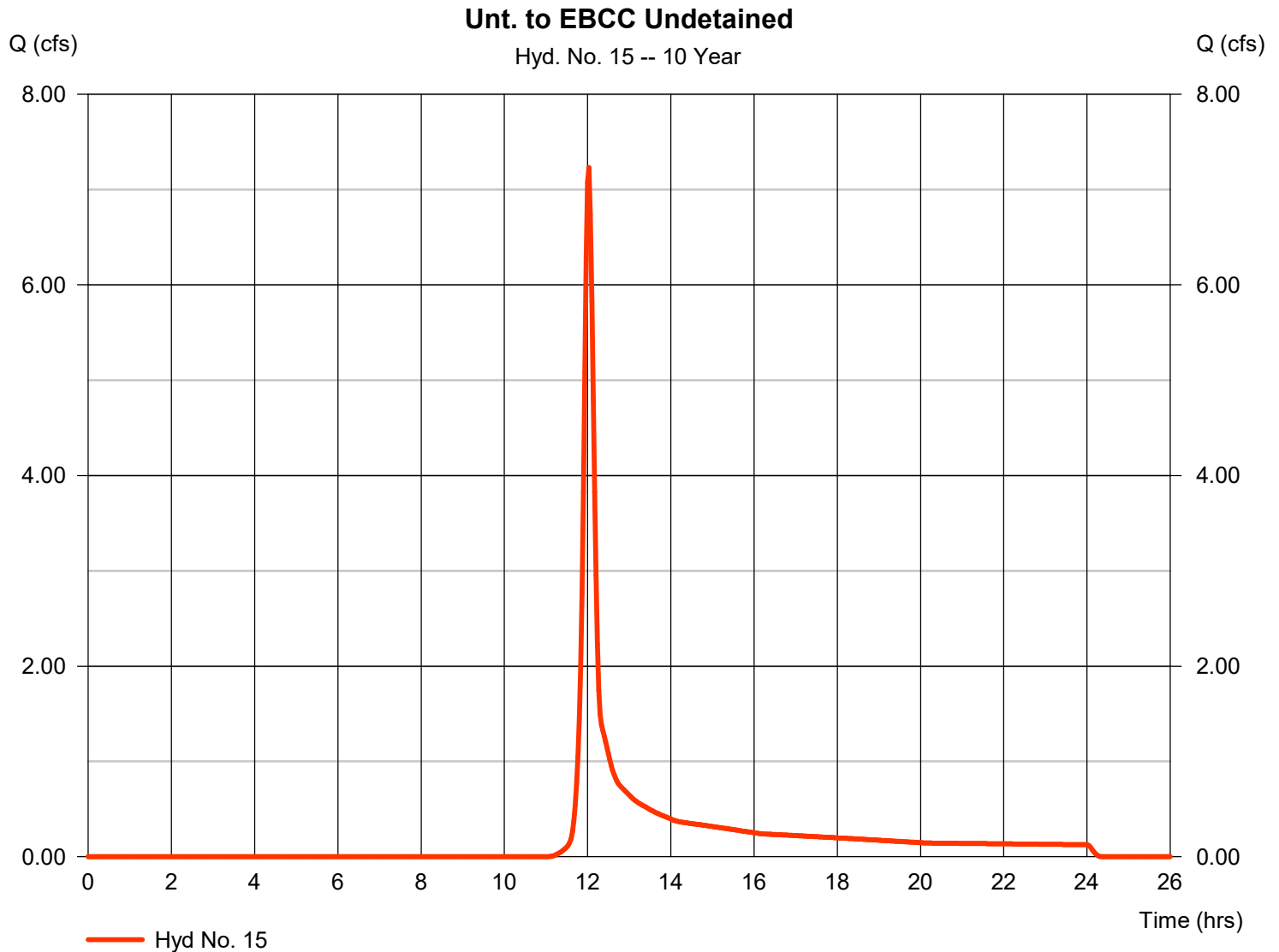


Hydrograph Report

Hyd. No. 15

Unt. to EBCC Undetained

Hydrograph type	= SCS Runoff	Peak discharge	= 7.232 cfs
Storm frequency	= 10 yrs	Time to peak	= 12.03 hrs
Time interval	= 2 min	Hyd. volume	= 19,516 cuft
Drainage area	= 3.590 ac	Curve number	= 64
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 12.00 min
Total precip.	= 4.80 in	Distribution	= Type II
Storm duration	= 24 hrs	Shape factor	= 484

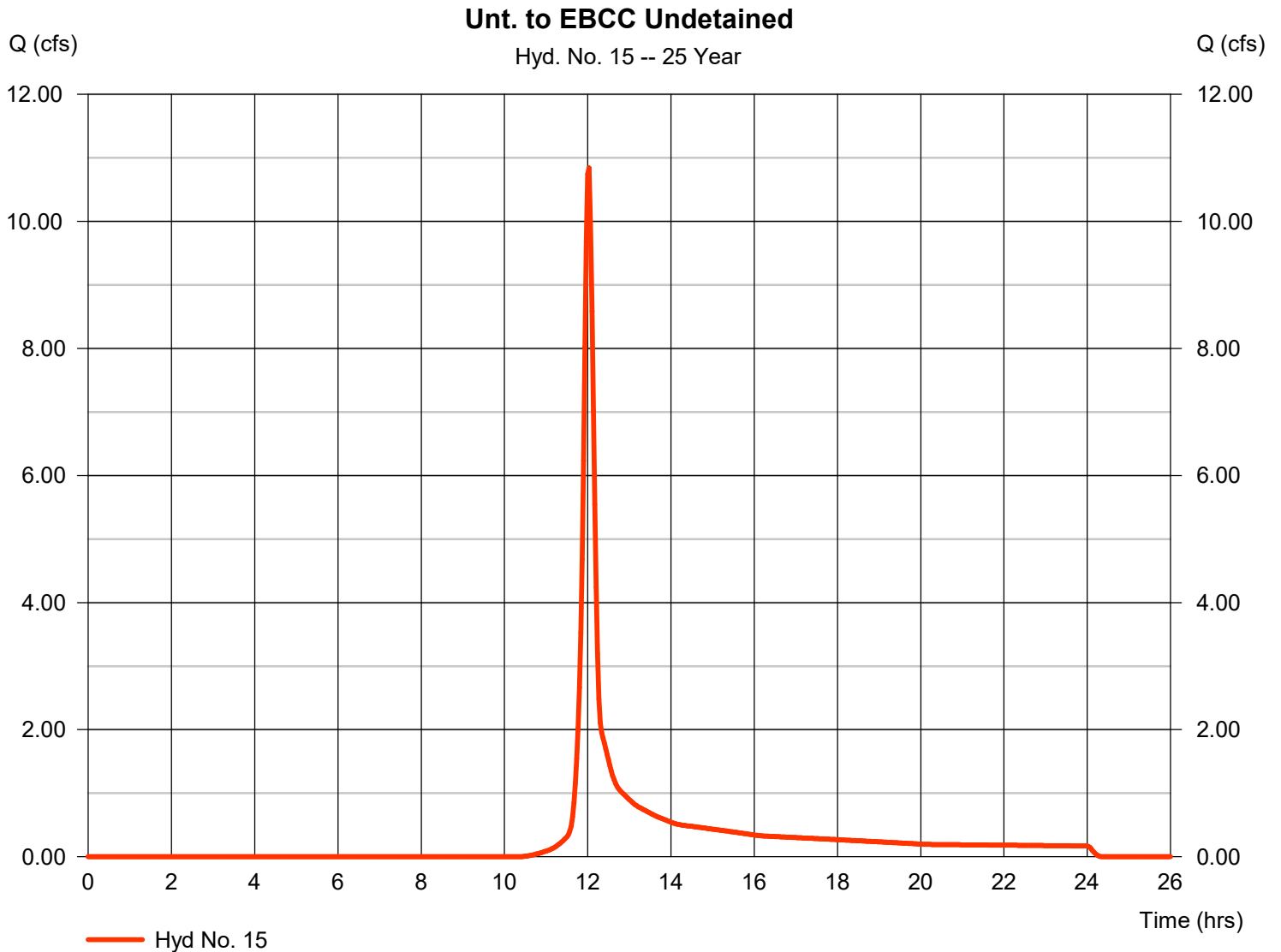


Hydrograph Report

Hyd. No. 15

Unt. to EBCC Undetained

Hydrograph type	= SCS Runoff	Peak discharge	= 10.84 cfs
Storm frequency	= 25 yrs	Time to peak	= 12.03 hrs
Time interval	= 2 min	Hyd. volume	= 28,610 cuft
Drainage area	= 3.590 ac	Curve number	= 64
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 12.00 min
Total precip.	= 5.81 in	Distribution	= Type II
Storm duration	= 24 hrs	Shape factor	= 484

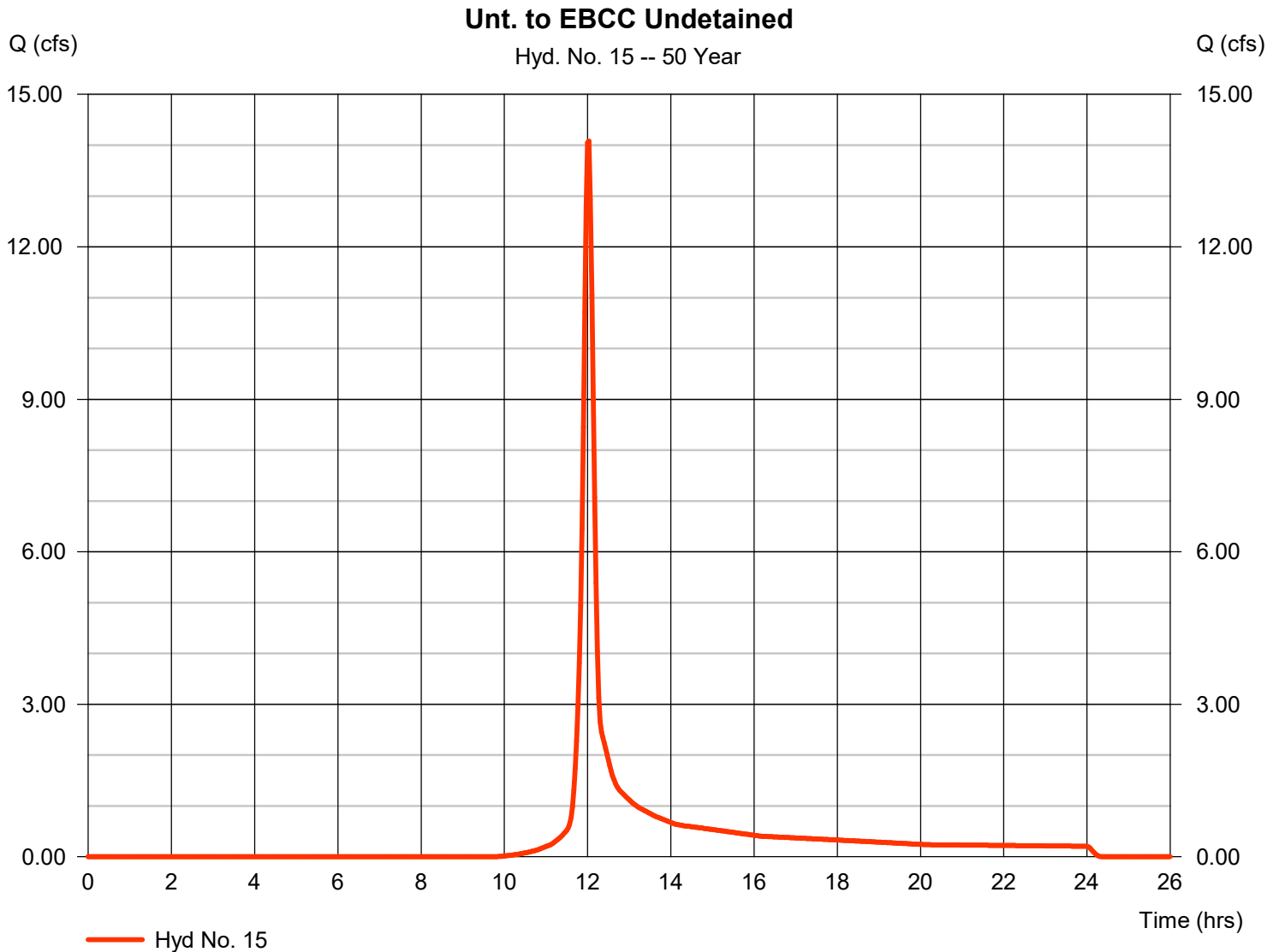


Hydrograph Report

Hyd. No. 15

Unt. to EBCC Undetained

Hydrograph type	= SCS Runoff	Peak discharge	= 14.08 cfs
Storm frequency	= 50 yrs	Time to peak	= 12.03 hrs
Time interval	= 2 min	Hyd. volume	= 36,892 cuft
Drainage area	= 3.590 ac	Curve number	= 64
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 12.00 min
Total precip.	= 6.66 in	Distribution	= Type II
Storm duration	= 24 hrs	Shape factor	= 484

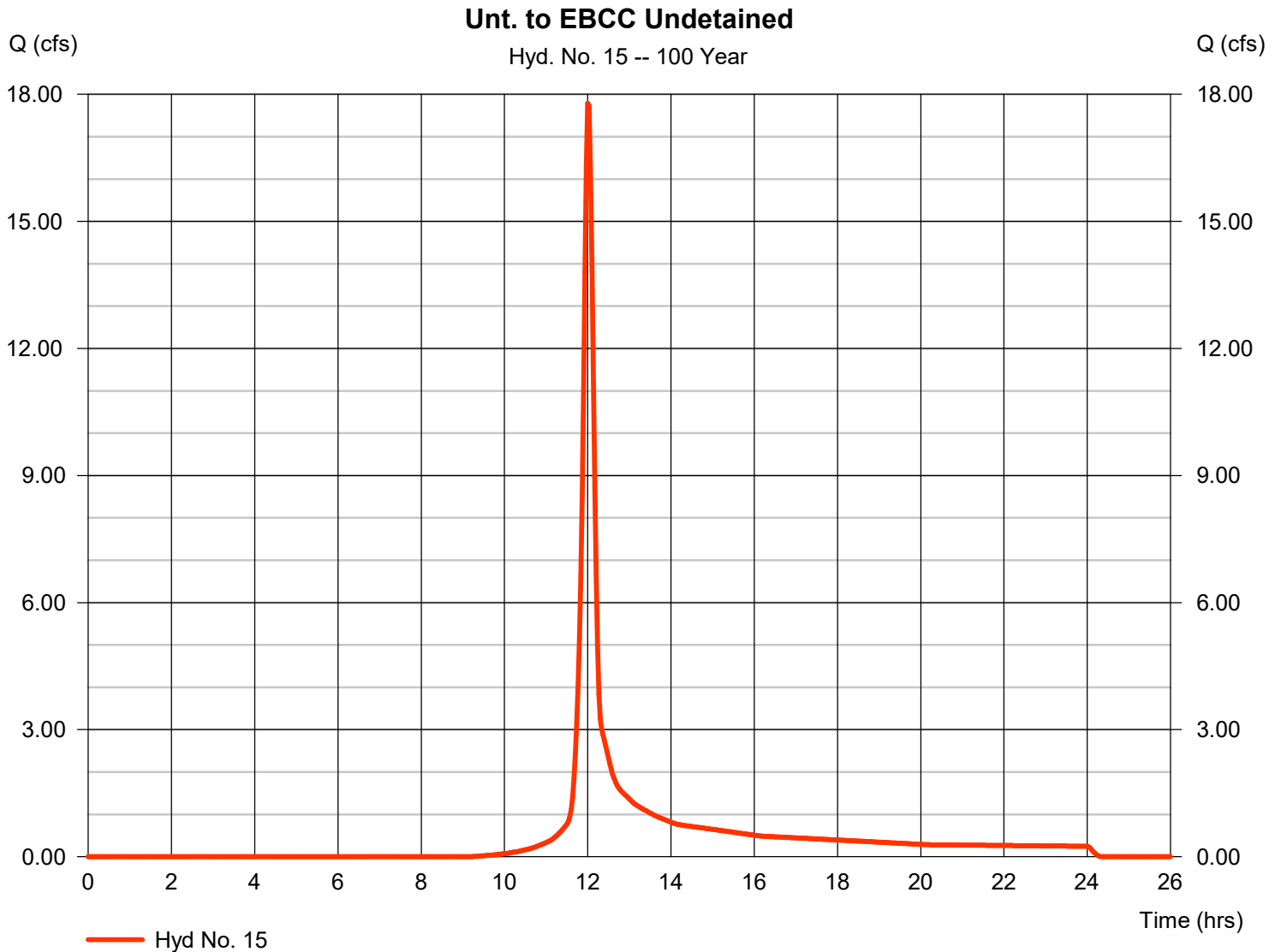


Hydrograph Report

Hyd. No. 15

Unt. to EBCC Undetained

Hydrograph type	= SCS Runoff	Peak discharge	= 17.79 cfs
Storm frequency	= 100 yrs	Time to peak	= 12.00 hrs
Time interval	= 2 min	Hyd. volume	= 46,354 cuft
Drainage area	= 3.590 ac	Curve number	= 64
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 12.00 min
Total precip.	= 7.58 in	Distribution	= Type II
Storm duration	= 24 hrs	Shape factor	= 484



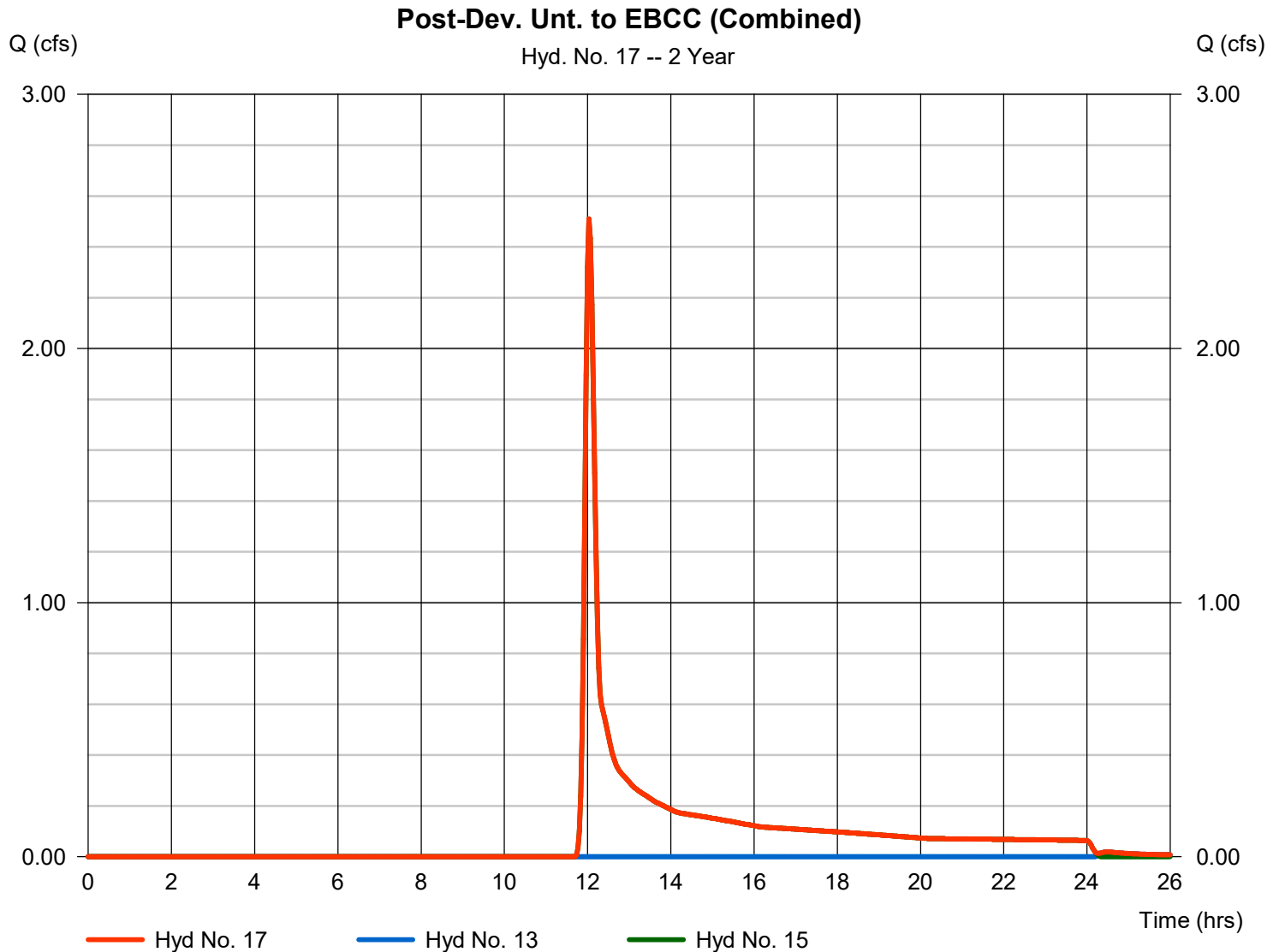
Hydrograph Report

Hyd. No. 17

Post-Dev. Unt. to EBCC (Combined)

Hydrograph type = Combine
Storm frequency = 2 yrs
Time interval = 2 min
Inflow hyds. = 13, 15

Peak discharge = 2.510 cfs
Time to peak = 12.03 hrs
Hyd. volume = 8,681 cuft
Contrib. drain. area = 3.590 ac



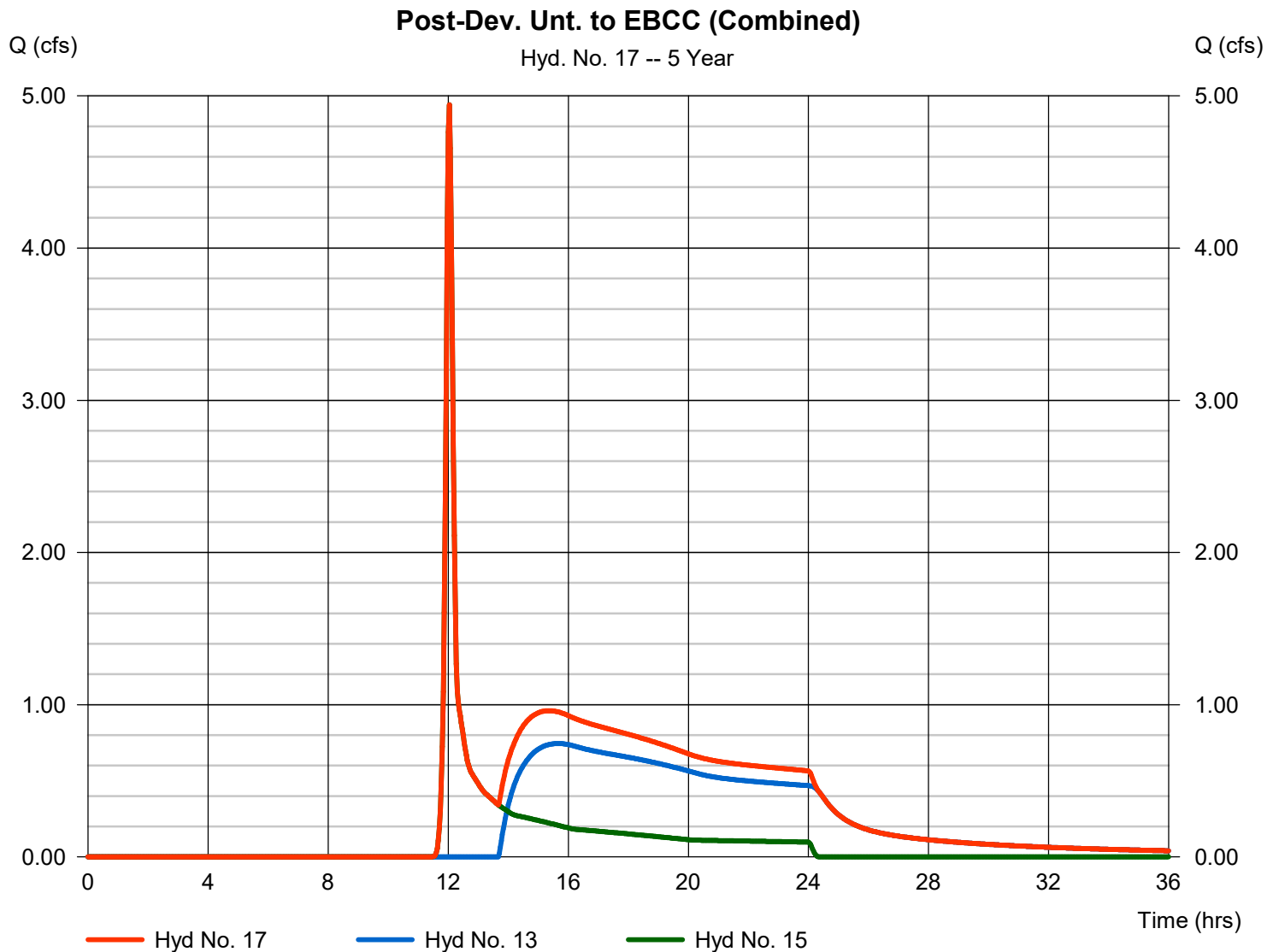
Hydrograph Report

Hyd. No. 17

Post-Dev. Unt. to EBCC (Combined)

Hydrograph type = Combine
Storm frequency = 5 yrs
Time interval = 2 min
Inflow hyds. = 13, 15

Peak discharge = 4.941 cfs
Time to peak = 12.03 hrs
Hyd. volume = 42,984 cuft
Contrib. drain. area = 3.590 ac



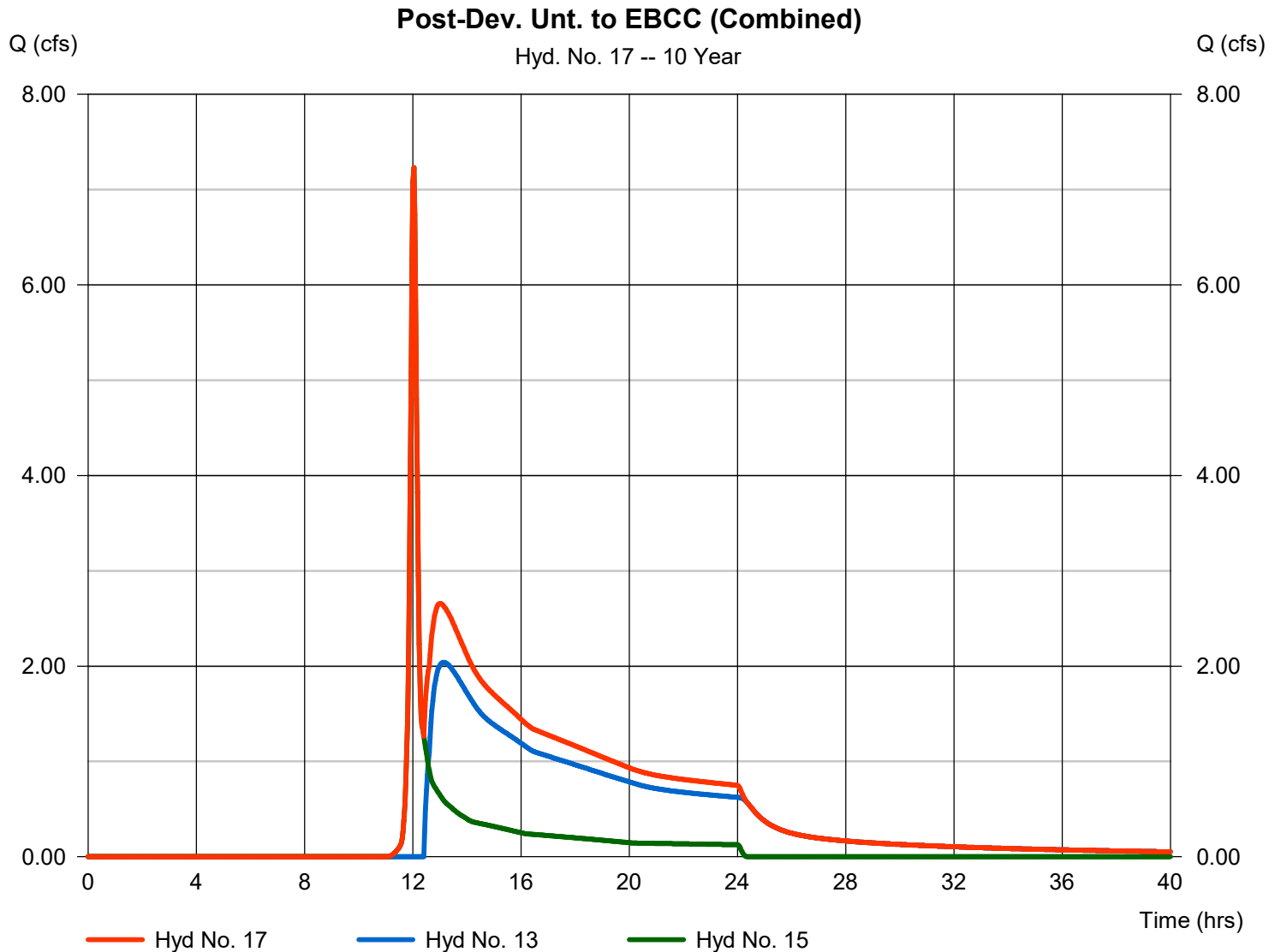
Hydrograph Report

Hyd. No. 17

Post-Dev. Unt. to EBCC (Combined)

Hydrograph type = Combine
Storm frequency = 10 yrs
Time interval = 2 min
Inflow hyds. = 13, 15

Peak discharge = 7.232 cfs
Time to peak = 12.03 hrs
Hyd. volume = 74,628 cuft
Contrib. drain. area = 3.590 ac



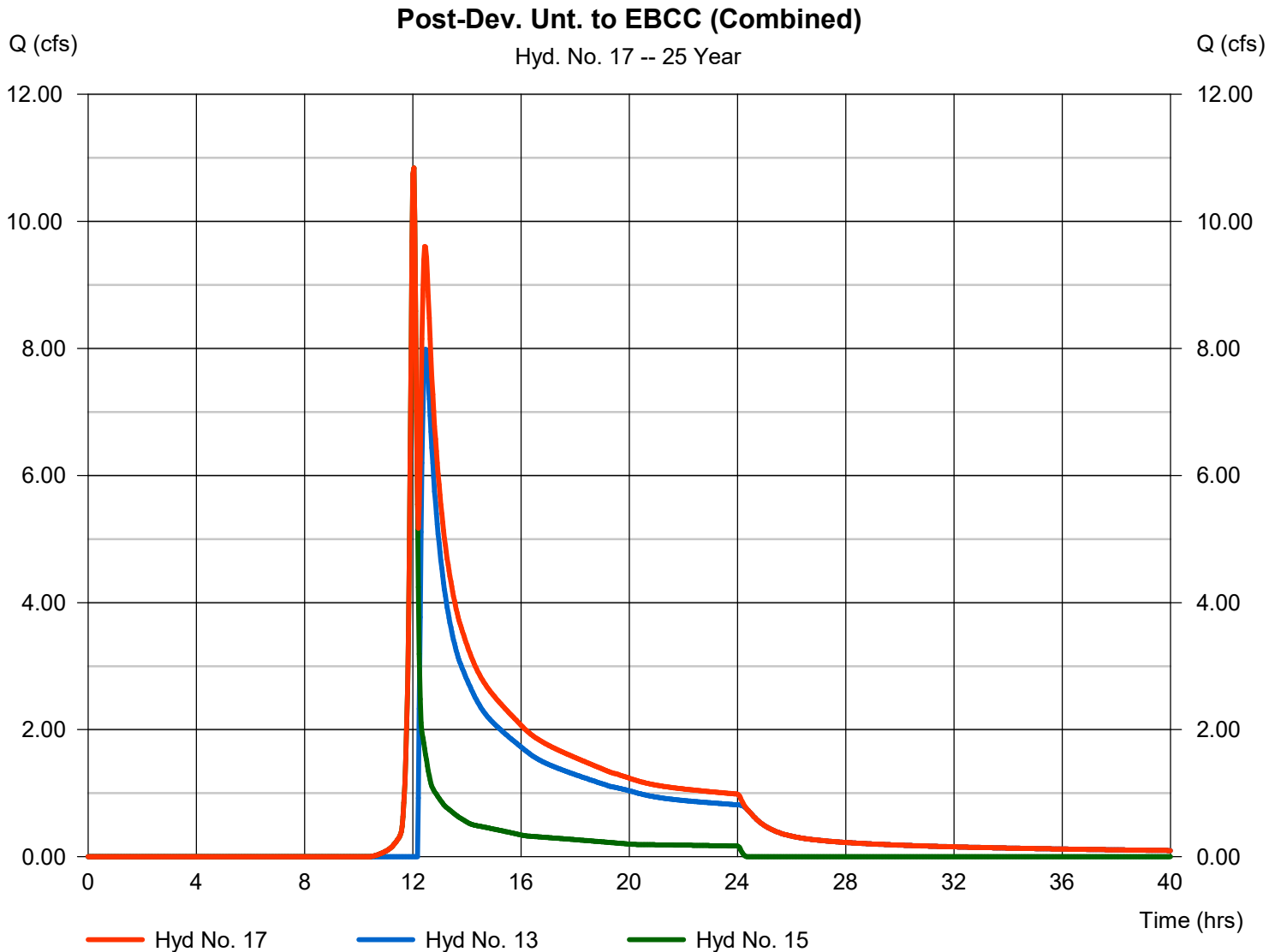
Hydrograph Report

Hyd. No. 17

Post-Dev. Unt. to EBCC (Combined)

Hydrograph type = Combine
Storm frequency = 25 yrs
Time interval = 2 min
Inflow hyds. = 13, 15

Peak discharge = 10.84 cfs
Time to peak = 12.03 hrs
Hyd. volume = 123,489 cuft
Contrib. drain. area = 3.590 ac



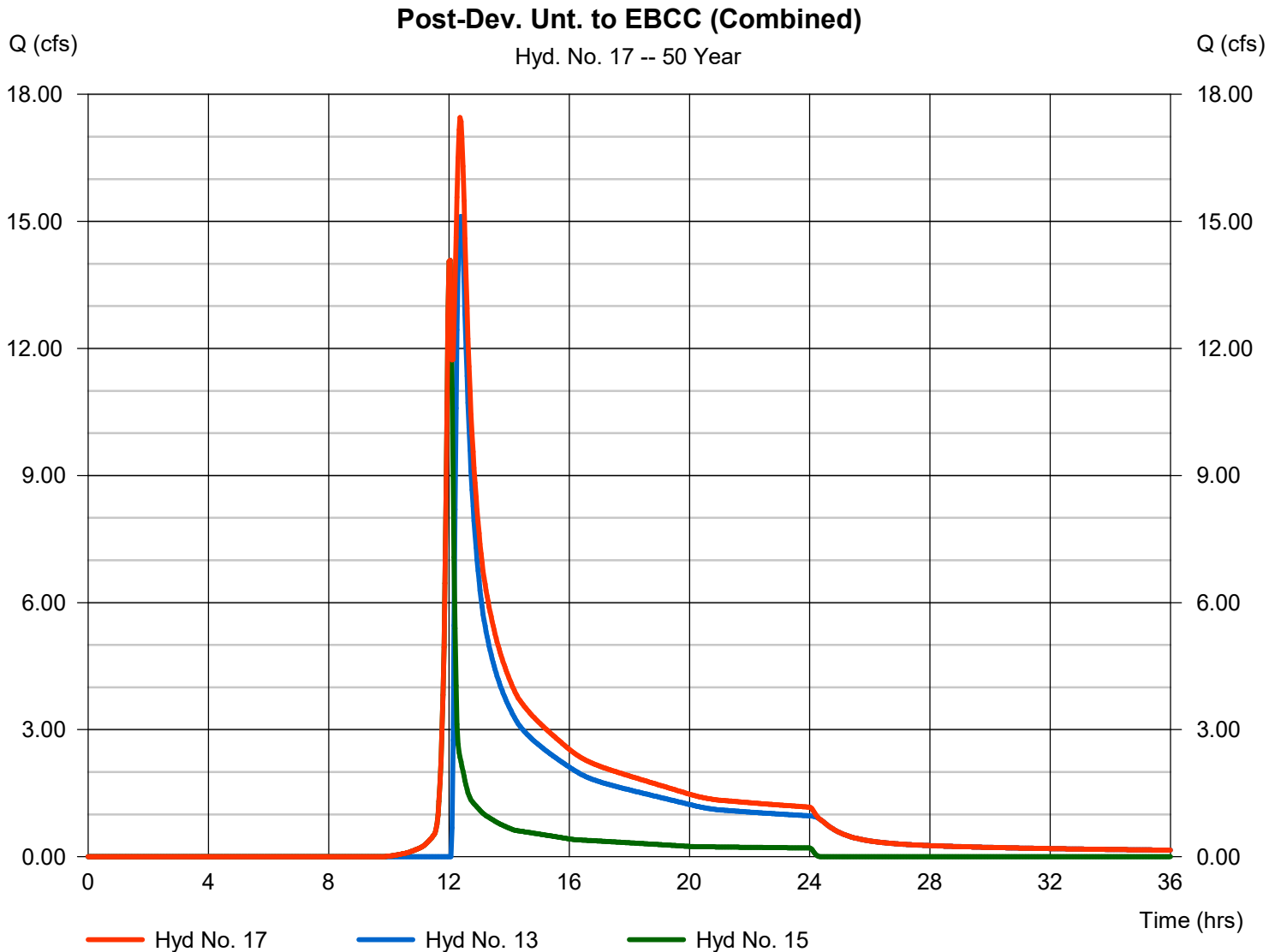
Hydrograph Report

Hyd. No. 17

Post-Dev. Unt. to EBCC (Combined)

Hydrograph type = Combine
Storm frequency = 50 yrs
Time interval = 2 min
Inflow hyds. = 13, 15

Peak discharge = 17.45 cfs
Time to peak = 12.37 hrs
Hyd. volume = 166,857 cuft
Contrib. drain. area = 3.590 ac



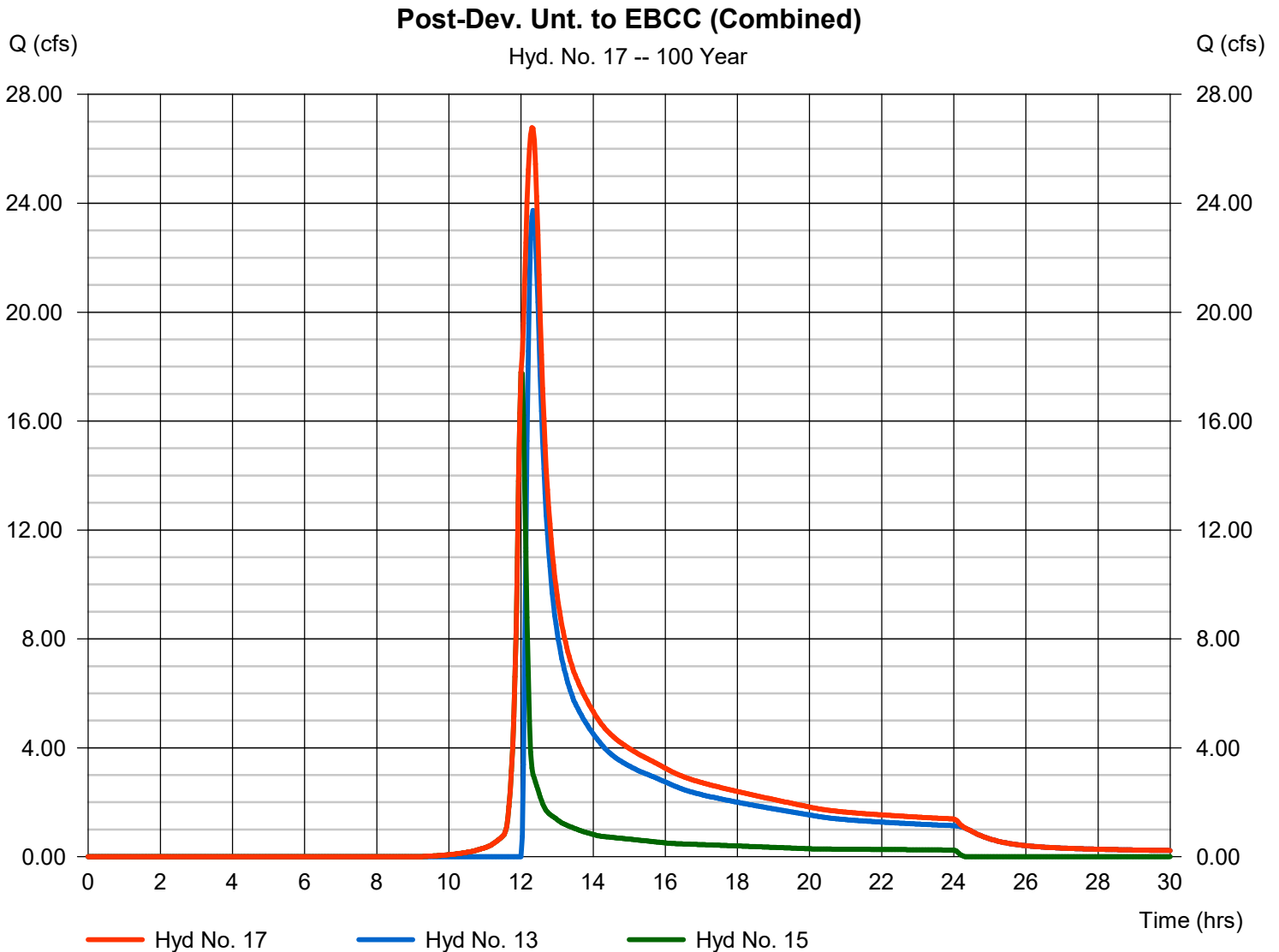
Hydrograph Report

Hyd. No. 17

Post-Dev. Unt. to EBCC (Combined)

Hydrograph type = Combine
Storm frequency = 100 yrs
Time interval = 2 min
Inflow hyds. = 13, 15

Peak discharge = 26.78 cfs
Time to peak = 12.30 hrs
Hyd. volume = 215,739 cuft
Contrib. drain. area = 3.590 ac



APPENDIX F

STORM SEWER CALCULATIONS

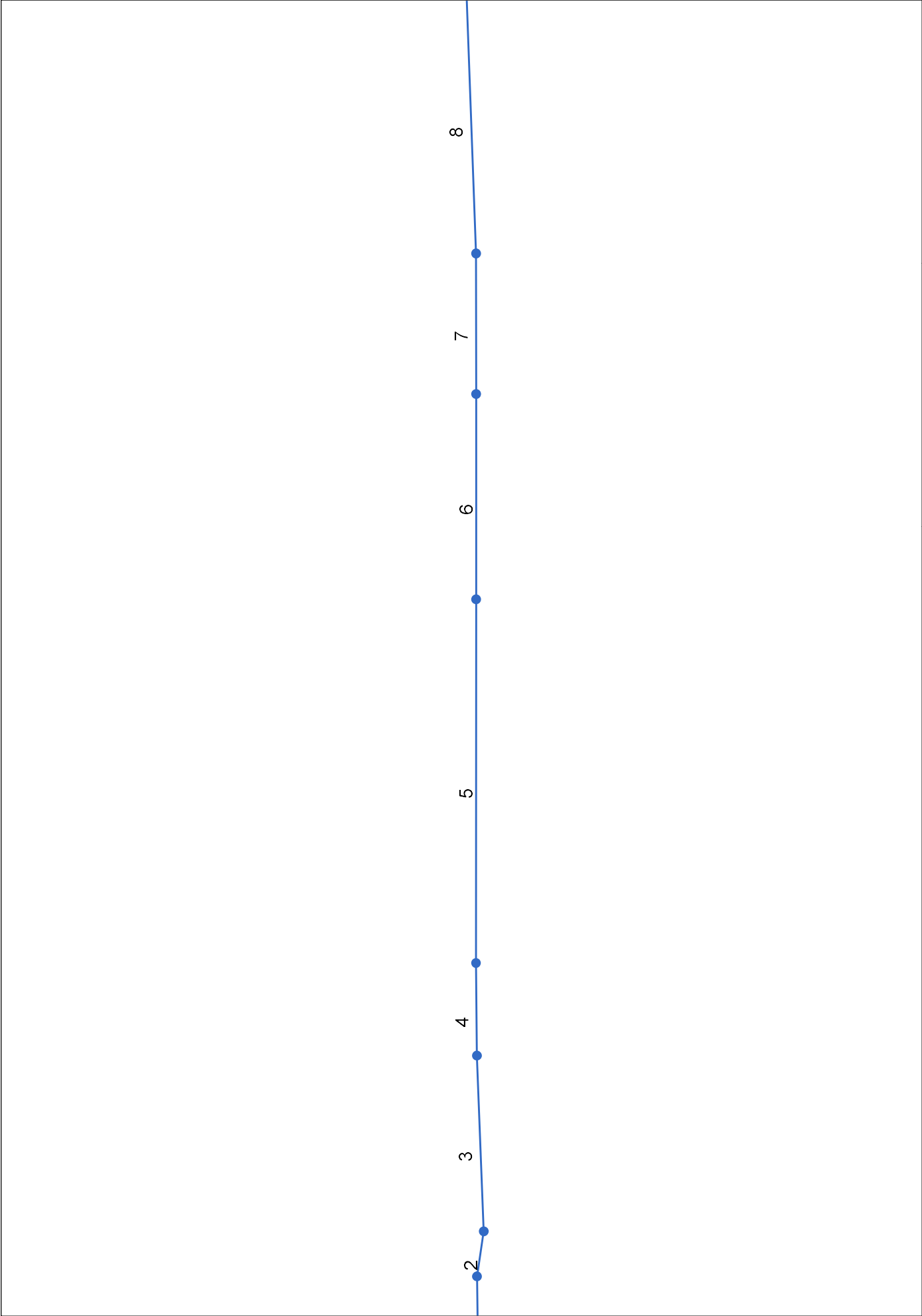


INLET AREA COEFFICIENTS AND SURFACE FLOWS

PROJECT: The Westtown School - Oak Lane Project
 LOCATION: Westtown Township
 COUNTY: Chester

INLET COVER TYPE	B SOIL			D SOIL		AREA (ac.)	COMP. C	Tc (min)	COMMENTS
	IMP	LAWN	WOODS	LAWN	WOODS				
C COEFFICIENTS	0.99	0.25	0.34	0.65	0.7				
I-A3	0.06	1.72	0.00	0.00	0.00	1.79	0.28	5	
I-A5	0.15	0.58	0.00	0.00	0.00	0.73	0.40	5	
I-A6	0.26	0.09	0.00	0.00	0.00	0.35	0.80	5	
I-A7	0.06	0.00	0.00	0.00	0.00	0.06	0.96	5	
I-A8	0.31	0.18	0.00	0.00	0.00	0.48	0.72	5	
I-A9	0.12	0.03	0.00	0.00	0.00	0.15	0.85	5	
I-A10	0.06	0.05	0.00	0.00	0.00	0.11	0.65	5	
I-A11	0.10	0.27	0.00	0.00	0.00	0.37	0.45	5	

Hydraflow Storm Sewers Extension for Autodesk® Civil 3D® Plan



Storm Sewer Tabulation

Station	Line	To Line	Len (ft)	Drng Area (ac)		Rnoff coeff (C)	Area x C		Tc		Rain (l) (in/hr)	Total flow (cfs)	Cap full (cfs)	Vel (ft/s)	Pipe		Invert Elev (ft)		HGL Elev (ft)		Grnd / Rim Elev (ft)		Line ID
				Incr	Total		Incr	Total	Inlet (min)	Syst (min)					Size (in)	Slope (%)	Dn	Up	Dn	Up	Dn	Up	
1	End		68.720	1.79	4.04	0.28	0.50	1.84	5.0	7.4	6.6	12.07	10.52	6.83	18	1.00	288.50	289.19	290.82	291.73	0.00	292.80	A3 to A2
2	1		23.270	0.00	2.25	0.00	0.00	1.34	0.0	7.3	6.6	8.81	18.21	4.99	18	3.01	290.05	290.75	292.09	292.25	292.80	296.20	A4 to A3
3	2		89.010	0.73	2.25	0.40	0.29	1.34	5.0	7.1	6.6	8.91	9.57	5.70	18	0.83	291.00	291.74	292.36	292.89	296.20	295.71	A5 to A4
4	3		46.880	0.35	1.52	0.80	0.28	1.05	5.0	7.0	6.7	7.01	11.63	6.33	15	3.24	291.84	293.36	292.89	294.42	295.71	296.86	A6 to A5
5	4		184.000	0.06	1.17	0.96	0.06	0.77	5.0	6.4	6.9	5.27	13.16	5.07	15	4.15	293.36	301.00	294.42	301.93	305.00	305.00	A7 to A6
6	5		103.890	0.48	1.11	0.72	0.35	0.71	5.0	6.0	7.0	4.95	6.40	5.47	15	0.98	301.10	302.12	303.02	303.02	305.00	306.00	A8 to A7
7	6		71.110	0.15	0.63	0.85	0.13	0.37	5.0	5.8	7.1	2.58	4.65	4.15	12	1.70	302.22	303.43	303.02	304.12	306.00	307.01	A9 to A8
8	7		136.000	0.11	0.48	0.65	0.07	0.24	5.0	5.1	7.3	1.73	3.44	3.72	12	0.93	303.53	304.80	304.12	305.36	307.01	308.37	A10 to A9
9	8		29.850	0.37	0.37	0.45	0.17	0.17	5.0	5.0	7.3	1.22	3.51	3.43	12	0.97	304.90	305.19	305.36	305.65	308.37	308.73	A11 to A10

Project File: Westtown-PIPES_A.stm

Run Date: 9/18/2023

Number of lines: 9

NOTES: Intensity = 50.00 / (Inlet time + 9.70) ^ 0.72; Return period = Yrs. 100 ; c = cir e = ellip b = box

ELA GROUP

ENGINEERS &
LANDSCAPE ARCHITECTS

737 S. BROAD STREET
LITITZ, PA 17543
(717) 626-72713

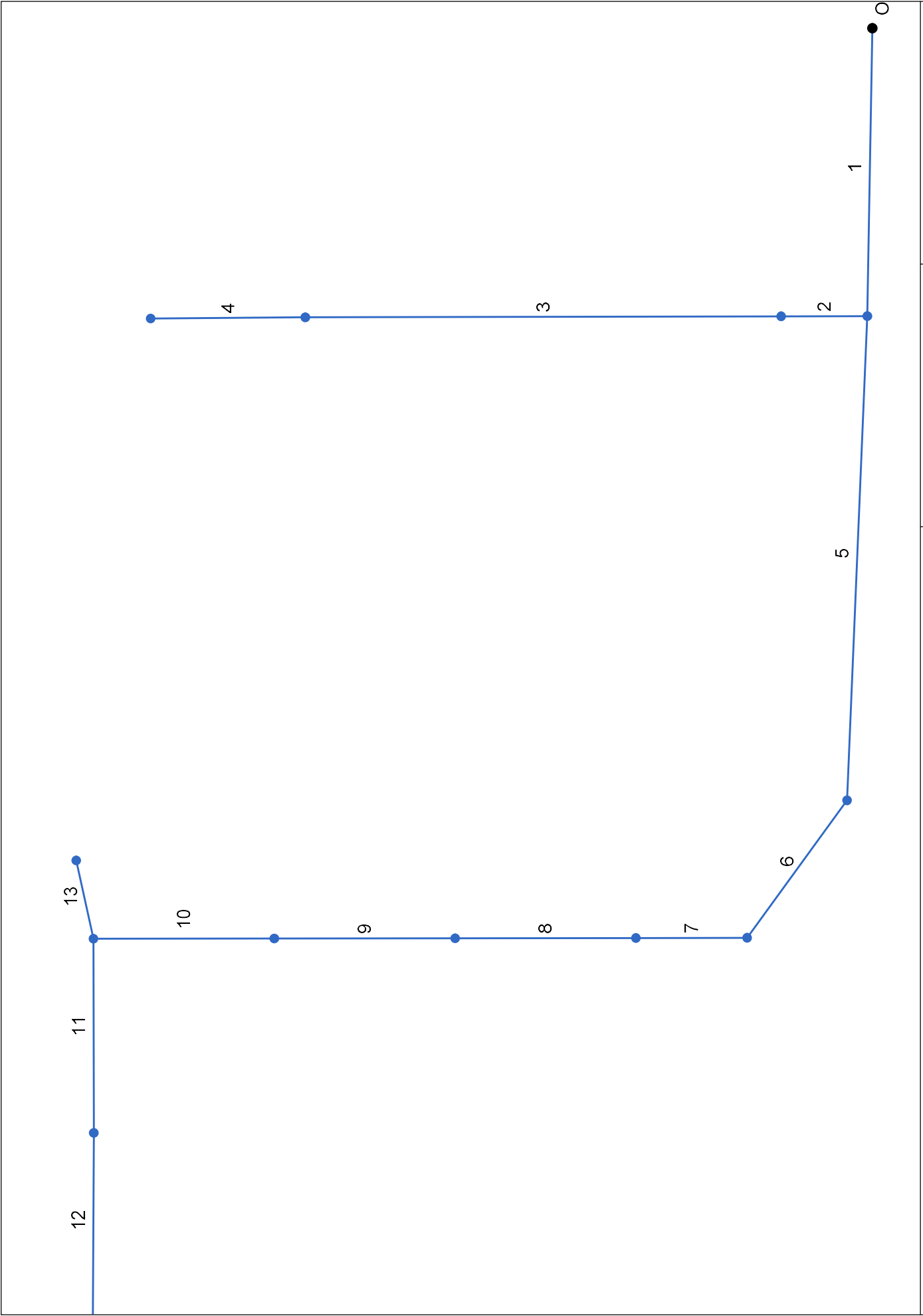


INLET AREA COEFFICIENTS AND SURFACE FLOWS

PROJECT: The Westtown School - Oak Lane Project
LOCATION: Westtown Township
COUNTY: Chester

INLET	TYPE	B SOIL			D SOIL		AREA (ac.)	COMP. C	Tc (min)	COMMENTS
		IMP	LAWN	CULTIVATED	LAWN	CULTIVATED				
	COVER TYPE									
	C COEFFICIENTS	0.99	0.25	0.43	0.65	0.67				
I-B4		0.00	0.00	0.00	0.00	0.00	0.00		5	0.25 CFS FROM B-3
I-B5		0.00	0.04	0.00	0.00	0.00	0.04	0.25	5	
I-B6		0.00	0.04	0.00	0.00	0.00	0.04	0.25	5	
I-B8		0.00	0.08	0.00	0.00	0.00	0.08	0.25	5	0.92 CFS FROM B-2
I-B9		0.00	0.12	0.00	0.00	0.00	0.12	0.25	5	
I-B10		0.06	0.05	0.00	0.00	0.00	0.11	0.65	5	
I-B11		0.01	0.09	0.00	0.00	0.00	0.11	0.33	5	
I-B12		0.08	0.13	0.00	0.00	0.00	0.21	0.54	5	
I-B12A		0.01	0.02	0.00	0.00	0.00	0.03	0.57	5	
I-B13		0.01	0.04	0.00	0.00	0.00	0.05	0.45	5	
I-B14		0.02	0.02	0.00	0.00	0.00	0.03	0.61	5	
I-B18		0.15	0.86	0.35	0.00	0.00	1.35	0.38	5	

Hydraflow Storm Sewers Extension for Autodesk® Civil 3D® Plan



Storm Sewer Tabulation

Station	Line	To Line	Len (ft)	Drng Area (ac)		Rnoff coeff (C)	Area x C		Tc		Rain (l) (in/hr)	Total flow (cfs)	Cap full (cfs)	Vel (ft/s)	Pipe		Invert Elev (ft)		HGL Elev (ft)		Grnd / Rim Elev (ft)		Line ID
				Incr	Total		Inlet (min)	Syst (min)	Incr	Slope (%)					Dn	Up	Dn	Up	Dn	Up			
1	End		148.240	0.00	0.82	0.00	0.00	0.35	5.0	11.6	5.6	4.51	4.59	3.73	15	0.51	310.00	310.75	311.25	311.91	0.00	316.00	MH-B3 TO EW-B2
2	1		44.610	0.00	0.08	0.00	0.00	0.02	5.0	7.2	6.6	0.57	11.74	1.72	12	10.87	311.15	316.00	312.13	316.31	316.00	322.25	I-B4 TO MH-B3
3	2		246.000	0.04	0.08	0.25	0.01	0.02	5.0	6.0	7.0	0.58	1.28	3.30	8	1.12	316.25	319.00	316.57	319.36	322.25	322.25	OCS-3 TO I-B4
4	3		80.000	0.04	0.04	0.25	0.01	0.01	5.0	5.0	7.3	0.07	1.22	1.36	8	1.01	319.19	320.00	319.36	320.12	322.25	322.00	I-B6 TO OCS-3
5	1		249.540	0.00	0.74	0.00	0.00	0.33	5.0	10.4	5.8	4.03	4.57	3.48	15	0.50	310.75	312.00	312.13	313.05	316.00	321.00	MH-B7 TO MH-B3
6	5		87.620	0.08	0.74	0.25	0.02	0.33	5.0	10.0	5.9	4.06	4.88	3.73	15	0.57	312.00	312.50	313.17	313.45	321.00	317.00	OCS-2 TO MH-B7
7	6		57.500	0.12	0.66	0.25	0.03	0.31	5.0	9.6	6.0	1.86	2.66	2.37	12	0.56	312.50	312.82	313.77	313.93	317.00	317.00	I-B9 TO OCS-2
8	7		93.500	0.11	0.54	0.65	0.07	0.28	5.0	8.9	6.2	1.72	2.52	2.28	12	0.50	312.82	313.29	313.97	314.17	317.00	317.00	I-B10 TO I-B9
9	8		93.500	0.11	0.43	0.33	0.04	0.21	5.0	8.3	6.3	1.31	1.55	2.47	10	0.50	313.29	313.76	314.21	314.52	317.00	317.00	I-B11 TO I-B10
10	9		93.500	0.21	0.32	0.54	0.11	0.17	5.0	7.7	6.5	1.11	1.55	2.43	10	0.50	313.76	314.23	314.57	314.80	317.00	317.00	I-B12 TO I-B11
11	10		100.000	0.05	0.08	0.45	0.02	0.04	5.0	6.3	6.9	0.28	0.85	1.17	8	0.50	314.23	314.73	314.98	315.08	317.00	317.00	I-B13 TO I-B12
12	11		100.000	0.03	0.03	0.61	0.02	0.02	5.0	5.0	7.3	0.13	0.87	1.31	8	0.52	314.73	315.25	315.10	315.42	317.00	317.00	I-B14 TO I-B13
13	10		41.260	0.03	0.03	0.57	0.02	0.02	5.0	5.0	7.3	0.12	0.86	0.38	8	0.51	314.23	314.44	314.98	314.99	317.00	318.65	I-B12A TO I-B12

Project File: Westtown-PIPES_B.stm

Number of lines: 13

Run Date: 9/18/2023

NOTES: Intensity = 50.00 / (Inlet time + 9.70) ^ 0.72; Return period = Yrs. 100 ; c = cir e = ellip b = box

APPENDIX G
SPILLWAY/ANTI-SEEP COLLAR
DESIGN CALCULATIONS

BMP 1 EMERGENCY SPILLWAY

PROJECT: The Westtown School - Oak Lane Project
 LOCATION: Westtown Township
 COUNTY: Chester

JOB # 1091-001
 DATE: 1/12/2023
 REVISED: 9/17/2023

Flow into basin for 100-year storm frequency:

$$Q = 29.58 \text{ cfs cfs (From Post-Development analysis)}$$

Capacity of the Emergency Spillway:

$$Q = CLH^{1.5}$$

$$\begin{aligned} C &= 2.8 \\ L &= 30 \text{ ft.} \\ H &= 1.00 \end{aligned}$$

$$Q = 84.00 \text{ cfs} > 30 \text{ cfs cfs} \quad \text{OK}$$

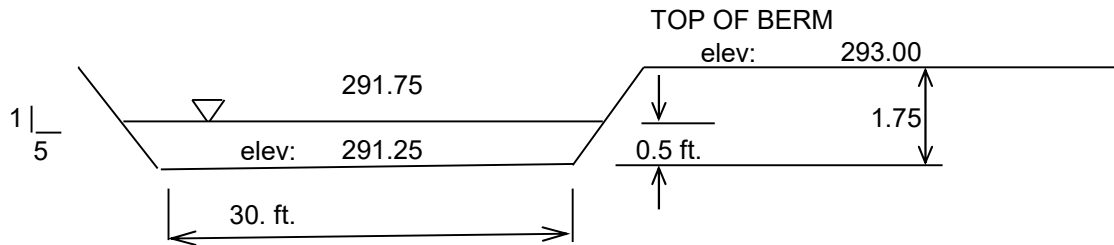
Check actual depth and velocity:

$$\begin{aligned} \text{Top of Berm Elevation} &= 293.00 \\ \text{Spillway Elevation} &= 291.25 \end{aligned}$$

$$\begin{aligned} H &= [Q/C*L]^{2/3} \\ &= 0.5 \text{ ft.} \quad \text{at elevation} \quad 291.75 \end{aligned}$$

$$\text{Freeboard:} \quad 293.00 - 291.75 = 1.25 \text{ ft.}$$

$$\begin{aligned} V &= Q/A \\ &= 1.8 \text{ fps} \end{aligned} \quad \text{Side Slope (H:V)} = 4.5$$



N.T.S.

BMP 4 EMERGENCY SPILLWAY

PROJECT: The Westtown School - Oak Lane Project
 LOCATION: Westtown Township
 COUNTY: Chester

JOB # 1091-001
 DATE: 1/12/2023
 REVISED: 9/17/2023

Flow into basin for 100-year storm frequency:

$$Q = 38.87 \text{ cfs cfs (From Post-Development analysis)}$$

Capacity of the Emergency Spillway:

$$Q = CLH^{1.5}$$

$$\begin{aligned} C &= 2.8 \\ L &= 40 \text{ ft.} \\ H &= 1.00 \end{aligned}$$

$$Q = 112.00 \text{ cfs} > 39 \text{ cfs cfs} \quad \text{OK}$$

Check actual depth and velocity:

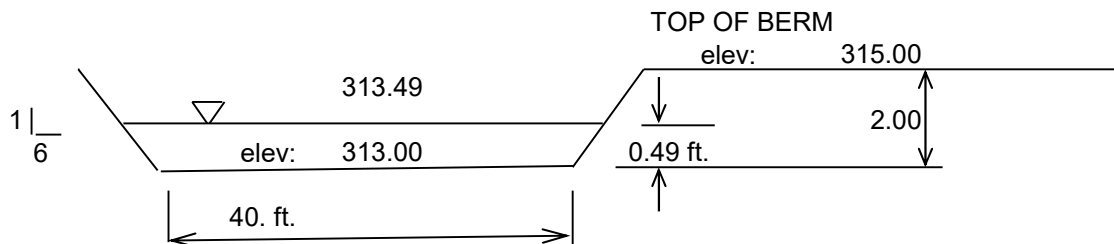
$$\begin{aligned} \text{Top of Berm Elevation} &= 315.00 \\ \text{Spillway Elevation} &= 313.00 \end{aligned}$$

$$H = [Q/C*L]^{2/3}$$

$$= 0.49 \text{ ft.} \quad \text{at elevation} \quad 313.49$$

$$\text{Freeboard:} \quad 315.00 - 313.49 = 1.51 \text{ ft.}$$

$$\begin{aligned} V &= Q/A & \text{Side Slope (H:V)} &= 6 \\ &= 1.8 \text{ fps} \end{aligned}$$



N.T.S.

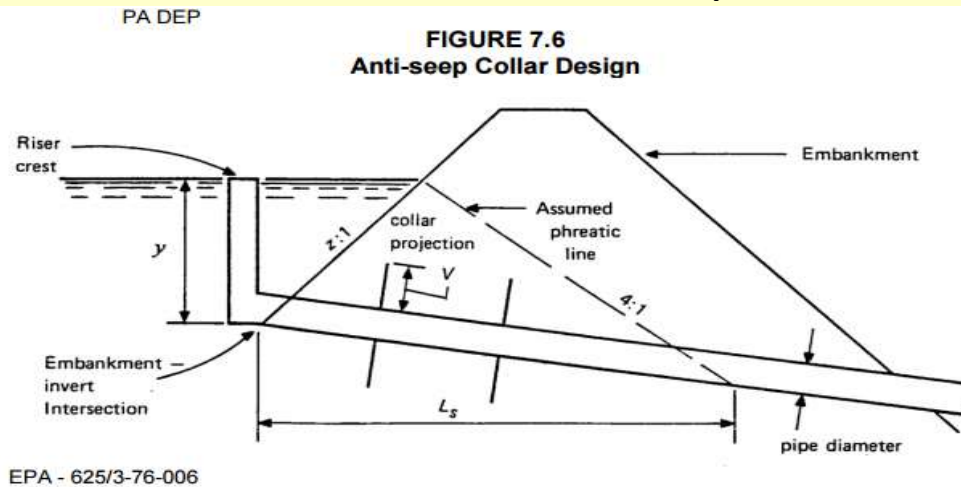
**MODIFIED WORK SHEET # 11
SPILLWAY STABILITY CALCULATIONS**

PROJECT: <u>The Westtown School - Oak Lane Project</u>	JOB #	1091-001
LOCATION: <u>Westtown Township</u>	Date	9/18/23
COUNTY: <u>Chester</u>	Revised	

x	BASIN SPILLWAY ID		BMP 1	BMP 4		
	TEMPORARY OR PERMANENT? (T OR P)		P	P		
	DESIGN STORM		100	100		
	Qr (REQUIRED CAPACITY)* (CFS)		29.58	38.61		
	Q (CALCULATED AT FLOW DEPTH d) (CFS)		29.59	38.62		
x	PROTECTIVE LINING ²		Flexamat	Flexamat		
	n (MANNING'S COEFFICIENT) ²		0.058	0.059		
	Va (ALLOWABLE VELOCITY) (FPS)		19	19		
	V (CALCULATED AT FLOW DEPTH d) (FPS)		4.05	4.69		
	ta (MAX ALLOWABLE SHEAR STRESS) (LB/FT ²)		24.00	24.00		
	td (CALC'D SHEAR STRESS AT FLOW DEPTH d) (LB/FT ²)		2.49	3.62		
	SPILLWAY BOTTOM WIDTH (FT)		30.0	40.0		
	SIDE SLOPES (H:V)		4.5:1	6:1		
	D (TOTAL DEPTH) (FT)		1.75	2.00		
	d (CALCULATED FLOW DEPTH) (FT)		0.24	0.20		
x	d ₅₀ STONE SIZE (IN) (IN)		N/A	N/A		
x	A (CROSS-SECTIONAL AREA) (SQ. FT.)		7.30	8.23		
x	R (HYDRAULIC RADIUS)		0.24	0.20		
x	S (BED SLOPE) ³ (FT/FT)		0.167	0.286		
x	FREEBOARD PROVIDED (FT)		1.51	1.80		
x	DESIGN METHOD FOR PROTECTIVE LINING **** PERMISSIBLE VELOCITY (V) OR SHEAR STRESS (S)		S	S		

ANTI-SEEP COLLAR DESIGN

Infiltration BMP 1/Sediment Trap 1



1. Determine length of pipe in saturated zone (L_s)

$$L_s = y(z+4) \left[1 + \frac{S}{(0.25 - S)} \right]$$

$$\begin{aligned} y &= 6.25 \\ z &= 3 \\ S &= 0.005 \end{aligned}$$

Where y = Distance from upstream invert of spillway riser to top of dewatering volume (ft)
 z = Horizontal component of upstream embankment slope (ft)
 S = Pipe slope ft/ft

$$L_s = \underline{44.64} \text{ ft}$$

2. Determine the required increase in flow path

$$L_F = 1.15 * L_s = \underline{51.34} \text{ ft}$$

3. The minimum collar projection (V) is equal to 1/2 the increase in flow length (for one collar). If more than one collar is used, it is the increase divided by twice the number of collars

$$\text{Number of collars: } \underline{2}$$

$$V_{\min} = \underline{1.67} \text{ ft}$$

4. The maximum spacing between collars should be $14 \times V$ or $L_s \div (\text{number of collars minus } 1)$

Minimum spacing should be $5 \times V$

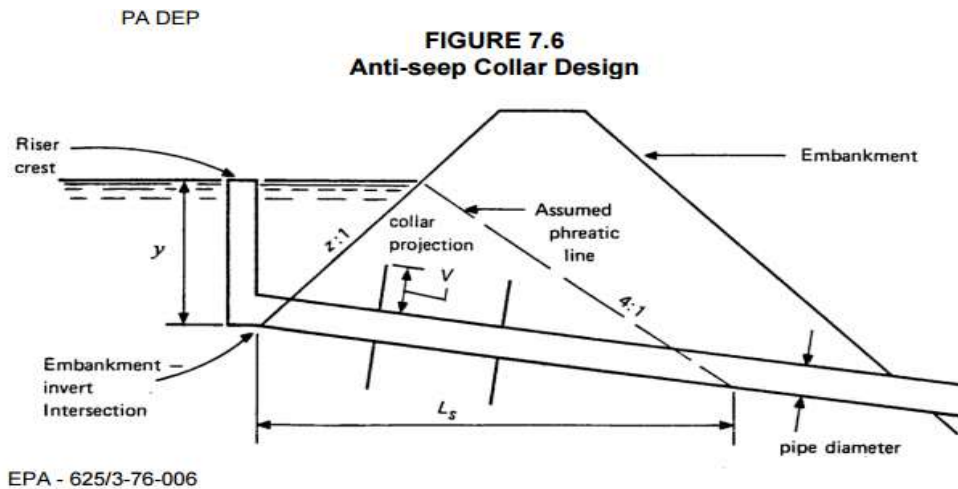
$$V = \underline{1.67} \text{ ft}$$

$$\text{Max} = 22 \text{ ft}$$

$$\text{Min} = 8.4 \text{ ft}$$

ANTI-SEEP COLLAR DESIGN

Infiltration BMP 4/Sediment Basin 4



1. Determine length of pipe in saturated zone (L_s)

$$L_s = y(z+4) \left[1 + \frac{S}{(0.25-S)} \right]$$

$y =$	3.75
$z =$	3
$s =$	0.0069

Where y = Distance from upstream invert of spillway riser to top of dewatering volume (ft)
 z = Horizontal component of upstream embankment slope (ft)
 S = Pipe slope ft/ft

$$L_s = \underline{27.00} \text{ ft}$$

2. Determine the required increase in flow path

$$L_F = 1.15 * L_s = \underline{31.04} \text{ ft}$$

3. The minimum collar projection (V) is equal to 1/2 the increase in flow length (for one collar). If more than one collar is used, it is the increase divided by twice the number of collars

Number of collars: 1

$$V_{min} = \underline{2.00} \text{ ft}$$

4. The maximum spacing between collars should be $14 \times V$ or $L_s \div (\text{number of collars minus } 1)$

Minimum spacing should be $5 \times V$

$$V = \underline{1} \text{ ft}$$

Max = 14 ft

Min = 5 ft

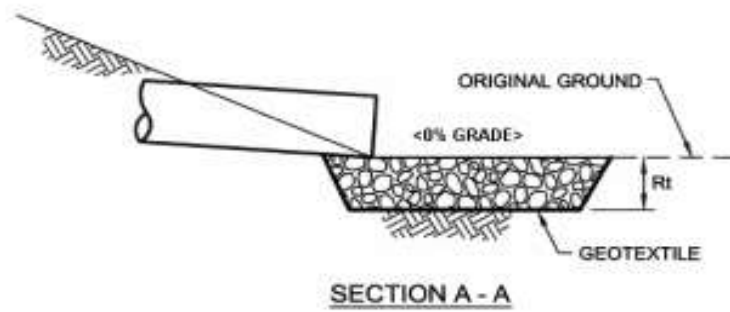
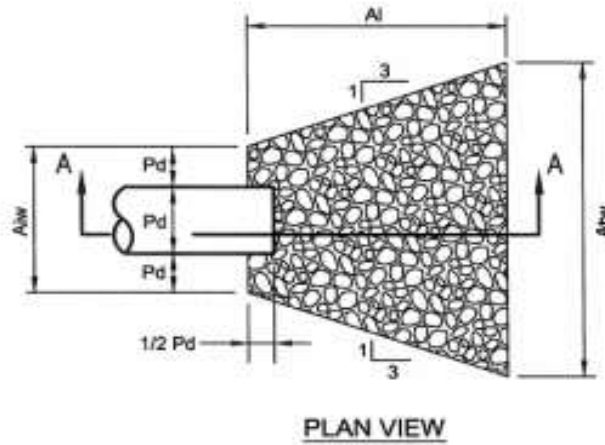
APPENDX H

RIP-RAP DESIGN CALCULATIONS

EROSION AND SEDIMENT POLLUTION CONTROL

**STANDARD E&S WORKSHEET #20
Riprap Apron Outlet Protection**

PROJECT: <u>The Westtown School - Oak Lane Project</u>	JOB #	1091-001
LOCATION: <u>Westtown Township</u>	DATE:	1/16/2023
COUNTY: <u>Chester</u>	REVISED:	10/23/2023
CHECKED BY: 		



NO.	PIPE DIA. Do (in.)	TAIL WATER COND. (Max or Min.)	MAN. "n" FOR PIPE	PIPE SLOPE (%)	Q (CFS)	V* (FPS)	RIPRAP SIZE	Rt (in)	Al (ft)	Aiw (ft)	Atw (ft)
EW-A1	18	Min.	0.012	0.50	13.7	7.75	R-4	18	12	4.50	16.50
EW-A2	18	Min.	0.012	1.00	12.0	6.83	R-4	18	12	4.50	16.50
EW-B1	24	Min.	0.012	0.67	23.7	7.56	R-4	18	14	6.00	20.00
EW-B2	15	Min.	0.012	0.51	4.51	3.73	R-3	9	9	3.75	12.75

*The anticipated velocity (V) should not exceed the maximum permissible shown in Table 6.6 for the proposed riprap protection. Adjust for less than full pipe flow. SEE TABLE 9, March 2000 E&S PROGRAM MANUAL. Use Manning's equation to calculate velocity for pipe slopes > 0.05 ft/ft. velocity for pipe slopes > 0.05 ft/ft.

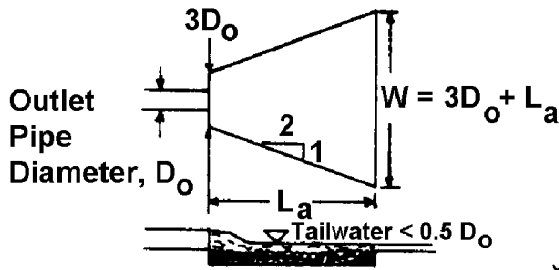
** Based on sediment basin flow through principle spillway

*** See attached Hydraflow Storm Sewers

EW-A1

DESIGN OF RIPRAP APRON OUTLET PROTECTION FROM A ROUND PIPE FLOWING FULL MINIMUM TAILWATER CONDITION ($T_w < 0.5$ DIAMETER)

Adapted from USDA - NRCS



Not to be used for Box Culverts

La = 12 FT

NOTE: Do not extrapolate

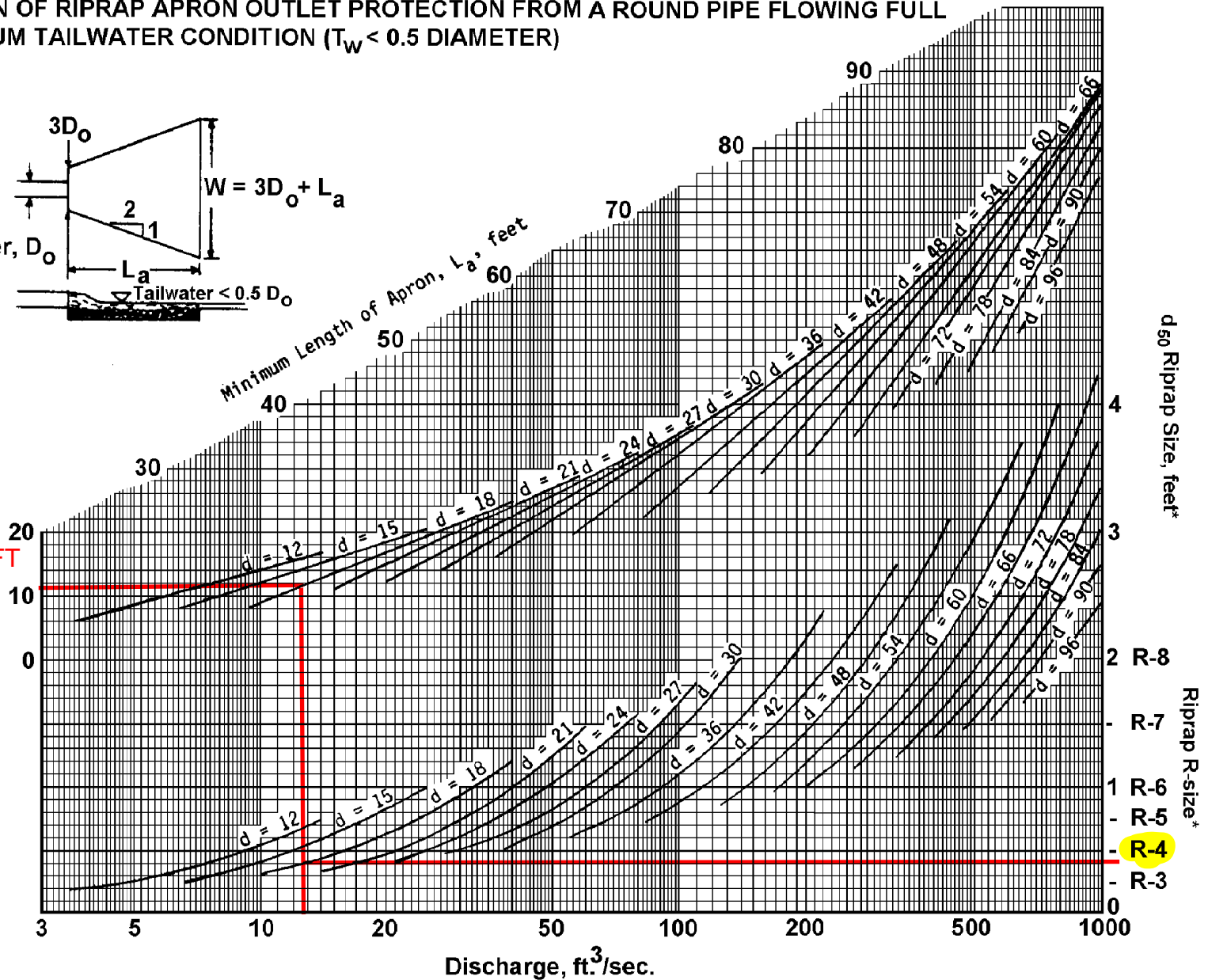


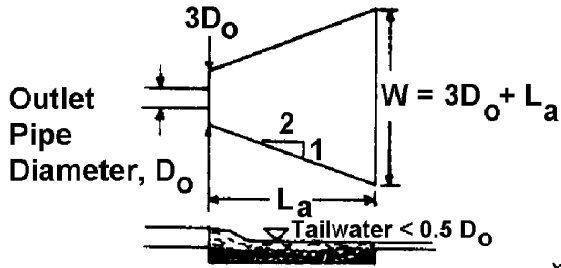
FIGURE 9.3
Riprap Apron Design, Minimum Tailwater Condition

* For discharge velocities exceeding Maximum Allowable for Riprap indicated, increase d_{50} stone size and/or provide velocity reduction device.

EW-A2

DESIGN OF RIPRAP APRON OUTLET PROTECTION FROM A ROUND PIPE FLOWING FULL MINIMUM TAILWATER CONDITION ($T_w < 0.5$ DIAMETER)

Adapted from USDA - NRCS



Not to be used for Box Culverts

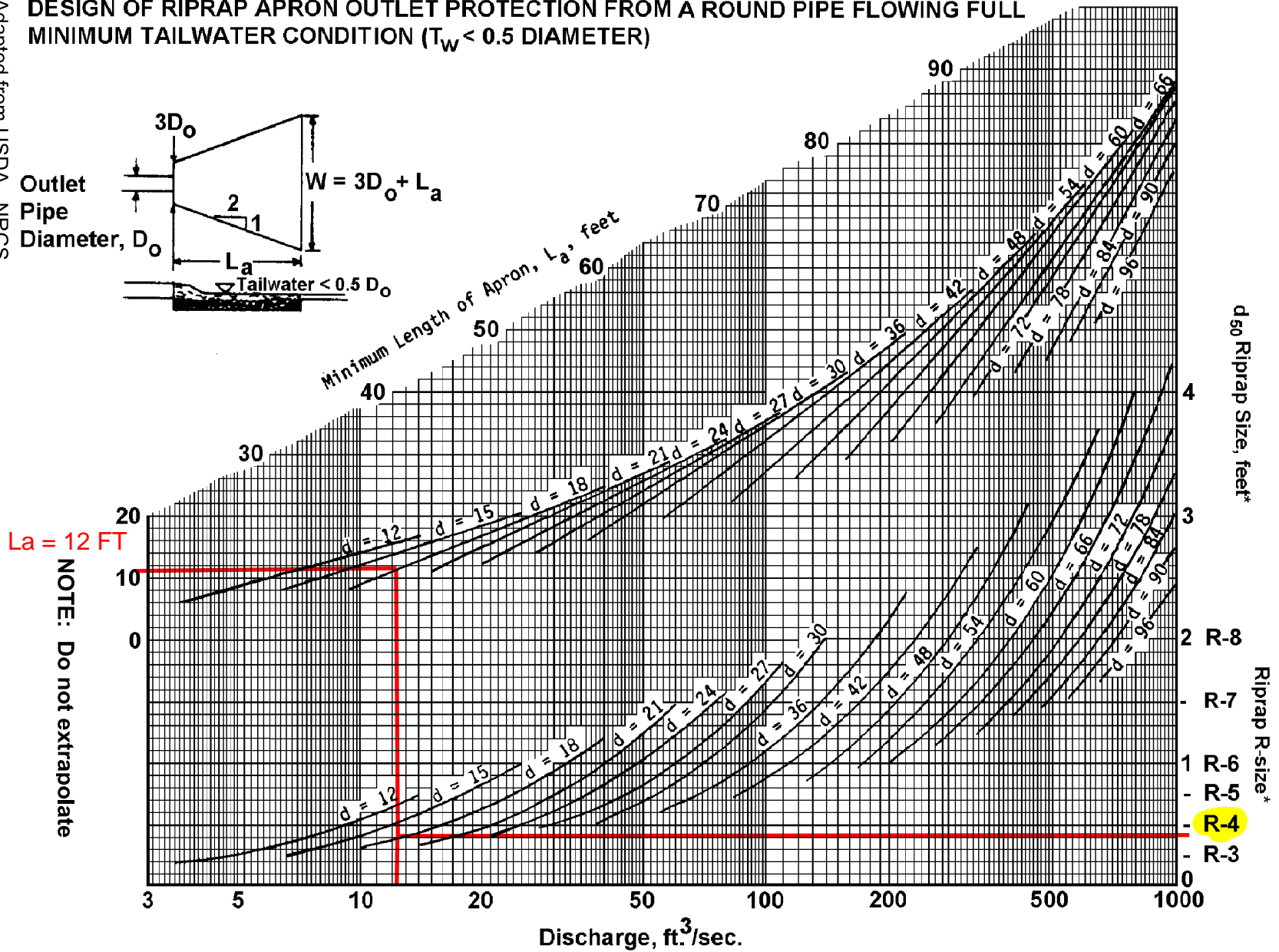


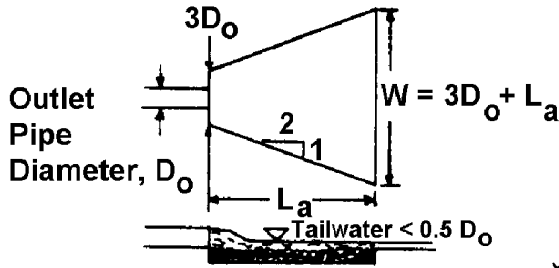
FIGURE 9.3
Riprap Apron Design, Minimum Tailwater Condition

* For discharge velocities exceeding Maximum Allowable for Riprap indicated, increase d_{50} stone size and/or provide velocity reduction device.

EW-B1

DESIGN OF RIPRAP APRON OUTLET PROTECTION FROM A ROUND PIPE FLOWING FULL MINIMUM TAILWATER CONDITION ($T_w < 0.5$ DIAMETER)

Adapted from USDA - NRCS



Not to be used for Box Culverts

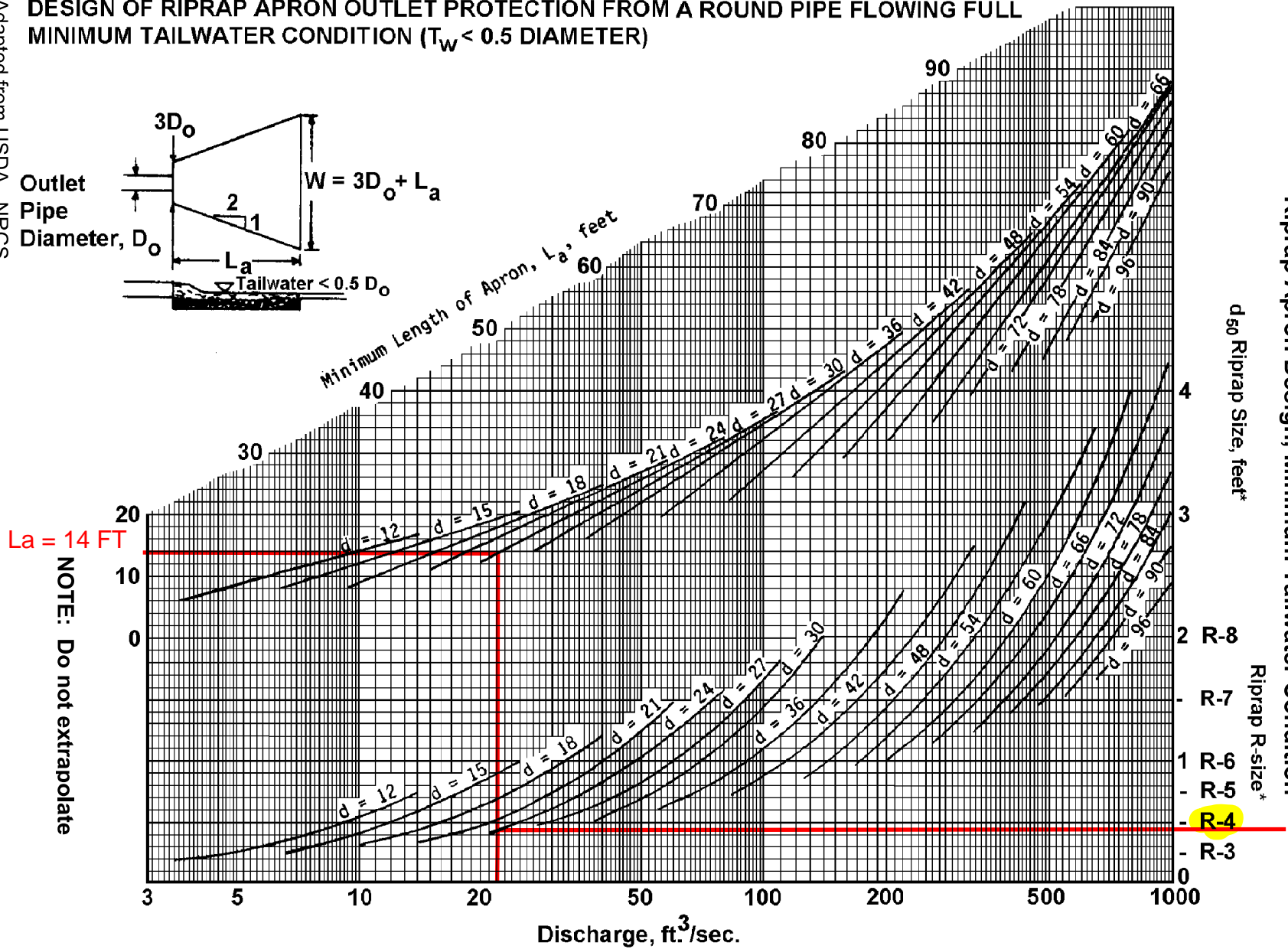


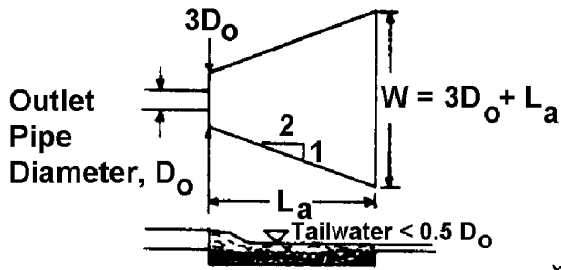
FIGURE 9.3
Riprap Apron Design, Minimum Tailwater Condition

* For discharge velocities exceeding Maximum Allowable for Riprap indicated, increase d_{50} stone size and/or provide velocity reduction device.

EW-B2

DESIGN OF RIPRAP APRON OUTLET PROTECTION FROM A ROUND PIPE FLOWING FULL MINIMUM TAILWATER CONDITION ($T_w < 0.5$ DIAMETER)

Adapted from USDA - NRCS



Not to be used for Box Culverts

La = 9 FT

NOTE: Do not extrapolate

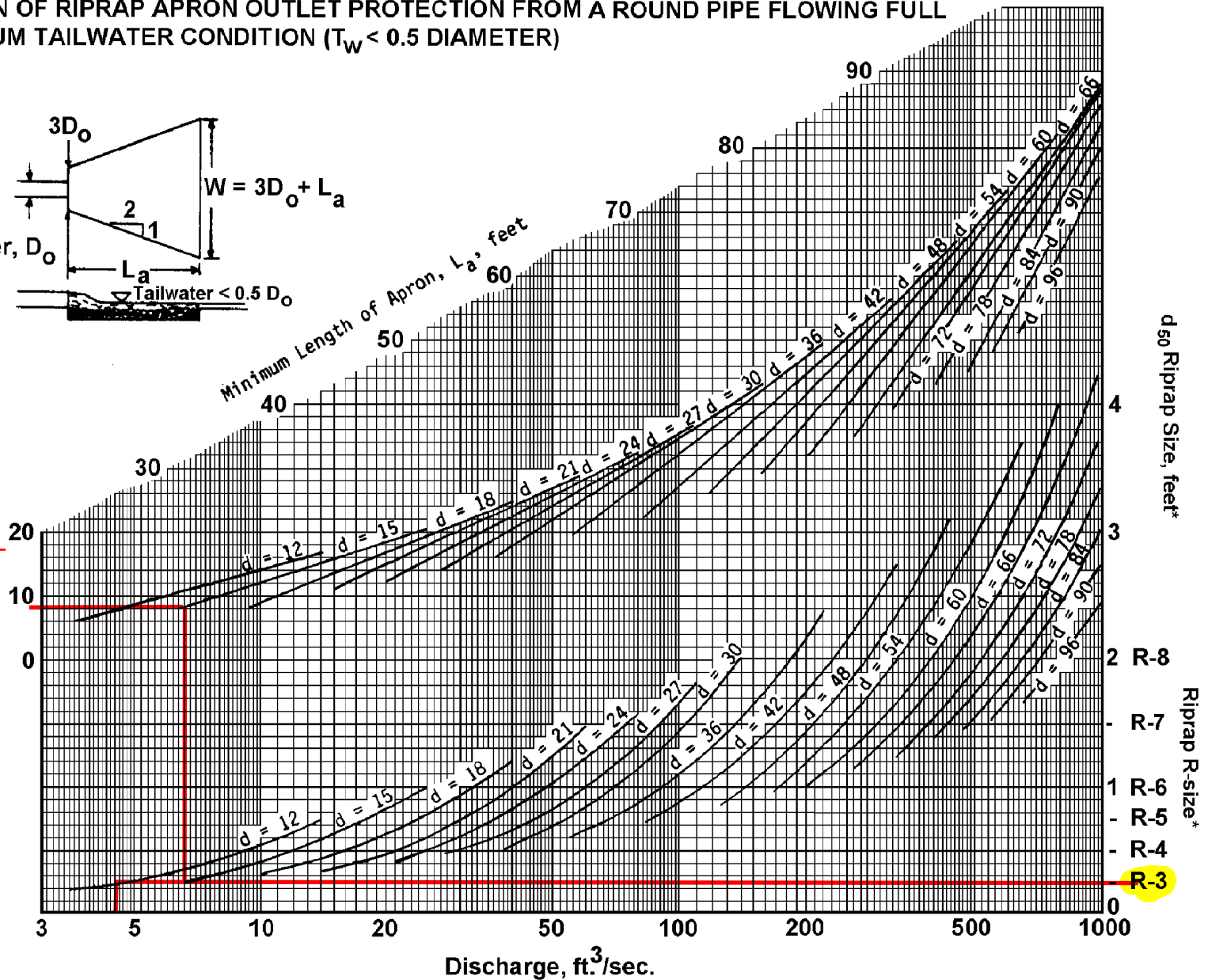


FIGURE 9.3
Riprap Apron Design, Minimum Tailwater Condition

* For discharge velocities exceeding Maximum Allowable for Riprap indicated, increase d_{50} stone size and/or provide velocity reduction device.

Anticipated Velocity Calculation for Less Than Full Pipe Flow

Outfall EW-B2

Full Flow Discharge: $Q_f = \frac{0.464}{n} D^{8/3} S^{1/2} = 5.01 \text{ cfs}$

Continuity Equation to determine full-flow velocity:

$$V_f = \frac{Q_f}{A} = 4.08 \text{ ft/sec}$$

Where: $A = 1.23 = \text{Cross Sectional Area (ft}^2\text{)}$

Ratio of Partial to Full-Flow Discharge:

$$d/D = \frac{Q_d}{Q_f} = 0.899$$

Where: $d/D = 0.90 = \text{Ratio of Part-Full to Full-Flow Discharge}$
 $Q_d = 4.50 = \text{Design Discharge (cfs)}$
 $Q_f = 5.01 = \text{Full-Flow Discharge (cfs)}$
 $D = 1.25 = \text{Diameter (ft)}$
 $S = 0.01 = \text{Slope of pipe (ft/ft)}$
 $n = 0.012 = \text{Mannings Coefficient}$

Velocity Ratio from Figure 9.1: 1.14

Design Velocity $V_d = 4.65 \text{ ft/s}$

EW-B2

CIRCULAR CHANNEL RATIOS

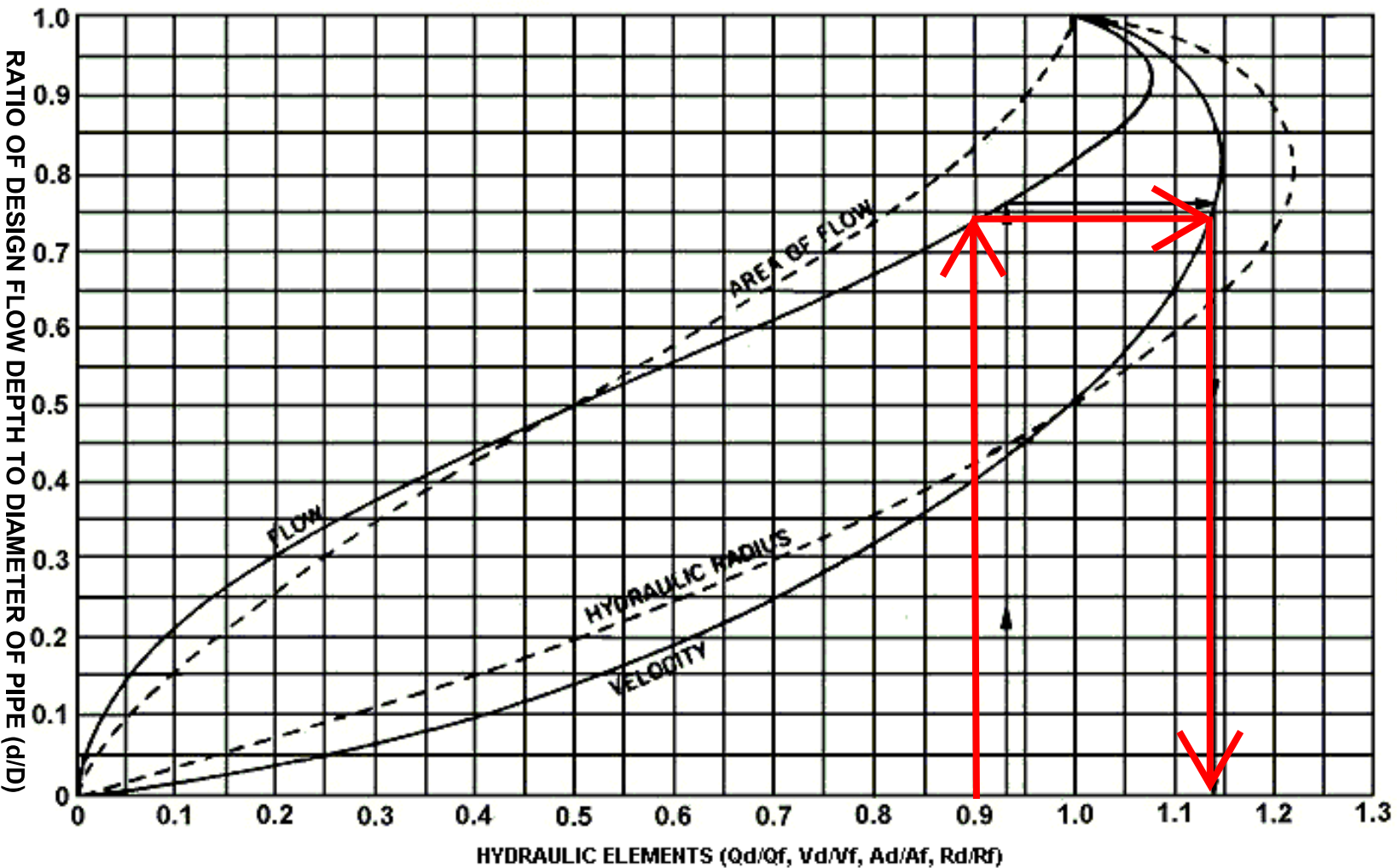


FIGURE 9.1 Velocity Adjustment Nomograph for Less Than Full Pipe Flow

Adapted from *Design and Construction of Sanitary and Storm Sewers*, p. 87, ASCE, 1969

Do not use this nomograph to determine “equivalent pipe sizes” for discharges (Q_d) that do not intersect curves corresponding to proposed pipe sizes on Figures 9.3 and 9.4.

APPENDIX I INFILTRATION REPORTS



October 8, 2018

Westtown School
975 Westtown Road
West Chester, PA 19382

c/o

Mr. Charles R. Haley, Jr., P.E.
ELA Group, Inc.
743 South Broad Street
Lititz, PA 17543

**RE: Stormwater Infiltration Feasibility Report
Westtown School Oak Lane – Infiltration
Westtown Township, Chester County, Pennsylvania
Advantage Project Number: 1800331001**

Dear Mr. Haley:

In accordance with your request, Advantage Engineers (Advantage) has completed an engineering analysis of the above referenced project site in order to evaluate the suitability of the subsurface soils for the infiltration of stormwater. This correspondence serves to transmit the results of our evaluation.

SITE AND PROJECT DESCRIPTION

The project site currently consists of outdoor athletic fields located east of Westtown Road in Westtown Township, Chester County, Pennsylvania. The site is bordered to the east by agricultural land and grass areas, to the south by Westtown School District buildings, to the west by Westtown Road and to the north by Westtown School District and wooded areas. The approximate location of the site in relation to the surrounding area is depicted on the *Topographic Map* (Figure 1) presented within the Appendix.

According to information provided by the Client, the improvements will include 2 synthetic turf multipurpose fields, 2 grass multipurpose fields, a softball field and a baseball field. Development of the site will also include new field lights, an outbuilding and new stormwater management facilities.

SCOPE OF WORK

The objective of our work was to determine the permeability of the invert soils, identify any limiting zones (i.e. bedrock, groundwater, or seasonal high water table) within the proposed stormwater management facilities, and address PADEP requirements as they relate to stormwater management. This objective was accomplished through completion of a scope of work which included the completion of a subsurface field exploration, laboratory testing program and preparation of this report. This report presents a summary of the scope of work completed, conditions encountered, and results of our engineering analysis of subsurface conditions.

SUBSURFACE FIELD EXPLORATION

In order to characterize subsurface conditions across the project site, 13 test pits were excavated on September 26 through 28, 2018. Supervision and monitoring of the field exploration was provided by a representative of Advantage. Test locations were marked out by ELA Group, Inc., based on the "Sketch Plan", dated July 24, 2017, prepared by Site Engineering Concepts, LLC. The approximate test locations, referenced as TP-1 through TP-13, are shown on the *Exploration Plan* (Figure 3) presented within the Appendix. Data pertaining to the subsurface exploration was documented in the field and is presented in detail on the *Test Pit Logs*, which contain detailed descriptions of the subsurface materials encountered and infiltration test depths. A general description of the soil conditions encountered is provided in the "Subsurface Conditions" section of this report.



LABORATORY ANALYSIS

Soil samples retrieved from the site were visually reviewed and classified by Advantage Engineers. Representative soil samples were subjected to laboratory analyses to verify visual classifications in accordance with the following schedule:

- Natural Moisture Content (ASTM D2216)
- Sieve Analysis (ASTM D422)
- Atterberg Limits Determination (ASTM D4318)

Unified Soil Classification System (USCS) Group Symbols and ASTM Group Names has been assigned to the soils analyzed. Graphical depictions of the laboratory testing completed are presented in the table below and within the Appendix.

STANDARD CLASSIFICATION RESULTS											
Location	Depth (ft)	Soil Type	% Gravel	% Sand	% Fines	LL	PL	PI	Natural Moisture Content	USCS Group Symbol	ASTM Group Name
TP-2	3	Stratum I	7.2	54.4	38.4	36	33	3	21.9%	SM	Silty SAND
TP-5	4 – 6		45.6	42.5	11.9	36	35	1	10.7%	GP-GM	Poorly Graded GRAVEL with Silt and Sand

LL-Liquid Limit; PL-Plastic Limit; PI-Plasticity Index

SUBSURFACE CONDITIONS

Geology

According to the Pennsylvania Geologic Survey's, Geologic Map of the State of Pennsylvania, 1980, the project site is underlain by politic schist of the Glenarm Wissahickon Formation (Geologic Symbol Xgw). This formation includes lenticular amphibolites bodies having ocean-floor basalt chemistry. The project site within its geologic setting is presented on the *Geologic Map* (Figure 2) found within the Appendix.

The Pennsylvania Geologic Survey publication, The Engineering Characteristics of the Rocks of Pennsylvania, Second Edition, 1982, describes the bedding in this formation as well developed, thin to fissile, and steeply dipping. Joints in this formation have an irregular pattern, are poorly formed, widely spaced, steeply dipping, and open. The schist of this formation is moderately resistant to weathering, and often weathers to a moderate depth. The resulting soil mantle is thin.

Soil

Surficial Materials

Each test pit was covered by approximately 6 to 28 inches of topsoil or tilled soil; however, the thickness of surficial materials may differ in unexplored areas of the project site.

Stratum I – Brown to gray Silty SAND and GRAVEL with Silt and Sand

Stratum I was encountered within each test pit completed except for TP-12 and TP-13 and extended to depths ranging from approximately 4.5 to 10 feet below existing site grades. Laboratory testing conducted on representative samples of Stratum I show this soil to be well graded and non-plastic with natural moisture contents of 21.9% and 10.7%. Stratum I is described under the USCS as Silty SAND (SM) and Poorly Graded GRAVEL with Silt and Sand (GP-GM).



Stratum II – Brown Silty SAND with Gravel (highly weathered rock)

Stratum II was encountered within test pits TP-10 and TP-11 and extended to depths of approximately 7.5 and 9.5 feet, respectively, below existing site grades. Upon review, the soils of Stratum II were found to be well graded, non-plastic and predominately comprised of Silty SAND with Gravel. The soils of Stratum II are anticipated to represent the highly weathered bedrock surface.

Stratum III – Orange brown to blue gray Sandy CLAY

Stratum III was encountered within test pits TP-12 and TP-13 and extended to depths of approximately 6 feet below existing site grades. Upon review, the soils of Stratum III were found to be moderately graded, plastic and comprised of Sandy CLAY.

Bedrock

The bedrock surface was encountered within test pits TP-10 and TP-11 at depths of approximately 7.5 and 9.5 feet below existing site grades, respectively. The bedrock surface was defined as the depth at which the bucket of the given excavation equipment could no longer excavate. Other equipment may yield different bedrock data.

Groundwater/Soil Mottling

Groundwater was encountered within test pits TP-7, TP-8, TP-12 and TP-13 at depths ranging from approximately 1.5 to 6 feet below existing site grades. Additionally, soil mottling (indication of seasonal high water table and/or poorly draining soils) was encountered within test pits TP-12 and IT-13, starting at a depth of approximately 2.5 feet below existing site grades and extending to 6 feet below existing site grades. It should be noted that standing water was observed at several areas including the agricultural field located in the eastern portion of the site and the portion of the site located north of Oak Lane. These observations were made at the time of the field operation and the groundwater table elevation will vary with daily, seasonal, and climatological variations.

INFILTRATION ANALYSIS

To evaluate the feasibility of infiltration of stormwater within the proposed stormwater management facilities, infiltration tests were completed utilizing the “double-ring” infiltrometer method in accordance with the Pennsylvania Stormwater Best Management Practices Manual, latest Edition. Based on the topsoil thickness encountered within test pit TP-4, the infiltration test was completed below the proposed test elevation. Based on the limiting zone encountered (groundwater and/or soil mottling) within test pits TP-8, TP-12 and TP-13, no infiltration tests were able to be completed. Based on the limiting zones encountered (groundwater/bedrock) within TP- 7, TP-10 and TP-11, the infiltration tests were completed above the proposed test elevations. The test pit locations, approximate surface elevation, proposed test elevation, actual test elevation(s), presence of limiting zones, and the infiltration rate(s) achieved at each location are presented in the table below.



INFILTRATION TEST RESULTS					
Test Location	Surface Elevation (ft)	Proposed Test Elevations (ft)	Actual Test Elevations (FT)	Limiting Zone Elevation (ft)	Infiltration Rate* (in/hr)
TP-1	319.5	316	316	Not Encountered @ 312	1.8
		314	314		6.0
TP-2	317	316	316	Not Encountered @ 312	0.0
		314	314		1.4
TP-3	321	317.5	317.5	Not Encountered @ 313.5	6.0
		315.5	315.5		12.0
TP-4	319.5	319	318.5	Not Encountered @ 315	1.2
		317	317		1.0
TP-5	321	319.5	319.5	Not Encountered @ 315	3.4
		317	317		4.8
TP-6	311	309	309	Not Encountered @ 305	1.0
		307	307		0.0
TP-7	313	309	311	Groundwater @ 307	0.0
		307	309		2.8
TP-8	311	309	No Test	Groundwater @ 309.5	No Test
		307	No Test		No Test
TP-9	303	292.5	295	Not Encountered @ 293	3.9
		291	295		4.0
TP-10	305	299	301	Bedrock @ 297.5	2.8
		297	299.5		4.8
TP-11	309	303	303	Bedrock @ 299.5	6.0
		301	301.5		5.4
TP-12	298	296	No Test	Soil Mottling @ 295.5-292 Groundwater @ 294.5	No Test
		294	No Test		No Test
TP-13	286	284	No Test	Groundwater @ 284.5 Soil Mottling @ 283.5-280	No Test
		282	No Test		No Test

*Infiltration rates represent the rates recorded in the field and no safety factor has been applied

-Shaded cells represent infiltration tests completed above or below proposed invert due to a limiting zone or topsoil thickness

-Bold cells indicate infiltration testing completed at shallower depths due to safety concerns

SUMMARY OF DATA & CONCLUSIONS

Based on the results of our field exploration and engineering analysis of the data obtained, we offer the following comments with regard to the infiltration of stormwater at the project site.

- The infiltration tests were conducted within the well graded, non-plastic, naturally-occurring soils of Stratum I and Stratum II.
- Groundwater was encountered within test pits TP-7, TP-8, TP-12 and TP-13 at depths ranging from approximately 1.5 to 6 feet below existing site grades.
- Soil mottling was encountered within test pits TP-12 and IT-13, starting at depths of approximately 2.5 feet below existing site grades and extending to 6 feet below existing site grades.



- The bedrock surface was encountered within test pits TP-10 and TP-11 at depths of approximately 7.5 and 9.5 feet below existing site grades, respectively
- Infiltration rates were found to range from no movement (0.0 inches per hour) to 12.0 inches per hour. These rates are unfactored. The PADEP recommended rate for infiltration of stormwater is 0.1 to 10 inches per hour.

LIMITATIONS

The conclusions contained in this report are based upon the subsurface data collected and on details stated in this report. Should conditions arise which differ from those specifically stated herein, our office should be notified immediately, so that our recommendations can be reviewed and revised, if necessary.

The conclusions presented herein should be applied only to the infiltration tests as depicted on the *Exploration Plan* for the proposed stormwater management facilities to be constructed for Westtown School in Westtown Township, Chester County, Pennsylvania. Advantage takes no responsibility in utilizing this information for any other purposes.

The scope of work was limited to the exploration of the subsurface soils. Oil, hazardous waste, radioactivity, irritants, pollutants, radon or other dangerous substances and conditions were not the subject of this study. Their presence and/or absence are not implied, inferred or suggested by this report or results of this study.

We trust that this is the information you require. Should you have any questions or if we may be of further assistance, please don't hesitate to contact our office.

Respectfully,
advantage engineers

A handwritten signature in black ink that reads "Bailey Jean Wildasin".

Bailey J. Wildasin
Geotechnical Specialist I

A handwritten signature in black ink that reads "David J. Buckwalter".

David J. Buckwalter
Senior Project Manager



APPENDIX

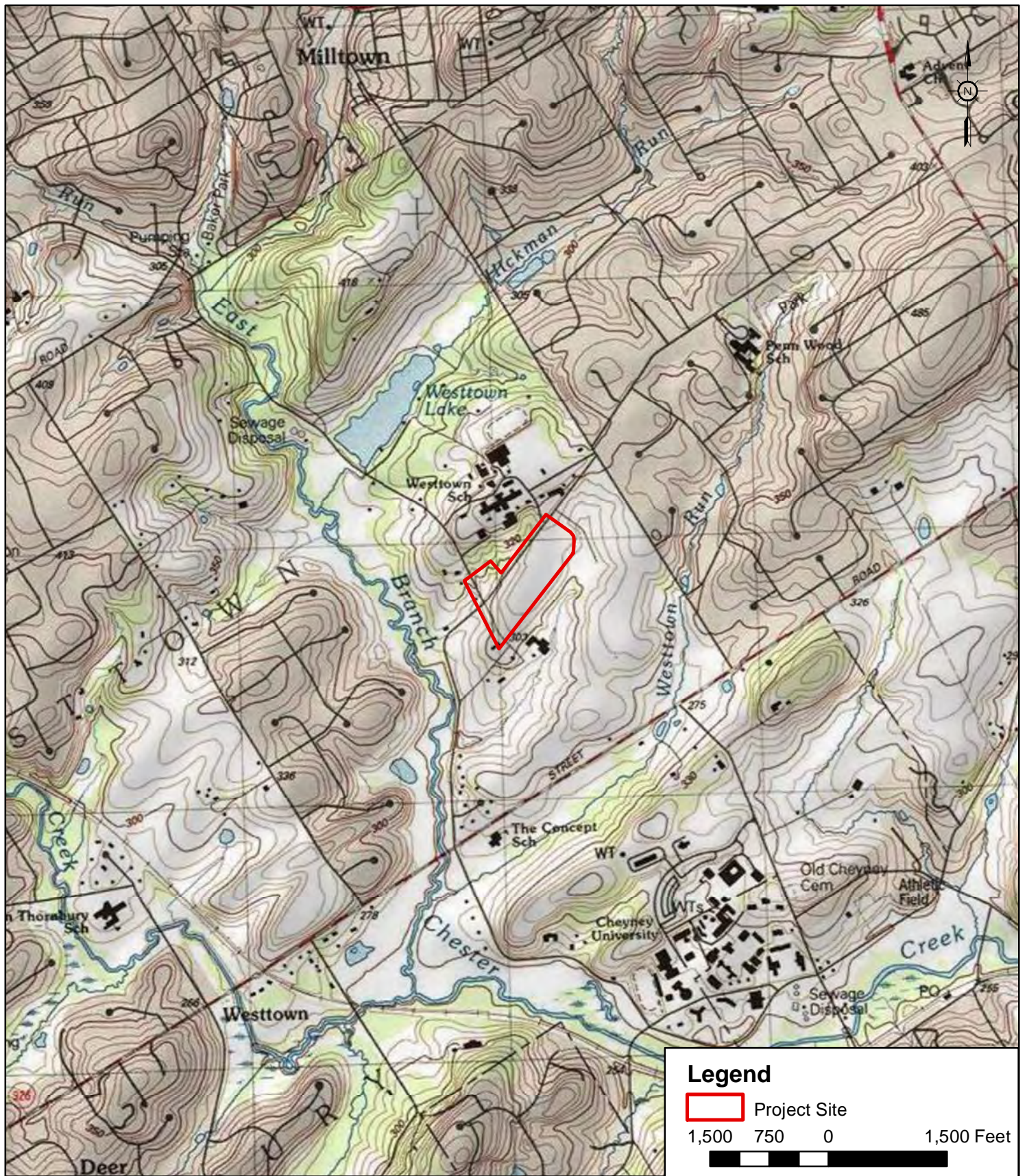
FIGURE 1 – TOPOGRAPHIC MAP

FIGURE 2 – GEOLOGIC MAP

FIGURE 3 – EXPLORATION PLAN

LABORATORY TEST RESULTS

TEST PIT LOGS



Service Layer Credits: Copyright:© 2013 National Geographic Society, i-cubed

SCALE: AS SHOWN	DRAWING NUMBER: FIGURE 1
DRAWN BY: B. WILDASIN	CHECKED BY: D. BUCKWALTER
APPROVED BY: M. GIUNTA	DATE: 9-10-2018

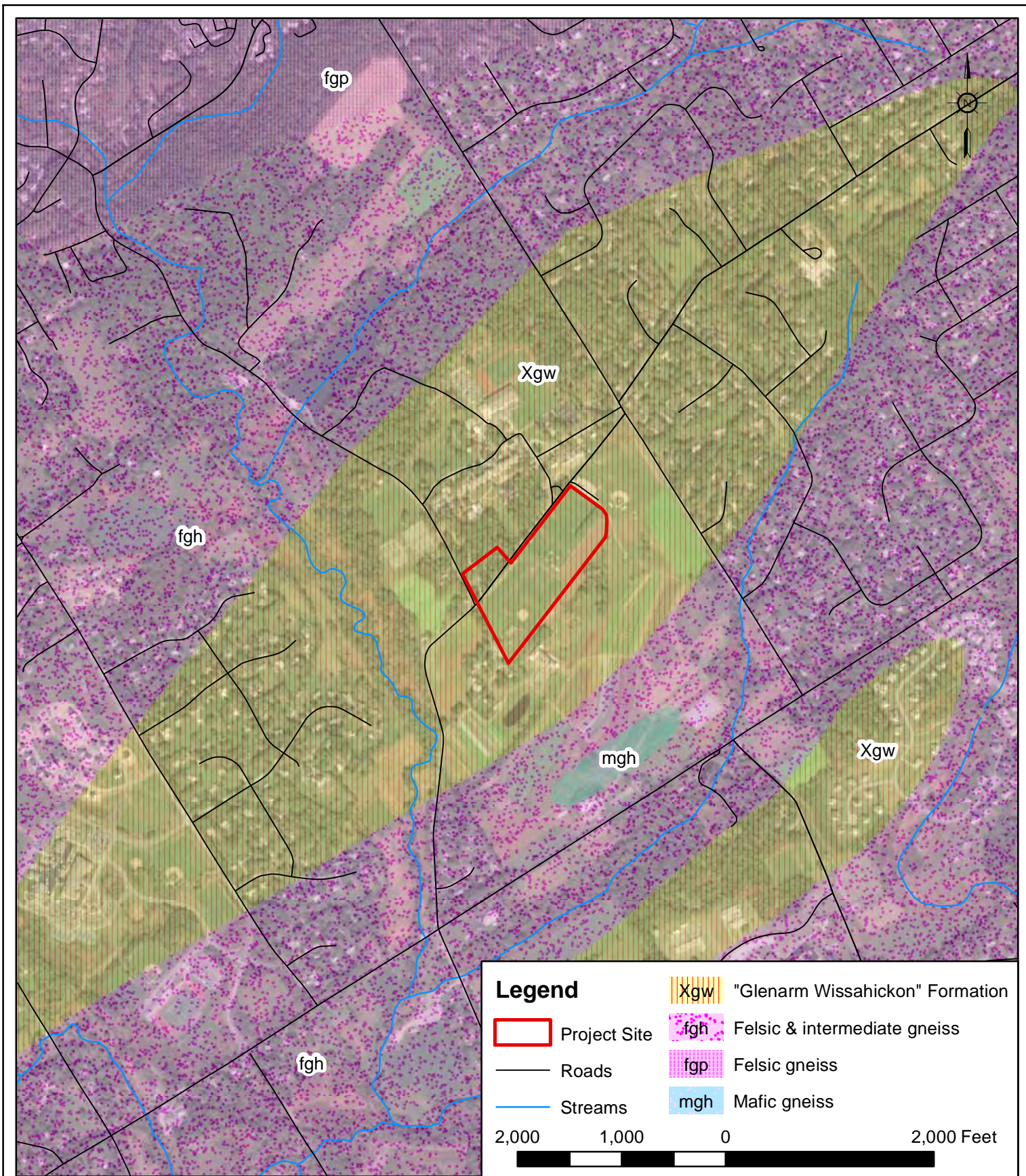
TOPOGRAPHIC MAP
PREPARED FOR
WESTTOWN SCHOOL OAK LANE - INFILTRATION

WESTTOWN TOWNSHIP CHESTER COUNTY PENNSYLVANIA



advantage engineers

435 INDEPENDENCE AVE., SUITE C
MECHANICSBURG, PA 17055
PH (717) 458-0800
FAX (717) 458-0801
221



Legend

- Project Site
- Roads
- Streams
- "Glenarm Wissahickon" Formation
- fgh Felsic & intermediate gneiss
- fgp Felsic gneiss
- mgh Mafic gneiss

2,000 1,000 0 2,000 Feet

*Source - Map 61 - Atlas of Preliminary Geologic Quadrangle Maps of Pennsylvania, 1981, Pa Geological Survey

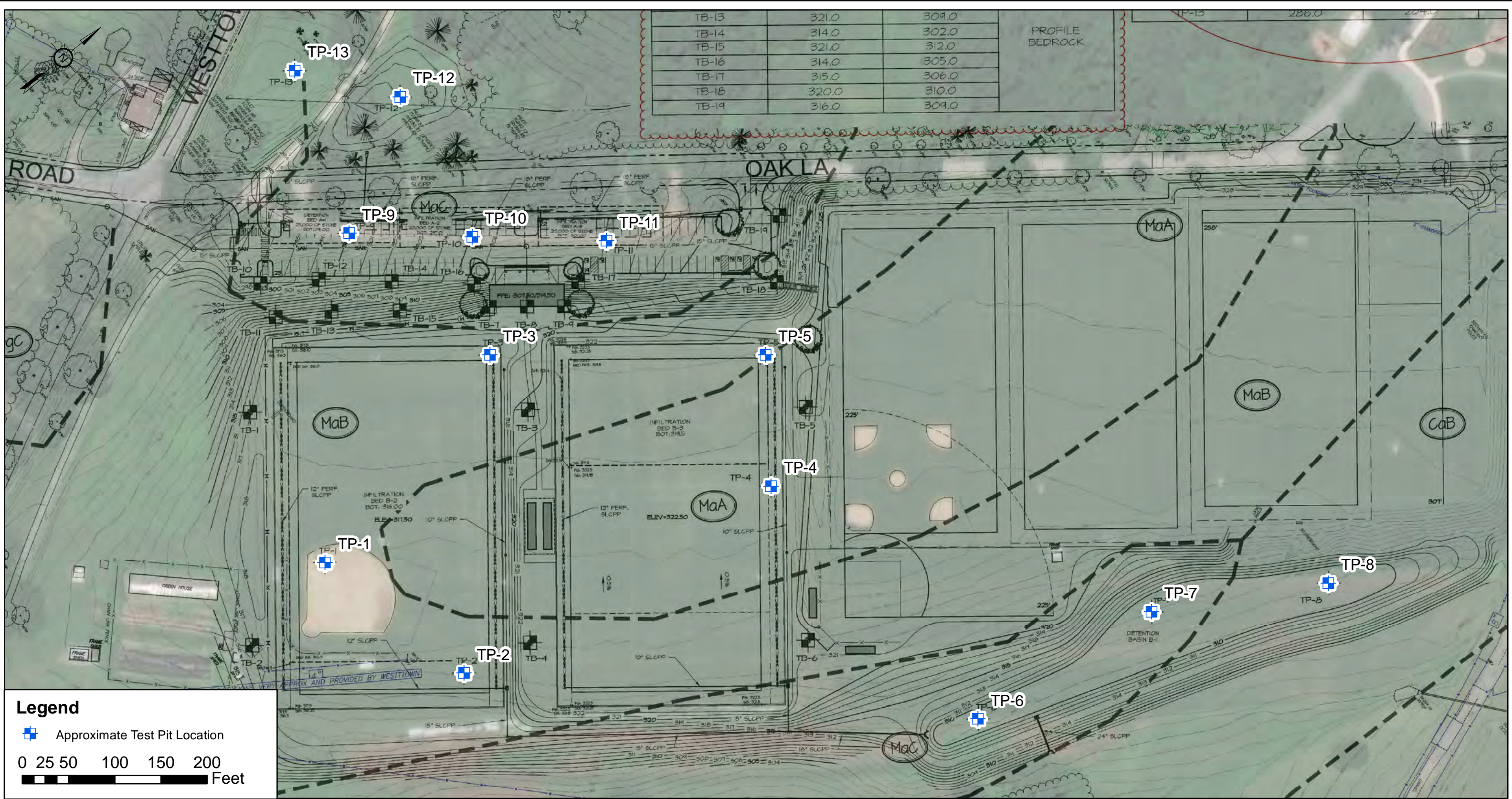
SCALE: AS SHOWN	DRAWING NUMBER: FIGURE 2
DRAWN BY: B. WILDASIN	CHECKED BY: D. BUCKWALTER
APPROVED BY: M. GIUNTA	DATE: 9-10-2018

GEOLOGIC MAP
PREPARED FOR
WESTTOWN SCHOOL OAK LANE - INFILTRATION

WESTTOWN TOWNSHIP CHESTER COUNTY PENNSYLVANIA

advantage engineers

435 INDEPENDENCE AVE., SUITE C
MECHANICSBURG, PA 17055
PH (717) 458-0800
FAX (717) 458-0801
222



TB-13	321.0	309.0
TB-14	314.0	302.0
TB-15	321.0	312.0
TB-16	314.0	305.0
TB-17	315.0	306.0
TB-18	320.0	310.0
TB-19	316.0	309.0

PROFILE
BEDROCK

Legend

Approximate Test Pit Location

0 25 50 100 150 200 Feet

Service Layer Credits: Source: Esri, DigitalGlobe, GeoEye, i-cubed, USDA, USGS, AEX, Getmapping, Aerogrid, IGN, IGP, swisstopo, and the GIS User Community

SCALE: AS SHOWN	DRAWING NUMBER: FIGURE 3
DRAWN BY: B. WILDASIN	CHECKED BY: D. BUCKWALTER
APPROVED BY: M. GIUNTA	DATE: 9-10-2018

BASE PLAN: Sketch Plan
PROVIDED BY: Site Engineering Concepts, LLC
DATE: 7-24-2017

EXPLORATION PLAN
PREPARED FOR
WESTTOWN SCHOOL OAK LANE - INFILTRATION

WESTTOWN TOWNSHIP CHESTER COUNTY PENNSYLVANIA

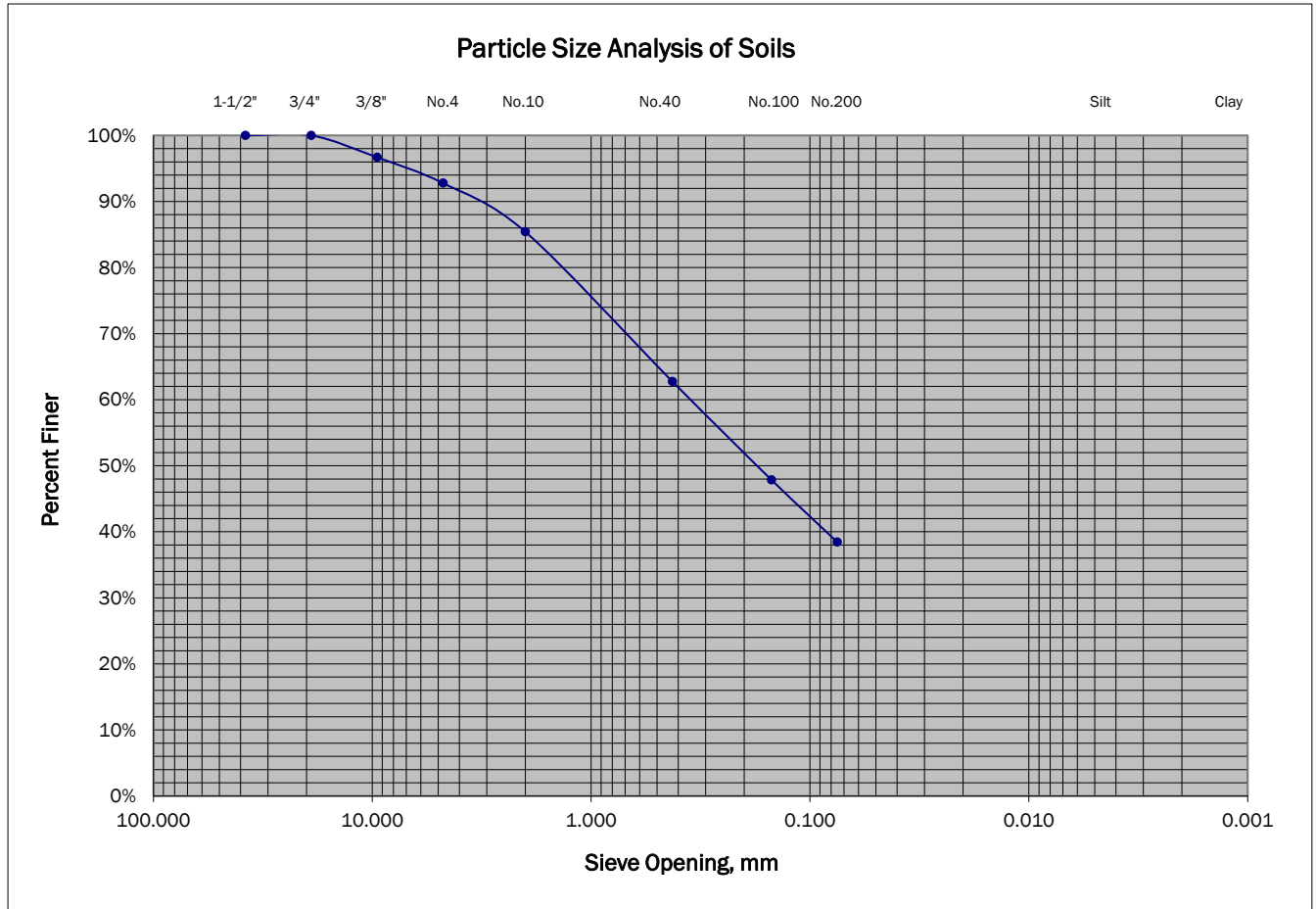


advantage engineers

435 INDEPENDENCE AVE., SUITE C
MECHANICSBURG, PA 17055
PH (717) 458-0800
FAX (717) 458-0801 223

Soil Classification Report

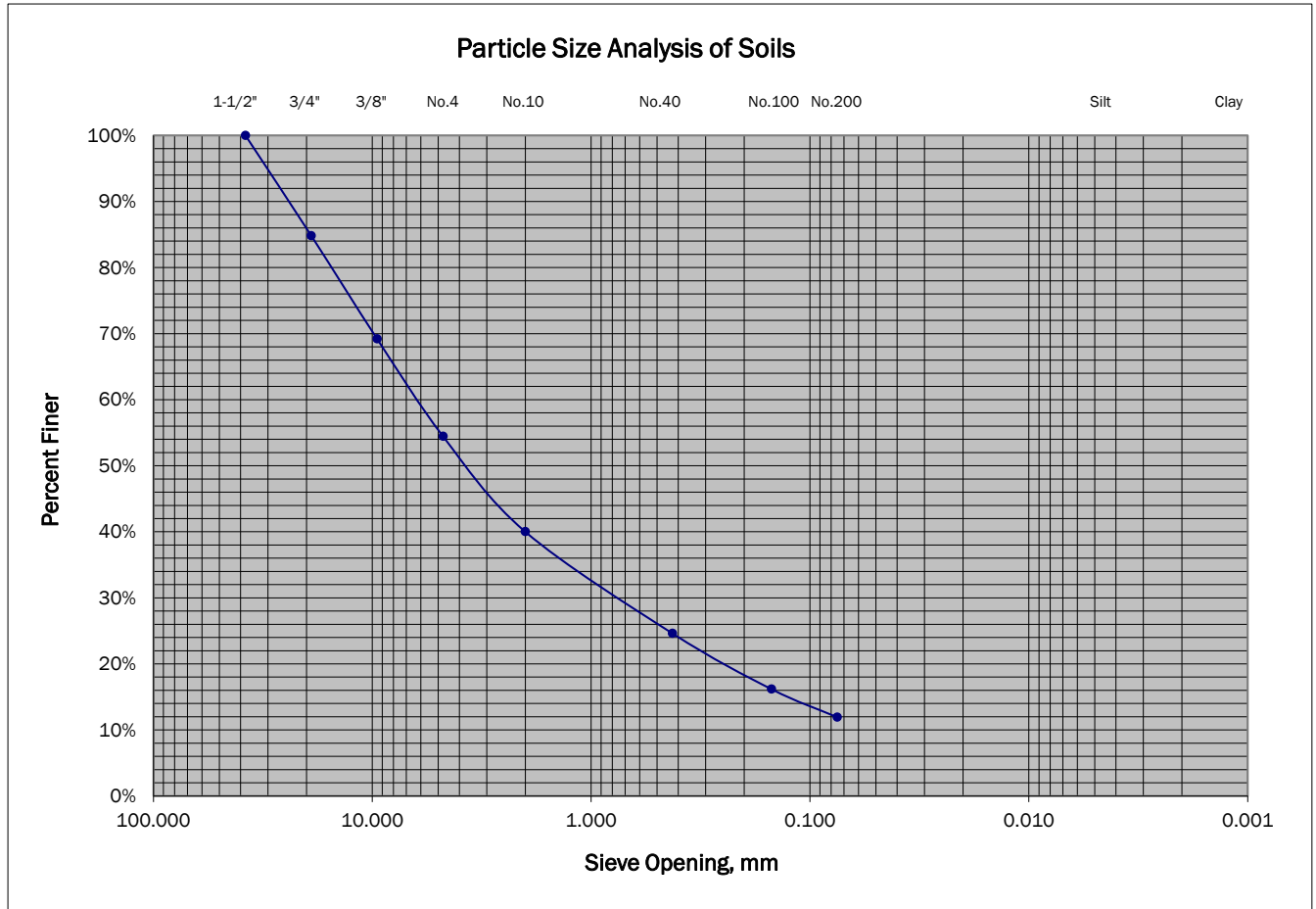
Per ASTM Designations D 2487 and D 2488



As-Received Moisture 21.9%		Particle Size Distribution					
USCS Classification: Silty SAND (SM)		US Standard Sieve Size		Opening (mm)	%Finer		
Gravel: 7.2%	Coarse: 0.0%	Fine: 7.2%		GRAVEL	Coarse		
Sand: 54.4%	Coarse: 7.4%	Medium: 22.7%	Fine: 24.3%		1-1/2"	38.0	100.0%
Fines: 38.4%	Silt:	Clay:			3/4"	19.0	100.0%
Gravel Description: Subangular to Subrounded		No. 4		4.75	92.8%		
Sand Description: Subangular		No. 10		2.00	85.4%		
Consistency: N/A		Dry Strength: Low		No. 40		0.425	62.7%
Dilatancy: Rapid		Toughness: Low		No. 100		0.150	47.9%
Structure: Homogeneous		Cementation: N/A		No. 200		0.075	38.4%
		Hydrometer Analysis		Silt Size		0.005	
				Clay Size		0.001	
		D ₆₀ :		D ₃₀ :	D ₁₀ :	Cu:	Cc:
Test Pit: TP-2		Atterberg Limits		LL: 36	PL: 33	PI: 3	
Sample: S1		Depth: 3'		Description: Brown Silty SAND			
Project: Westtown School Oak Lane - Infiltration		Remarks: Stratum I					
Client: ELA Group, Inc.							
Advantage Project Number: 1800331001		Report Date: October 4, 2018					

Soil Classification Report

Per ASTM Designations D 2487 and D 2488



As-Received Moisture 10.7%		Particle Size Distribution							
USCS Classification: Poorly Graded GRAVEL with Silt and Sand (GP-GM)		US Standard Sieve Size		Opening (mm)	%Finer				
Gravel: 45.6%	Coarse: 15.2%	Fine: 30.4%		GRAVEL	Coarse	1-1/2"	38.0	100.0%	
Sand: 42.5%	Coarse: 14.4%	Medium: 15.4%	Fine: 12.7%		Fine	3/4"	19.0	84.8%	
Fines: 11.9%	Silt:	Clay:				3/8"	9.50	69.2%	
Gravel Description: Subangular						No. 4	4.75	54.4%	
Sand Description: Subangular				SAND	Coarse	No. 10	2.00	40.0%	
Consistency: N/A	Dry Strength: Low				Medium	No. 40	0.425	24.6%	
Dilatancy: Rapid	Toughness: Low				Fine	No. 100	0.150	16.2%	
Structure: Homogeneous	Cementation: N/A					No. 200	0.075	11.9%	
				Hydrometer Analysis	Silt Size	0.005			
					Clay Size	0.001			
				D ₆₀ : 6.3	D ₃₀ : 0.75	D ₁₀ : 0.57	Cu: 11	Cc: 0.16	
Test Pit: TP-5			Atterberg Limits		LL: 36	PL: 35	PI: 1		
Sample: S1	Depth: 4' - 6'		Description:		Brown GRAVEL with Silt and Sand				
Project: Westtown School Oak Lane - Infiltration				Remarks:		Stratum I			
Client: ELA Group, Inc.									
Advantage Project Number: 1800331001				Report Date:		October 4, 2018			

TEST PIT LOG

PROJECT NAME: Westtown School Oak Lane - Infiltration

TEST PIT NO.: TP-1

PROJECT NO.: 1800331001 CLIENT: ELA Group, Inc.

TOP OF GROUND: ±319.5'

LOCATION: See Exploration Plan (Figure 3)

GROUNDWATER DATA: Dry

FIELD SURVEYED

TOPO ESTIMATE

DEPTH: Not Encountered Time: Completion

DEPTH (feet)	SOIL DESCRIPTION	REMARKS			
	0.0' - 0.5' Tan Clayey SAND	Baseball Infield			
	0.5' - 7.5' Brown Silty SAND				
5					
	Brown Silty SAND with Gravel				
	-End of Test Pit at 7.5 Feet-				
10	Infiltration Tests Conducted at 3.5 Feet (316') and 5.5 Feet (314')				
	Stratum I				
15					
	DOUBLE RING INFILTRMETER DATA				
	Test Depth:	3.5'	5.5'		
		Time (min)	Drop (inches')	Time (min)	Drop (inches)
20	Pre-soak 1	30	1.7	30	5.0
	Pre-soak 2	30	1.2	30	5.0
	Reading 1	30	1.0	10	1.0
	Reading 2	30	0.8	10	1.0
	Reading 3	30	0.8	10	1.0
25	Reading 4	30	1.0	10	1.0
	Reading 5			10	1.0
	Reading 6			10	1.0
	Reading 7				
	Reading 8				
30	Average Rate (inches per hour)		1.8		6.0



435 Independence Avenue, Suite C, Mechanicsburg, PA 17055
 Office: (717) 458-0800 Fax: (717) 458-0801
 www.advantageengineers.com

EXCAVATION METHOD: Mini-excavator
 ADVANTAGE REPRESENTATIVE: B. Wildasin
 DATE EXCAVATED: September 27, 2018
 DRAWN/COMPILED BY: B. Wildasin

TEST PIT LOG

PROJECT NAME: Westtown School Oak Lane - Infiltration

TEST PIT NO.: TP-2

PROJECT NO.: 1800331001 CLIENT: ELA Group, Inc.

TOP OF GROUND: ±317'

LOCATION: See Exploration Plan (Figure 3)

GROUNDWATER DATA: Dry

FIELD SURVEYED

TOPO ESTIMATE

DEPTH: Not Encountered Time: Completion

DEPTH (feet)	SOIL DESCRIPTION	REMARKS																																																								
	0.0' - 0.8' Brown organic soil	Topsoil																																																								
	0.8' - 5.0' Brown Sandy SILT Brown Silty SAND																																																									
5		Stratum I																																																								
	-End of Test Pit at 5 Feet-																																																									
10	Infiltration Tests Conducted at 1 Foot (316') and 3 Feet (314')																																																									
	<table border="1" style="margin: auto; border-collapse: collapse;"> <thead> <tr> <th colspan="4" style="text-align: center;">DOUBLE RING INFILTROMETER DATA</th> </tr> <tr> <th style="text-align: center;">Test Depth:</th> <th colspan="2" style="text-align: center;">1'</th> <th style="text-align: center;">3'</th> </tr> <tr> <th></th> <th style="text-align: center;">Time (min)</th> <th style="text-align: center;">Drop (inches)</th> <th style="text-align: center;">Drop (inches)</th> </tr> </thead> <tbody> <tr> <td style="text-align: center;">Pre-soak 1</td> <td style="text-align: center;">30</td> <td style="text-align: center;">no movement</td> <td style="text-align: center;">1</td> </tr> <tr> <td style="text-align: center;">Pre-soak 2</td> <td style="text-align: center;">30</td> <td style="text-align: center;">no movement</td> <td style="text-align: center;">0.7</td> </tr> <tr> <td style="text-align: center;">Reading 1</td> <td style="text-align: center;">30</td> <td style="text-align: center;">no movement</td> <td style="text-align: center;">0.8</td> </tr> <tr> <td style="text-align: center;">Reading 2</td> <td style="text-align: center;">30</td> <td style="text-align: center;">no movement</td> <td style="text-align: center;">0.8</td> </tr> <tr> <td style="text-align: center;">Reading 3</td> <td style="text-align: center;">30</td> <td style="text-align: center;">no movement</td> <td style="text-align: center;">0.6</td> </tr> <tr> <td style="text-align: center;">Reading 4</td> <td style="text-align: center;">30</td> <td style="text-align: center;">no movement</td> <td style="text-align: center;">0.6</td> </tr> <tr> <td style="text-align: center;">Reading 5</td> <td></td> <td></td> <td></td> </tr> <tr> <td style="text-align: center;">Reading 6</td> <td></td> <td></td> <td></td> </tr> <tr> <td style="text-align: center;">Reading 7</td> <td></td> <td></td> <td></td> </tr> <tr> <td style="text-align: center;">Reading 8</td> <td></td> <td></td> <td></td> </tr> <tr> <td colspan="2" style="text-align: center;">Average Rate (inches per hour)</td> <td style="text-align: center;">0.0 (no movement)</td> <td style="text-align: center;">1.4</td> </tr> </tbody> </table>		DOUBLE RING INFILTROMETER DATA				Test Depth:	1'		3'		Time (min)	Drop (inches)	Drop (inches)	Pre-soak 1	30	no movement	1	Pre-soak 2	30	no movement	0.7	Reading 1	30	no movement	0.8	Reading 2	30	no movement	0.8	Reading 3	30	no movement	0.6	Reading 4	30	no movement	0.6	Reading 5				Reading 6				Reading 7				Reading 8				Average Rate (inches per hour)		0.0 (no movement)	1.4
DOUBLE RING INFILTROMETER DATA																																																										
Test Depth:	1'		3'																																																							
	Time (min)	Drop (inches)	Drop (inches)																																																							
Pre-soak 1	30	no movement	1																																																							
Pre-soak 2	30	no movement	0.7																																																							
Reading 1	30	no movement	0.8																																																							
Reading 2	30	no movement	0.8																																																							
Reading 3	30	no movement	0.6																																																							
Reading 4	30	no movement	0.6																																																							
Reading 5																																																										
Reading 6																																																										
Reading 7																																																										
Reading 8																																																										
Average Rate (inches per hour)		0.0 (no movement)	1.4																																																							
15																																																										
20																																																										
25																																																										
30																																																										



advantage engineers

435 Independence Avenue, Suite C, Mechanicsburg, PA 17055
 Office: (717) 458-0800 Fax: (717) 458-0801
 www.advantageengineers.com

EXCAVATION METHOD: Mini-excavator

ADVANTAGE REPRESENTATIVE: B. Wildasin

DATE EXCAVATED: September 27, 2018

DRAWN/COMPILED BY: B. Wildasin

TEST PIT LOG

PROJECT NAME: Westtown School Oak Lane - Infiltration

TEST PIT NO.: TP-3

PROJECT NO.: 1800331001 CLIENT: ELA Group, Inc.

TOP OF GROUND: ±321'

LOCATION: See Exploration Plan (Figure 3)

GROUNDWATER DATA: Dry

FIELD SURVEYED

TOPO ESTIMATE

DEPTH: Not Encountered Time: Completion

DEPTH (feet)	SOIL DESCRIPTION	REMARKS																																																								
	0.0' - 0.8' Brown organic soil	Topsoil																																																								
	0.8' - 7.5' Brown Silty SAND																																																									
5	Brown Silty SAND with Gravel																																																									
10	-End of Test Pit at 7.5 Feet-																																																									
	Infiltration Tests Conducted at 3.5 Feet (317.5') and 5.5 Feet (315.5')																																																									
15																																																										
	<table border="1" style="margin: auto; border-collapse: collapse;"> <thead> <tr> <th colspan="4" style="text-align: center;">DOUBLE RING INFILTROMETER DATA</th> </tr> <tr> <th style="text-align: left;">Test Depth:</th> <th></th> <th style="text-align: center;">3.5'</th> <th style="text-align: center;">5.5'</th> </tr> <tr> <td></td> <th style="text-align: center;">Time (min)</th> <th style="text-align: center;">Drop (inches)</th> <th style="text-align: center;">Drop (inches)</th> </tr> </thead> <tbody> <tr> <td>Pre-soak 1</td> <td style="text-align: center;">30</td> <td style="text-align: center;">3.7</td> <td style="text-align: center;">5.0</td> </tr> <tr> <td>Pre-soak 2</td> <td style="text-align: center;">30</td> <td style="text-align: center;">3.6</td> <td style="text-align: center;">5.0</td> </tr> <tr> <td>Reading 1</td> <td style="text-align: center;">10</td> <td style="text-align: center;">1.2</td> <td style="text-align: center;">3.2</td> </tr> <tr> <td>Reading 2</td> <td style="text-align: center;">10</td> <td style="text-align: center;">0.9</td> <td style="text-align: center;">1.9</td> </tr> <tr> <td>Reading 3</td> <td style="text-align: center;">10</td> <td style="text-align: center;">0.9</td> <td style="text-align: center;">2.0</td> </tr> <tr> <td>Reading 4</td> <td style="text-align: center;">10</td> <td style="text-align: center;">1.1</td> <td style="text-align: center;">2.1</td> </tr> <tr> <td>Reading 5</td> <td style="text-align: center;">10</td> <td style="text-align: center;">1.0</td> <td style="text-align: center;">1.9</td> </tr> <tr> <td>Reading 6</td> <td style="text-align: center;">10</td> <td style="text-align: center;">1.0</td> <td style="text-align: center;">2.0</td> </tr> <tr> <td>Reading 7</td> <td></td> <td></td> <td></td> </tr> <tr> <td>Reading 8</td> <td></td> <td></td> <td></td> </tr> <tr> <td colspan="2" style="text-align: center;">Average Rate (inches per hour)</td> <td style="text-align: center;">6.0</td> <td style="text-align: center;">12.0</td> </tr> </tbody> </table>		DOUBLE RING INFILTROMETER DATA				Test Depth:		3.5'	5.5'		Time (min)	Drop (inches)	Drop (inches)	Pre-soak 1	30	3.7	5.0	Pre-soak 2	30	3.6	5.0	Reading 1	10	1.2	3.2	Reading 2	10	0.9	1.9	Reading 3	10	0.9	2.0	Reading 4	10	1.1	2.1	Reading 5	10	1.0	1.9	Reading 6	10	1.0	2.0	Reading 7				Reading 8				Average Rate (inches per hour)		6.0	12.0
DOUBLE RING INFILTROMETER DATA																																																										
Test Depth:		3.5'	5.5'																																																							
	Time (min)	Drop (inches)	Drop (inches)																																																							
Pre-soak 1	30	3.7	5.0																																																							
Pre-soak 2	30	3.6	5.0																																																							
Reading 1	10	1.2	3.2																																																							
Reading 2	10	0.9	1.9																																																							
Reading 3	10	0.9	2.0																																																							
Reading 4	10	1.1	2.1																																																							
Reading 5	10	1.0	1.9																																																							
Reading 6	10	1.0	2.0																																																							
Reading 7																																																										
Reading 8																																																										
Average Rate (inches per hour)		6.0	12.0																																																							
20																																																										
25																																																										
30																																																										

Stratum I



advantage engineers

435 Independence Avenue, Suite C, Mechanicsburg, PA 17055
 Office: (717) 458-0800 Fax: (717) 458-0801
www.advantageengineers.com

EXCAVATION METHOD: Mini-excavator
 ADVANTAGE REPRESENTATIVE: B. Wildasin
 DATE EXCAVATED: September 27, 2018
 DRAWN/COMPILED BY: B. Wildasin

TEST PIT LOG

PROJECT NAME: Westtown School Oak Lane - Infiltration

TEST PIT NO.: TP-4

PROJECT NO.: 1800331001 CLIENT: ELA Group, Inc.

TOP OF GROUND: ±319.5'

LOCATION: See Exploration Plan (Figure 3)

GROUNDWATER DATA: Dry

FIELD SURVEYED

TOPO ESTIMATE

DEPTH: Not Encountered Time: Completion

DEPTH (feet)	SOIL DESCRIPTION	REMARKS
	0.0' - 0.8' Brown organic soil	Topsoil
	0.8' - 4.5' Brown Sandy SILT	
5		Stratum I
	-End of Test Pit at 4.5 Feet-	
10		
15		
20		
25		
30		

Infiltration Tests Conducted at 1 Foot (318.5') and 2.5 Feet (317')

DOUBLE RING INFILTROMETER DATA			
Test Depth:		1'	2.5'
	Time (min)	Drop (inches)	Drop (inches)
Pre-soak 1	30	0.6	0.7
Pre-soak 2	30	0.6	0.6
Reading 1	30	0.6	0.6
Reading 2	30	0.6	0.5
Reading 3	30	0.6	0.5
Reading 4	30	0.6	0.5
Reading 5			
Reading 6			
Reading 7			
Reading 8			
Average Rate (inches per hour)		1.2	1.0



435 Independence Avenue, Suite C, Mechanicsburg, PA 17055
 Office: (717) 458-0800 Fax: (717) 458-0801
 www.advantageengineers.com

EXCAVATION METHOD: Mini-excavator
 ADVANTAGE REPRESENTATIVE: B. Wildasin
 DATE EXCAVATED: September 26, 2018
 DRAWN/COMPILED BY: B. Wildasin

TEST PIT LOG

PROJECT NAME: Westtown School Oak Lane - Infiltration

TEST PIT NO.: TP-6

PROJECT NO.: 1800331001 CLIENT: ELA Group, Inc.

TOP OF GROUND: ±311'

LOCATION: See Exploration Plan (Figure 3)

GROUNDWATER DATA: Dry

FIELD SURVEYED

TOPO ESTIMATE

DEPTH: Not Encountered Time: Completion

DEPTH (feet)	SOIL DESCRIPTION	REMARKS																																																								
	0.0' - 1.5' Dark brown organic soil	Tilled Soil																																																								
	1.5' - 6.0' Brown Sandy SILT																																																									
5		Stratum I																																																								
-End of Test Pit at 6 Feet-																																																										
10	Infiltration Tests Conducted at 2 Feet (309') and 4 Feet (307')																																																									
15																																																										
<table border="1" style="margin: auto; border-collapse: collapse;"> <thead> <tr> <th colspan="4" style="text-align: center;">DOUBLE RING INFILTROMETER DATA</th> </tr> <tr> <th style="text-align: left;">Test Depth:</th> <th colspan="2" style="text-align: center;">2'</th> <th style="text-align: center;">4'</th> </tr> <tr> <td></td> <th style="text-align: center;">Time (min)</th> <th style="text-align: center;">Drop (inches)</th> <th style="text-align: center;">Drop (inches)</th> </tr> </thead> <tbody> <tr> <td>Pre-soak 1</td> <td style="text-align: center;">30</td> <td style="text-align: center;">0.6</td> <td style="text-align: center;">no movement</td> </tr> <tr> <td>Pre-soak 2</td> <td style="text-align: center;">30</td> <td style="text-align: center;">0.4</td> <td style="text-align: center;">no movement</td> </tr> <tr> <td>Reading 1</td> <td style="text-align: center;">30</td> <td style="text-align: center;">0.5</td> <td style="text-align: center;">no movement</td> </tr> <tr> <td>Reading 2</td> <td style="text-align: center;">30</td> <td style="text-align: center;">0.5</td> <td style="text-align: center;">no movement</td> </tr> <tr> <td>Reading 3</td> <td style="text-align: center;">30</td> <td style="text-align: center;">0.5</td> <td style="text-align: center;">no movement</td> </tr> <tr> <td>Reading 4</td> <td style="text-align: center;">30</td> <td style="text-align: center;">0.5</td> <td style="text-align: center;">no movement</td> </tr> <tr> <td>Reading 5</td> <td></td> <td></td> <td></td> </tr> <tr> <td>Reading 6</td> <td></td> <td></td> <td></td> </tr> <tr> <td>Reading 7</td> <td></td> <td></td> <td></td> </tr> <tr> <td>Reading 8</td> <td></td> <td></td> <td></td> </tr> <tr> <td colspan="2" style="text-align: center;">Average Rate (inches per hour)</td> <td style="text-align: center;">1.0</td> <td style="text-align: center;">0.0 (no movement)</td> </tr> </tbody> </table>			DOUBLE RING INFILTROMETER DATA				Test Depth:	2'		4'		Time (min)	Drop (inches)	Drop (inches)	Pre-soak 1	30	0.6	no movement	Pre-soak 2	30	0.4	no movement	Reading 1	30	0.5	no movement	Reading 2	30	0.5	no movement	Reading 3	30	0.5	no movement	Reading 4	30	0.5	no movement	Reading 5				Reading 6				Reading 7				Reading 8				Average Rate (inches per hour)		1.0	0.0 (no movement)
DOUBLE RING INFILTROMETER DATA																																																										
Test Depth:	2'		4'																																																							
	Time (min)		Drop (inches)	Drop (inches)																																																						
Pre-soak 1	30		0.6	no movement																																																						
Pre-soak 2	30		0.4	no movement																																																						
Reading 1	30	0.5	no movement																																																							
Reading 2	30	0.5	no movement																																																							
Reading 3	30	0.5	no movement																																																							
Reading 4	30	0.5	no movement																																																							
Reading 5																																																										
Reading 6																																																										
Reading 7																																																										
Reading 8																																																										
Average Rate (inches per hour)		1.0	0.0 (no movement)																																																							
20																																																										
25																																																										
30																																																										



advantage engineers

435 Independence Avenue, Suite C, Mechanicsburg, PA 17055
 Office: (717) 458-0800 Fax: (717) 458-0801
www.advantageengineers.com

EXCAVATION METHOD: Mini-excavator
 ADVANTAGE REPRESENTATIVE: B. Wildasin
 DATE EXCAVATED: September 26, 2018
 DRAWN/COMPILED BY: B. Wildasin

TEST PIT LOG

PROJECT NAME: Westtown School Oak Lane - Infiltration

TEST PIT NO.: TP-7

PROJECT NO.: 1800331001 CLIENT: ELA Group, Inc.

TOP OF GROUND: ±313'

LOCATION: See Exploration Plan (Figure 3)

GROUNDWATER DATA: Wet

FIELD SURVEYED

TOPO ESTIMATE

DEPTH: 6'

Time: Completion

DEPTH (feet)	SOIL DESCRIPTION	REMARKS																																																								
	0.0' - 1.3' Brown organic soil	Tilled Soil																																																								
	1.3' - 8.0' Brown Sandy SILT Brown Silty SAND																																																									
5		H₂O @ 6'																																																								
		Stratum I																																																								
	-End of Test Pit at 8 Feet-																																																									
10	Infiltration Tests Conducted at 2 Feet (311') and 4 Feet (309')																																																									
	<table border="1" style="margin: auto; border-collapse: collapse;"> <thead> <tr> <th colspan="4" style="text-align: center;">DOUBLE RING INFILTROMETER DATA</th> </tr> <tr> <th style="text-align: center;">Test Depth:</th> <th colspan="2" style="text-align: center;">2'</th> <th style="text-align: center;">4'</th> </tr> <tr> <th></th> <th style="text-align: center;">Time (min)</th> <th style="text-align: center;">Drop (inches)</th> <th style="text-align: center;">Drop (inches)</th> </tr> </thead> <tbody> <tr> <td style="text-align: center;">Pre-soak 1</td> <td style="text-align: center;">30</td> <td style="text-align: center;">0.1</td> <td style="text-align: center;">2.7</td> </tr> <tr> <td style="text-align: center;">Pre-soak 2</td> <td style="text-align: center;">30</td> <td style="text-align: center;">no movement</td> <td style="text-align: center;">1.7</td> </tr> <tr> <td style="text-align: center;">Reading 1</td> <td style="text-align: center;">30</td> <td style="text-align: center;">no movement</td> <td style="text-align: center;">1.5</td> </tr> <tr> <td style="text-align: center;">Reading 2</td> <td style="text-align: center;">30</td> <td style="text-align: center;">no movement</td> <td style="text-align: center;">1.5</td> </tr> <tr> <td style="text-align: center;">Reading 3</td> <td style="text-align: center;">30</td> <td style="text-align: center;">no movement</td> <td style="text-align: center;">1.4</td> </tr> <tr> <td style="text-align: center;">Reading 4</td> <td style="text-align: center;">30</td> <td style="text-align: center;">no movement</td> <td style="text-align: center;">1.4</td> </tr> <tr> <td style="text-align: center;">Reading 5</td> <td></td> <td></td> <td></td> </tr> <tr> <td style="text-align: center;">Reading 6</td> <td></td> <td></td> <td></td> </tr> <tr> <td style="text-align: center;">Reading 7</td> <td></td> <td></td> <td></td> </tr> <tr> <td style="text-align: center;">Reading 8</td> <td></td> <td></td> <td></td> </tr> <tr> <td colspan="2" style="text-align: center;">Average Rate (inches per hour)</td> <td style="text-align: center;">0.0 (no movement)</td> <td style="text-align: center;">2.8</td> </tr> </tbody> </table>		DOUBLE RING INFILTROMETER DATA				Test Depth:	2'		4'		Time (min)	Drop (inches)	Drop (inches)	Pre-soak 1	30	0.1	2.7	Pre-soak 2	30	no movement	1.7	Reading 1	30	no movement	1.5	Reading 2	30	no movement	1.5	Reading 3	30	no movement	1.4	Reading 4	30	no movement	1.4	Reading 5				Reading 6				Reading 7				Reading 8				Average Rate (inches per hour)		0.0 (no movement)	2.8
DOUBLE RING INFILTROMETER DATA																																																										
Test Depth:	2'		4'																																																							
	Time (min)	Drop (inches)	Drop (inches)																																																							
Pre-soak 1	30	0.1	2.7																																																							
Pre-soak 2	30	no movement	1.7																																																							
Reading 1	30	no movement	1.5																																																							
Reading 2	30	no movement	1.5																																																							
Reading 3	30	no movement	1.4																																																							
Reading 4	30	no movement	1.4																																																							
Reading 5																																																										
Reading 6																																																										
Reading 7																																																										
Reading 8																																																										
Average Rate (inches per hour)		0.0 (no movement)	2.8																																																							
15																																																										
20																																																										
25																																																										
30																																																										



advantage engineers

435 Independence Avenue, Suite C, Mechanicsburg, PA 17055
 Office: (717) 458-0800 Fax: (717) 458-0801
www.advantageengineers.com

EXCAVATION METHOD: Mini-excavator
 ADVANTAGE REPRESENTATIVE: B. Wildasin
 DATE EXCAVATED: September 26, 2018
 DRAWN/COMPILED BY: B. Wildasin

TEST PIT LOG

PROJECT NAME: Westtown School Oak Lane - Infiltration

TEST PIT NO.: TP-8

PROJECT NO.: 1800331001 CLIENT: ELA Group, Inc.

TOP OF GROUND: ±311'

LOCATION: See Exploration Plan (Figure 3)

GROUNDWATER DATA: Wet

FIELD SURVEYED

TOPO ESTIMATE

DEPTH: 1.5'

Time: Completion

DEPTH (feet)	SOIL DESCRIPTION	REMARKS
	0.0' - 1.5' Brown organic soil	Tilled Soil
	1.5' - 6.0' Brown Silty SAND	
5		H₂O @ 1.5'
		Stratum I
	-End of Test Pit at 6 Feet-	
10		
	No infiltration tests conducted due to groundwater at 1.5 Feet (309.5')	
15		
20		
25		
30		



435 Independence Avenue, Suite C, Mechanicsburg, PA 17055
 Office: (717) 458-0800 Fax: (717) 458-0801
 www.advantageengineers.com

EXCAVATION METHOD: Mini-excavator
 ADVANTAGE REPRESENTATIVE: B. Wildasin
 DATE EXCAVATED: September 26, 2018
 DRAWN/COMPILED BY: B. Wildasin

TEST PIT LOG

PROJECT NAME: Westtown School Oak Lane - Infiltration

TEST PIT NO.: TP-9

PROJECT NO.: 1800331001 CLIENT: ELA Group, Inc.

TOP OF GROUND: ±303'

LOCATION: See Exploration Plan (Figure 3)

GROUNDWATER DATA: Dry

FIELD SURVEYED

TOPO ESTIMATE

DEPTH: Not Encountered Time: Completion

DEPTH (feet)	SOIL DESCRIPTION	REMARKS																																																								
	0.0' - 0.9' Brown organic soil	Topsoil																																																								
	0.9' - 10.0' Brown Silty SAND																																																									
5	Brown Silty SAND with Gravel																																																									
10																																																										
	-Extent of Equipment at 10 Feet- -End of Test Pit at 10 Feet- Infiltration Tests Conducted at 8 Feet (295')																																																									
15	<table border="1" style="margin: auto; border-collapse: collapse;"> <thead> <tr> <th colspan="4" style="text-align: center;">DOUBLE RING INFILTROMETER DATA</th> </tr> <tr> <th style="text-align: left;">Test Depth:</th> <th></th> <th style="text-align: center;">8'</th> <th style="text-align: center;">8'</th> </tr> <tr> <td></td> <th style="text-align: center;">Time (min)</th> <th style="text-align: center;">Drop (inches)</th> <th style="text-align: center;">Drop (inches)</th> </tr> </thead> <tbody> <tr> <td>Pre-soak 1</td> <td style="text-align: center;">30</td> <td style="text-align: center;">4.0</td> <td style="text-align: center;">4.0</td> </tr> <tr> <td>Pre-soak 2</td> <td style="text-align: center;">30</td> <td style="text-align: center;">2.3</td> <td style="text-align: center;">2.5</td> </tr> <tr> <td>Reading 1</td> <td style="text-align: center;">10</td> <td style="text-align: center;">0.7</td> <td style="text-align: center;">0.7</td> </tr> <tr> <td>Reading 2</td> <td style="text-align: center;">10</td> <td style="text-align: center;">0.7</td> <td style="text-align: center;">0.7</td> </tr> <tr> <td>Reading 3</td> <td style="text-align: center;">10</td> <td style="text-align: center;">0.6</td> <td style="text-align: center;">0.7</td> </tr> <tr> <td>Reading 4</td> <td style="text-align: center;">10</td> <td style="text-align: center;">0.6</td> <td style="text-align: center;">0.6</td> </tr> <tr> <td>Reading 5</td> <td></td> <td></td> <td></td> </tr> <tr> <td>Reading 6</td> <td></td> <td></td> <td></td> </tr> <tr> <td>Reading 7</td> <td></td> <td></td> <td></td> </tr> <tr> <td>Reading 8</td> <td></td> <td></td> <td></td> </tr> <tr> <td colspan="2" style="text-align: center;">Average Rate (inches per hour)</td> <td style="text-align: center;">3.9</td> <td style="text-align: center;">4.0</td> </tr> </tbody> </table>		DOUBLE RING INFILTROMETER DATA				Test Depth:		8'	8'		Time (min)	Drop (inches)	Drop (inches)	Pre-soak 1	30	4.0	4.0	Pre-soak 2	30	2.3	2.5	Reading 1	10	0.7	0.7	Reading 2	10	0.7	0.7	Reading 3	10	0.6	0.7	Reading 4	10	0.6	0.6	Reading 5				Reading 6				Reading 7				Reading 8				Average Rate (inches per hour)		3.9	4.0
DOUBLE RING INFILTROMETER DATA																																																										
Test Depth:		8'	8'																																																							
	Time (min)	Drop (inches)	Drop (inches)																																																							
Pre-soak 1	30	4.0	4.0																																																							
Pre-soak 2	30	2.3	2.5																																																							
Reading 1	10	0.7	0.7																																																							
Reading 2	10	0.7	0.7																																																							
Reading 3	10	0.6	0.7																																																							
Reading 4	10	0.6	0.6																																																							
Reading 5																																																										
Reading 6																																																										
Reading 7																																																										
Reading 8																																																										
Average Rate (inches per hour)		3.9	4.0																																																							
20		Stratum I																																																								
25																																																										
30																																																										



435 Independence Avenue, Suite C, Mechanicsburg, PA 17055
 Office: (717) 458-0800 Fax: (717) 458-0801
 www.advantageengineers.com

EXCAVATION METHOD: Mini-excavator
 ADVANTAGE REPRESENTATIVE: B. Wildasin
 DATE EXCAVATED: September 28, 2018
 DRAWN/COMPILED BY: B. Wildasin

TEST PIT LOG

PROJECT NAME: Westtown School Oak Lane - Infiltration

TEST PIT NO.: TP-10

PROJECT NO.: 1800331001 CLIENT: ELA Group, Inc.

TOP OF GROUND: ±305'

LOCATION: See Exploration Plan (Figure 3)

GROUNDWATER DATA: Dry

FIELD SURVEYED

TOPO ESTIMATE

DEPTH: Not Encountered Time: Completion

DEPTH (feet)	SOIL DESCRIPTION	REMARKS			
	0.0' - 0.9' Brown organic soil	Topsoil			
	0.9' - 6.0' Brown Silty SAND	Stratum I			
5					
	6.0' - 7.5' Brown Silty SAND with Gravel (highly weathered rock)	Stratum II			
	-Bucket Refusal at 7.5 Feet- -End of Test Pit at 7.5 Feet-				
10					
	Infiltration Tests Conducted at 4 Feet (301') and 5.5 Feet (299.5')				
15					
	DOUBLE RING INFILTRMETER DATA				
	Test Depth:	4'	5.5'		
		Time (min)	Drop (inches)	Time (min)	Drop (inches)
20	Pre-soak 1	30	2.2	30	3.5
	Pre-soak 2	30	1.5	30	2.7
	Reading 1	30	1.4	10	0.9
	Reading 2	30	1.4	10	0.6
	Reading 3	30	1.4	10	0.8
25	Reading 4	30	1.4	10	0.8
	Reading 5			10	0.8
	Reading 6			10	0.8
	Reading 7				
	Reading 8				
30	Average Rate (inches per hour)		2.8		4.8



435 Independence Avenue, Suite C, Mechanicsburg, PA 17055
 Office: (717) 458-0800 Fax: (717) 458-0801
 www.advantageengineers.com

EXCAVATION METHOD: Mini-excavator
 ADVANTAGE REPRESENTATIVE: B. Wildasin
 DATE EXCAVATED: September 28, 2018
 DRAWN/COMPILED BY: B. Wildasin

TEST PIT LOG

PROJECT NAME: Westtown School Oak Lane - Infiltration

TEST PIT NO.: TP-11

PROJECT NO.: 1800331001 CLIENT: ELA Group, Inc.

TOP OF GROUND: ±309'

LOCATION: See Exploration Plan (Figure 3)

GROUNDWATER DATA: Dry

FIELD SURVEYED

TOPO ESTIMATE

DEPTH: Not Encountered Time: Completion

DEPTH (feet)	SOIL DESCRIPTION	REMARKS
	0.0' - 0.8' Brown organic soil	Topsoil
	0.8' - 6.0' Brown Silty SAND	
5		
	6.0' - 9.5' Brown Silty SAND with Gravel (highly weathered rock)	
10		
	-Bucket Refusal at 9.5 Feet- -End of Test Pit at 9.5 Feet-	
	Infiltration Tests Conducted at 6 Feet (303') and 7.5 Feet (301.5')	
15		
20		
25		
30		

DOUBLE RING INFILTROMETER DATA			
Test Depth:		6'	7.5'
	Time (min)	Drop (inches)	Drop (inches)
Pre-soak 1	30	4.0	3.5
Pre-soak 2	30	4.0	3.0
Reading 1	10	1.2	0.9
Reading 2	10	1.0	0.8
Reading 3	10	1.0	0.9
Reading 4	10	1.0	0.9
Reading 5			
Reading 6			
Reading 7			
Reading 8			
Average Rate (inches per hour)		6.0	5.4



advantage engineers

435 Independence Avenue, Suite C, Mechanicsburg, PA 17055
 Office: (717) 458-0800 Fax: (717) 458-0801
 www.advantageengineers.com

EXCAVATION METHOD: Mini-excavator
 ADVANTAGE REPRESENTATIVE: B. Wildasin
 DATE EXCAVATED: September 27, 2018
 DRAWN/COMPILED BY: B. Wildasin

TEST PIT LOG

PROJECT NAME: Westtown School Oak Lane - Infiltration

TEST PIT NO.: TP-12

PROJECT NO.: 1800331001 CLIENT: ELA Group, Inc.

TOP OF GROUND: ±298'

LOCATION: See Exploration Plan (Figure 3)

GROUNDWATER DATA: Wet

FIELD SURVEYED

TOPO ESTIMATE

DEPTH: 3.5'

Time: Completion

DEPTH (feet)	SOIL DESCRIPTION	REMARKS
	0.0' - 2.3' Brown organic soil	
		Topsoil
5	2.3' - 6.0' Brown to gray Sandy CLAY (Soil Mottling 2.5' - 6.0')	H₂O @ 3.5'
		Stratum III
	-End of Test Pit at 6 Feet-	
10	No infiltration tests conducted due to Soil Mottling at 2.5 Feet (295.5') and Groundwater at 3.5 Feet (294.5')	
15		
20		
25		
30		



435 Independence Avenue, Suite C, Mechanicsburg, PA 17055
 Office: (717) 458-0800 Fax: (717) 458-0801
 www.advantageengineers.com

EXCAVATION METHOD: Mini-excavator
 ADVANTAGE REPRESENTATIVE: B. Wildasin
 DATE EXCAVATED: September 28, 2018
 DRAWN/COMPILED BY: B. Wildasin

TEST PIT LOG

PROJECT NAME: Westtown School Oak Lane - Infiltration

TEST PIT NO.: TP-13

PROJECT NO.: 1800331001 CLIENT: ELA Group, Inc.

TOP OF GROUND: ±286'

LOCATION: See Exploration Plan (Figure 3)

GROUNDWATER DATA: Wet

FIELD SURVEYED

TOPO ESTIMATE

DEPTH: 1.5'

Time: Completion

DEPTH (feet)	SOIL DESCRIPTION	REMARKS
	0.0' - 1.5' Brown organic soil	Topsoil
	1.5' - 6.0' Brown to gray Sandy CLAY (Soil Mottling 2.5' - 6.0')	H₂O @ 1.5'
5		Stratum III
	-End of Test Pit at 6 Feet-	
10	No infiltration tests conducted due to Groundwater at 1.5 Feet (284.5') and Soil Mottling at 2.5 Feet (283.5')	
15		
20		
25		
30		



435 Independence Avenue, Suite C, Mechanicsburg, PA 17055
 Office: (717) 458-0800 Fax: (717) 458-0801
 www.advantageengineers.com

EXCAVATION METHOD: Mini-excavator
 ADVANTAGE REPRESENTATIVE: B. Wildasin
 DATE EXCAVATED: September 28, 2018
 DRAWN/COMPILED BY: B. Wildasin



November 9, 2018

Westtown School
975 Westtown Road
West Chester, PA 19382

c/o

Mr. Charles R. Haley, Jr., P.E.
ELA Group, Inc.
743 South Broad Street
Lititz, PA 17543

**RE: Supplemental Infiltration Feasibility Report
Westtown School Oak Lane – Supplemental Infiltration
Westtown Township, Chester County, Pennsylvania
Advantage Project Number: 1800331001**

Dear Mr. Haley:

In accordance with your request, Advantage Engineers (Advantage) has completed supplemental infiltration testing for the above referenced project site. This correspondence serves to transmit the results of our supplemental evaluation.

SCOPE OF WORK

The objective of our work was to determine the permeability of the invert soils, identify any limiting zones (i.e. bedrock, groundwater, or seasonal high water table) within the proposed stormwater management facility, and address PADEP requirements as they relate to stormwater management. Our scope of work included the completion of a subsurface exploration and preparation of this report. This report presents a summary of the scope of work completed, conditions encountered, and results of the supplemental infiltration testing engineering analysis of subsurface conditions.

SUBSURFACE FIELD EXPLORATION

In order to characterize subsurface conditions, 3 test pits were excavated on October 31, 2018. Supervision and monitoring of the field exploration was provided by a representative of Advantage who field located the test locations based on the "Updated Sketch Plan", prepared by Site Engineering Concepts, LLC. The approximate test locations, referenced as TP-14 through TP-16, are shown on the attached *Exploration Plan* (Figure 1). Data pertaining to the subsurface exploration was documented in the field and is presented in detail on the *Test Pit Logs*, which contain detailed descriptions of the subsurface materials encountered and infiltration test depths/elevations. A general description of the soil conditions encountered is provided in the "Subsurface Conditions" section of this report.

SUBSURFACE CONDITIONS

Soil

Surficial Materials

Each test pit was covered by approximately 16 inches of tilled soil; however, the thickness of surficial materials may differ in unexplored areas of the project site.



Stratum I – Brown Silty SAND/Sandy SILT

Stratum I was encountered within test pits TP-14 and TP-16 and extended to depths of approximately 5 feet below existing site grades. Upon review, the soils of Stratum I were found to be moderately well graded, non-plastic and comprised of Silty SAND and Sandy SILT.

Stratum II – Brown Silty SAND with Gravel (highly weathered rock)

Stratum II was only encountered within test pit TP-16 and extended to its termination depth of approximately 7 feet below existing site grades. Upon review, the soils of Stratum II were found to be well graded, non-plastic and predominately comprised of Silty SAND with Gravel. The soils of Stratum II represent the highly weathered bedrock surface.

Stratum III – Brown Sandy CLAY

Stratum III was only encountered within test pit TP-15 and extended to its termination depth of approximately 5 feet below existing site grades. Upon review, the soils of Stratum III were found to be poorly graded, plastic and comprised of Sandy CLAY.

Bedrock

The bedrock surface was not encountered within the test pits excavated. The bedrock surface would have been defined as the depth at which the bucket of the given excavation equipment could no longer excavate.

Groundwater/Soil Mottling

Neither groundwater nor soil mottling was encountered within the test pits excavated. These observations were made at the time of the field operation and groundwater table elevations will vary with daily, seasonal, and climatological variations.

INFILTRATION ANALYSIS

To evaluate the feasibility of stormwater infiltration within the proposed stormwater management facility, infiltration tests were completed utilizing the “double-ring” infiltrometer method in accordance with the Pennsylvania Stormwater Best Management Practices Manual, latest Edition. It should be noted that the shallow tests in both TP-14 and TP-15 were completed 6-inches below the proposed test elevations due to the thickness of the tilled soil. The test pit locations, approximate surface elevations, proposed test elevations, actual test elevations, presence of limiting zones, and the infiltration rates achieved at each location are presented in the table below.

INFILTRATION TEST RESULTS					
Test Location	Surface Elevation (ft)	Proposed Test Elevations (ft)	Actual Test Elevations (FT)	Limiting Zone Elevation (ft)	Infiltration Rate* (in/hr)
TP-14	290	289	288.5	Not Encountered @ 285	0.2
		287	287		1.0
TP-15	290	289	288.5	Not Encountered @ 285	0.0
		287	287		0.0
TP-16	292	289	289	Not Encountered @ 285	2.7
		287	287		6.0

**Infiltration rates represent the rates recorded in the field and no safety factor has been applied*



SUMMARY OF DATA & CONCLUSIONS

Based on the results of our field exploration and engineering analysis of the data obtained, we offer the following comments with regard to the infiltration of stormwater at the project site.

- The infiltration tests were conducted within the naturally-occurring soils of Stratum I, Stratum II and Stratum III.
- No limiting zones (i.e. bedrock, groundwater and/or soil mottling) were encountered within the test pits excavated.
- The unfactored infiltration rates were found to range from no movement (0.0 inches per hour) to 6.0 inches per hour. The PADEP recommended rate for infiltration of stormwater is 0.1 to 10 inches per hour.

LIMITATIONS

The conclusions contained in this report are based upon the subsurface data collected and on details stated in this report. Should conditions arise which differ from those specifically stated herein, our office should be notified immediately, so that our recommendations can be reviewed and revised, if necessary.

The conclusions presented herein should be applied only to the infiltration tests as depicted on the *Exploration Plan* for the proposed Westtown School improvements in Westtown Township, Chester County, Pennsylvania. Advantage takes no responsibility in utilizing this information for any other purposes.

The scope of work was limited to the exploration of the subsurface subsoils. Oil, hazardous waste, radioactivity, irritants, pollutants, radon or other dangerous substances and conditions were not the subject of this study. Their presence and/or absence are not implied, inferred or suggested by this report or results of this study.

We trust that this is the information you require. Should you have any questions or if we may be of further assistance, please don't hesitate to contact our office.

Respectfully,
advantage engineers

A handwritten signature in black ink that reads "Bailey Jean Wildasin".

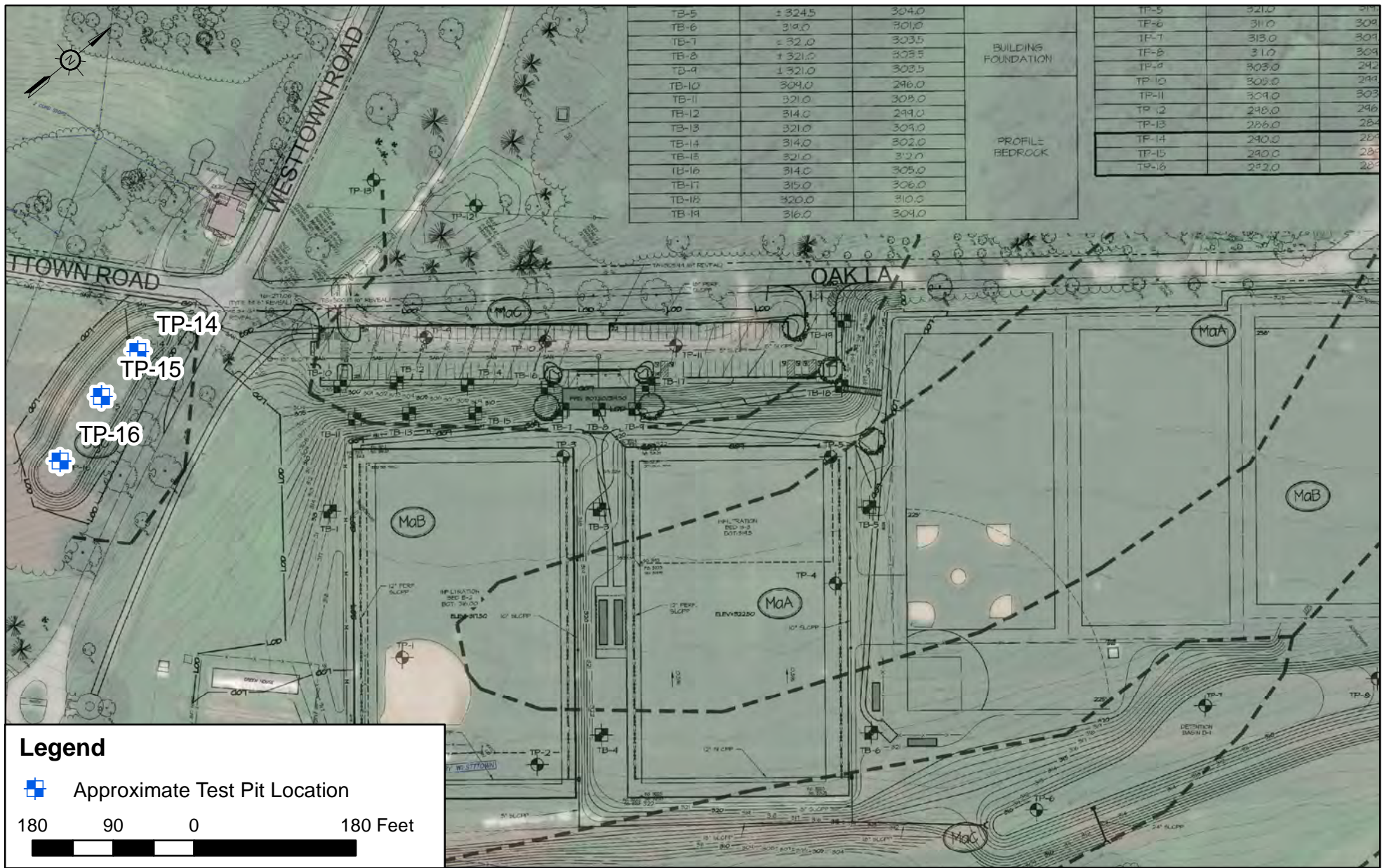
Bailey J. Wildasin
Geotechnical Specialist I

A handwritten signature in black ink that reads "David J. Buckwalter".

David J. Buckwalter
Senior Project Manager

Attachments:

Exploration Plan – Figure 1
Test Pit Logs



TB-5	± 324.5	304.0
TB-6	319.0	301.0
TB-7	± 32.0	303.5
TB-8	± 321.0	303.5
TB-9	1 321.0	303.5
TB-10	309.0	296.0
TB-11	321.0	303.0
TB-12	314.0	299.0
TB-13	321.0	309.0
TB-14	314.0	302.0
TB-15	321.0	312.0
TB-16	314.0	305.0
TB-17	315.0	306.0
TB-18	320.0	310.0
TB-19	316.0	304.0

TP-5	321.0	311.0
TP-6	311.0	309.0
TP-7	313.0	309.0
TP-8	311.0	309.0
TP-9	303.0	292.0
TP-10	309.0	299.0
TP-11	309.0	303.0
TP-12	298.0	296.0
TP-13	286.0	284.0
TP-14	290.0	284.0
TP-15	290.0	284.0
TP-16	292.0	284.0

Legend

Approximate Test Pit Location



*Source - "Updated Sketch Plan" provided by Site Engineering Concepts, LLC, received 10-24-2018

SCALE: AS SHOWN	DRAWING NUMBER: FIGURE 1
DRAWN BY: B. WILDASIN	CHECKED BY: D. BUCKWALTER
APPROVED BY: M. GIUNTA	DATE: 10-26-2018

EXPLORATION PLAN
PREPARED FOR
WESTTOWN SCHOOL OAK LANE - SUPPLEMENTAL INFILTRATION

WESTTOWN TOWNSHIPCHESTER COUNTYPENNSYLVANIA



advantage engineers
435 INDEPENDENCE AVE., SUITE C
MECHANICSBURG, PA 17055
PH (717) 458-0800
FAX (717)458-0801*243

TEST PIT LOG

SHEET 1 OF 1

PROJECT NAME: Westtown School Oak Lane - Supplemental Infiltration

TEST PIT NO.: TP-14

PROJECT NO.: 1800331001 CLIENT: ELA Group, Inc.

TOP OF GROUND: ±290'

LOCATION: See Exploration Plan (Figure 3)

GROUNDWATER DATA: Dry

FIELD SURVEYED

TOPO ESTIMATE

DEPTH: Not Encountered Time: Completion

DEPTH (feet)	SOIL DESCRIPTION	REMARKS																																																								
	0.0' - 1.3' Brown organic soil	Tilled Soil																																																								
	1.3' - 5.0' Brown Sandy SILT Brown Silty SAND																																																									
5		Stratum I																																																								
-End of Test Pit at 5 Feet-																																																										
10																																																										
Infiltration Tests Conducted at 1.5 Feet (288.5') and 3 Feet (287')																																																										
15																																																										
<table border="1" style="margin: auto; border-collapse: collapse;"> <thead> <tr> <th colspan="4" style="text-align: center;">DOUBLE RING INFILTROMETER DATA</th> </tr> <tr> <th style="text-align: center;">Test Depth:</th> <th colspan="2" style="text-align: center;">1.5'</th> <th style="text-align: center;">3'</th> </tr> <tr> <th></th> <th style="text-align: center;">Time (min)</th> <th style="text-align: center;">Drop (inches)</th> <th style="text-align: center;">Drop (inches)</th> </tr> </thead> <tbody> <tr> <td style="text-align: center;">Pre-soak 1</td> <td style="text-align: center;">30</td> <td style="text-align: center;">0.3</td> <td style="text-align: center;">0.8</td> </tr> <tr> <td style="text-align: center;">Pre-soak 2</td> <td style="text-align: center;">30</td> <td style="text-align: center;">0.2</td> <td style="text-align: center;">0.7</td> </tr> <tr> <td style="text-align: center;">Reading 1</td> <td style="text-align: center;">30</td> <td style="text-align: center;">0.1</td> <td style="text-align: center;">0.5</td> </tr> <tr> <td style="text-align: center;">Reading 2</td> <td style="text-align: center;">30</td> <td style="text-align: center;">0.1</td> <td style="text-align: center;">0.5</td> </tr> <tr> <td style="text-align: center;">Reading 3</td> <td style="text-align: center;">30</td> <td style="text-align: center;">0.1</td> <td style="text-align: center;">0.5</td> </tr> <tr> <td style="text-align: center;">Reading 4</td> <td style="text-align: center;">30</td> <td style="text-align: center;">0.1</td> <td style="text-align: center;">0.5</td> </tr> <tr> <td style="text-align: center;">Reading 5</td> <td></td> <td></td> <td></td> </tr> <tr> <td style="text-align: center;">Reading 6</td> <td></td> <td></td> <td></td> </tr> <tr> <td style="text-align: center;">Reading 7</td> <td></td> <td></td> <td></td> </tr> <tr> <td style="text-align: center;">Reading 8</td> <td></td> <td></td> <td></td> </tr> <tr> <td colspan="2" style="text-align: center;">Average Rate (inches per hour)</td> <td style="text-align: center;">0.2</td> <td style="text-align: center;">1.0</td> </tr> </tbody> </table>			DOUBLE RING INFILTROMETER DATA				Test Depth:	1.5'		3'		Time (min)	Drop (inches)	Drop (inches)	Pre-soak 1	30	0.3	0.8	Pre-soak 2	30	0.2	0.7	Reading 1	30	0.1	0.5	Reading 2	30	0.1	0.5	Reading 3	30	0.1	0.5	Reading 4	30	0.1	0.5	Reading 5				Reading 6				Reading 7				Reading 8				Average Rate (inches per hour)		0.2	1.0
DOUBLE RING INFILTROMETER DATA																																																										
Test Depth:	1.5'		3'																																																							
	Time (min)	Drop (inches)	Drop (inches)																																																							
Pre-soak 1	30	0.3	0.8																																																							
Pre-soak 2	30	0.2	0.7																																																							
Reading 1	30	0.1	0.5																																																							
Reading 2	30	0.1	0.5																																																							
Reading 3	30	0.1	0.5																																																							
Reading 4	30	0.1	0.5																																																							
Reading 5																																																										
Reading 6																																																										
Reading 7																																																										
Reading 8																																																										
Average Rate (inches per hour)		0.2	1.0																																																							
20																																																										
25																																																										
30																																																										



advantage engineers

435 Independence Avenue, Suite C, Mechanicsburg, PA 17055
 Office: (717) 458-0800 Fax: (717) 458-0801
www.advantageengineers.com

EXCAVATION METHOD: Backhoe
 ADVANTAGE REPRESENTATIVE: B. Wildasin
 DATE EXCAVATED: October 31, 2018
 DRAWN/COMPILED BY: B. Wildasin

TEST PIT LOG

SHEET 1 OF 1

PROJECT NAME: Westtown School Oak Lane - Supplemental Infiltration

TEST PIT NO.: TP-15

PROJECT NO.: 1800331001 CLIENT: ELA Group, Inc.

TOP OF GROUND: ±290'

LOCATION: See Exploration Plan (Figure 3)

GROUNDWATER DATA: Dry

FIELD SURVEYED

TOPO ESTIMATE

DEPTH: Not Encountered Time: Completion

DEPTH (feet)	SOIL DESCRIPTION	REMARKS																																																								
	0.0' - 1.3' Brown organic soil	Tilled Soil																																																								
	1.3' - 5.0' Brown Sandy CLAY																																																									
5		Stratum III																																																								
-End of Test Pit at 5 Feet-																																																										
10																																																										
Infiltration Tests Conducted at 1.5 Feet (288.5') and 3 Feet (287')																																																										
15																																																										
<table border="1" style="margin: auto; border-collapse: collapse;"> <thead> <tr> <th colspan="4" style="text-align: center;">DOUBLE RING INFILTROMETER DATA</th> </tr> <tr> <th style="text-align: center;">Test Depth:</th> <th colspan="2" style="text-align: center;">1.5'</th> <th style="text-align: center;">3'</th> </tr> <tr> <th></th> <th style="text-align: center;">Time (min)</th> <th style="text-align: center;">Drop (inches)</th> <th style="text-align: center;">Drop (inches)</th> </tr> </thead> <tbody> <tr> <td style="text-align: center;">Pre-soak 1</td> <td style="text-align: center;">30</td> <td style="text-align: center;">0.2</td> <td style="text-align: center;">0.0</td> </tr> <tr> <td style="text-align: center;">Pre-soak 2</td> <td style="text-align: center;">30</td> <td style="text-align: center;">0.0</td> <td style="text-align: center;">0.0</td> </tr> <tr> <td style="text-align: center;">Reading 1</td> <td style="text-align: center;">30</td> <td style="text-align: center;">0.0</td> <td style="text-align: center;">0.0</td> </tr> <tr> <td style="text-align: center;">Reading 2</td> <td style="text-align: center;">30</td> <td style="text-align: center;">0.0</td> <td style="text-align: center;">0.0</td> </tr> <tr> <td style="text-align: center;">Reading 3</td> <td style="text-align: center;">30</td> <td style="text-align: center;">0.0</td> <td style="text-align: center;">0.0</td> </tr> <tr> <td style="text-align: center;">Reading 4</td> <td style="text-align: center;">30</td> <td style="text-align: center;">0.0</td> <td style="text-align: center;">0.0</td> </tr> <tr> <td style="text-align: center;">Reading 5</td> <td></td> <td></td> <td></td> </tr> <tr> <td style="text-align: center;">Reading 6</td> <td></td> <td></td> <td></td> </tr> <tr> <td style="text-align: center;">Reading 7</td> <td></td> <td></td> <td></td> </tr> <tr> <td style="text-align: center;">Reading 8</td> <td></td> <td></td> <td></td> </tr> <tr> <td colspan="2" style="text-align: center;">Average Rate (inches per hour)</td> <td style="text-align: center;">0.0 (no movement)</td> <td style="text-align: center;">0.0 (no movement)</td> </tr> </tbody> </table>			DOUBLE RING INFILTROMETER DATA				Test Depth:	1.5'		3'		Time (min)	Drop (inches)	Drop (inches)	Pre-soak 1	30	0.2	0.0	Pre-soak 2	30	0.0	0.0	Reading 1	30	0.0	0.0	Reading 2	30	0.0	0.0	Reading 3	30	0.0	0.0	Reading 4	30	0.0	0.0	Reading 5				Reading 6				Reading 7				Reading 8				Average Rate (inches per hour)		0.0 (no movement)	0.0 (no movement)
DOUBLE RING INFILTROMETER DATA																																																										
Test Depth:	1.5'		3'																																																							
	Time (min)	Drop (inches)	Drop (inches)																																																							
Pre-soak 1	30	0.2	0.0																																																							
Pre-soak 2	30	0.0	0.0																																																							
Reading 1	30	0.0	0.0																																																							
Reading 2	30	0.0	0.0																																																							
Reading 3	30	0.0	0.0																																																							
Reading 4	30	0.0	0.0																																																							
Reading 5																																																										
Reading 6																																																										
Reading 7																																																										
Reading 8																																																										
Average Rate (inches per hour)		0.0 (no movement)	0.0 (no movement)																																																							
20																																																										
25																																																										
30																																																										



advantage engineers

435 Independence Avenue, Suite C, Mechanicsburg, PA 17055
 Office: (717) 458-0800 Fax: (717) 458-0801
 www.advantageengineers.com

EXCAVATION METHOD: Backhoe
 ADVANTAGE REPRESENTATIVE: B. Wildasin
 DATE EXCAVATED: October 31, 2018
 DRAWN/COMPILED BY: B. Wildasin

TEST PIT LOG

SHEET 1 OF 1

PROJECT NAME: Westtown School Oak Lane - Supplemental Infiltration

TEST PIT NO.: TP-16

PROJECT NO.: 1800331001 CLIENT: ELA Group, Inc.

TOP OF GROUND: ±292'

LOCATION: See Exploration Plan (Figure 3)

GROUNDWATER DATA: Dry

FIELD SURVEYED

TOPO ESTIMATE

DEPTH: Not Encountered Time: Completion

DEPTH (feet)	SOIL DESCRIPTION	REMARKS
	0.0' - 1.3' Brown organic soil	Tilled Soil
	1.3' - 5.0' Brown Silty SAND	
5		Stratum I
	5.0' - 7.0' Brown Silty SAND with Gravel (highly weathered rock)	Stratum II
	-End of Test Pit at 7 Feet-	
10		
	Infiltration Tests Conducted at 3 Feet (289') and 5 Feet (287')	
15		
	DOUBLE RING INFILTROMETER DATA	
	Test Depth:	3'
		5'
		Time (min)
		Drop (inches)
		Time (min)
		Drop (inches)
20	Pre-soak 1	30
		1.9
	Pre-soak 2	30
		1.4
	Reading 1	30
		1.4
	Reading 2	30
		1.3
	Reading 3	30
		1.3
25	Reading 4	30
		1.4
	Reading 5	10
		1.0
	Reading 6	
	Reading 7	
	Reading 8	
30	Average Rate (inches per hour)	2.7
		6.0



435 Independence Avenue, Suite C, Mechanicsburg, PA 17055
 Office: (717) 458-0800 Fax: (717) 458-0801
 www.advantageengineers.com

EXCAVATION METHOD: Backhoe
 ADVANTAGE REPRESENTATIVE: B. Wildasin
 DATE EXCAVATED: October 31, 2018
 DRAWN/COMPILED BY: B. Wildasin