

STORMWATER MANAGEMENT PLAN NARRATIVE

Prepared for:

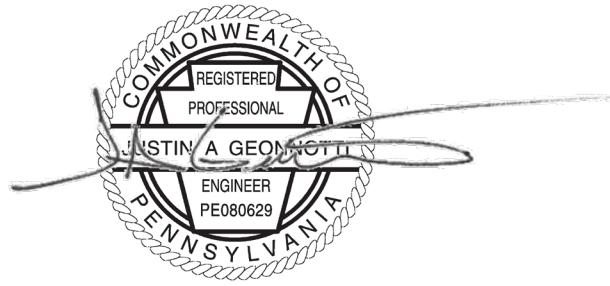
Westtown AM West TIC, LLC

*Proposed Bank
Parcel No. 67-2-42.4
1506 Route 3 (West Chester Pike)
Township of Westtown
Chester County, PA*

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I. SITE DESCRIPTION

This Narrative has been prepared to describe the stormwater drainage conditions that will occur as a result of the proposed Chase Bank located at 1506 PA State Highway Route 3 (West Chester Pike), in Westtown Township Chester County, Pennsylvania. The site is identified as Tax Parcel Number 67-2-42.4. This report should be reviewed in conjunction with the Stormwater Management Plan drawing that is included in the Overall Site Plan prepared by Dynamic Engineering Consultants, PC. Under current conditions the overall site is developed with a shopping center in which the portion which we proposed to develop is being used as an accessory asphalt parking area. The subject site is bound to the north by PA State Highway Route 3 (West Chester Pike), to the east by retail use and beyond, to the south by accessory parking for retail use, and to the west by accessory parking for retail use. The site has been in its current condition for over 25 years based on historical aerial imagery.

II. PROJECT DESCRIPTION

The site is presently developed as a shopping center. The proposed Chase Bank pad is to be added within the existing parking lot. The proposal includes the construction of the new 3,294 SF Chase Bank and associated improvements such as lighting, landscaping, grading, walkways, driveways, utilities, parking, and other associated items. The total limit of disturbance is 33,327 SF (0.76 acres).

III. DESIGN OVERVIEW

This Stormwater Management Plan Narrative identifies and describes the manner by which the stormwater management design satisfies the performance measures set forth by the Westtown Township Stormwater Management Ordinance, Westtown Township Subdivision & Land Development Ordinance (SALDO), the requirements of Chester County Conservation District (CCCD) to minimize adverse impact of the stormwater runoff to receiving water bodies and surrounding areas in the Chester Creek Watershed.

The scope of this study includes the proposed Chase Bank, associated parking areas, utilities, and proposed on-site stormwater management features as depicted on accompanying engineering plans. Based upon the scope of the project, the development is classified as a “regulated activity” per the regulator agencies and, as such the project has been designed to meet the water quality, volume reduction and stormwater runoff rate standards set forth in the Chester Creek Stormwater Management District.

Runoff generated by the subject site drains to Tributary 00607 of the Chester Creek, which is located within the Chester Creek Watershed. The Chester Creek Watershed is ultimately tributary to the Lower Delaware River. Tributary 00607 is classified as Trout Stocking (TSF) and Migratory Fish (MF) water per Pennsylvania’s Water Quality Criteria (PA Code Title 25, Chapter 93) and is not considered a Special Protection or Exceptional Value water. This report will address the specific design elements required by the State, County and Township for discharges to surface waters of this type.

Accordingly, the following items are addressed within this report:

- Standards for nonstructural stormwater management project design
- Water quality and streambank erosion protection
- Evaluation of the non-discharge alternative
- Volume control and runoff quantity standards
- Calculation of stormwater runoff and groundwater recharge

A hydrological evaluation is provided for the 1, 2, 10 and 100-year design storm events utilizing the Urban Hydrology for Small Watershed TR55 method. Per the Chester Creek Stormwater Management District, the post-development runoff rates are not to exceed the pre-development runoff rates as listed in the table below:

Proposed Condition Design Storm	Reduce to Predevelopment Condition Design Storm
2-year	2-year
10-year	10-year
100-year	100-year

The stormwater analysis includes the requirements set forth in the Ordinance as follows:

- The analysis in Appendix F demonstrates that the proposed subsurface infiltration basin BMP will manage the net change for storms when compared to preconstruction runoff volume and water quality.
- The existing pre-development non-forested pervious areas are considered meadow in good condition in the existing condition analysis.
- The water quality volume and treatment has been maximized to the extent practicable.
- The analysis demonstrates the proposed BMPs will meet the rate requirements specified in the Chester Creek Stormwater Management District; and manage the net change in peak rate for the 1-, 2-, 10-, and 100-year/24-hour storm event to not exceed the maximum allowable rates. The below sections discuss compliance with the applicable peak discharge rate.

IV. EXISTING DRAINAGE CONDITIONS

The subject site is currently developed with asphalt pavement parking.

No stream, wetlands, floodway, watercourse, or riparian forest buffers are located on or near the direct vicinity of the subject site.

Under the existing conditions, stormwater runoff generated by the subject site drains to the East Branch Chester Creek. This stormwater analysis will focus primarily on the proposed Chase Bank. The limits of the drainage study have been delineated to accommodate the proposed development and any off-site discharge to the subject site. Two (2) points of interest (POIs) have been analyzed for this project. The points of interest ensure post-development runoff rates and volume are reduced/equal in post development conditions. One (1) point of interest (POI) has been analyzed for this project. The point of interest ensures post-development runoff rates and volumes are reduced to the existing conveyance system and will not be negatively impacted. The point of interest is ultimately tributary to the Chester Creek Watershed. The tract has been evaluated with the following drainage sub watershed areas as depicted on the Existing Drainage Area Map included within Appendix L of this report.

Pre-Development POD 001/POI 001: POD 1 is identified on the Drainage Area Maps (Appendix L) as an existing inlet tributary to the existing stormwater basin (Basin B) for the existing shopping center located to the southwest of the property. The analyzed drainage area includes approximately eighty six of the subject property, the site's frontage along the Route 3 (West Chester Pike). Under existing conditions, stormwater runoff from these areas flows uncontrolled sheet flow to an existing inlet located south of the site. The post-

developed flow rate and volume will be reduced to the maximum allowable rate set forth within the Chester Creek ACT 167 at POD 1.

Pre-Development POD 002/POI 002: POI D is identified on the Drainage Area Maps (Appendix L) as bypass off the southeast portion of the lot to an existing basin (Basin C) located to the southeast of the site. The analyzed drainage area includes the remaining portion of the subject property and the remaining portion of the site not included in POI 1. Under existing conditions, stormwater run-off from these areas flows shallow concentrated flow to the existing basin used to manage existing site. The post-developed flow rate and volume will be reduced to the maximum allowable rate set forth within the Chester Creek ACT 167 at POI 2.

Based upon the USDA Natural Resources Conservation Service (NRCS) Soil Survey, the soil type native to the site are:

CHESTER COUNTY SOIL SURVEY INFORMATION		
SOIL TYPE (SYMBOL)	SOIL TYPE (NAME)	HYDROLOGIC SOIL GROUP (HSG)
UrB	Urban land, 0 to 8 percent slopes	B

These soils types are further described as follows:

Urban land, zero to eight percent slopes (UrB): This soil series is generally mapped beneath the entire subject property. The parent material is reported to be pavement, buildings, and other artificially covered areas of human transported material. The typical soil profile and depth to seasonal high groundwater is not reported.

V. PROPOSED DRAINAGE CONDITIONS

Under the proposed conditions, the site will be developed with 3,294 SF Chase Bank and associated improvements such as lighting, landscaping, grading, walkways, driveways, utilities, parking, and a subsurface infiltration basin. The intent of the proposed design is to maintain the existing runoff characteristics where practicable and manage the peak flow and volume to the point of interest (POD). All storm events will be released within the allowable reduction limits. The site improvements have been designed to respect and maintain the existing drainage patterns and minimize soil disturbance to the fullest extent possible. The post-development conditions were modeled utilizing drainage sub-watershed areas similar to the existing conditions model. These drainage sub-watershed areas are depicted on the Proposed Drainage Map included within Appendix L of this narrative and are further described below:

Post-Development POD 001/POI 001: POD 001 is identified on the Drainage Area Maps (Appendix L) as an existing inlet tributary to the existing stormwater basin (Basin B) for the existing shopping center located to the southwest of the property. The analyzed drainage area includes a majority of the subject property as well as the site's frontage along the Route 3. A majority of the runoff generated from this area is conveyed via a proposed stormwater conveyance system to one (1) proposed subsurface infiltration basin. An infiltration rate of 0.20 in/hr was assumed for the design of the infiltration basin. For these reasons, a subsurface infiltration basin is proposed to be utilized for this project. A further, more detailed discussion of the proposed subsurface infiltration basin is provided in subsequent sections of this narrative. Volume reduction will be achieved utilizing the subsurface infiltration basin BMP and an outlet control structure with low flow orifices. However, this system will ultimately be tributary to the existing inlet within the stormwater conveyance system located to the west of the development near the shopping center access driveway. The remaining portion of runoff

generated by this area bypasses the proposed subsurface infiltration basin and flows via sheet flow directly to the aforementioned existing inlet in the stormwater conveyance system to the south of the site. The post-developed flow rate and volume will be reduced to the maximum allowable rate set forth within the Chester Creek ACT 167 at POI 001.

Post-Development POD 002/POI 002: POI 002 is identified on the Drainage Area Maps (Appendix L) as bypass off the southeast portion of the lot to an existing basin (Basin C) located to the southeast of the site. The analyzed drainage area includes the remaining portion of the subject property and the remaining portion of the site not included in POI 001. The runoff generated by this area will shallow concentrated flow and bypass to the existing basin (Basin C) located to the southeast of the property. The proposed drainage patterns have been designed to significantly reduce the pre-development bypass area at POI-002 in post-development conditions, stormwater runoff generated by the overall site is conveyed to the proposed on-site stormwater management system to the maximum extent possible (associated with POI 001). The post-developed flow rate and volume will be reduced to the maximum allowable rate set forth within the Neshaminy Creek ACT 167 at POI 002. When both Points of Interest are analyzed together, the development will ultimately decrease total stormwater runoff rate and volume to the existing inlet associated with the existing stormwater conveyance system within the Veterans Highway right-of-way and the northwest corner of the property in post conditions.

VI. DESIGN METHODOLOGY

The intent of the design of the proposed stormwater management plan for this redevelopment project is to provide measures as required to address applicable aspects of the Township Ordinances and PA Code Title 25. In order to prepare the stormwater management design for the subject project, extensive initial investigation of the property and topographic survey were performed. On-site review of the tract was performed by Dynamic Engineering Consultants, PC and Dynamic Earth to verify existing site conditions and land cover characteristics. Dynamic Survey, LLC, prepared an overall boundary, location and topographic survey.

Based on review of the existing site conditions, the Drainage Area Maps were prepared for the existing and proposed site conditions as defined within this report. A site layout is proposed within the tract area of the previously existing development to the maximum extent possible, and a grading plan was developed with consideration to the existing drainage patterns. The plan was designed to maintain drainage patterns and reduce peak flow rates and volumes from post-development to pre-development conditions to the maximum extent feasible.

Stormwater runoff generated by the proposed improvements will be collected by a series of inlets and directed into the proposed subsurface infiltration basin within the parking lot or sheet flow directly into the existing stormwater conveyance system. The stormwater conveyance system has been designed to safely convey the 100-year storm event. The pipe sizes have been calculated utilizing the Rational Method. See Appendix I of this narrative for pipe sizing calculations.

Runoff volumes for the site were modeled utilizing HydroCAD 10.20-5a computer software, utilizing the Urban Hydrology for Small Watershed TR55 method for the applicable design storms. The 1, 2-, 10- and 100-year design rainfall depths were obtained from NOAA Atlas 14 for the site with a type II distribution. The rainfall depth values are included in Appendix E of this narrative. Existing and proposed curve number calculations have been included within Appendix C and D of this report and are based upon the associated Hydrological Soil Groups. Since the project has a relatively small footprint and a majority of the site is impervious, the existing time of concentration utilized is 6 minutes. Associated hydrographs are included in Appendixes G and H of this narrative.

VII. BMP DESIGN

The proposed Stormwater Management BMPs have been designed in conformance with the Pennsylvania Stormwater Best Management Practices Manual. The BMPs have been designed to provide improved water quality functions as well as to slow the rate of runoff from the subject parcel.

Subsurface Infiltration Bed (BMP 6.4.3)

The subsurface infiltration basin has been proposed on-site and located beneath the standard duty asphalt pavement. Stormwater runoff from the site is collected in the inlets and piped to the subsurface infiltration basin. Design elements incorporated into the subsurface detention basin include the following:

- 24" HDPE Perforated Pipe System;
- Basin designed with flat bottom for infiltration;
- Proposed outlet control structure to control rate of discharge, and
- Not installed on recently placed fill (<5 years)

VIII. BMP LOADING RATIOS

Loading ratios are one of the most integral aspects related to the design of infiltration BMPs. Overloading is the most common reason for failure of a BMP. This is due to the increased presence of total suspended solids (TSS). The loading ratio is determined by comparing the drainage area and infiltration area. The Pennsylvania BMP manual recommends loading ratios of 5:1 for impervious areas and 8:1 for overall.

The recommended loading ratios are exceeded for the subsurface infiltration basin on this project, however, there are multiple reasons why the exceeded loading ratios are justified for these BMPs. A portion of the impervious area (3,294 SF) which drains to the infiltration BMPs is clean roof area. Roof area provides about one-quarter of TSS as compared to traveled streets.

Although some infiltration BMP areas for this project have a loading ratio in excess of the recommend ratios found in the Pennsylvania BMP manual, it is with the understanding of the justifications above that these BMPs will be able to function as designed, provided that they are properly maintained. The area calculations are as follows:

Surface and Impervious Area to Infiltration Area (Subsurface Infiltration Basin)	
Total Tributary Area	31,404 SF
Impervious Area	20,941 SF
Roof Area	3,294 SF
Infiltration Area (2-Year WSEL)	3,090 SF

BASIN LOADING RATIOS (Subsurface Infiltration Basin)		
Basin # 1	Ratio of Total Tributary Area (8:1 recommended)	Ratio of Impervious Tributary Area (5:1 recommended)
With Roof Impervious	10.1:1	6.7:1
Without Roof Impervious	9.1:1	5.7:1

IX. WATER QUALITY AND STREAMBANK EROSION PROTECTION

The water quality and streambank erosion protection design has been developed to satisfy the applicable requirements of the Township Ordinances via a subsurface infiltration basin. The intent of the drainage design is to maintain the existing drainage patterns and discharge points while satisfying the applicable water quality and streambank erosion protection criteria. As previously mentioned, the subject site is previously developed. The proposed redevelopment has been designed to remain largely within the limits of the previously developed area. Based on the fact that existing flow patterns are maintained, runoff is reduced and existing outlet protection measures are adequate, no negative downstream impacts are anticipated from the proposed improvements.

X. RUNOFF RATE REDUCTION PERFORMANCE

Per the Township Ordinances, specific post-development peak flow rate reductions are required. The proposed development has been designed to limit the impervious coverage on site as well as provide stormwater BMPs to meet these reduction requirements. The following table provides the existing and proposed peak runoff rate performance for the point of interest also found in Appendix F:

Westtown AM West TIC, LLC POD 001/POI 001				
Design Storm	Pre-Development (CFS)	Max Allowable (CFS)	Post-Development (CFS)	Reduction in Flow (CFS)
1 YR	0.79	0.79	0.33	-0.46
2 YR	1.02	1.02	0.50	-0.52
5 YR	1.40	1.40	1.24	-0.16
10 YR	1.75	1.75	1.73	-0.02
25 YR	2.28	2.28	2.21	-0.07
50 YR	2.74	2.74	2.55	-0.19
100 YR	3.26	3.26	2.92	-0.34

Westtown AM West TIC, LLC POD 002 / POI 002				
Design Storm	Pre-Development (CFS)	Max Allowable (CFS)	Post-Development (CFS)	Reduction in Flow (CFS)
1 YR	0.17	0.17	0.17	0.00
2 YR	0.23	0.23	0.22	-0.01
5 YR	0.34	0.34	0.29	-0.05
10 YR	0.43	0.43	0.35	-0.08
25 YR	0.58	0.58	0.44	-0.14
50 YR	0.72	0.72	0.52	-0.20
100 YR	0.87	0.87	0.60	-0.27

Westtown AM West TIC, LLC				
SITE TOTAL (POI 001 & POI 002)				
Design Storm	Pre-Development (CFS)	Max Allowable (CFS)	Post-Development (CFS)	Reduction in Flow (CFS)
1 YR	0.96	0.96	0.50	-0.46
2 YR	1.24	1.24	0.66	-0.58
5 YR	1.74	1.74	1.51	-0.23
10 YR	2.19	2.19	1.95	-0.24
25 YR	2.86	2.86	2.45	-0.41
50 YR	3.46	3.46	2.84	-0.62
100 YR	4.13	4.13	3.24	-0.89

XI. GROUNDWATER RECHARGE

An infiltration rate of 0.20 inches per hour was selected for the proposed subsurface infiltration basin. This rate was chosen based on the soil characteristics and existing hydrological data of the area. It is sufficient to ensure effective water management, preventing both surface flooding and excessive groundwater recharge. Additionally, this rate allows for the gradual infiltration of stormwater, promoting groundwater recharge and reducing the risk of erosion. The assumed rate aligns with local regulations and best practices for sustainable stormwater management, ensuring the basin operates efficiently under typical storm conditions.

XIII. CONCLUSION

In compliance with Township, County and State requirements, the proposed redevelopment of the subject property is designed with provisions for safe and efficient control of stormwater runoff in a manner that will not adversely affect the existing drainage patterns, the adjacent roadways, or adjacent parcels. The proposed development will comply with the Township Ordinances and State requirements for stormwater runoff quality, volume, and quantity. Based on the information summarized in this report, the proposed development will limit impacts on the existing stormwater management system and meet or exceed water quality, runoff rates, and volume requirements to the maximum extent feasible.

APPENDIX

A. NRCS SOIL SURVEY



United States
Department of
Agriculture



Natural
Resources
Conservation
Service

A product of the National Cooperative Soil Survey, a joint effort of the United States Department of Agriculture and other Federal agencies, State agencies including the Agricultural Experiment Stations, and local participants

Custom Soil Resource Report for Chester County, Pennsylvania



Preface

Soil surveys contain information that affects land use planning in survey areas. They highlight soil limitations that affect various land uses and provide information about the properties of the soils in the survey areas. Soil surveys are designed for many different users, including farmers, ranchers, foresters, agronomists, urban planners, community officials, engineers, developers, builders, and home buyers. Also, conservationists, teachers, students, and specialists in recreation, waste disposal, and pollution control can use the surveys to help them understand, protect, or enhance the environment.

Various land use regulations of Federal, State, and local governments may impose special restrictions on land use or land treatment. Soil surveys identify soil properties that are used in making various land use or land treatment decisions. The information is intended to help the land users identify and reduce the effects of soil limitations on various land uses. The landowner or user is responsible for identifying and complying with existing laws and regulations.

Although soil survey information can be used for general farm, local, and wider area planning, onsite investigation is needed to supplement this information in some cases. Examples include soil quality assessments (<http://www.nrcs.usda.gov/wps/portal/nrcs/main/soils/health/>) and certain conservation and engineering applications. For more detailed information, contact your local USDA Service Center (<https://offices.sc.egov.usda.gov/locator/app?agency=nrcs>) or your NRCS State Soil Scientist (http://www.nrcs.usda.gov/wps/portal/nrcs/detail/soils/contactus/?cid=nrcs142p2_053951).

Great differences in soil properties can occur within short distances. Some soils are seasonally wet or subject to flooding. Some are too unstable to be used as a foundation for buildings or roads. Clayey or wet soils are poorly suited to use as septic tank absorption fields. A high water table makes a soil poorly suited to basements or underground installations.

The National Cooperative Soil Survey is a joint effort of the United States Department of Agriculture and other Federal agencies, State agencies including the Agricultural Experiment Stations, and local agencies. The Natural Resources Conservation Service (NRCS) has leadership for the Federal part of the National Cooperative Soil Survey.

Information about soils is updated periodically. Updated information is available through the NRCS Web Soil Survey, the site for official soil survey information.

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How Soil Surveys Are Made

Soil surveys are made to provide information about the soils and miscellaneous areas in a specific area. They include a description of the soils and miscellaneous areas and their location on the landscape and tables that show soil properties and limitations affecting various uses. Soil scientists observed the steepness, length, and shape of the slopes; the general pattern of drainage; the kinds of crops and native plants; and the kinds of bedrock. They observed and described many soil profiles. A soil profile is the sequence of natural layers, or horizons, in a soil. The profile extends from the surface down into the unconsolidated material in which the soil formed or from the surface down to bedrock. The unconsolidated material is devoid of roots and other living organisms and has not been changed by other biological activity.

Currently, soils are mapped according to the boundaries of major land resource areas (MLRAs). MLRAs are geographically associated land resource units that share common characteristics related to physiography, geology, climate, water resources, soils, biological resources, and land uses (USDA, 2006). Soil survey areas typically consist of parts of one or more MLRA.

The soils and miscellaneous areas in a survey area occur in an orderly pattern that is related to the geology, landforms, relief, climate, and natural vegetation of the area. Each kind of soil and miscellaneous area is associated with a particular kind of landform or with a segment of the landform. By observing the soils and miscellaneous areas in the survey area and relating their position to specific segments of the landform, a soil scientist develops a concept, or model, of how they were formed. Thus, during mapping, this model enables the soil scientist to predict with a considerable degree of accuracy the kind of soil or miscellaneous area at a specific location on the landscape.

Commonly, individual soils on the landscape merge into one another as their characteristics gradually change. To construct an accurate soil map, however, soil scientists must determine the boundaries between the soils. They can observe only a limited number of soil profiles. Nevertheless, these observations, supplemented by an understanding of the soil-vegetation-landscape relationship, are sufficient to verify predictions of the kinds of soil in an area and to determine the boundaries.

Soil scientists recorded the characteristics of the soil profiles that they studied. They noted soil color, texture, size and shape of soil aggregates, kind and amount of rock fragments, distribution of plant roots, reaction, and other features that enable them to identify soils. After describing the soils in the survey area and determining their properties, the soil scientists assigned the soils to taxonomic classes (units).

Taxonomic classes are concepts. Each taxonomic class has a set of soil characteristics with precisely defined limits. The classes are used as a basis for comparison to classify soils systematically. Soil taxonomy, the system of taxonomic classification used in the United States, is based mainly on the kind and character of soil properties and the arrangement of horizons within the profile. After the soil

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scientists classified and named the soils in the survey area, they compared the individual soils with similar soils in the same taxonomic class in other areas so that they could confirm data and assemble additional data based on experience and research.

The objective of soil mapping is not to delineate pure map unit components; the objective is to separate the landscape into landforms or landform segments that have similar use and management requirements. Each map unit is defined by a unique combination of soil components and/or miscellaneous areas in predictable proportions. Some components may be highly contrasting to the other components of the map unit. The presence of minor components in a map unit in no way diminishes the usefulness or accuracy of the data. The delineation of such landforms and landform segments on the map provides sufficient information for the development of resource plans. If intensive use of small areas is planned, onsite investigation is needed to define and locate the soils and miscellaneous areas.

Soil scientists make many field observations in the process of producing a soil map. The frequency of observation is dependent upon several factors, including scale of mapping, intensity of mapping, design of map units, complexity of the landscape, and experience of the soil scientist. Observations are made to test and refine the soil-landscape model and predictions and to verify the classification of the soils at specific locations. Once the soil-landscape model is refined, a significantly smaller number of measurements of individual soil properties are made and recorded. These measurements may include field measurements, such as those for color, depth to bedrock, and texture, and laboratory measurements, such as those for content of sand, silt, clay, salt, and other components. Properties of each soil typically vary from one point to another across the landscape.

Observations for map unit components are aggregated to develop ranges of characteristics for the components. The aggregated values are presented. Direct measurements do not exist for every property presented for every map unit component. Values for some properties are estimated from combinations of other properties.

While a soil survey is in progress, samples of some of the soils in the area generally are collected for laboratory analyses and for engineering tests. Soil scientists interpret the data from these analyses and tests as well as the field-observed characteristics and the soil properties to determine the expected behavior of the soils under different uses. Interpretations for all of the soils are field tested through observation of the soils in different uses and under different levels of management. Some interpretations are modified to fit local conditions, and some new interpretations are developed to meet local needs. Data are assembled from other sources, such as research information, production records, and field experience of specialists. For example, data on crop yields under defined levels of management are assembled from farm records and from field or plot experiments on the same kinds of soil.

Predictions about soil behavior are based not only on soil properties but also on such variables as climate and biological activity. Soil conditions are predictable over long periods of time, but they are not predictable from year to year. For example, soil scientists can predict with a fairly high degree of accuracy that a given soil will have a high water table within certain depths in most years, but they cannot predict that a high water table will always be at a specific level in the soil on a specific date.

After soil scientists located and identified the significant natural bodies of soil in the survey area, they drew the boundaries of these bodies on aerial photographs and

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identified each as a specific map unit. Aerial photographs show trees, buildings, fields, roads, and rivers, all of which help in locating boundaries accurately.

Soil Map

The soil map section includes the soil map for the defined area of interest, a list of soil map units on the map and extent of each map unit, and cartographic symbols displayed on the map. Also presented are various metadata about data used to produce the map, and a description of each soil map unit.

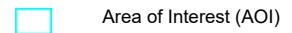
Custom Soil Resource Report
Soil Map



Custom Soil Resource Report

MAP LEGEND

Area of Interest (AOI)



Area of Interest (AOI)

Soils



Soil Map Unit Polygons



Soil Map Unit Lines



Soil Map Unit Points

Special Point Features



Blowout



Borrow Pit



Clay Spot



Closed Depression



Gravel Pit



Gravelly Spot



Landfill



Lava Flow



Marsh or swamp



Mine or Quarry



Miscellaneous Water



Perennial Water



Rock Outcrop



Saline Spot



Sandy Spot



Severely Eroded Spot



Sinkhole



Slide or Slip



Sodic Spot

Spoil Area



Stony Spot



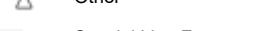
Very Stony Spot



Wet Spot

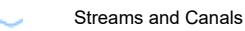


Other



Special Line Features

Water Features



Streams and Canals

Transportation



Rails



Interstate Highways



US Routes



Major Roads



Local Roads

Background



Aerial Photography

MAP INFORMATION

The soil surveys that comprise your AOI were mapped at 1:24,000.

Warning: Soil Map may not be valid at this scale.

Enlargement of maps beyond the scale of mapping can cause misunderstanding of the detail of mapping and accuracy of soil line placement. The maps do not show the small areas of contrasting soils that could have been shown at a more detailed scale.

Please rely on the bar scale on each map sheet for map measurements.

Source of Map: Natural Resources Conservation Service

Web Soil Survey URL:

Coordinate System: Web Mercator (EPSG:3857)

Maps from the Web Soil Survey are based on the Web Mercator projection, which preserves direction and shape but distorts distance and area. A projection that preserves area, such as the Albers equal-area conic projection, should be used if more accurate calculations of distance or area are required.

This product is generated from the USDA-NRCS certified data as of the version date(s) listed below.

Soil Survey Area: Chester County, Pennsylvania

Survey Area Data: Version 16, Sep 4, 2023

Soil map units are labeled (as space allows) for map scales 1:50,000 or larger.

Date(s) aerial images were photographed: Jun 5, 2022—Jul 4, 2022

The orthophoto or other base map on which the soil lines were compiled and digitized probably differs from the background imagery displayed on these maps. As a result, some minor shifting of map unit boundaries may be evident.

Map Unit Legend

Map Unit Symbol	Map Unit Name	Acres in AOI	Percent of AOI
GdB	Gladstone gravelly loam, 3 to 8 percent slopes	0.3	2.0%
UrB	Urban land, 0 to 8 percent slopes	13.2	81.5%
UugD	Urban land-Udorthents, schist and gneiss complex, 8 to 25 percent slopes	2.7	16.5%
Totals for Area of Interest		16.2	100.0%

Map Unit Descriptions

The map units delineated on the detailed soil maps in a soil survey represent the soils or miscellaneous areas in the survey area. The map unit descriptions, along with the maps, can be used to determine the composition and properties of a unit.

A map unit delineation on a soil map represents an area dominated by one or more major kinds of soil or miscellaneous areas. A map unit is identified and named according to the taxonomic classification of the dominant soils. Within a taxonomic class there are precisely defined limits for the properties of the soils. On the landscape, however, the soils are natural phenomena, and they have the characteristic variability of all natural phenomena. Thus, the range of some observed properties may extend beyond the limits defined for a taxonomic class. Areas of soils of a single taxonomic class rarely, if ever, can be mapped without including areas of other taxonomic classes. Consequently, every map unit is made up of the soils or miscellaneous areas for which it is named and some minor components that belong to taxonomic classes other than those of the major soils.

Most minor soils have properties similar to those of the dominant soil or soils in the map unit, and thus they do not affect use and management. These are called noncontrasting, or similar, components. They may or may not be mentioned in a particular map unit description. Other minor components, however, have properties and behavioral characteristics divergent enough to affect use or to require different management. These are called contrasting, or dissimilar, components. They generally are in small areas and could not be mapped separately because of the scale used. Some small areas of strongly contrasting soils or miscellaneous areas are identified by a special symbol on the maps. If included in the database for a given area, the contrasting minor components are identified in the map unit descriptions along with some characteristics of each. A few areas of minor components may not have been observed, and consequently they are not mentioned in the descriptions, especially where the pattern was so complex that it was impractical to make enough observations to identify all the soils and miscellaneous areas on the landscape.

The presence of minor components in a map unit in no way diminishes the usefulness or accuracy of the data. The objective of mapping is not to delineate pure taxonomic classes but rather to separate the landscape into landforms or

landform segments that have similar use and management requirements. The delineation of such segments on the map provides sufficient information for the development of resource plans. If intensive use of small areas is planned, however, onsite investigation is needed to define and locate the soils and miscellaneous areas.

An identifying symbol precedes the map unit name in the map unit descriptions. Each description includes general facts about the unit and gives important soil properties and qualities.

Soils that have profiles that are almost alike make up a *soil series*. Except for differences in texture of the surface layer, all the soils of a series have major horizons that are similar in composition, thickness, and arrangement.

Soils of one series can differ in texture of the surface layer, slope, stoniness, salinity, degree of erosion, and other characteristics that affect their use. On the basis of such differences, a soil series is divided into *soil phases*. Most of the areas shown on the detailed soil maps are phases of soil series. The name of a soil phase commonly indicates a feature that affects use or management. For example, Alpha silt loam, 0 to 2 percent slopes, is a phase of the Alpha series.

Some map units are made up of two or more major soils or miscellaneous areas. These map units are complexes, associations, or undifferentiated groups.

A *complex* consists of two or more soils or miscellaneous areas in such an intricate pattern or in such small areas that they cannot be shown separately on the maps. The pattern and proportion of the soils or miscellaneous areas are somewhat similar in all areas. Alpha-Beta complex, 0 to 6 percent slopes, is an example.

An *association* is made up of two or more geographically associated soils or miscellaneous areas that are shown as one unit on the maps. Because of present or anticipated uses of the map units in the survey area, it was not considered practical or necessary to map the soils or miscellaneous areas separately. The pattern and relative proportion of the soils or miscellaneous areas are somewhat similar. Alpha-Beta association, 0 to 2 percent slopes, is an example.

An *undifferentiated group* is made up of two or more soils or miscellaneous areas that could be mapped individually but are mapped as one unit because similar interpretations can be made for use and management. The pattern and proportion of the soils or miscellaneous areas in a mapped area are not uniform. An area can be made up of only one of the major soils or miscellaneous areas, or it can be made up of all of them. Alpha and Beta soils, 0 to 2 percent slopes, is an example.

Some surveys include *miscellaneous areas*. Such areas have little or no soil material and support little or no vegetation. Rock outcrop is an example.

Chester County, Pennsylvania

GdB—Gladstone gravelly loam, 3 to 8 percent slopes

Map Unit Setting

National map unit symbol: 2v7gk

Elevation: 250 to 1,200 feet

Mean annual precipitation: 30 to 64 inches

Mean annual air temperature: 46 to 79 degrees F

Frost-free period: 131 to 178 days

Farmland classification: All areas are prime farmland

Map Unit Composition

Gladstone and similar soils: 85 percent

Minor components: 15 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Gladstone

Setting

Landform: Hills

Landform position (two-dimensional): Shoulder

Landform position (three-dimensional): Side slope

Down-slope shape: Linear

Across-slope shape: Convex

Parent material: Loamy colluvium derived from granite and gneiss and/or loamy residuum weathered from granite and gneiss

Typical profile

Ap - 0 to 10 inches: gravelly loam

Bt1 - 10 to 22 inches: sandy clay loam

Bt2 - 22 to 37 inches: loam

C - 37 to 66 inches: sandy loam

R - 66 to 76 inches: bedrock

Properties and qualities

Slope: 3 to 8 percent

Depth to restrictive feature: 60 to 80 inches to lithic bedrock

Drainage class: Well drained

Capacity of the most limiting layer to transmit water (Ksat): Very low to moderately low (0.00 to 0.06 in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: None

Frequency of ponding: None

Available water supply, 0 to 60 inches: Moderate (about 8.4 inches)

Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 2e

Hydrologic Soil Group: B

Ecological site: F148XY024PA - Moist, Piedmont - felsic, Upland, Mixed Oak - Hardwood - Conifer Forest

Hydric soil rating: No

Minor Components

Parker

Percent of map unit: 5 percent
Landform: Hills
Landform position (two-dimensional): Shoulder
Landform position (three-dimensional): Side slope
Down-slope shape: Convex
Across-slope shape: Linear
Hydric soil rating: No

Califon

Percent of map unit: 5 percent
Landform: Flats
Landform position (two-dimensional): Foothslope
Landform position (three-dimensional): Base slope
Down-slope shape: Concave
Across-slope shape: Linear
Hydric soil rating: No

Annandale

Percent of map unit: 5 percent
Landform: Hills
Landform position (two-dimensional): Summit
Landform position (three-dimensional): Interfluve
Down-slope shape: Convex
Across-slope shape: Linear
Hydric soil rating: No

UrB—Urban land, 0 to 8 percent slopes

Map Unit Setting

National map unit symbol: 1r3nt
Elevation: 800 to 1,500 feet
Mean annual precipitation: 36 to 46 inches
Mean annual air temperature: 41 to 62 degrees F
Frost-free period: 130 to 170 days
Farmland classification: Not prime farmland

Map Unit Composition

Urban land: 90 percent
Minor components: 10 percent
Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Urban Land

Setting

Parent material: Pavement, buildings and other artificially covered areas human transported material

Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 8s

Hydric soil rating: No

Minor Components

Udorthents, unstable fill

Percent of map unit: 10 percent

Down-slope shape: Linear

Across-slope shape: Linear

Hydric soil rating: No

UugD—Urban land-Udorthents, schist and gneiss complex, 8 to 25 percent slopes

Map Unit Setting

National map unit symbol: pjnz

Elevation: 200 to 2,000 feet

Mean annual precipitation: 35 to 55 inches

Mean annual air temperature: 45 to 61 degrees F

Frost-free period: 110 to 235 days

Farmland classification: Not prime farmland

Map Unit Composition

Urban land: 80 percent

Udorthents, schist and gneiss, and similar soils: 15 percent

Minor components: 5 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Urban Land

Setting

Landform: Hills

Landform position (two-dimensional): Summit, shoulder, backslope

Landform position (three-dimensional): Interfluve, side slope, nose slope

Down-slope shape: Convex, linear

Across-slope shape: Linear, convex

Parent material: Pavement, buildings and other artificially covered areas

Typical profile

C - 0 to 6 inches: variable

Properties and qualities

Slope: 8 to 25 percent

Depth to restrictive feature: 10 to 99 inches to lithic bedrock

Available water supply, 0 to 60 inches: Very low (about 0.0 inches)

Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 8s

Hydric soil rating: No

Description of Udorthents, Schist And Gneiss

Setting

Landform: Hills

Landform position (two-dimensional): Summit, shoulder, backslope

Landform position (three-dimensional): Interfluve, side slope, nose slope

Down-slope shape: Convex, linear

Across-slope shape: Linear, convex

Parent material: Graded areas of schist and/or gneiss

Typical profile

Ap - 0 to 6 inches: loam

C - 6 to 40 inches: silty clay loam

R - 40 to 60 inches: bedrock

Properties and qualities

Slope: 8 to 25 percent

Depth to restrictive feature: 20 to 70 inches to paralithic bedrock

Drainage class: Well drained

Runoff class: High

Capacity of the most limiting layer to transmit water (Ksat): Moderately low to moderately high (0.06 to 0.20 in/hr)

Depth to water table: About 60 inches

Frequency of flooding: None

Frequency of ponding: None

Available water supply, 0 to 60 inches: Moderate (about 6.8 inches)

Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 7e

Hydrologic Soil Group: C

Hydric soil rating: No

Minor Components

Gladstone

Percent of map unit: 1 percent

Landform: Hillslopes

Landform position (two-dimensional): Summit, shoulder

Landform position (three-dimensional): Nose slope, side slope

Down-slope shape: Convex, linear

Across-slope shape: Linear, convex

Hydric soil rating: No

Glenelg

Percent of map unit: 1 percent

Landform: Hillslopes

Landform position (two-dimensional): Summit, shoulder, backslope

Landform position (three-dimensional): Interfluve, side slope, nose slope

Down-slope shape: Convex, linear

Across-slope shape: Linear, convex

Hydric soil rating: No

Baile

Percent of map unit: 1 percent

Landform: Depressions

Custom Soil Resource Report

Landform position (two-dimensional): Foothslope
Landform position (three-dimensional): Base slope
Down-slope shape: Concave, linear
Across-slope shape: Concave, linear
Hydric soil rating: Yes

Edgemont

Percent of map unit: 1 percent
Landform: Ridges
Landform position (two-dimensional): Summit
Landform position (three-dimensional): Mountaintop
Down-slope shape: Convex, linear
Across-slope shape: Linear, convex
Hydric soil rating: No

Glenville

Percent of map unit: 1 percent
Landform: Hillslopes
Landform position (two-dimensional): Foothslope, backslope
Landform position (three-dimensional): Side slope, head slope
Down-slope shape: Concave, linear
Across-slope shape: Linear, concave
Hydric soil rating: No

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Custom Soil Resource Report

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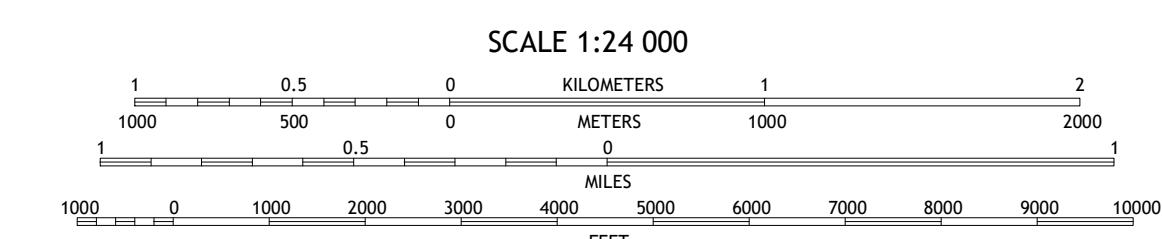
B. USGS MAP


Produced by the United States Geological Survey

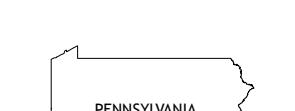
Map ID: 2023-00000000000000000000000000000000
 World Geodetic System of 1984 (WGS84) - Projection and
 1:000,000 per-unit Universal Transverse Mercator, Zone 18S
 This map is not a legal document. Boundaries may be
 generalized for this map scale. Private lands within government
 reservations may not be shown. Obtain permission before
 entering private lands.

Imagery.....NAIP, June 2017 - December 2017
 Roads.....U.S. Census Bureau, 2016 - 2020
 Names.....GNIS, 1979 - 2023
 Hydrography.....National Hydrography Dataset, 2001 - 2022
 Contours.....National Elevation Dataset, 2016
 Boundaries.....Multiple sources; see metadata file
 Wetlands.....FWS National Wetlands Inventory 1981 - 1999

11°43' 2023
 0.22 0.7 Miles
 MN GN
 UTM GRID AND 2023 MAGNETIC NORTH
 DECLINATION AT CENTER OF SHEET
 U.S. National Grid
 100,000-m Square ID
 VK
 Grid Zone Designation
 18T 40°N
 18S



CONTOUR INTERVAL 10 FEET
 NORTH AMERICAN VERTICAL DATUM OF 1988
 This map was produced to conform with the
 National Geospatial Program US Topo Product Standard.

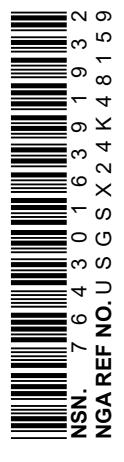


QUADRANGLE LOCATION

ROAD CLASSIFICATION
 Expressway
 Secondary Hwy
 Ramp
 Interstate Route
 Local Connector
 Local Road
 4WD
 US Route
 State Route

1	2	3
4	5	
6	7	8

ADJOINING QUADRANGLES
 1 Downingtown
 2 Malvern
 3 Valley Forge
 4 Kennettville
 5 Media
 6 Kennett Square
 7 Wilmington North
 8 Marcus Hook



**C. RUNOFF CURVE NUMBER (CN)
CALCULATIONS - EXISTING**



EXISTING DRAINAGE AREA SUMMARY AND AVERAGE CURVE NUMBER(CN) CALCULATIONS

Project: Paramount - Westtown (Chase Bank)

Job #: 1478-99-191

Location: 1502 West Chester Pike, Westtown, PA

Computed By:KDS

Checked By: MTM

Date: 11/2/2024

Drainage Area	Impervious Area (acre)	Impervious Area (sf)	Curve Number (CN) Used	HSG B - Meadow	HSG B - Meadow (sf)	Curve Number (CN) Used	HSG B - Lawn	HSG B - Lawn (sf)	Curve Number (CN) Used	HSG B - Woods	HSG B - Woods (sf)	Curve Number (CN) Used	Total Previous Area (acres)	Total Area (acres)	TC (Min.)
DP 001 Existing Basin B (POI 1)	0.29	12,510	98	0.11	4,833	58	0.00	-	61	0.00	-	55	0.11	0.40	6.7
40% Onsite Impervious to Meadow (POI 1)**	0.00	-	98	0.19	8,339	58	0.00	-	61	0.00	-	55	0.19	0.19	6.7
DP 002 Existing Basin C (POI 2)	0.06	2,622	98	0.07	3,251	58	0.00	-	61	0.00	-	55	0.07	0.13	6.2
40% Onsite Impervious to Meadow (POI 2)**	0.00	-	98	0.04	1,748	58	0.00	-	61	0.00	-	55	0.04	0.04	6.2
On-Site Total	0.35	0.42			0.00		0.00		0.42				0.76		

Per County Soil Survey	Urb	HSG	B	Soil	Urban Land, 0 to 8 percent slopes
Per County Soil Survey					

Description	Runoff Curve Number (CN) (HSG A)	Runoff Curve Number (CN) B)	(HSG	Runoff Curve Number (CN) (HSG C)	Runoff Curve Number (CN) (HSG D)
Impervious Surface	98		98	98	98
Open Space (lawn) (good)	39	61		74	80
Woods (good)	30	55		70	77
Meadow	30	58		71	78

**D. RUNOFF CURVE NUMBER (CN)
CALCULATIONS – PROPOSED**



PROPOSED DRAINAGE AREA SUMMARY AND AVERAGE CURVE NUMBER(CN) CALCULATIONS

Project: Paramount - Westtown (Chase Bank)

Job #: 1478-99-191

Location: 1502 West Chester Pike, Westtown, PA

Computed By: KDS

Checked By: SRM

Date: 11/2/2024

Drainage Area	Impervious Area (acre)	Impervious Area (sf)	Curve Number (CN) Used	HSG B - Meadow (acre)	HSG B - Meadow (sf)	Curve Number (CN) Used	HSG B - Lawn (acre)	HSG B - Lawn (sf)	Curve Number (CN) Used	HSG B - Woods (acre)	HSG B - Woods (sf)	Curve Number (CN) Used	Total Pervious Area (acres)	Total Area (acres)	TC (Min.)	
PROP ONSITE TO UG BASIN	0.40	17,521	98	0.00		58	0.10	4,382	61	0.00		-	55	0.10	0.50	6.0
PROP OFFSITE TO UG BASIN	0.08	3,420	98	0.00		58	0.14	6,081	61	0.00		-	55	0.14	0.22	6.0
PROP ONSITE BYPASS TO POD 1	0.12	5,107	98	0.00		58	0.04	1,828	61	0.00		-	55	0.04	0.16	6.0
PROP ONSITE BYPASS POD 002	0.06	2,726	98	0.00	-	58	0.03	1,216	61	0.00		-	55	0.03	0.09	6.0
Total	0.66						0.31						0.31	0.97		

Per County Soil Survey	UrB	HSG	B	Soil	Urban Land, 0 to 8 percent slopes
Per County Soil Survey					

Description	Runoff Curve Number (CN)	Runoff Curve Number (CN)	Runoff Curve Number (CN)	(HSG)	Runoff Curve Number (CN)	(HSG)
Impervious Surface	98	98	98		98	
Open Space (lawn) (good)	39	61	74		80	
Woods (good)	30	55	70		77	
Meadow	30	58	71		78	

E. NOAA RAINFALL DATA



NOAA Atlas 14, Volume 2, Version 3
Location name: Bristol, Pennsylvania, USA*
Latitude: 40.1072°, Longitude: -74.8772°
Elevation: 29.17 ft**
 * source: ESRI Maps
 ** source: USGS



POINT PRECIPITATION FREQUENCY ESTIMATES

G.M. Bonnin, D. Martin, B. Lin, T. Parzybok, M. Yekta, and D. Riley

NOAA, National Weather Service, Silver Spring, Maryland

[PF tabular](#) | [PF graphical](#) | [Maps & aerials](#)

PF tabular

Duration	Average recurrence interval (years)									
	1	2	5	10	25	50	100	200	500	1000
5-min	0.347 (0.316-0.381)	0.414 (0.378-0.455)	0.492 (0.447-0.539)	0.548 (0.496-0.601)	0.617 (0.556-0.676)	0.668 (0.599-0.733)	0.718 (0.641-0.790)	0.764 (0.678-0.844)	0.822 (0.723-0.914)	0.868 (0.756-0.970)
10-min	0.555 (0.505-0.609)	0.663 (0.604-0.728)	0.788 (0.715-0.864)	0.876 (0.794-0.961)	0.984 (0.887-1.08)	1.06 (0.954-1.17)	1.14 (1.02-1.25)	1.21 (1.08-1.34)	1.30 (1.14-1.45)	1.37 (1.19-1.53)
15-min	0.693 (0.632-0.761)	0.833 (0.759-0.915)	0.996 (0.905-1.09)	1.11 (1.00-1.22)	1.25 (1.12-1.37)	1.35 (1.21-1.48)	1.44 (1.29-1.59)	1.53 (1.36-1.69)	1.64 (1.44-1.82)	1.72 (1.49-1.92)
30-min	0.950 (0.866-1.04)	1.15 (1.05-1.26)	1.42 (1.29-1.55)	1.61 (1.46-1.76)	1.85 (1.67-2.02)	2.03 (1.82-2.23)	2.21 (1.97-2.43)	2.38 (2.11-2.63)	2.61 (2.29-2.90)	2.78 (2.42-3.10)
60-min	1.19 (1.08-1.30)	1.44 (1.32-1.59)	1.82 (1.65-1.99)	2.09 (1.90-2.29)	2.46 (2.22-2.70)	2.75 (2.46-3.02)	3.04 (2.72-3.35)	3.34 (2.96-3.69)	3.74 (3.29-4.15)	4.05 (3.53-4.53)
2-hr	1.43 (1.29-1.57)	1.74 (1.58-1.91)	2.19 (1.99-2.41)	2.54 (2.30-2.79)	3.02 (2.71-3.31)	3.41 (3.04-3.73)	3.80 (3.37-4.18)	4.20 (3.70-4.63)	4.76 (4.14-5.29)	5.20 (4.48-5.81)
3-hr	1.56 (1.42-1.73)	1.90 (1.73-2.10)	2.41 (2.18-2.66)	2.80 (2.52-3.09)	3.35 (3.00-3.69)	3.79 (3.38-4.17)	4.25 (3.76-4.70)	4.73 (4.14-5.24)	5.39 (4.65-6.01)	5.94 (5.06-6.65)
6-hr	1.97 (1.79-2.18)	2.39 (2.17-2.65)	3.02 (2.73-3.33)	3.52 (3.17-3.89)	4.25 (3.80-4.69)	4.86 (4.31-5.36)	5.51 (4.84-6.09)	6.21 (5.40-6.88)	7.22 (6.16-8.06)	8.06 (6.77-9.06)
12-hr	2.40 (2.19-2.67)	2.91 (2.65-3.23)	3.69 (3.35-4.09)	4.35 (3.93-4.82)	5.34 (4.77-5.90)	6.19 (5.48-6.85)	7.13 (6.23-7.90)	8.16 (7.02-9.10)	9.71 (8.16-10.9)	11.0 (9.11-12.5)
24-hr	2.76 (2.56-2.98)	3.34 (3.10-3.60)	4.25 (3.95-4.59)	5.03 (4.65-5.42)	6.19 (5.68-6.65)	7.19 (6.54-7.71)	8.29 (7.48-8.89)	9.51 (8.49-10.2)	11.3 (9.96-12.2)	12.9 (11.2-13.9)
2-day	3.18 (2.95-3.46)	3.86 (3.57-4.19)	4.92 (4.55-5.35)	5.81 (5.35-6.31)	7.12 (6.52-7.70)	8.23 (7.48-8.90)	9.45 (8.52-10.2)	10.8 (9.62-11.7)	12.7 (11.2-13.8)	14.4 (12.5-15.7)
3-day	3.37 (3.14-3.65)	4.08 (3.79-4.42)	5.18 (4.81-5.61)	6.10 (5.64-6.59)	7.43 (6.84-8.01)	8.56 (7.82-9.22)	9.78 (8.88-10.5)	11.1 (10.0-12.0)	13.1 (11.6-14.1)	14.7 (12.9-15.9)
4-day	3.56 (3.32-3.84)	4.31 (4.01-4.64)	5.44 (5.07-5.87)	6.38 (5.93-6.88)	7.75 (7.15-8.33)	8.89 (8.16-9.55)	10.1 (9.24-10.9)	11.5 (10.4-12.3)	13.4 (12.0-14.4)	15.0 (13.3-16.2)
7-day	4.18 (3.90-4.49)	5.02 (4.69-5.40)	6.26 (5.84-6.73)	7.30 (6.78-7.83)	8.79 (8.13-9.42)	10.0 (9.25-10.8)	11.4 (10.4-12.2)	12.8 (11.7-13.7)	14.9 (13.4-16.0)	16.7 (14.9-17.9)
10-day	4.77 (4.47-5.10)	5.71 (5.36-6.11)	7.01 (6.57-7.49)	8.07 (7.55-8.61)	9.58 (8.92-10.2)	10.8 (10.0-11.5)	12.1 (11.2-12.9)	13.5 (12.4-14.4)	15.4 (14.0-16.4)	17.0 (15.3-18.2)
20-day	6.46 (6.11-6.83)	7.67 (7.26-8.11)	9.19 (8.71-9.72)	10.4 (9.84-11.0)	12.1 (11.4-12.7)	13.4 (12.6-14.1)	14.7 (13.8-15.5)	16.1 (15.0-17.0)	17.9 (16.6-19.0)	19.4 (17.8-20.6)
30-day	8.02 (7.63-8.44)	9.47 (9.00-9.97)	11.1 (10.6-11.7)	12.4 (11.8-13.1)	14.2 (13.4-14.9)	15.5 (14.6-16.3)	16.8 (15.8-17.7)	18.1 (17.0-19.1)	19.9 (18.6-21.0)	21.2 (19.7-22.4)
45-day	10.3 (9.78-10.7)	12.1 (11.5-12.6)	14.0 (13.3-14.6)	15.4 (14.7-16.1)	17.2 (16.4-18.0)	18.6 (17.7-19.5)	19.9 (18.9-20.9)	21.2 (20.0-22.3)	22.8 (21.5-24.0)	24.0 (22.5-25.3)
60-day	12.3 (11.7-12.8)	14.4 (13.8-15.1)	16.5 (15.8-17.2)	18.1 (17.3-18.9)	20.1 (19.2-21.0)	21.5 (20.5-22.5)	22.9 (21.8-23.9)	24.1 (22.9-25.3)	25.7 (24.4-27.0)	26.9 (25.4-28.2)

¹ Precipitation frequency (PF) estimates in this table are based on frequency analysis of partial duration series (PDS).

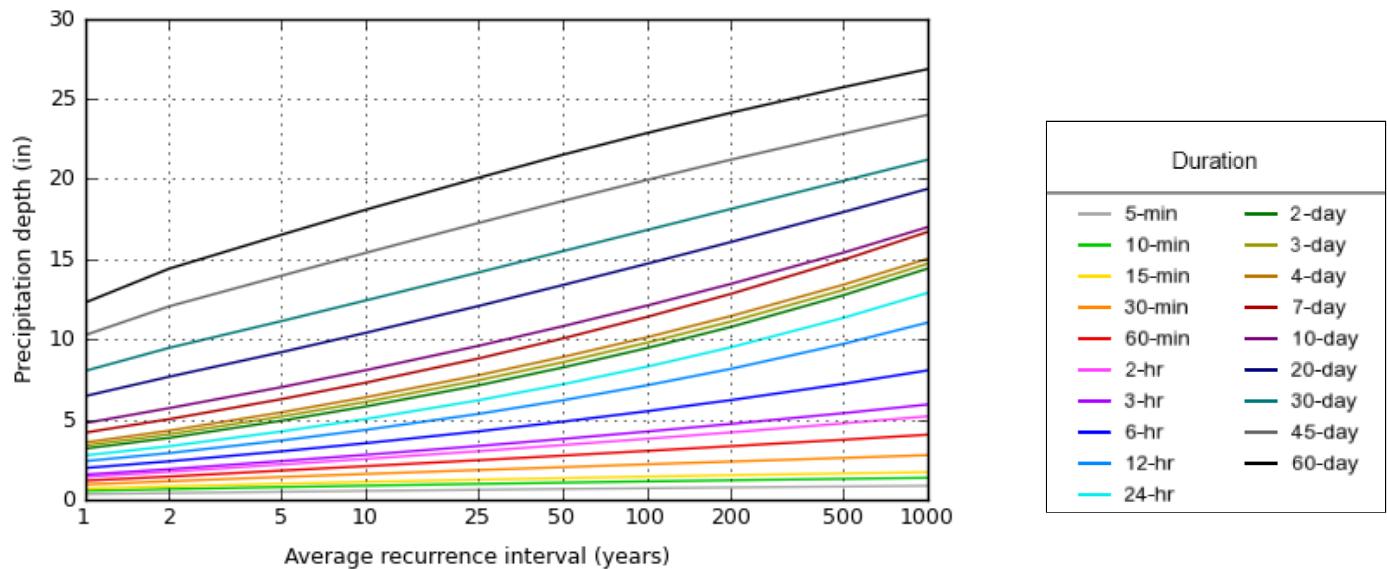
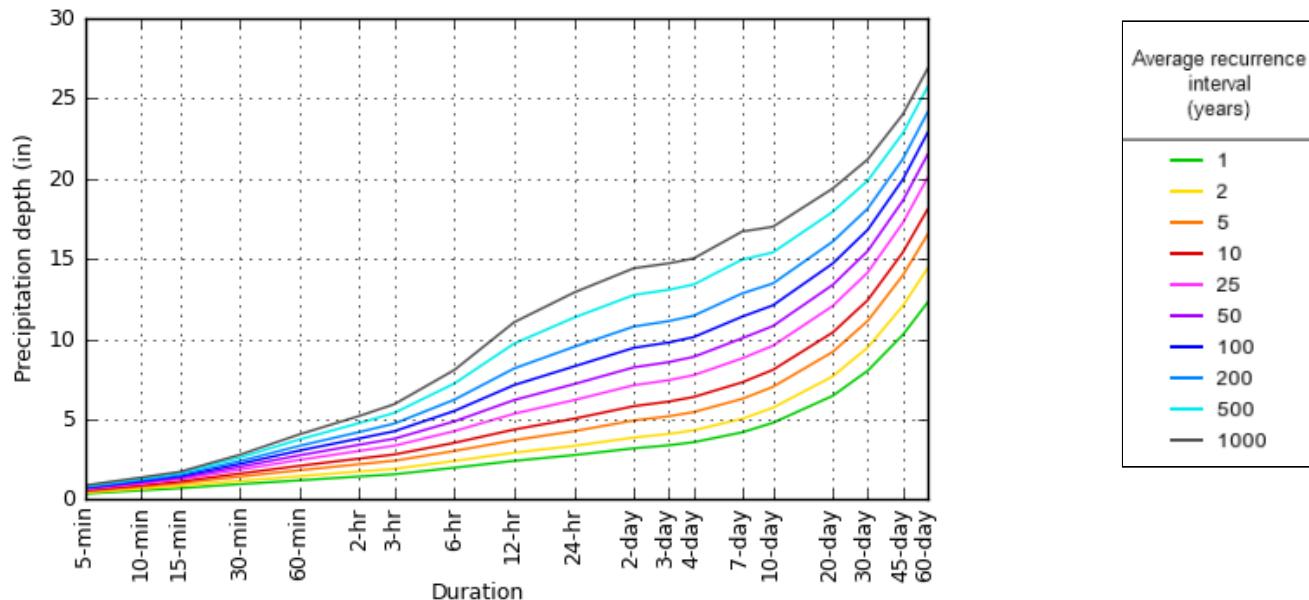
Numbers in parenthesis are PF estimates at lower and upper bounds of the 90% confidence interval. The probability that precipitation frequency estimates (for a given duration and average recurrence interval) will be greater than the upper bound (or less than the lower bound) is 5%. Estimates at upper bounds are not checked against probable maximum precipitation (PMP) estimates and may be higher than currently valid PMP values.

Please refer to NOAA Atlas 14 document for more information.

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PF graphical

PDS-based depth-duration-frequency (DDF) curves
Latitude: 40.1072°, Longitude: -74.8772°



NOAA Atlas 14, Volume 2, Version 3

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1325 East West Highway
Silver Spring, MD 20910
Questions?: HDSC.Questions@noaa.gov

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F. PEAK RATE SUMMARY

POD-01				
Design Storm	Pre-Development (CFS)	Max Allowable (CFS)	Post-Development (CFS)	Reduction in Flow (CFS)
1 YR	0.79	0.79	0.33	-0.46
2 YR	1.02	1.02	0.58	-0.44
5 YR	1.40	1.40	1.24	-0.16
10 YR	1.75	1.75	1.61	-0.14
25 YR	2.28	2.28	2.03	-0.25
50 YR	2.74	2.74	2.34	-0.40
100 YR	3.26	3.26	2.67	-0.59

POD-02				
Design Storm	Pre-Development (CFS)	Max Allowable (CFS)	Post-Development (CFS)	Reduction in Flow (CFS)
1 YR	0.17	0.17	0.17	0.00
2 YR	0.23	0.23	0.22	-0.01
5 YR	0.34	0.34	0.29	-0.05
10 YR	0.43	0.43	0.35	-0.08
25 YR	0.58	0.58	0.44	-0.14
50 YR	0.72	0.72	0.52	-0.20
100 YR	0.87	0.87	0.60	-0.27

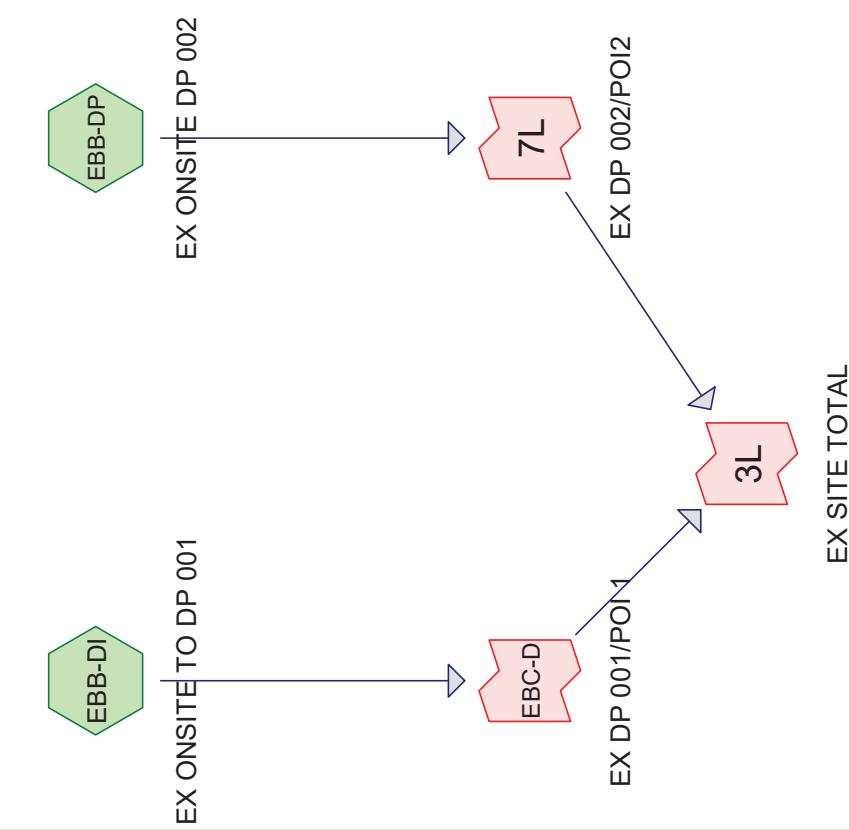
SITE TOTAL				
Design Storm	Pre-Development (CFS)	Max Allowable (CFS)	Post-Development (CFS)	Reduction in Flow (CFS)
1 YR	0.96	0.96	0.50	-0.46
2 YR	1.24	1.24	0.66	-0.58
5 YR	1.74	1.74	1.51	-0.23
10 YR	2.19	2.19	1.95	-0.24
25 YR	2.86	2.86	2.45	-0.41
50 YR	3.46	3.46	2.84	-0.62
100 YR	4.13	4.13	3.24	-0.89

**G. HYDROGRAPH SUMMARY REPORTS -
EXISTING CONDITIONS
1 YR, 2 YR, 5 YR, 10 YR, 25 YR, 50 YR & 100 YR**

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Project Notes

Rainfall events imported from "NJ-Rain.txt" for 6614 NJ Ocean-D
Rainfall events imported from "NJ-Rain.txt" for 6603 NJ Camden-C
Rainfall events imported from "NJ-Rain.txt" for 6603 NJ Camden-C
Rainfall events imported from "Atlas-14-Rain.txt" for 643 PA Adams
Rainfall events imported from "Atlas-14-Rain.txt" for 643 PA Adams
Rainfall events imported from "Atlas-14-Rain.txt" for 657 PA Chester
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Rainfall Events Listing (selected events)

Event#	Event Name	Storm Type	Curve	Mode	Duration (hours)	BfB	Depth (inches)	AMC
1	100-Year NOAA 24-hr	C	Default		24.00	1	7.55	2

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Area Listing (selected nodes)

	Area (sq-ft)	CN	Description (subcatchment-numbers)
	18,171	58	(EBB-DI, EBB-DP)
	15,132	98	Paved parking, HSG B (EBB-DI, EBB-DP)
TOTAL AREA	33,303	76	

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Soil Listing (selected nodes)

Area (sq-ft)	Soil Group	Subcatchment Numbers	
0	HSG A		
15,132	HSG B	EBB-DI, EBB-DP	
0	HSG C		
0	HSG D		
18,171	Other	EBB-DI, EBB-DP	
33,303		TOTAL AREA	

Ground Covers (selected nodes)

	HSG-A (sq-ft)	HSG-B (sq-ft)	HSG-C (sq-ft)	HSG-D (sq-ft)	Other (sq-ft)	Total (sq-ft)	Ground Cover	Subcatchmen Numbers
	0	0	0	0	0	18,171	18,171	
	0	15,132	0	0	0	15,132	15,132	Paved parking
	0	15,132	0	0	0	18,171	33,303	TOTAL AREA

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 NOAA 24-hr C 100-Year Rainfall=7.55"
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Time span=0.00-192.00 hrs, dt=0.05 hrs, 3841 points
 Runoff by SCS TR-20 method, UH=SCS, Weighted-Q

Reach routing by S stor-Ind+Trans method - Pond routing by Stor-Ind method

Subcatchment EBB-DI: EX ONSITE TO DP Runoff Area=25,682 sf 48.71% Impervious Runoff Depth=4.99" Tc=6.7 min CN=WQ Runoff=3.26 cfs 10,684 cf
Subcatchment EBB-DP: EX ONSITE DP 002 Runoff Area=7,621 sf 34.40% Impervious Runoff Depth=4.35" Tc=6.2 min CN=WQ Runoff=0.87 cfs 2,760 cf

Inflow=4.13 cfs 13,444 cf Primary=4.13 cfs 13,444 cf
 Inflow=0.87 cfs 2,760 cf Primary=0.87 cfs 2,760 cf

Inflow=3.26 cfs 10,684 cf Primary=3.26 cfs 10,684 cf
Total Runoff Area = 33,303 sf Runoff Volume = 13,444 cf Average Runoff Depth = 4.84"
 54.56% Pervious = 18,171 sf 45.44% Impervious = 15,132 sf

Link 3L: EX SITE TOTAL

Link 7L: EX DP 002/POI2

Link EBC-D: EX DP 001/POI 1

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 NOAA 24-hr C 100-Year Rainfall=7.55"
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Summary for Subcatchment EBB-DI: EX ONSITE TO DP 001

Runoff = 3.26 cfs @ 12.14 hrs, Volume= 10,684 cf, Depth= 4.99"
 Routed to Link EBC-D : EX DP 001/POI 1

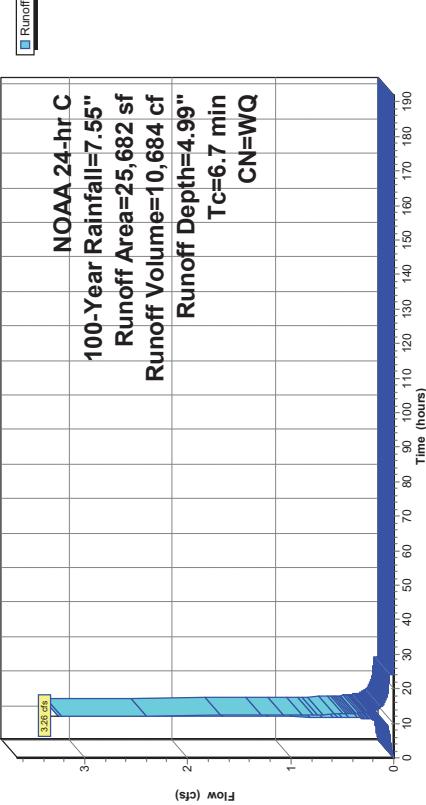
Runoff by SCS TR-20 method, UH=SCS, Weighted-Q, Time Span= 0.00-192.00 hrs, dt= 0.05 hrs
 NOAA 24-hr C 100-Year Rainfall=7.55"

Area (sf)	CN	Description
12,510	98	Paved parking, HSG B
*	58	
4,833	58	
*	58	
8,339	58	
25,682	Weighted Average	
13,172	58	51.29% Pervious Area
12,510	98	48.71% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.7	6.7				Direct Entry, Flow Path

Subcatchment EBB-DI: EX ONSITE TO DP 001

Hydrograph



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NOAA 24-hr C 100-Year Rainfall=7.55"
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West Chester HydroCAD - REV2
 NOAA 24-hr C 100-Year Rainfall=7.55"
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Summary for Subcatchment EBB-DP: EX ONSITE DP 002

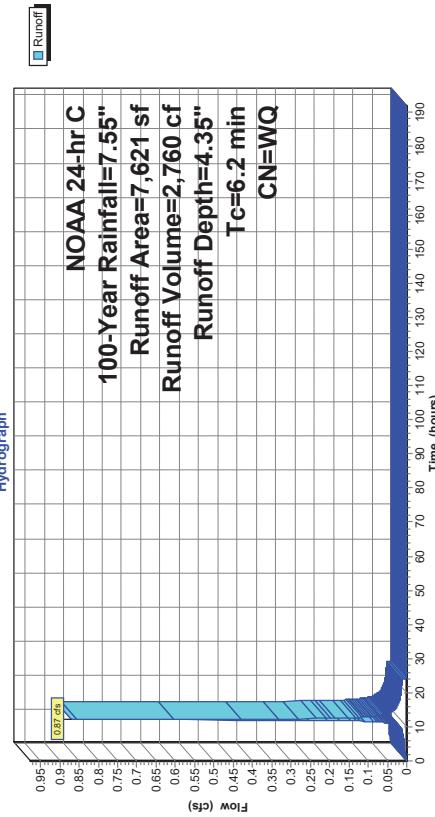
Runoff = 0.87 cfs @ 12.13 hrs, Volume= 2,760 cf, Depth= 4.35"
 Routed to Link 7L : EX DP 002/PO12

Runoff by SCS TR-20 method, UH=SCS, Weighted-Q, Time Span= 0.00-192.00 hrs, dt= 0.05 hrs

NOAA 24-hr C 100-Year Rainfall=7.55"

Area (sf)	CN	Description			
2,622	98	Paved parking, HSG B			
3,251	58	Weighted Average			
*	1,748	65.60% Pervious Area			
7,621	58	34.40% Impervious Area			
4,999	98				
2,622	98				
Tc	Length	Slope	Velocity	Capacity	Description
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
6.2					Direct Entry, TC Path

Subcatchment EBB-DP: EX ONSITE DP 002



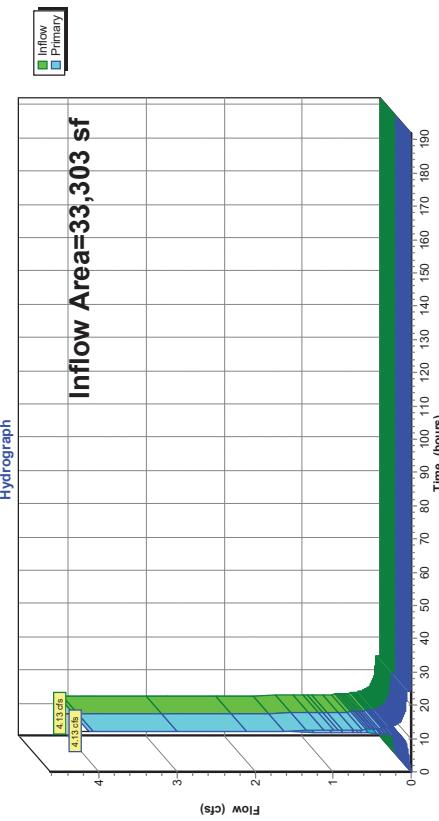
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 NOAA 24-hr C 100-Year Rainfall=7.55"
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NOAA 24-hr C 100-Year Rainfall=7.55"
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Summary for Link 3L: EX SITE TOTAL

Inflow Area = 33,303 sf, 45.44% Impervious, Inflow Depth = 4.84" for 100-Year event
 Inflow = 4.13 cfs @ 12.14 hrs, Volume= 13,444 cf
 Primary = 4.13 cfs @ 12.14 hrs, Volume= 13,444 cf, Atten= 0%, Lag= 0.0 min
 Primary outflow = Inflow, Time Span= 0.00-192.00 hrs, dt= 0.05 hrs

Link 3L: EX SITE TOTAL



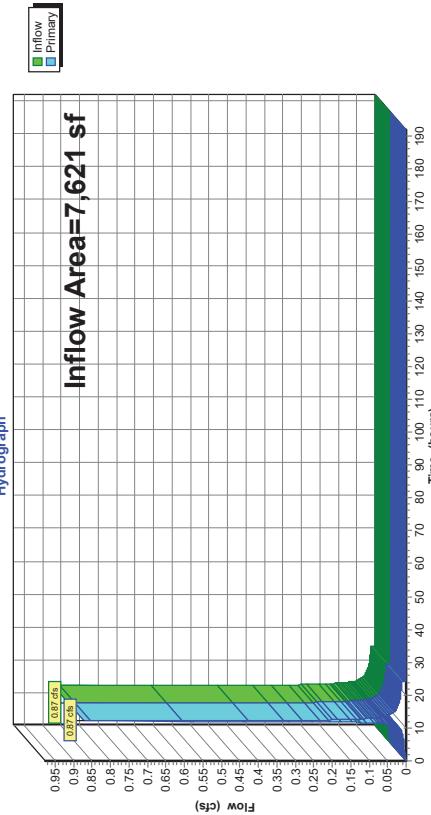
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Inflow Area = 7,621 sf, 34.40% Impervious, Inflow Depth = 4.35" for 100-Year event
 Inflow = 0.87 cfs @ 12.13 hrs, Volume= 2,760 cf
 Primary = 0.87 cfs @ 12.13 hrs, Volume= 2,760 cf, Atten= 0%, Lag= 0.0 min
 Routed to Link 3L : EX SITE TOTAL

Primary outflow = Inflow, Time Span= 0.00-192.00 hrs, dt= 0.05 hrs

Link 7L: EX DP 002/POI2



Link 7L: EX DP 002/POI2



Link EBC-D: EX DP 001/POI 1

Inflow Area = 25,682 sf, 48.71% Impervious, Inflow Depth = 4.99" for 100-Year event
 Inflow = 3.26 cfs @ 12.14 hrs, Volume= 10,684 cf
 Primary = 3.26 cfs @ 12.14 hrs, Volume= 10,684 cf, Atten= 0%, Lag= 0.0 min
 Routed to Link 3L : EX SITE TOTAL

Primary outflow = Inflow, Time Span= 0.00-192.00 hrs, dt= 0.05 hrs

Link EBC-D: EX DP 001/POI 1



Summary for Link 7L: EX DP 002/POI2

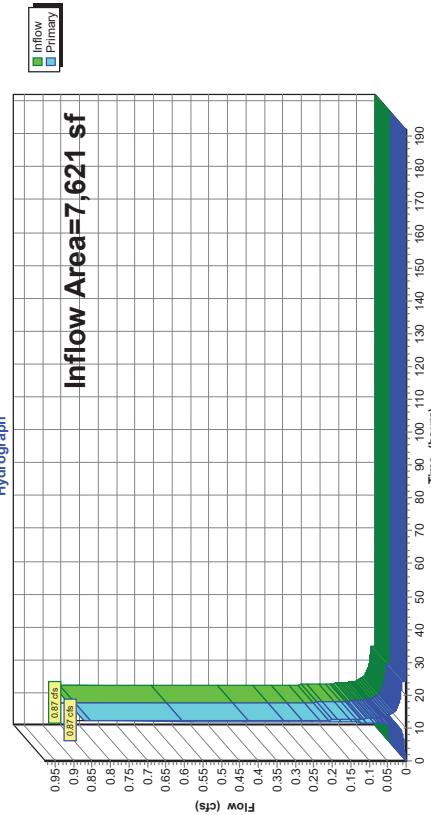
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 NOAA 24-hr C 100-Year Rainfall=7.55"
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Inflow Area = 7,621 sf, 34.40% Impervious, Inflow Depth = 4.35" for 100-Year event
 Inflow = 0.87 cfs @ 12.13 hrs, Volume= 2,760 cf
 Primary = 0.87 cfs @ 12.13 hrs, Volume= 2,760 cf, Atten= 0%, Lag= 0.0 min
 Routed to Link 3L : EX SITE TOTAL

Primary outflow = Inflow, Time Span= 0.00-192.00 hrs, dt= 0.05 hrs

Link 7L: EX DP 002/POI2



Summary for Link EBC-D: EX DP 001/POI 1

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 NOAA 24-hr C 100-Year Rainfall=7.55"
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 NOAA 24-hr C 100-Year Rainfall=7.55"
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Inflow Area = 25,682 sf, 48.71% Impervious, Inflow Depth = 4.99" for 100-Year event
 Inflow = 3.26 cfs @ 12.14 hrs, Volume= 10,684 cf
 Primary = 3.26 cfs @ 12.14 hrs, Volume= 10,684 cf, Atten= 0%, Lag= 0.0 min
 Routed to Link 3L : EX SITE TOTAL

Primary outflow = Inflow, Time Span= 0.00-192.00 hrs, dt= 0.05 hrs

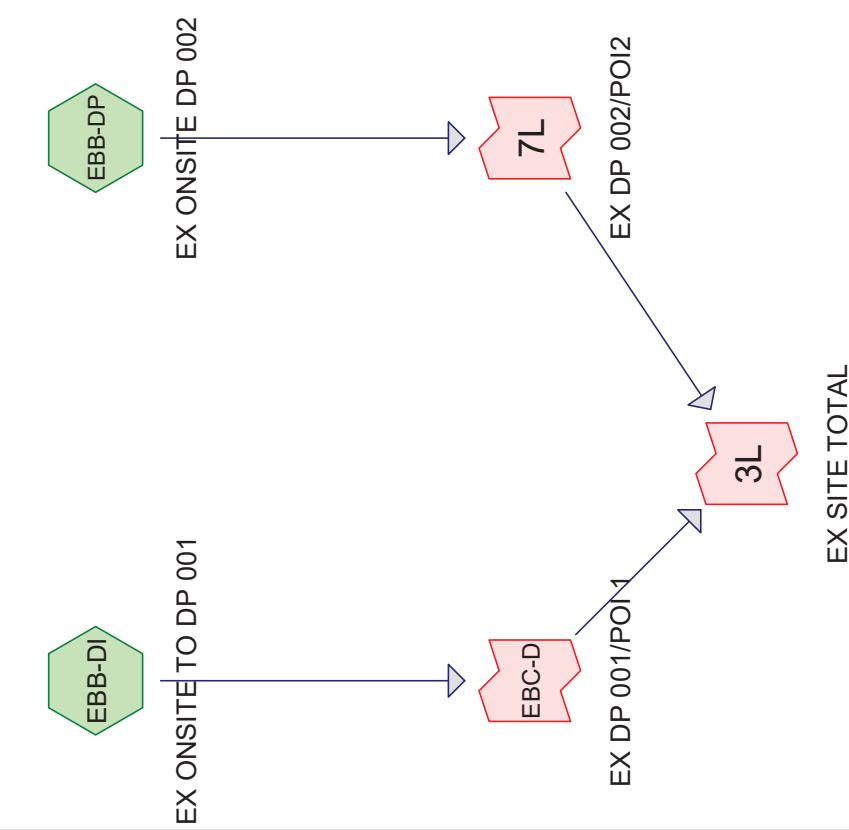
Link EBC-D: EX DP 001/POI 1



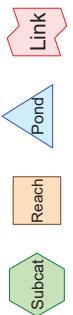
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Routing Diagram for West Chester HydroCAD - REV2
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Project Notes

Rainfall events imported from "NJ-Rain.txt" for 6614 NJ Ocean-D
Rainfall events imported from "NJ-Rain.txt" for 6603 NJ Camden-C
Rainfall events imported from "NJ-Rain.txt" for 6603 NJ Camden-C
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Rainfall events imported from "Atlas-14-Rain.txt" for 657 PA Chester
Rainfall events imported from "Atlas-14-Rain.txt" for 657 PA Chester
Rainfall events imported from "Atlas-14-Rain.txt" for 657 PA Chester

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Area Listing (selected nodes)

Area (sq-ft)	CN	Description (subcatchment-numbers)
18,171	58	(EBB-DI, EBB-DP)
15,132	98	Paved parking, HSG B (EBB-DI, EBB-DP)
33,303	76	TOTAL AREA

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Soil Listing (selected nodes)

Area (sq-ft)	Soil Group	Subcatchment Numbers
0	HSG A	
15,132	HSG B	EBB-DI, EBB-DP
0	HSG C	
0	HSG D	
18,171	Other	EBB-DI, EBB-DP
33,303		TOTAL AREA

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HydroCAD® 10.20-5c s/n 08640 © 2023 HydroCAD Software Solutions LLC**Ground Covers (selected nodes)**

HSG-A (sq-ft)	HSG-B (sq-ft)	HSG-C (sq-ft)	HSG-D (sq-ft)	Other (sq-ft)	Total (sq-ft)	Ground Cover	Subcatchmen Numbers
0	0	0	0	0	18,171	18,171	
0	15,132	0	0	0	15,132	Paved parking	
0	15,132	0	0	0	18,171	33,303	TOTAL AREA

Time span=0.00-192.00 hrs, dt=0.05 hrs, 3841 points
 Runoff by SCS TR-20 method, UH=SCS, Weighted-Q
 Reach routing by Stor-ind+Trans method - Pond routing by Stor-ind method

Subcatchment EBB-D: EX ONSITE TO DP Runoff Area=25,682 sf 48.71% Impervious Runoff Depth=4.98" Tc=6.7 min CN=WQ Runoff=3,26 cfs 10,684 cf

Subcatchment EBB-DP: EX ONSITE DP 002 Runoff Area=7,621 sf 34.40% Impervious Runoff Depth=4.35" Tc=6.2 min CN=WQ Runoff=.87 cfs 2,760 cf

Link 31: EX SITE TOTAL

Link 71: EX DP 002/POI2

Link EBC-D: EX DP 001/POI 1

Total Runoff Area = 33,303 sf Runoff Volume = 13,444 cf Average Runoff Depth = 4.84"
 54.56% Pervious = 18,171 sf 45.44% Impervious = 15,132 sf

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Summary for Subcatchment EBB-DI: EX ONSITE TO DP 001

Runoff = 3.26 cfs @ 12.14 hrs, Volume= 10,684 cf, Depth= 4.99"

Routed to Link EBC-D : EX DP 001/POI 1

Runoff by SCS TR-20 method, UH=SCS, Weighted-Q, Time Span= 0.00-192.00 hrs, dt= 0.05 hrs

NOAA 24-hr C 100-Year Rainfall=7.55"

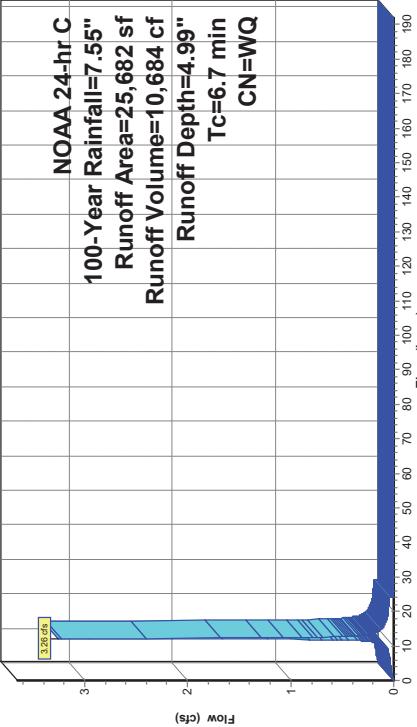
Area (sf)	CN	Description
12,510	98	Paved parking, HSG B
4,833	58	
*	8,339	58

Tc	Length	Slope	Velocity	Capacity	Description
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
13.172	58	51.29%	Average		
12,510	98	48.71%	Impervious Area		

Tc	Length	Slope	Velocity	Capacity	Description
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
6.7	6.2	0.0000	0.0000	0.0000	Direct Entry, Flow Path

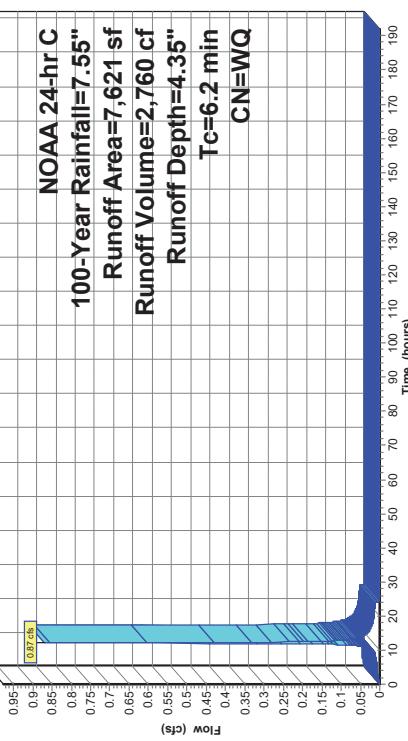
Subcatchment EBB-DI: EX ONSITE TO DP 001

Hydrograph



Summary for Subcatchment EBB-DP: EX ONSITE DP 002

Hydrograph



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NOAA 24-hr C 100-Year Rainfall=7.55"
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Summary for Link 3L: EX SITE TOTAL

Inflow Area = 33,303 sf, 45.44% Impervious, Inflow Depth = 4.84" for 100-Year event
Inflow = 4.13 cfs @ 12.14 hrs, Volume= 13,444 cf
Primary = 4.13 cfs @ 12.14 hrs, Volume= 13,444 cf, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-192.00 hrs, dt= 0.05 hrs

Link 3L: EX SITE TOTAL

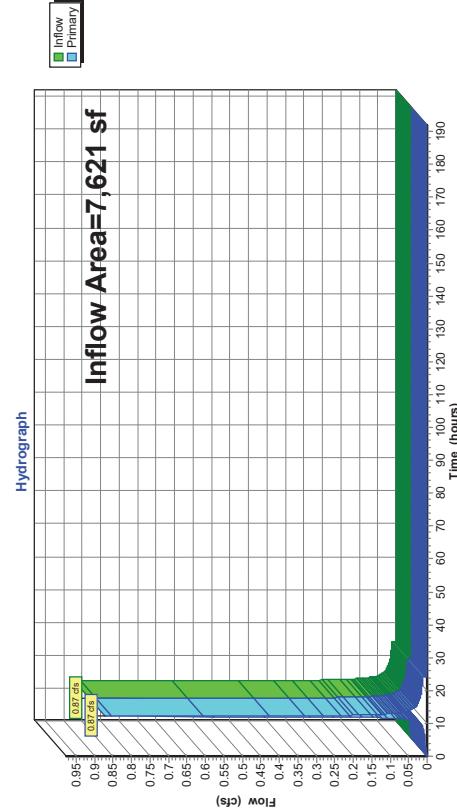


Summary for Link 7L: EX DP 002/PO12

Inflow Area = 7,621 sf, 34.40% Impervious, Inflow Depth = 4.35" for 100-Year event
Inflow = 0.87 cfs @ 12.13 hrs, Volume= 2,760 cf
Primary = 0.87 cfs @ 12.13 hrs, Volume= 2,760 cf, Atten= 0%, Lag= 0.0 min
Routed to Link 3L : EX SITE TOTAL

Primary outflow = Inflow, Time Span= 0.00-192.00 hrs, dt= 0.05 hrs

Link 7L: EX DP 002/PO12



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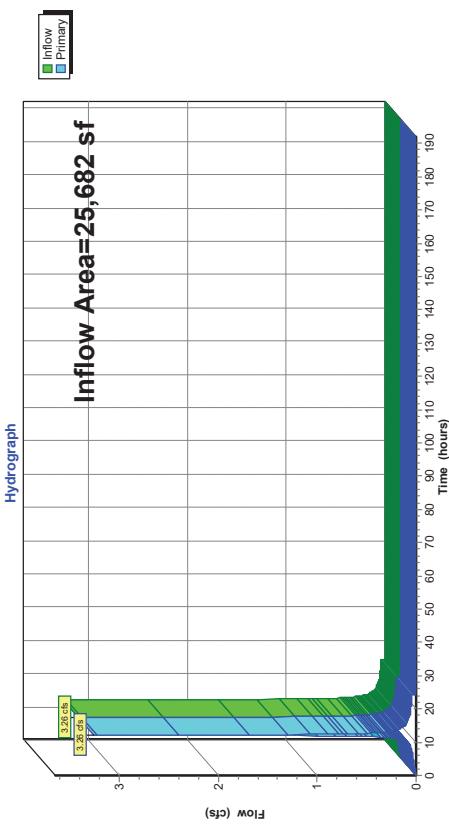
NOAA 24-hr C 100-Year Rainfall=7.55"
Printed 11/2/2024

Summary for Link EBC-D: EX DP 001/POI 1

Inflow Area = 25,682 sf, 48.71% Impervious, Inflow Depth = 4.99" for 100-Year event
Inflow = 3.26 cfs @ 12.14 hrs, Volume= 10,684 cf
Primary = 3.26 cfs @ 12.14 hrs, Volume= 10,684 cf, Atten= 0%, Lag= 0 min
Routed to Link 31 : EX SITE TOTAL

Primary outflow = Inflow, Time Span= 0.00-192.00 hrs, dt= 0.05 hrs

Link EBC-D: EX DP 001/POI 1



**H. HYDROGRAPH SUMMARY REPORTS –
PROPOSED CONDITIONS
1 YR, 2 YR, 5 YR, 10 YR, 25 YR, 50 YR & 100 YR**

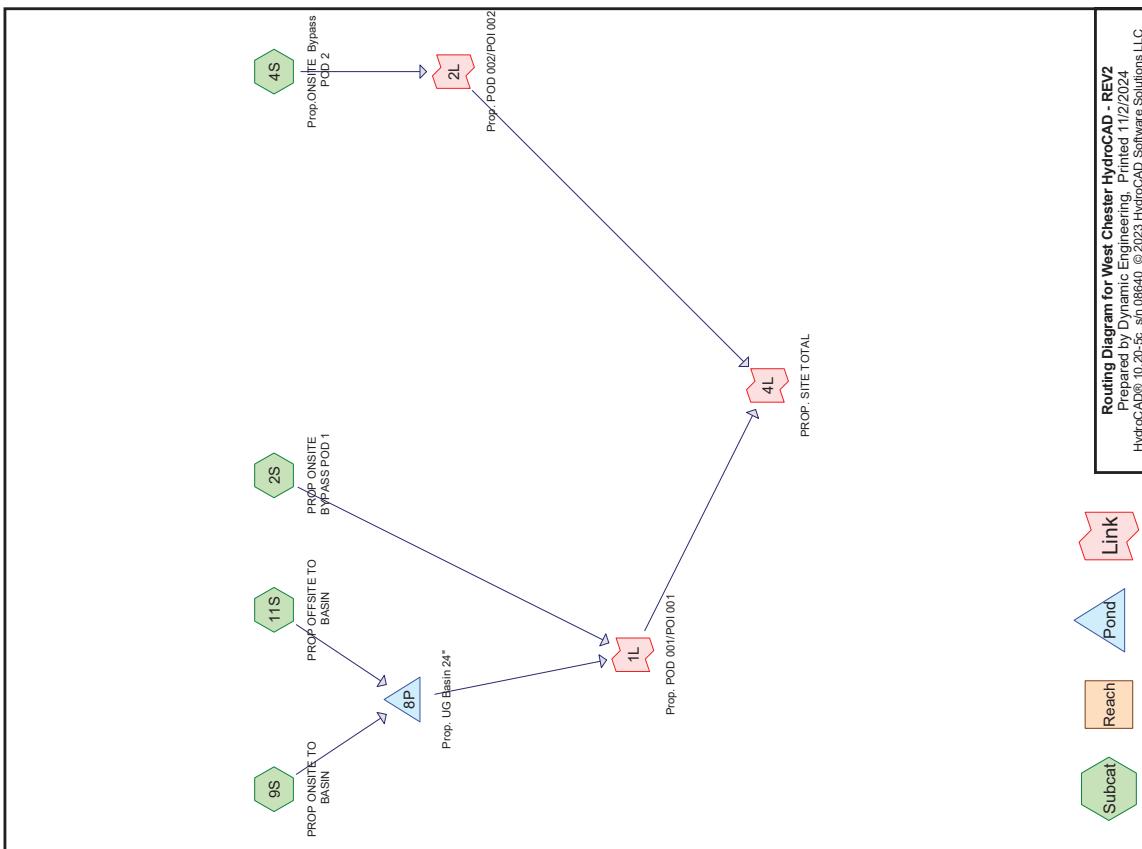
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Project Notes

Rainfall events imported from "NJ-Rain.txt" for 6614 NJ Ocean-D
Rainfall events imported from "NJ-Rain.txt" for 6603 NJ Camden-C
Rainfall events imported from "NJ-Rain.txt" for 6603 NJ Camden-C
Rainfall events imported from "Atlas-14-Rain.txt" for 643 PA Adams
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Rainfall events imported from "Atlas-14-Rain.txt" for 657 PA Chester



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Area Listing (selected nodes)

Area (sq-ft)	CN	Description (subcatchment-numbers)
8,527	98	(2S, 11S) (2S, 9S, 11S)
12,291	61	Paved parking, HSG B (4S, 9S)
20,247	98	Sewer Ex per (4S)
1,216	61	
42,281	86	TOTAL AREA

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Soil Listing (selected nodes)

Area (sq-ft)	Soil Group	Subcatchment Numbers
0	HSG A	
20,247	HSG B	4S, 9S
0	HSG C	
0	HSG D	
22,034	Other	2S, 4S, 9S, 11S
42,281		TOTAL AREA

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Ground Covers (selected nodes)

HSG-A (sq-ft)	HSG-B (sq-ft)	HSG-C (sq-ft)	HSG-D (sq-ft)	Other (sq-ft)	Total (sq-ft)	Ground Cover	Subcatchmen Numbers
0	0	0	0	0	20,818	20,818	2
0	20,247	0	0	0	0	20,247	Paved parking 4
0	0	0	0	0	1,216	1,216	Sewer Ext per 4
0	20,247	0	0	0	22,034	42,281	TOTAL AREA

Pipe Listing (selected nodes)

Line#	Node Number	In-Invert (feet)	Out-Invert (feet)	Length (feet)	Slope (ft/ft)	n	Width (inches)	Diam/Height (inches)	Inside-Fill (inches)	Node Name
1	8P	407.10	406.45	129.0	0.0050	0.012	0.0	15.0	0.0	

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NOAA 24-hr C 100-Year Rainfall=7.55"
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Time span=0-00:192.00 hrs, dt=0.05 hrs, 3841 points
 Runoff by SCS TR-20 method, UH=SCS, Weighted-Q

Reach routing by S stor-Ind+Trans method - Pond routing by Stor-Ind method
Subcatchment 2S: PROP ONSITE BYPASS Runoff Area=6,935 sf 73.64% Impervious Runoff Depth=6.20"
 $T_c=6.0 \text{ min}$ CN=WQ Runoff=1.08 cfs 3.584 cf

Subcatchment 4S: Prop.ONBSITE Bypass Runoff Area=3,942 sf 69.15% Impervious Runoff Depth=6.01"
 $T_c=6.0 \text{ min}$ CN=WQ Runoff=0.60 cfs 1.975 cf

Subcatchment 9S: PROP ONSITE TO Runoff Area=21,903 sf 79.99% Impervious Runoff Depth=6.47"
 $T_c=6.0 \text{ min}$ CN=WQ Runoff=3.54 cfs 11.808 cf

Subcatchment 11S: PROP OFFSITE TO Runoff Area=9,501 sf 36.00% Impervious Runoff Depth=4.62"
 $T_c=6.0 \text{ min}$ CN=WQ Runoff=1.16 cfs 3.657 cf

Pond 8P: Prop. UG Basin 24" Peak Elev=409.47' Storage=5,172 cf Inflow=4.71 cfs 15.465 cf
 Discarded=0.01 cfs 3.646 cf Primary=2.36 cfs 11.820 cf Outflow=2.38 cfs 15.465 cf
 Inflow=2.92 cfs 15.404 cf Primary=2.92 cfs 15.404 cf

Link 1L: Prop. POD 001/POI 001

Inflow=0.60 cfs 1.975 cf
 Primary=0.60 cfs 1.975 cf

Link 2L: Prop. POD 002/POI 002

Inflow=3.49 cfs 17.379 cf
 Primary=3.49 cfs 17.379 cf

Link 4L: PROP. SITE TOTAL

Total Runoff Area = 42,281 sf Runoff Volume = 21,025 cf Average Runoff Depth = 5.97"
 31.95% Pervious = 13,507 sf 68.05% Impervious = 28,774 sf

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NOAA 24-hr C 100-Year Rainfall=7.55"
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Summary for Subcatchment 2S: PROP ONSITE BYPASS POD 1

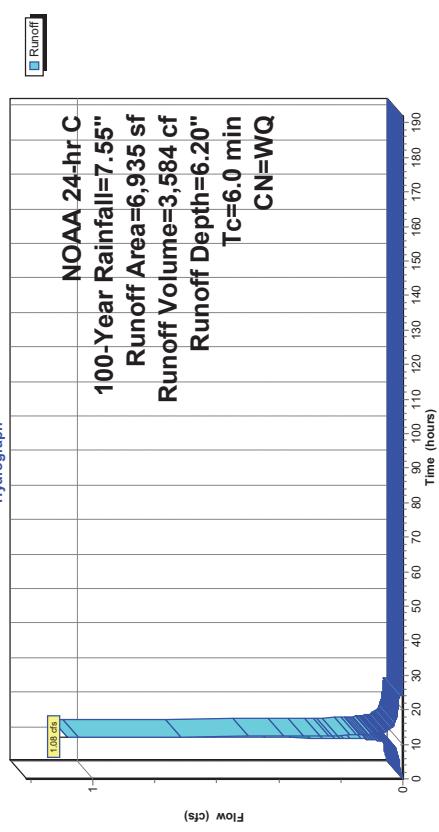
Runoff = 1.08 cfs @ 12.13 hrs, Volume= 3,584 cf, Depth= 6.20"
 Routed to Link 1L : Prop. POD 001/POI 001

Runoff by SCS TR-20 method, UH=SCS, Weighted-Q, Time Span= 0.00-192.00 hrs, dt= 0.05 hrs
 NOAA 24-hr C 100-Year Rainfall=7.55"

Area (sf)	CN	Description
*	5,107	98
*	1,828	61

T _c (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.0	6,935	Weighted Average	1,828	61	26.36% Pervious Area
*	5,107	98	1,828	61	73.64% Impervious Area

Subcatchment 2S: PROP ONSITE BYPASS POD 1



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Summary for Subcatchment 4S: Prop.ONSITE Bypass POD 2

Runoff = 0.60 cfs @ 12.13 hrs, Volume= 1.975 cf, Depth= 6.01"
 Routed to Link 2L : Prop. POD 002/POI 002

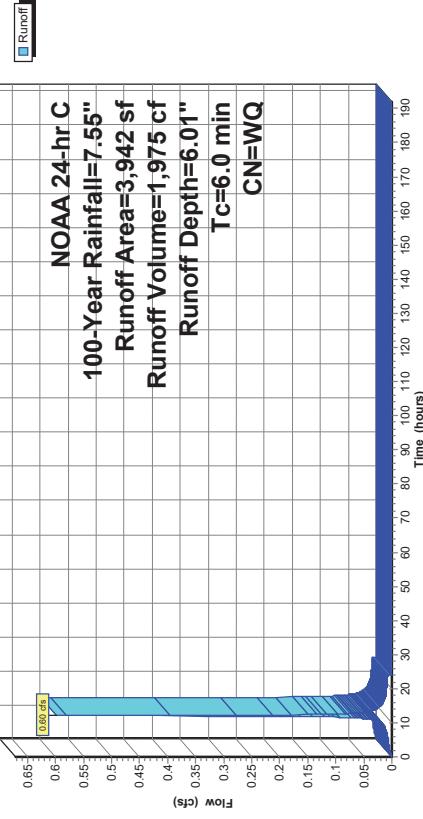
Runoff by SCS TR-20 method, UH=SCS, Weighted-Q, Time Span= 0.00-192.00 hrs, dt= 0.05 hrs
 NOAA 24-hr C 100-Year Rainfall=7.55"

Area (sf)	CN	Description
2,726	98	Paved parking, HSG B
*	1,216	61 Sewer Ext per

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.0	6.0	0.00	0.00	0.00	Direct Entry, Flow Path

Subcatchment 4S: Prop.ONSITE Bypass POD 2

Hydrograph



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Summary for Subcatchment 9S: PROP ONSITE TO BASIN

Runoff = 3.54 cfs @ 12.13 hrs, Volume= 11,808 cf, Depth= 6.47"
 Routed to Pond 8P : Prop. UG Basin 24"

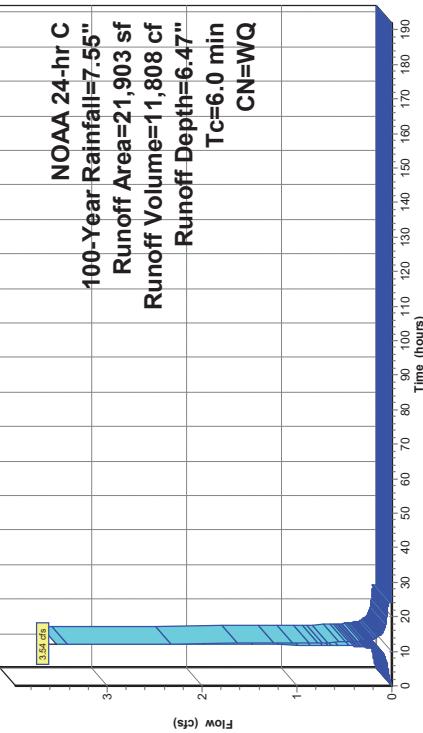
Runoff by SCS TR-20 method, UH=SCS, Weighted-Q, Time Span= 0.00-192.00 hrs, dt= 0.05 hrs
 NOAA 24-hr C 100-Year Rainfall=7.55"

Area (sf)	CN	Description
*	17,521	98 Paved parking, HSG B
*	4,382	61 Weighted Average
	4,382	61 20.01% Pervious Area
	17,521	98 79.99% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.0	6.0	0.00	0.00	0.00	Direct Entry, Flow Path

Subcatchment 9S: PROP ONSITE TO BASIN

Hydrograph



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NOAA 24-hr C 100-Year Rainfall=7.55"
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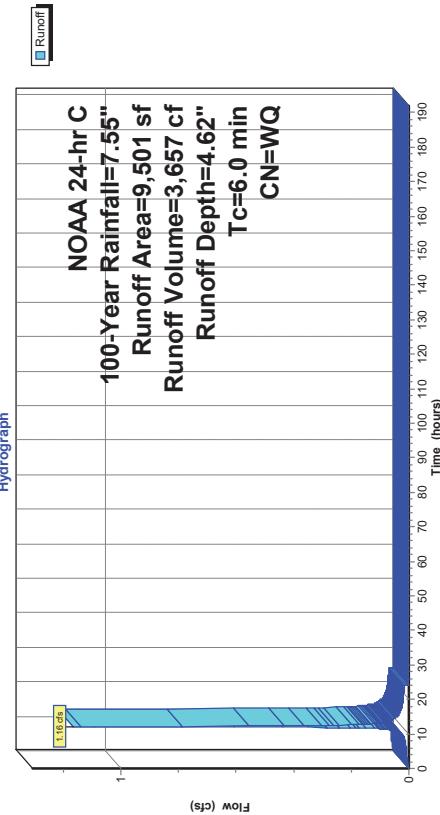
Summary for Subcatchment 11S: PROP OFFSITE TO BASIN

Runoff	=	1.16 cfs @ 12.13 hrs, Volume= 3,657 cf, Depth= 4.62"
Routed to Pond 8P : Prop. UG Basin 24"		
Runoff by SCS TR-20 method, UH=SCS, Weighted-Q, Time Span= 0.00-192.00 hrs, dt= 0.05 hrs		
NOAA 24-hr C 100-Year Rainfall=7.55"		
Area (sf)	CN	Description
*	3,420	98
*	6,081	61

Tc	Length	Slope	Velocity	Capacity	Description
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
3.420	9501	Weighted Average			
6,081	61	64.00% Pervious Area			
3.420	98	36.00% Impervious Area			

Hydrograph	Direct Entry, Flow Path
6.0	16.65

Subcatchment 11S: PROP OFFSITE TO BASIN



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Summary for Pond 8P: Prop. UG Basin 24"

Inflow Area =	31,404 sf, 66.68% Impervious, Inflow Depth = 5.91"	for 100-Year event
Inflow =	4.71 cfs @ 12.13 hrs, Volume= 15,465 cf	
Outflow =	2.38 cfs @ 12.25 hrs, Volume= 15,465 cf	
Discarded =	0.01 cfs @ 2.00 hrs, Volume= 3,646 cf	
Primary =	2.36 cfs @ 12.25 hrs, Volume= 11,820 cf	
Routed to Link 1L : Prop. POD 001/POI 001		
Routing by Stor-Ind method, Time Span= 0.00-192.00 hrs, dt= 0.05 hrs		
Peak Elev= 409.47' @ 12.25 hrs Surf.Area= 3,090 sf Storage= 5,172 cf		
Plug-Flow detention time= 393.5 min calculated for 15,461 cf (100% of inflow)		
Center-of-Mass det. time= 394.2 min (1,155.6 - 761.5)		
Volume	Invert	Avail.Storage
#1A	406.00'	3,834 cf 20.83'W x 148.33'L x 3.83'H Field A
#2A	407.00'	1,788 cf ADS N-12 "24" x 28 Inside #1
		Inside= 23.8" W x 23.8" H => 3.10 sf x 20.00'L = 62.0 cf
		Outside= 28.0" W x 28.0" H => 3.92 sf x 20.00'L = 78.4 cf
		28 Chambers in 4 Rows
		16.83 Header x 3.10 sf x 1 = 52.2 cf Inside
		5,622 cf Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Primary	407.10'	15.0" Round Culvert
		L= 129.0' CPP projecting, no headwall, Ke= 0.900	
		Inlet / Outlet Invert= 407.10' / 406.45' S= 0.0050 '/' Cc= 0.900	
		n= 0.012 Corrugated PP, smooth interior, Flow Area= 1.23 sf	
#2	Discarded	406.00'	0.200 in/hr Exfiltration over Surface area
#3	Device 1	407.80'	17.0" W x 3.0" H Vert. 3"x17" Orifice C= 0.600
#4	Device 1	409.40'	4.0" long Sharp-Crested Vee/Trap Weir Cv= 2.62 (C= 3.28)
			Discarded OutFlow Max=0.01 cfs @ 2.00 hrs HW=406.04' (Free Discharge)
			2=Exfiltration (Exfiltration Controls 0.01 cfs)
			Primary OutFlow Max=2.35 cfs @ 12.25 hrs HW=409.47' (Free Discharge)
			1=Culvert (Passes 2.35 cfs potential flow)
			3-3"x17" Orifice (Orifice Controls 2.12 cfs @ 5.98 fps)
			4=Sharp-Crested Vee/Trap Weir (Weir Controls 0.23 cfs @ 0.85 fps)

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Pond 8P: Prop. UG Basin 24" - Chamber Wizard Field A

Chamber Model = ADS N-12" 24" (ADS N-12® Pipe)

Inside= 23.8" W x 23.8" H => 3.10 sf x 20.00'L = 62.0 cf
 Outside= 28.0" W x 28.0" H => 3.92 sf x 20.00'L = 78.4 cf

28.0" Wide + 30.0" Spacing = 58.0" C-C Row Spacing

7 Chambers/Row x 20.00' Long +2.33' Header x 1 = 142.33' Row Length +36.0" End Stone x 2 = 148.33'

Base Length 4 Rows x 28.0" Wide + 30.0" Spacing x 3 + 24.0" Side Stone x 2 = 20.83' Base Width

12.0" Stone Base + 28.0" Chamber Height + 6.0" Stone Cover = 3.83' Field Height

28 Chambers x 62.0 cf + 16.83 Header x 3.10 sf = 1.788.2 cf Chamber Storage

28 Chambers x 78.4 cf + 16.83 Header x 3.92 sf = 2.261.9 cf Displacement

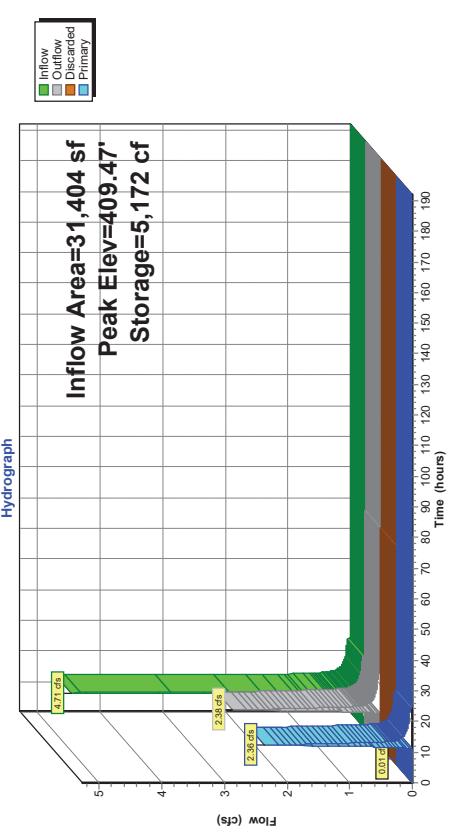
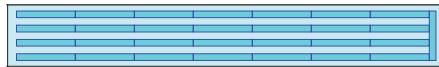
11,846.3 cf Field - 2,261.9 cf Chambers = 9,584.4 cf Stone x 40.0% Voids = 3,833.8 cf Stone Storage

Chamber Storage + Stone Storage = 5,621.9 cf = 0.129 af

Overall Storage Efficiency = 47.5%

Overall System Size = 148.33' x 20.83' x 3.83'

28 Chambers
 438.8 cy Field
 355.0 cy Stone



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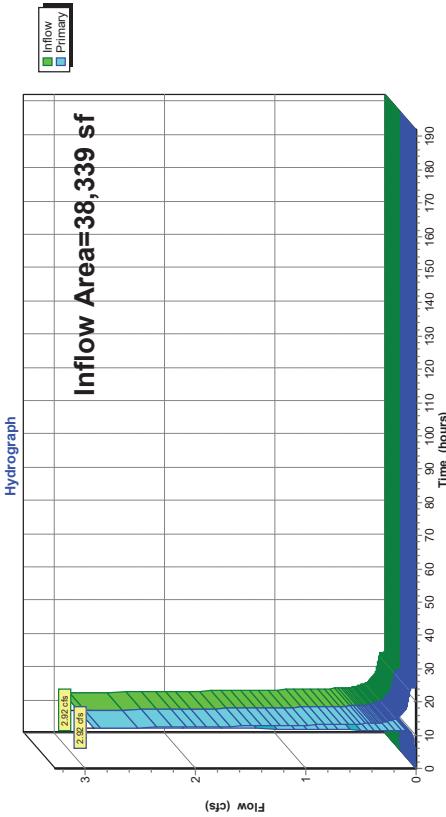
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 NOAA 24-hr C 100-Year Rainfall=7.55"
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Summary for Link 1L: Prop. POD 001/POI 001

Inflow Area = 38,339 sf, 67.94% Impervious, Inflow Depth = 4.82" for 100-Year event
 Inflow = 2.92 cfs @ 12.16 hrs, Volume= 15,404 cf
 Primary = 2.92 cfs @ 12.16 hrs, Volume= 15,404 cf, Atten= 0%, Lag= 0.0 min
 Routed to Link 4L : PROP. SITE TOTAL

Primary outflow = Inflow, Time Span= 0.00-192.00 hrs, dt= 0.05 hrs

Link 1L: Prop. POD 001/POI 001

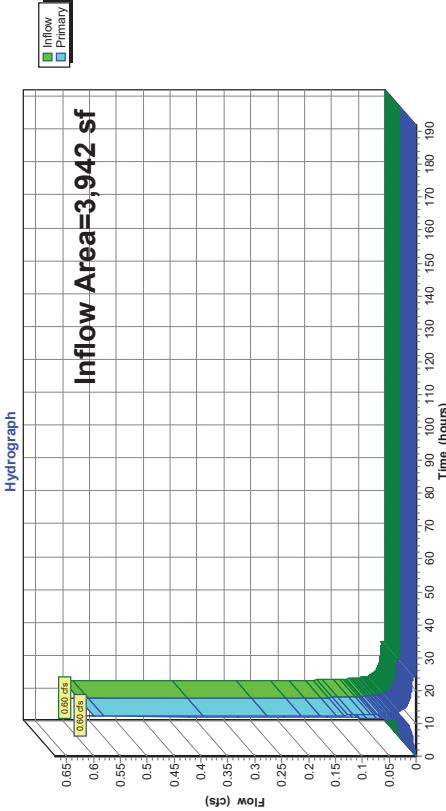


Summary for Link 2L: Prop. POD 002/POI 002

Inflow Area = 3,942 sf, 69.15% Impervious, Inflow Depth = 6.01" for 100-Year event
 Inflow = 0.60 cfs @ 12.13 hrs, Volume= 1,975 cf
 Primary = 0.60 cfs @ 12.13 hrs, Volume= 1,975 cf, Atten= 0%, Lag= 0.0 min
 Routed to Link 4L : PROP. SITE TOTAL

Primary outflow = Inflow, Time Span= 0.00-192.00 hrs, dt= 0.05 hrs

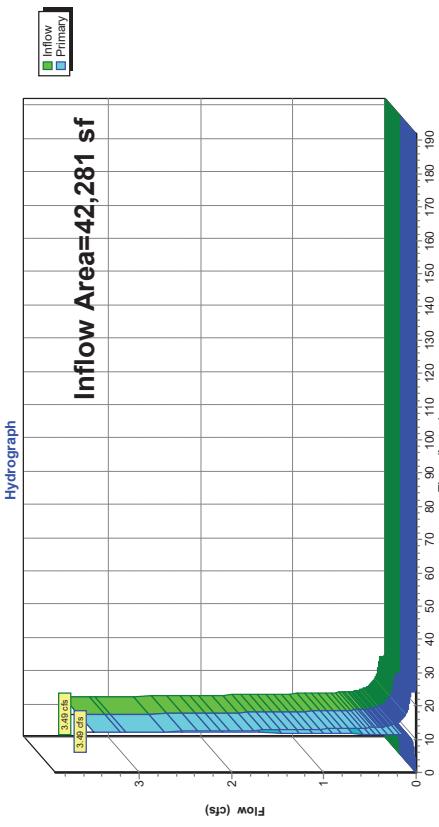
Link 2L: Prop. POD 002/POI 002



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HydroCAD® 10.20-5c s/n 08640 © 2023 HydroCAD Software Solutions LLCNOAA 24-hr C 100-Year Rainfall=7.55"
Printed 11/2/2024**Summary for Link 4L: PROP. SITE TOTAL**

Inflow Area = 42,281 sf, 68.05% Impervious, Inflow Depth = 4.93" for 100-Year event
Inflow = 3.49 cfs @ 12.15 hrs, Volume= 17,379 cf
Primary = 3.49 cfs @ 12.15 hrs, Volume= 17,379 cf, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-192.00 hrs, dt= 0.05 hrs

Link 4L: PROP. SITE TOTAL

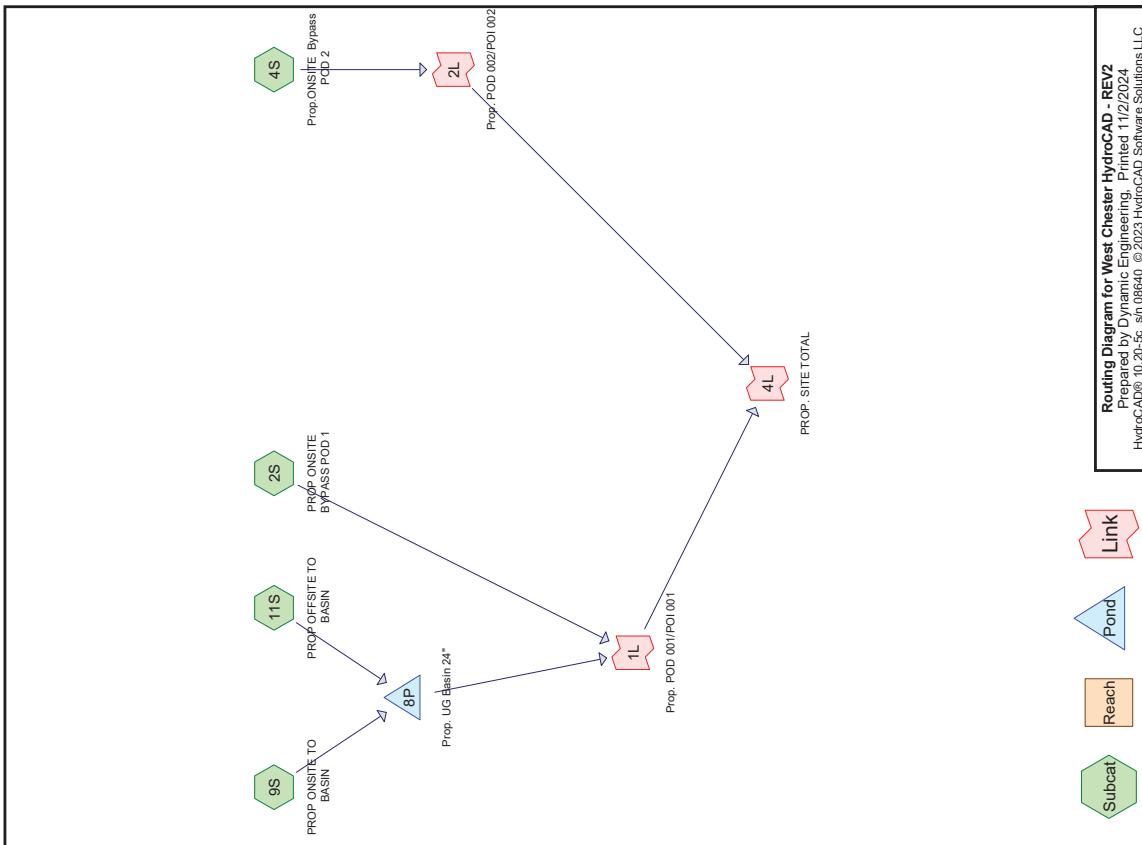
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Project Notes

Rainfall events imported from "NJ-Rain.txt" for 6614 NJ Ocean-D
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Rainfall Events Listing (selected events)

Event#	Event Name	Storm Type	Curve	Mode	Duration (hours)	BfB	Depth (inches)	AMC
1	100-Year NOAA 24-hr	C	Default		24.00	1	7.55	2

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Area Listing (selected nodes)

	Area (sq-ft)	CN	Description (subcatchment-numbers)
	8,527	98	(2S, 11S)
	12,291	61	(2S, 9S, 11S)
	20,247	98	Paved parking, HSG B (4S, 9S)
	1,216	61	Sewer Ext per (4S)
42,281	86		TOTAL AREA

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Soil Listing (selected nodes)

Area (sq-ft)	Soil Group	Subcatchment Numbers
0	HSG A	
20,247	HSG B	4S, 9S
0	HSG C	
0	HSG D	
22,034	Other	2S, 4S, 9S, 11S
42,281	TOTAL AREA	

Ground Covers (selected nodes)

	HSG-A (sq-ft)	HSG-B (sq-ft)	HSG-C (sq-ft)	HSG-D (sq-ft)	Other (sq-ft)	Total (sq-ft)	Ground Cover	Subcatchmen Numbers
	0	0	0	0	0	20,818	20,818	2
	0	20,247	0	0	0	0	20,247	Paved parking 4
	0	0	0	0	0	1,216	1,216	Sewer Ext per 4
	0	20,247	0	0	0	22,034	42,281	TOTAL AREA

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HydroCAD® 10.20-5c s/n 08640 © 2023 HydroCAD Software Solutions LLC**Pipe Listing (selected nodes)**

Line#	Node Number	In-Invert (feet)	Out-Invert (feet)	Length (feet)	Slope (ft/ft)	n	Width (inches)	Diam/Height (inches)	Inside-Fill (inches)	Name
1	8P	407.10	406.45	129.0	0.0050	0.012	0.0	15.0	0.0	

Time span=0.00-192.00 hrs, dt=0.05 hrs, 3841 points
 Runoff by SCS TR-20 method, UH=SCS, Weighted-Q
 Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method
 To=6.0 min CN=WQ Runoff=1.08 cfs 3.584 cfs

Subcatchment 2S: PROP ONSITE BYPASS Runoff Area=6,935 sf 73.64% Impervious Runoff Depth=6.20"
 Runoff by SCS TR-20 method, UH=SCS, Weighted-Q
 To=6.0 min CN=WQ Runoff=1.08 cfs 3.584 cfs

Subcatchment 4S: Prop.ONBSITE Bypass Runoff Area=3,942 sf 69.15% Impervious Runoff Depth=6.01"
 Runoff by SCS TR-20 method, UH=SCS, Weighted-Q
 To=6.0 min CN=WQ Runoff=1.975 cfs

Subcatchment 9S: PROP ONSITE TO Runoff Area=21,903 sf 79.99% Impervious Runoff Depth=6.47"
 Runoff by SCS TR-20 method, UH=SCS, Weighted-Q
 To=6.0 min CN=NQ Runoff=3.54 cfs 11.808 cfs

Subcatchment 11S: PROP OFFSITE TO Runoff Area=9,501 sf 36.00% Impervious Runoff Depth=4.62"
 Runoff by SCS TR-20 method, UH=SCS, Weighted-Q
 To=6.0 min CN=WQ Runoff=1.16 cfs 3.657 cfs

Pond 8P: Prop. UG Basin 24" Peak Elevation=409.47' Storage=5,172 cf Inflow=4,71 cfs 15,465 cf
 Discarded=0.01 cfs 3,646 cf Primary=2,36 cfs 11,820 cf Outflow=2,38 cfs 15,465 cf

Link 1L: Prop. POD 001/POI 001 Inflow=2,92 cfs 15,404 cf
 Primary=2,92 cfs 15,404 cf

Link 2L: Prop. POD 002/POI 002 Inflow=0.60 cfs 1.975 cf
 Primary=0.60 cfs 1.975 cf

Link 4L: PROP. SITE TOTAL Inflow=3.49 cfs 17.378 cf
 Primary=3.49 cfs 17.378 cf

Total Runoff Area = 42,281 sf Runoff Volume = 21,025 cf Average Runoff Depth = 5.97"
 31.95% Pervious = 13,507 sf 68.05% Impervious = 28,774 sf

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Summary for Subcatchment 2S: PROP ONSITE BYPASS POD 1

Runoff = 1.08 cfs @ 12.13 hrs, Volume= 3,584 cf, Depth= 6.20"
 Routed to Link 1L : Prop.POD 001/POI 001

Runoff by SCS TR-20 method, UH=SCS, Weighted-Q, Time Span= 0.00-192.00 hrs, dt= 0.05 hrs
 NOAA 24-hr C 100-Year Rainfall=7.55"

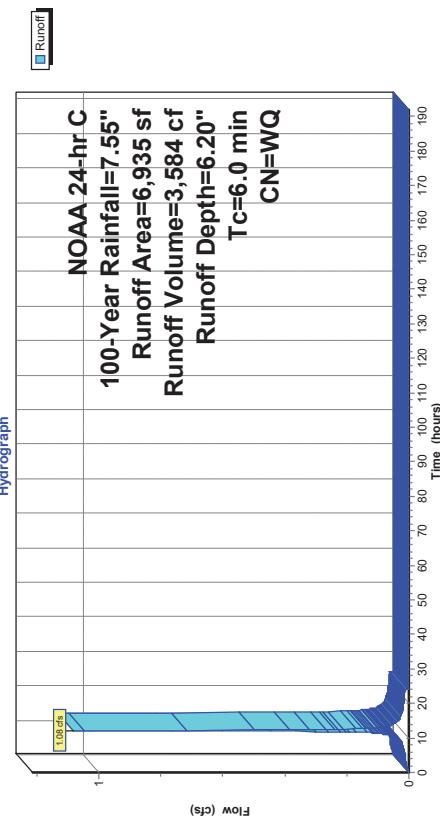
Area (sf)	CN	Description
* 5,107	98	
* 1,828	61	

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.0	6,935	Weighted Average			
	1,828	61	26.36% Pervious Area		
	5,107	98	73.64% Impervious Area		

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.0	6,935	Weighted Average			
	1,828	61	26.36% Pervious Area		
	5,107	98	73.64% Impervious Area		

Direct Entry,

Subcatchment 2S: PROP ONSITE BYPASS POD 1



Summary for Subcatchment 4S: Prop.ONBSITE Bypass POD 2

Runoff = 0.60 cfs @ 12.13 hrs, Volume= 1,975 cf, Depth= 6.01"
 Routed to Link 2L : Prop.POD 002/POI 002

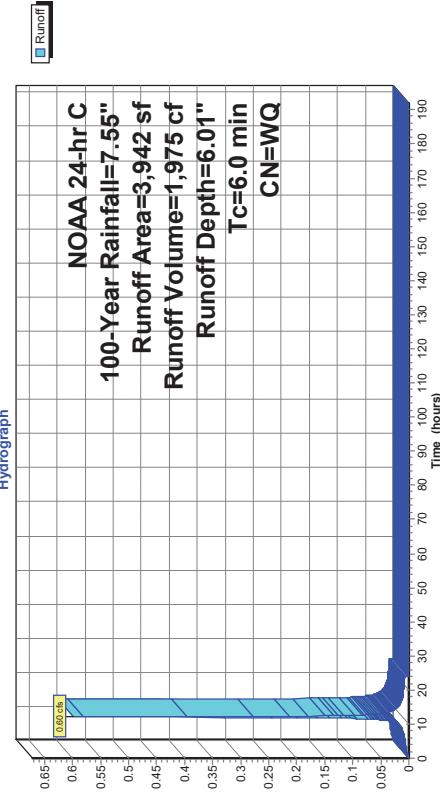
Runoff by SCS TR-20 method, UH=SCS, Weighted-Q, Time Span= 0.00-192.00 hrs, dt= 0.05 hrs
 NOAA 24-hr C 100-Year Rainfall=7.55"

Area (sf)	CN	Description
* 2,726	98	Paved parking, HSG B
* 1,216	61	Sewer Ext per

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.0	3,942	Weighted Average			
	1,216	61	30.85% Pervious Area		
	2,726	98	69.15% Impervious Area		

Direct Entry, Flow Path

Subcatchment 4S: Prop.ONBSITE Bypass POD 2



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Summary for Subcatchment 9S: PROP ONSITE TO BASIN

Runoff = 3.54 cfs @ 12.13 hrs, Volume= 11,808 cf, Depth= 6.47"
 Routed to Pond 8P : Prop. UG Basin 24"

Runoff by SCS TR-20 method, UH=SCS, Weighted-Q, Time Span= 0.00-192.00 hrs, dt= 0.05 hrs
 NOAA 24-hr C 100-Year Rainfall=7.55"

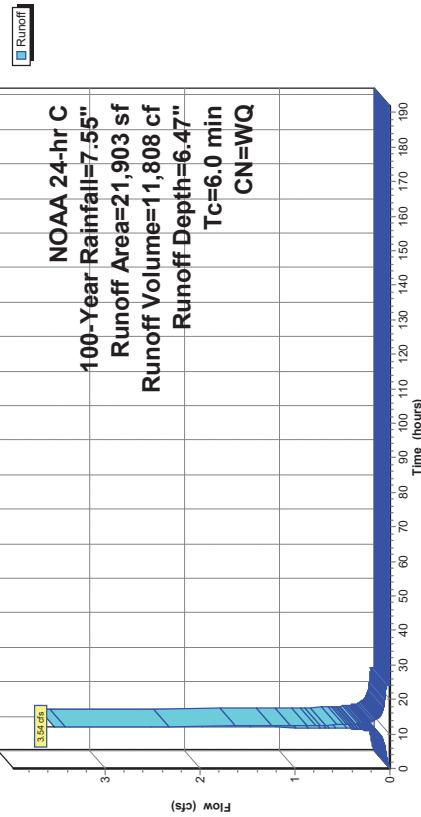
Area (sf)	CN	Description
17,521	98	Paved parking, HSG B
*	4,382	61

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
21,903	Weighted Average	4,382	61	20.0%	Pervious Area
17,521	79.99% Impervious Area	98			

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.0	Direct Entry, Flow Path				

Subcatchment 9S: PROP ONSITE TO BASIN

Hydrograph



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Summary for Subcatchment 11S: PROP OFFSITE TO BASIN

Runoff = 1.16 cfs @ 12.13 hrs, Volume= 3,657 cf, Depth= 4.62"
 Routed to Pond 8P : Prop. UG Basin 24"

Runoff by SCS TR-20 method, UH=SCS, Weighted-Q, Time Span= 0.00-192.00 hrs, dt= 0.05 hrs
 NOAA 24-hr C 100-Year Rainfall=7.55"

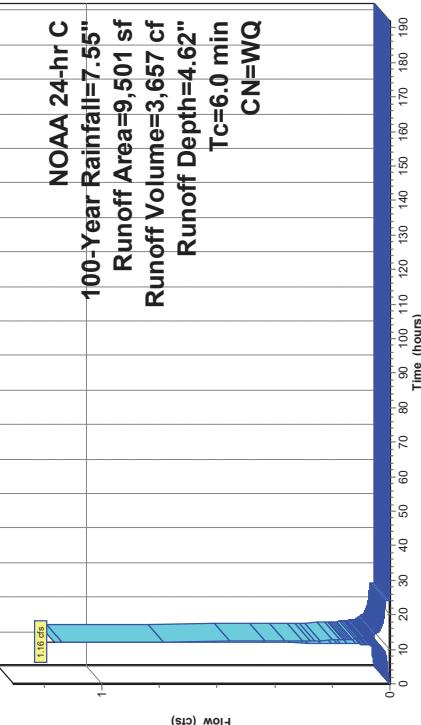
Area (sf)	CN	Description
*	3,420	98
*	6,081	61

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
9,501	Weighted Average	6,081	61	64.00%	Pervious Area
3,420	36.00% Impervious Area	98			

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.0	Direct Entry, Flow Path				

Subcatchment 11S: PROP OFFSITE TO BASIN

Hydrograph



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Summary for Pond 8P: Prop. UG Basin 24"

Inflow Area =	31,404 sf	66.68% Impervious, Inflow Depth = 5.91"	for 100-Year event
Inflow =	4.71 cfs @ 12.13 hrs.	Volume= 15,465 cf	
Outflow =	2.38 cfs @	Volume= 15,465 cf, Attent= 49%, Lag= 7.4 min	
Discarded =	0.01 cfs @	Volume= 3,646 cf	
Primary =	2.36 cfs @ 12.25 hrs,	Volume= 11,820 cf	Routed to Link 1L : Prop. POD 001/POI 001

Routing by Stor-Ind method, Time Span= 0.00-192.00 hrs, dt= 0.05 hrs
 Peak Elev= 409.47' @ 12.25 hrs Surf.Area= 3,090 sf Storage= 5,172 cf

Plug-Flow detention time= 393.5 min calculated for 15,461 cf (100% of inflow)
 Center-of-Mass det. time= 394.2 min (1,155.6 - 761.5)

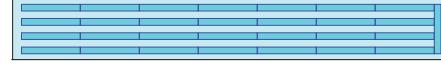
Volume	Invert	Avail.Storage	Storage Description
#1A	406.00'	3,834 cf	20.83'W x 148.33'L x 3.83'H Field A
#2A	407.00'	1,788 cf	11,846 cf Overall - 2,262 cf Embedded = 9,584 cf x 40.0% Voids
#3	407.10	406.00'	ADS N-12 24" x 28 Inside #1
#4	407.10	407.80'	Inside= 23.8" W x 23.8" H => 3.10 sf x 20.00'L = 62.0 cf
		409.40'	Outside= 28.0" W x 28.0" H => 3.92 sf x 20.00'L = 78.4 cf
			28 Chambers in 4 Rows
			16.83 Header x 3.10 sf x 1 = 52.2 cf Inside
			5,622 cf Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Primary	407.10	15.0" Round Culvert
			L= 129.0' CPP projecting, no headwall, Ke= 0.900
			Inlet / Outlet Invert= 407.10 / 406.45' S= 0.0050 '/' Cc= 0.900
			n= 0.012 Corrugated PP, smooth interior, Flow Area= 1.23 sf
#2	Discarded	406.00'	0.200 in/hr Exfiltration over Surface area
#3	Device 1	407.80'	17.0" W x 3.0" H Vert. 3"x17" Office C= 0.600
#4	Device 1	409.40'	Limited to weir flow at low heads
			4.0" long Sharp-Crested VeeTrap Weir Cv= 2.62 (C= 3.28)

Discarded OutFlow Max=0.01 cfs @ 2.00 hrs HW=406.04' (Free Discharge)
 ↓=Exfiltration (Exfiltration Controls 0.01 cfs)

Primary OutFlow Max=2.35 cfs @ 12.25 hrs HW=409.47' (Free Discharge)
 ↓=1=Culvert (Passes 2.35 cfs of 6.16 cfs potential flow)
 ↓=3"x17" Office (Office Controls 2.12 cfs @ 5.98 fps)
 ↓=Sharp-Crested VeeTrap Weir (Weir Controls 0.23 cfs @ 0.85 fps)



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Pond 8P: Prop. UG Basin 24" - Chamber Wizard Field A

Chamber Model = ADS N-12 24" (ADS N-12® Pipe)
 Inside= 23.8"W x 23.8"H => 3.10 sf x 20.00'L = 62.0 cf
 Outside= 28.0"W x 28.0H => 3.92 sf x 20.00'L = 78.4 cf

28.0" Wide + 30.0" Spacing = 58.0" C-C Row Spacing

7 Chambers/Row x 20.00' Long +2.33' Header x 1 = 142.33' Row Length +36.0" End Stone x 2 = 148.33'

Base Length
 4 Rows x 28.0" Wide + 30.0" Spacing x 3 + 24.0" Side Stone x 2 = 20.83' Base Width
 12.0" Stone Base + 28.0" Chamber Height + 6.0" Stone Cover = 3.83' Field Height

28 Chambers x 62.0 cf + 16.83 Header x 3.10 sf = 1.788.2 cf Chamber Storage

28 Chambers x 78.4 cf + 16.83 Header x 3.92 sf = 2.261.9 cf Displacement
 11,846.3 cf Field - 2.261.9 cf Chambers = 9,584.4 cf Stone x 40.0% Voids = 3,833.8 cf Stone Storage

Chamber Storage + Stone Storage = 5,621.9 cf = 0.129 af
 Overall Storage Efficiency = 47.5%
 Overall System Size = 148.33' x 20.83 x 3.83'

28 Chambers
 438.8 cy Field
 355.0 cy Stone

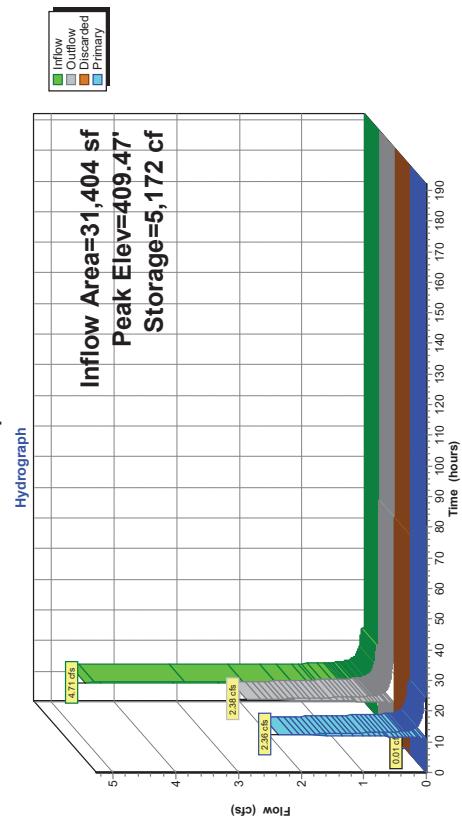
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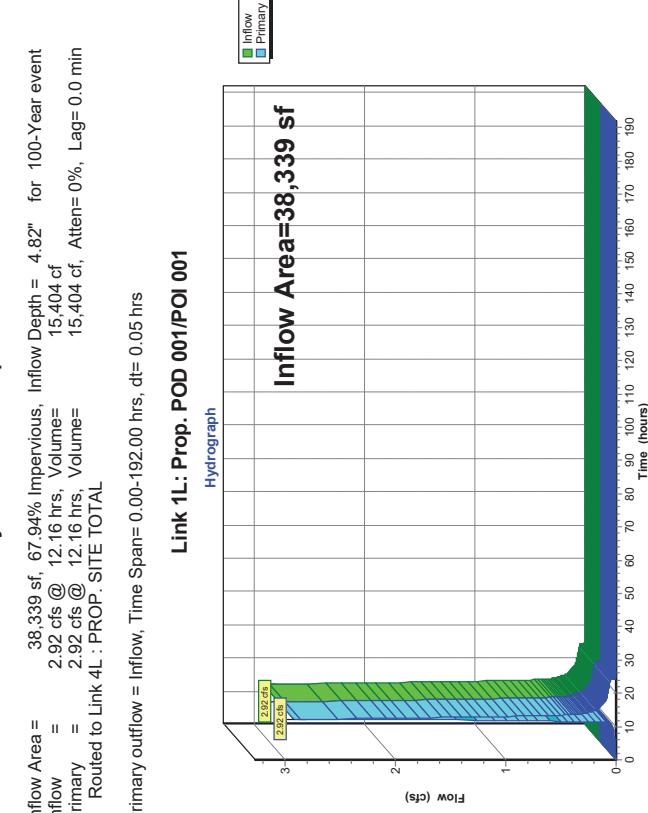
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Pond 8P: Prop. UG Basin 24"



Link 1L: Prop. POD 001/POI 001



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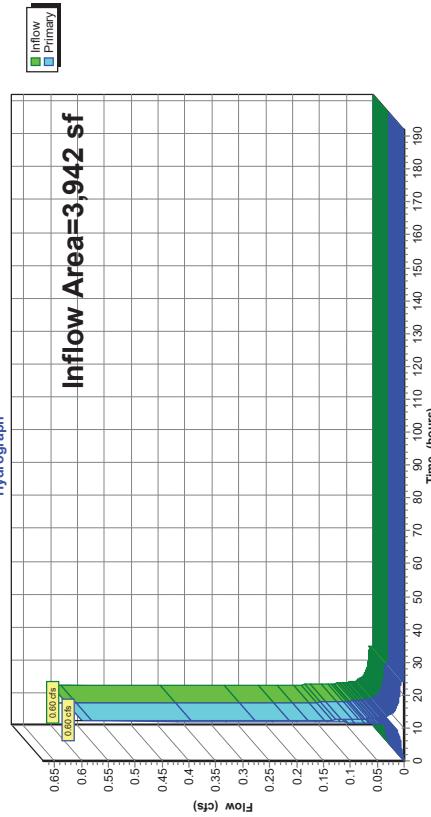
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Summary for Link 2L: Prop. POD 002/POI 002

Inflow Area = 3,942 sf, 69.15% Impervious, Inflow Depth = 6.01" for 100-Year event
 Inflow = 0.60 cfs @ 12.13 hrs, Volume= 1,975 cf
 Primary = 0.60 cfs @ 12.13 hrs, Volume= 1,975 cf, Atten= 0%, Lag= 0.0 min
 Routed to Link 4L : PROP. SITE TOTAL

Primary outflow = Inflow, Time Span= 0.00-192.00 hrs, dt= 0.05 hrs

Link 2L: Prop. POD 002/POI 002



Summary for Link 4L: PROP. SITE TOTAL

Inflow Area = 42,281 sf, 68.05% Impervious, Inflow Depth = 4.93" for 100-Year event
 Inflow = 3.49 cfs @ 12.15 hrs, Volume= 17,379 cf
 Primary = 3.49 cfs @ 12.15 hrs, Volume= 17,379 cf, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-192.00 hrs, dt= 0.05 hrs

Link 4L: PROP. SITE TOTAL



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Pond 8P: Prop. UG Basin 24" - Chamber Wizard Field A

Chamber Model = ADS N-12 24" (ADS N-12® Pipe)

Inside= 23.8" W x 23.8" H => 3.10 sf x 20.00'L = 62.0 cf
 Outside= 28.0" W x 28.0" H => 3.92 sf x 20.00'L = 78.4 cf

28.0" Wide + 30.0" Spacing = 58.0" C-C Row Spacing

7 Chambers/Row x 20.00' Long +2.33' Header x 1 = 142.33' Row Length +36.0" End Stone x 2 = 148.33'

Base Length

4 Rows x 28.0" Wide + 30.0" Spacing x 3 + 24.0" Side Stone x 2 = 20.83' Base Width

12.0" Stone Base + 28.0" Chamber Height + 6.0" Stone Cover = 3.83' Field Height

28 Chambers x 62.0 cf + 16.83 Header x 3.10 sf = 1.788.2 cf Chamber Storage

28 Chambers x 78.4 cf + 16.83 Header x 3.92 sf = 2.261.9 cf Displacement

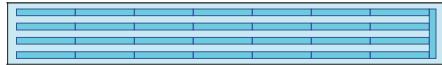
11,846.3 cf Field - 2.261.9 cf Chambers = 9,584.4 cf Stone x 40.0% Voids = 3,833.8 cf Stone Storage

Chamber Storage + Stone Storage = 5,621.9 cf = 0.129 af

Overall Storage Efficiency = 47.5%

Overall System Size = 148.33' x 20.83' x 3.83'

28 Chambers
 438.8 cy Field
 355.0 cy Stone



NOAA 24-hr C 1-Year Rainfall=2.70"
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Hydrograph for Pond 8P: Prop. UG Basin 24"

Time (hours)	Inflow (cfs)	Storage (cubic-feet)	Elevation (feet)	Outflow (cfs)	Discarded (cfs)	Primary (cfs)
0.00	0.00	0	406.00	0.00	0.00	0.00
5.00	0.01	32	406.03	0.01	0.01	0.00
10.00	0.05	229	406.19	0.01	0.01	0.04
15.00	0.04	2,509	407.84	0.05	0.01	0.01
20.00	0.02	2,460	407.81	0.02	0.01	0.00
25.00	0.00	2,397	407.78	0.01	0.01	0.00
30.00	0.00	2,140	407.64	0.01	0.01	0.00
35.00	0.00	1,882	407.49	0.01	0.01	0.00
40.00	0.00	1,625	407.33	0.01	0.01	0.00
45.00	0.00	1,367	407.12	0.01	0.01	0.00
50.00	0.00	1,110	406.90	0.01	0.01	0.00
55.00	0.00	852	406.69	0.01	0.01	0.00
60.00	0.00	594	406.48	0.01	0.01	0.00
65.00	0.00	337	406.27	0.01	0.01	0.00
70.00	0.00	79	406.06	0.01	0.01	0.00
75.00	0.00	0	406.00	0.00	0.00	0.00
80.00	0.00	0	406.00	0.00	0.00	0.00
85.00	0.00	0	406.00	0.00	0.00	0.00
90.00	0.00	0	406.00	0.00	0.00	0.00
95.00	0.00	0	406.00	0.00	0.00	0.00
100.00	0.00	0	406.00	0.00	0.00	0.00
105.00	0.00	0	406.00	0.00	0.00	0.00
110.00	0.00	0	406.00	0.00	0.00	0.00
115.00	0.00	0	406.00	0.00	0.00	0.00
120.00	0.00	0	406.00	0.00	0.00	0.00
125.00	0.00	0	406.00	0.00	0.00	0.00
130.00	0.00	0	406.00	0.00	0.00	0.00
135.00	0.00	0	406.00	0.00	0.00	0.00
140.00	0.00	0	406.00	0.00	0.00	0.00
145.00	0.00	0	406.00	0.00	0.00	0.00
150.00	0.00	0	406.00	0.00	0.00	0.00
155.00	0.00	0	406.00	0.00	0.00	0.00
160.00	0.00	0	406.00	0.00	0.00	0.00
165.00	0.00	0	406.00	0.00	0.00	0.00
170.00	0.00	0	406.00	0.00	0.00	0.00
175.00	0.00	0	406.00	0.00	0.00	0.00
180.00	0.00	0	406.00	0.00	0.00	0.00
185.00	0.00	0	406.00	0.00	0.00	0.00
190.00	0.00	0	406.00	0.00	0.00	0.00

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Pond 8P: Prop. UG Basin 24" - Chamber Wizard Field A

Chamber Model = ADS N-12 24" (ADS N-12® Pipe)

Inside= 23.8" W x 23.8" H => 3.10 sf x 20.00'L = 62.0 cf
 Outside= 28.0" W x 28.0" H => 3.92 sf x 20.00'L = 78.4 cf

28.0" Wide + 30.0" Spacing = 58.0" C-C Row Spacing

7 Chambers/Row x 20.00' Long +2.33' Header x 1 = 142.33' Row Length +36.0" End Stone x 2 = 148.33'

Base Length

4 Rows x 28.0" Wide + 30.0" Spacing x 3 + 24.0" Side Stone x 2 = 20.83' Base Width

12.0" Stone Base + 28.0" Chamber Height + 6.0" Stone Cover = 3.83' Field Height

28 Chambers x 62.0 cf + 16.83 Header x 3.10 sf = 1.788.2 cf Chamber Storage

28 Chambers x 78.4 cf + 16.83 Header x 3.92 sf = 2.261.9 cf Displacement

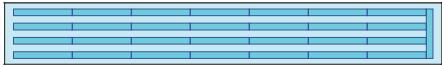
11,846.3 cf Field - 2.261.9 cf Chambers = 9,584.4 cf Stone x 40.0% Voids = 3,833.8 cf Stone Storage

Chamber Storage + Stone Storage = 5,621.9 cf = 0.129 af

Overall Storage Efficiency = 47.5%

Overall System Size = 148.33' x 20.83' x 3.83'

28 Chambers
 438.8 cy Field
 355.0 cy Stone



NOAA 24-hr C 2-Year Rainfall=3.26"
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Hydrograph for Pond 8P: Prop. UG Basin 24"

Time (hours)	Inflow (cfs)	Storage (cubic-feet)	Elevation (feet)	Outflow (cfs)	Discarded (cfs)	Primary (cfs)
0.00	0.00	0	406.00	0.01	0.01	0.00
5.00	0.02	44	406.04	0.01	0.01	0.00
10.00	0.06	347	406.28	0.01	0.01	0.05
15.00	0.06	2,525	407.85	0.06	0.01	0.01
20.00	0.03	2,471	407.82	0.03	0.01	0.01
25.00	0.00	2,406	407.78	0.01	0.01	0.00
30.00	0.00	2,149	407.64	0.01	0.01	0.00
35.00	0.00	1,891	407.49	0.01	0.01	0.00
40.00	0.00	1,634	407.33	0.01	0.01	0.00
45.00	0.00	1,376	407.13	0.01	0.01	0.00
50.00	0.00	1,119	406.91	0.01	0.01	0.00
55.00	0.00	861	406.70	0.01	0.01	0.00
60.00	0.00	604	406.49	0.01	0.01	0.00
65.00	0.00	346	406.28	0.01	0.01	0.00
70.00	0.00	89	406.07	0.01	0.01	0.00
75.00	0.00	0	406.00	0.00	0.00	0.00
80.00	0.00	0	406.00	0.00	0.00	0.00
85.00	0.00	0	406.00	0.00	0.00	0.00
90.00	0.00	0	406.00	0.00	0.00	0.00
95.00	0.00	0	406.00	0.00	0.00	0.00
100.00	0.00	0	406.00	0.00	0.00	0.00
105.00	0.00	0	406.00	0.00	0.00	0.00
110.00	0.00	0	406.00	0.00	0.00	0.00
115.00	0.00	0	406.00	0.00	0.00	0.00
120.00	0.00	0	406.00	0.00	0.00	0.00
125.00	0.00	0	406.00	0.00	0.00	0.00
130.00	0.00	0	406.00	0.00	0.00	0.00
135.00	0.00	0	406.00	0.00	0.00	0.00
140.00	0.00	0	406.00	0.00	0.00	0.00
145.00	0.00	0	406.00	0.00	0.00	0.00
150.00	0.00	0	406.00	0.00	0.00	0.00
155.00	0.00	0	406.00	0.00	0.00	0.00
160.00	0.00	0	406.00	0.00	0.00	0.00
165.00	0.00	0	406.00	0.00	0.00	0.00
170.00	0.00	0	406.00	0.00	0.00	0.00
175.00	0.00	0	406.00	0.00	0.00	0.00
180.00	0.00	0	406.00	0.00	0.00	0.00
185.00	0.00	0	406.00	0.00	0.00	0.00
190.00	0.00	0	406.00	0.00	0.00	0.00

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Pond 8P: Prop. UG Basin 24" - Chamber Wizard Field A

Chamber Model = ADS N-12 24" (ADS N-12® Pipe)

Inside= 23.8" W x 23.8" H => 3.10 sf x 20.00'L = 62.0 cf
 Outside= 28.0" W x 28.0" H => 3.92 sf x 20.00'L = 78.4 cf

28.0" Wide + 30.0" Spacing = 58.0" C-C Row Spacing

7 Chambers/Row x 20.00' Long +2.33' Header x 1 = 142.33' Row Length +36.0" End Stone x 2 = 148.33'

Base Length

4 Rows x 28.0" Wide + 30.0" Spacing x 3 + 24.0" Side Stone x 2 = 20.83' Base Width

12.0" Stone Base + 28.0" Chamber Height + 6.0" Stone Cover = 3.83' Field Height

28 Chambers x 62.0 cf + 16.83 Header x 3.10 sf = 1.788.2 cf Chamber Storage

28 Chambers x 78.4 cf + 16.83 Header x 3.92 sf = 2.261.9 cf Displacement

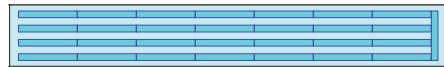
11,846.3 cf Field - 2.261.9 cf Chambers = 9,584.4 cf Stone x 40.0% Voids = 3,833.8 cf Stone Storage

Chamber Storage + Stone Storage = 5,621.9 cf = 0.129 af

Overall Storage Efficiency = 47.5%

Overall System Size = 148.33' x 20.83' x 3.83'

28 Chambers
 438.8 cy Field
 355.0 cy Stone



NOAA 24-hr C 5-Year Rainfall=4.09"
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Hydrograph for Pond 8P: Prop. UG Basin 24"

Time (hours)	Inflow (cfs)	Storage (cubic-feet)	Elevation (feet)	Outflow (cfs)	Discarded (cfs)	Primary (cfs)
0.00	0.00	0	406.00	0.01	0.00	0.00
5.00	0.02	71	406.06	0.01	0.01	0.00
10.00	0.08	550	406.44	0.01	0.01	0.00
15.00	0.07	2,547	407.86	0.08	0.01	0.07
20.00	0.04	2,485	407.83	0.04	0.01	0.02
25.00	0.00	2,415	407.79	0.01	0.01	0.00
30.00	0.00	2,157	407.65	0.01	0.01	0.00
35.00	0.00	1,900	407.50	0.01	0.01	0.00
40.00	0.00	1,642	407.34	0.01	0.01	0.00
45.00	0.00	1,385	407.14	0.01	0.01	0.00
50.00	0.00	1,127	406.91	0.01	0.01	0.00
55.00	0.00	870	406.70	0.01	0.01	0.00
60.00	0.00	612	406.50	0.01	0.01	0.00
65.00	0.00	354	406.29	0.01	0.01	0.00
70.00	0.00	97	406.08	0.01	0.01	0.00
75.00	0.00	1	406.00	0.00	0.00	0.00
80.00	0.00	0	406.00	0.00	0.00	0.00
85.00	0.00	0	406.00	0.00	0.00	0.00
90.00	0.00	0	406.00	0.00	0.00	0.00
95.00	0.00	0	406.00	0.00	0.00	0.00
100.00	0.00	0	406.00	0.00	0.00	0.00
105.00	0.00	0	406.00	0.00	0.00	0.00
110.00	0.00	0	406.00	0.00	0.00	0.00
115.00	0.00	0	406.00	0.00	0.00	0.00
120.00	0.00	0	406.00	0.00	0.00	0.00
125.00	0.00	0	406.00	0.00	0.00	0.00
130.00	0.00	0	406.00	0.00	0.00	0.00
135.00	0.00	0	406.00	0.00	0.00	0.00
140.00	0.00	0	406.00	0.00	0.00	0.00
145.00	0.00	0	406.00	0.00	0.00	0.00
150.00	0.00	0	406.00	0.00	0.00	0.00
155.00	0.00	0	406.00	0.00	0.00	0.00
160.00	0.00	0	406.00	0.00	0.00	0.00
165.00	0.00	0	406.00	0.00	0.00	0.00
170.00	0.00	0	406.00	0.00	0.00	0.00
175.00	0.00	0	406.00	0.00	0.00	0.00
180.00	0.00	0	406.00	0.00	0.00	0.00
185.00	0.00	0	406.00	0.00	0.00	0.00
190.00	0.00	0	406.00	0.00	0.00	0.00

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Pond 8P: Prop. UG Basin 24" - Chamber Wizard Field A

Chamber Model = ADS N-12 24" (ADS N-12® Pipe)

Inside= 23.8" W x 23.8" H => 3.10 sf x 20.00'L = 62.0 cf
 Outside= 28.0" W x 28.0" H => 3.92 sf x 20.00'L = 78.4 cf

28.0" Wide + 30.0" Spacing = 58.0" C-C Row Spacing

7 Chambers/Row x 20.00' Long +2.33' Header x 1 = 142.33' Row Length +36.0" End Stone x 2 = 148.33'

Base Length

4 Rows x 28.0" Wide + 30.0" Spacing x 3 + 24.0" Side Stone x 2 = 20.83' Base Width

12.0" Stone Base + 28.0" Chamber Height + 6.0" Stone Cover = 3.83' Field Height

28 Chambers x 62.0 cf + 16.83 Header x 3.10 sf = 1.788.2 cf Chamber Storage

28 Chambers x 78.4 cf + 16.83 Header x 3.92 sf = 2.261.9 cf Displacement

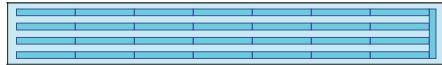
11,846.3 cf Field - 2.261.9 cf Chambers = 9,584.4 cf Stone x 40.0% Voids = 3,833.8 cf Stone Storage

Chamber Storage + Stone Storage = 5,621.9 cf = 0.129 af

Overall Storage Efficiency = 47.5%

Overall System Size = 148.33' x 20.83' x 3.83'

28 Chambers
 438.8 cy Field
 355.0 cy Stone



NOAA 24-hr C 10-Year Rainfall=4.79"
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Hydrograph for Pond 8P: Prop. UG Basin 24"

Time (hours)	Inflow (cfs)	Storage (cubic-feet)	Elevation (feet)	Outflow (cfs)	Discarded (cfs)	Primary (cfs)
0.00	0.00	0	406.00	0.01	0.00	0.00
5.00	0.03	109	406.09	0.01	0.01	0.00
10.00	0.09	736	406.60	0.01	0.01	0.09
15.00	0.09	2,564	407.87	0.10	0.01	0.03
20.00	0.04	2,496	407.83	0.04	0.01	0.00
25.00	0.00	2,419	407.79	0.01	0.01	0.00
30.00	0.00	2,161	407.65	0.01	0.01	0.00
35.00	0.00	1,904	407.50	0.01	0.01	0.00
40.00	0.00	1,646	407.34	0.01	0.01	0.00
45.00	0.00	1,389	407.14	0.01	0.01	0.00
50.00	0.00	1,131	406.92	0.01	0.01	0.00
55.00	0.00	874	406.71	0.01	0.01	0.00
60.00	0.00	616	406.50	0.01	0.01	0.00
65.00	0.00	359	406.29	0.01	0.01	0.00
70.00	0.00	101	406.08	0.01	0.01	0.00
75.00	0.00	1	406.00	0.00	0.00	0.00
80.00	0.00	0	406.00	0.00	0.00	0.00
85.00	0.00	0	406.00	0.00	0.00	0.00
90.00	0.00	0	406.00	0.00	0.00	0.00
95.00	0.00	0	406.00	0.00	0.00	0.00
100.00	0.00	0	406.00	0.00	0.00	0.00
105.00	0.00	0	406.00	0.00	0.00	0.00
110.00	0.00	0	406.00	0.00	0.00	0.00
115.00	0.00	0	406.00	0.00	0.00	0.00
120.00	0.00	0	406.00	0.00	0.00	0.00
125.00	0.00	0	406.00	0.00	0.00	0.00
130.00	0.00	0	406.00	0.00	0.00	0.00
135.00	0.00	0	406.00	0.00	0.00	0.00
140.00	0.00	0	406.00	0.00	0.00	0.00
145.00	0.00	0	406.00	0.00	0.00	0.00
150.00	0.00	0	406.00	0.00	0.00	0.00
155.00	0.00	0	406.00	0.00	0.00	0.00
160.00	0.00	0	406.00	0.00	0.00	0.00
165.00	0.00	0	406.00	0.00	0.00	0.00
170.00	0.00	0	406.00	0.00	0.00	0.00
175.00	0.00	0	406.00	0.00	0.00	0.00
180.00	0.00	0	406.00	0.00	0.00	0.00
185.00	0.00	0	406.00	0.00	0.00	0.00
190.00	0.00	0	406.00	0.00	0.00	0.00

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NOAA 24-hr C 25-Year Rainfall=5.79"
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NOAA 24-hr C 25-Year Rainfall=5.79"
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Pond 8P: Prop. UG Basin 24" - Chamber Wizard Field A

Chamber Model = ADS N-12 24" (ADS N-12® Pipe)

Inside= 23.8" W x 23.8" H => 3.10 sf x 20.00'L = 62.0 cf
 Outside= 28.0" W x 28.0" H => 3.92 sf x 20.00'L = 78.4 cf

28.0" Wide + 30.0" Spacing = 58.0" C-C Row Spacing

7 Chambers/Row x 20.00' Long +2.33' Header x 1 = 142.33' Row Length +36.0" End Stone x 2 = 148.33'

Base Length

4 Rows x 28.0" Wide + 30.0" Spacing x 3 + 24.0" Side Stone x 2 = 20.83' Base Width

12.0" Stone Base + 28.0" Chamber Height + 6.0" Stone Cover = 3.83' Field Height

28 Chambers x 62.0 cf + 16.83 Header x 3.10 sf = 1.788.2 cf Chamber Storage

28 Chambers x 78.4 cf + 16.83 Header x 3.92 sf = 2.261.9 cf Displacement

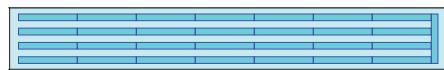
11,846.3 cf Field - 2.261.9 cf Chambers = 9,584.4 cf Stone x 40.0% Voids = 3,833.8 cf Stone Storage

Chamber Storage + Stone Storage = 5,621.9 cf = 0.129 af

Overall Storage Efficiency = 47.5%

Overall System Size = 148.33' x 20.83' x 3.83'

28 Chambers
 438.8 cy Field
 355.0 cy Stone



Hydrograph for Pond 8P: Prop. UG Basin 24"

Time (hours)	Inflow (cfs)	Storage (cubic-feet)	Elevation (feet)	Outflow (cfs)	Discarded (cfs)	Primary (cfs)
0.00	0.00	0	406.14	0.01	0.01	0.00
5.00	0.04	178	406.14	0.01	0.01	0.00
10.00	0.12	1,016	406.82	0.12	0.01	0.11
15.00	0.11	2,587	407.88	0.12	0.01	0.04
20.00	0.05	2,512	407.84	0.05	0.01	0.00
25.00	0.00	2,424	407.79	0.01	0.01	0.00
30.00	0.00	2,166	407.65	0.01	0.01	0.00
35.00	0.00	1,909	407.50	0.01	0.01	0.00
40.00	0.00	1,651	407.34	0.01	0.01	0.00
45.00	0.00	1,394	407.15	0.01	0.01	0.00
50.00	0.00	1,136	406.92	0.01	0.01	0.00
55.00	0.00	879	406.71	0.01	0.01	0.00
60.00	0.00	621	406.50	0.01	0.01	0.00
65.00	0.00	364	406.29	0.01	0.01	0.00
70.00	0.00	106	406.09	0.01	0.01	0.00
75.00	0.00	1	406.00	0.00	0.00	0.00
80.00	0.00	0	406.00	0.00	0.00	0.00
85.00	0.00	0	406.00	0.00	0.00	0.00
90.00	0.00	0	406.00	0.00	0.00	0.00
95.00	0.00	0	406.00	0.00	0.00	0.00
100.00	0.00	0	406.00	0.00	0.00	0.00
105.00	0.00	0	406.00	0.00	0.00	0.00
110.00	0.00	0	406.00	0.00	0.00	0.00
115.00	0.00	0	406.00	0.00	0.00	0.00
120.00	0.00	0	406.00	0.00	0.00	0.00
125.00	0.00	0	406.00	0.00	0.00	0.00
130.00	0.00	0	406.00	0.00	0.00	0.00
135.00	0.00	0	406.00	0.00	0.00	0.00
140.00	0.00	0	406.00	0.00	0.00	0.00
145.00	0.00	0	406.00	0.00	0.00	0.00
150.00	0.00	0	406.00	0.00	0.00	0.00
155.00	0.00	0	406.00	0.00	0.00	0.00
160.00	0.00	0	406.00	0.00	0.00	0.00
165.00	0.00	0	406.00	0.00	0.00	0.00
170.00	0.00	0	406.00	0.00	0.00	0.00
175.00	0.00	0	406.00	0.00	0.00	0.00
180.00	0.00	0	406.00	0.00	0.00	0.00
185.00	0.00	0	406.00	0.00	0.00	0.00
190.00	0.00	0	406.00	0.00	0.00	0.00

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Pond 8P: Prop. UG Basin 24" - Chamber Wizard Field A

Chamber Model = ADS N-12" 24" (ADS N-12® Pipe)

Inside= 23.8" W x 23.8" H => 3.10 sf x 20.00'L = 62.0 cf
 Outside= 28.0" W x 28.0" H => 3.92 sf x 20.00'L = 78.4 cf

28.0" Wide + 30.0" Spacing = 58.0" C-C Row Spacing

7 Chambers/Row x 20.00' Long +2.33' Header x 1 = 142.33' Row Length +36.0" End Stone x 2 = 148.33'

Base Length

4 Rows x 28.0" Wide + 30.0" Spacing x 3 + 24.0" Side Stone x 2 = 20.83' Base Width

12.0" Stone Base + 28.0" Chamber Height + 6.0" Stone Cover = 3.83' Field Height

28 Chambers x 62.0 cf + 16.83 Header x 3.10 sf = 1.788.2 cf Chamber Storage

28 Chambers x 78.4 cf + 16.83 Header x 3.92 sf = 2.261.9 cf Displacement

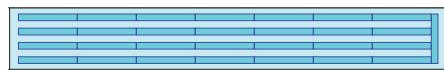
11,846.3 cf Field - 2.261.9 cf Chambers = 9,584.4 cf Stone x 40.0% Voids = 3,833.8 cf Stone Storage

Chamber Storage + Stone Storage = 5,621.9 cf = 0.129 af

Overall Storage Efficiency = 47.5%

Overall System Size = 148.33' x 20.83' x 3.83'

28 Chambers
 438.8 cy Field
 355.0 cy Stone



NOAA 24-hr C 50-Year Rainfall=6.64"
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Hydrograph for Pond 8P: Prop. UG Basin 24"

Time (hours)	Inflow (cfs)	Storage (cubic-feet)	Elevation (feet)	Outflow (cfs)	Discarded (cfs)	Primary (cfs)
0.00	0.00	0	406.20	0.01	0.00	0.00
5.00	0.04	245	406.20	0.01	0.01	0.00
10.00	0.13	1,261	407.02	0.01	0.01	0.00
15.00	0.13	2,606	407.89	0.14	0.01	0.13
20.00	0.06	2,523	407.85	0.06	0.01	0.05
25.00	0.00	2,428	407.80	0.01	0.01	0.00
30.00	0.00	2,170	407.65	0.01	0.01	0.00
35.00	0.00	1,913	407.50	0.01	0.01	0.00
40.00	0.00	1,655	407.35	0.01	0.01	0.00
45.00	0.00	1,397	407.15	0.01	0.01	0.00
50.00	0.00	1,140	406.92	0.01	0.01	0.00
55.00	0.00	882	406.71	0.01	0.01	0.00
60.00	0.00	625	406.51	0.01	0.01	0.00
65.00	0.00	367	406.30	0.01	0.01	0.00
70.00	0.00	110	406.09	0.01	0.01	0.00
75.00	0.00	1	406.00	0.00	0.00	0.00
80.00	0.00	0	406.00	0.00	0.00	0.00
85.00	0.00	0	406.00	0.00	0.00	0.00
90.00	0.00	0	406.00	0.00	0.00	0.00
95.00	0.00	0	406.00	0.00	0.00	0.00
100.00	0.00	0	406.00	0.00	0.00	0.00
105.00	0.00	0	406.00	0.00	0.00	0.00
110.00	0.00	0	406.00	0.00	0.00	0.00
115.00	0.00	0	406.00	0.00	0.00	0.00
120.00	0.00	0	406.00	0.00	0.00	0.00
125.00	0.00	0	406.00	0.00	0.00	0.00
130.00	0.00	0	406.00	0.00	0.00	0.00
135.00	0.00	0	406.00	0.00	0.00	0.00
140.00	0.00	0	406.00	0.00	0.00	0.00
145.00	0.00	0	406.00	0.00	0.00	0.00
150.00	0.00	0	406.00	0.00	0.00	0.00
155.00	0.00	0	406.00	0.00	0.00	0.00
160.00	0.00	0	406.00	0.00	0.00	0.00
165.00	0.00	0	406.00	0.00	0.00	0.00
170.00	0.00	0	406.00	0.00	0.00	0.00
175.00	0.00	0	406.00	0.00	0.00	0.00
180.00	0.00	0	406.00	0.00	0.00	0.00
185.00	0.00	0	406.00	0.00	0.00	0.00
190.00	0.00	0	406.00	0.00	0.00	0.00

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Pond 8P: Prop. UG Basin 24" - Chamber Wizard Field A

Chamber Model = ADS N-12 24" (ADS N-12® Pipe)

Inside= 23.8" W x 23.8" H => 3.10 sf x 20.00'L = 62.0 cf
 Outside= 28.0" W x 28.0" H => 3.92 sf x 20.00'L = 78.4 cf

28.0" Wide + 30.0" Spacing = 58.0" C-C Row Spacing

7 Chambers/Row x 20.00' Long +2.33' Header x 1 = 142.33' Row Length +36.0" End Stone x 2 = 148.33'

Base Length

4 Rows x 28.0" Wide + 30.0" Spacing x 3 + 24.0" Side Stone x 2 = 20.83' Base Width

12.0" Stone Base + 28.0" Chamber Height + 6.0" Stone Cover = 3.83' Field Height

28 Chambers x 62.0 cf + 16.83 Header x 3.10 sf = 1.788.2 cf Chamber Storage

28 Chambers x 78.4 cf + 16.83 Header x 3.92 sf = 2.261.9 cf Displacement

11,846.3 cf Field - 2.261.9 cf Chambers = 9,584.4 cf Stone x 40.0% Voids = 3,833.8 cf Stone Storage

Chamber Storage + Stone Storage = 5,621.9 cf = 0.129 af

Overall Storage Efficiency = 47.5%

Overall System Size = 148.33' x 20.83' x 3.83'

28 Chambers
 438.8 cy Field
 355.0 cy Stone



NOAA 24-hr C 100-Year Rainfall=7.55"
 Printed 11/2/2024

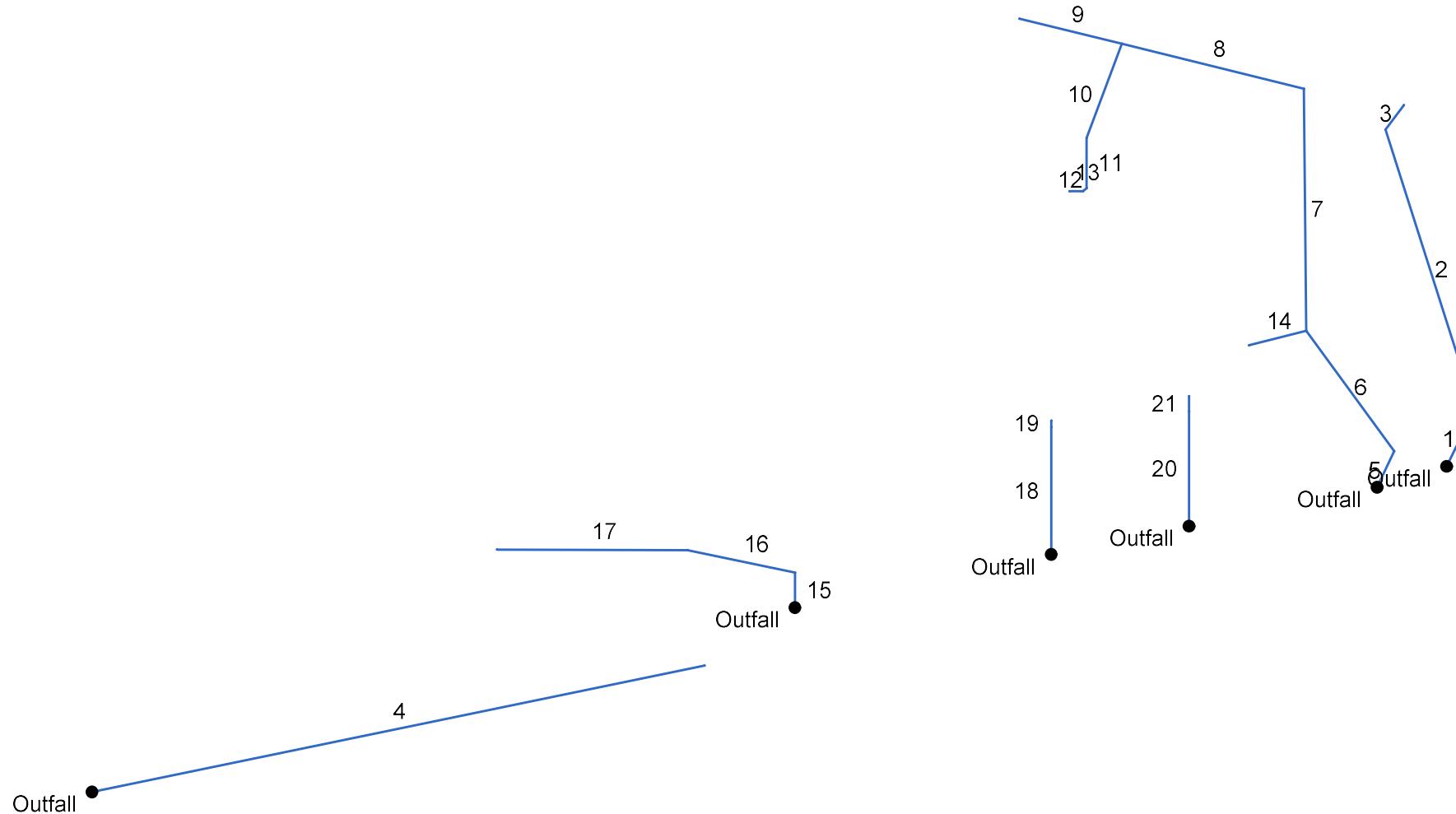
Prepared by Dynamic Engineering
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Hydrograph for Pond 8P: Prop. UG Basin 24"

Time (hours)	Inflow (cfs)	Storage (cubic-feet)	Elevation (feet)	Outflow (cfs)	Discarded (cfs)	Primary (cfs)
0.00	0.00	0	406.00	0.00	0.00	0.00
5.00	0.05	322	406.26	0.01	0.01	0.00
10.00	0.15	1,529	407.26	0.01	0.01	0.15
15.00	0.15	2,625	407.90	0.17	0.01	0.06
20.00	0.07	2,534	407.85	0.07	0.01	0.00
25.00	0.00	2,480	407.80	0.01	0.01	0.00
30.00	0.00	2,173	407.66	0.01	0.01	0.00
35.00	0.00	1,915	407.51	0.01	0.01	0.00
40.00	0.00	1,658	407.35	0.01	0.01	0.00
45.00	0.00	1,400	407.15	0.01	0.01	0.00
50.00	0.00	1,143	406.92	0.01	0.01	0.00
55.00	0.00	885	406.72	0.01	0.01	0.00
60.00	0.00	628	406.51	0.01	0.01	0.00
65.00	0.00	370	406.30	0.01	0.01	0.00
70.00	0.00	113	406.09	0.01	0.01	0.00
75.00	0.00	1	406.00	0.00	0.00	0.00
80.00	0.00	0	406.00	0.00	0.00	0.00
85.00	0.00	0	406.00	0.00	0.00	0.00
90.00	0.00	0	406.00	0.00	0.00	0.00
95.00	0.00	0	406.00	0.00	0.00	0.00
100.00	0.00	0	406.00	0.00	0.00	0.00
105.00	0.00	0	406.00	0.00	0.00	0.00
110.00	0.00	0	406.00	0.00	0.00	0.00
115.00	0.00	0	406.00	0.00	0.00	0.00
120.00	0.00	0	406.00	0.00	0.00	0.00
125.00	0.00	0	406.00	0.00	0.00	0.00
130.00	0.00	0	406.00	0.00	0.00	0.00
135.00	0.00	0	406.00	0.00	0.00	0.00
140.00	0.00	0	406.00	0.00	0.00	0.00
145.00	0.00	0	406.00	0.00	0.00	0.00
150.00	0.00	0	406.00	0.00	0.00	0.00
155.00	0.00	0	406.00	0.00	0.00	0.00
160.00	0.00	0	406.00	0.00	0.00	0.00
165.00	0.00	0	406.00	0.00	0.00	0.00
170.00	0.00	0	406.00	0.00	0.00	0.00
175.00	0.00	0	406.00	0.00	0.00	0.00
180.00	0.00	0	406.00	0.00	0.00	0.00
185.00	0.00	0	406.00	0.00	0.00	0.00
190.00	0.00	0	406.00	0.00	0.00	0.00

**I. STORMWATER COLLECTION SYSTEM
CALCULATIONS (STORM SEWERS)**

Hydraflow Storm Sewers Extension for Autodesk® Civil 3D® Plan



Storm Sewer Inventory Report

Line No.	Alignment				Flow Data				Physical Data								Line ID
	Dnstr Line No.	Line Length (ft)	Defl angle (deg)	Junc Type	Known Q (cfs)	Drng Area (ac)	Runoff Coeff (C)	Inlet Time (min)	Invert El Dn (ft)	Line Slope (%)	Invert El Up (ft)	Line Size (in)	Line Shape	N Value (n)	J-Loss Coeff (K)	Inlet/Rim El (ft)	
1	End	15.546	-69.005	None	0.00	0.00	0.00	5.0	413.25	1.03	413.41	18	Cir	0.012	0.63	417.61	502 TO 501
2	1	73.372	-35.274	None	0.00	0.00	0.00	5.0	413.41	5.12	417.17	18	Cir	0.012	0.76	421.44	503 TO 502
3	2	7.268	45.569	None	0.00	0.56	0.95	5.0	417.34	0.00	417.34	18	Cir	0.012	1.00	419.98	503 TO 503
4	End	129.461	-14.379	None	2.36	0.00	0.00	5.0	406.33	0.52	407.00	15	Cir	0.012	1.00	411.68	101 TO 27
5	End	9.823	-69.279	None	0.00	0.14	0.95	5.0	407.00	0.51	407.05	15	Cir	0.012	0.81	412.48	202 TO 201
6	5	35.439	-50.970	None	0.00	0.07	0.95	5.0	407.22	0.51	407.40	15	Cir	0.012	0.98	413.37	203 TO 202
7	6	61.502	29.662	None	0.00	0.00	0.00	5.0	407.57	0.49	407.87	15	Cir	0.012	0.96	414.33	204 TO 203
8	7	39.038	-72.310	None	0.00	0.00	0.00	5.0	408.04	0.51	408.24	15	Cir	0.012	1.00	414.44	204A TO 204
9	8	21.809	-0.276	None	0.00	0.17	0.95	5.0	408.24	0.50	408.35	15	Cir	0.012	1.00	413.50	205 TO 204A
10	8	25.059	-90.276	None	0.00	0.00	0.00	5.0	408.24	1.00	408.49	4	Cir	0.012	0.34	414.01	32 TO 204A
11	10	12.776	-16.827	None	0.00	0.00	0.00	5.0	408.49	1.02	408.62	4	Cir	0.012	0.76	414.64	35 TO 32
12	11	1.078	46.146	None	0.00	0.00	0.00	5.0	408.62	0.93	408.63	4	Cir	0.012	0.73	414.65	34 TO 35
13	12	2.657	43.522	None	0.00	0.02	0.95	5.0	408.63	0.75	408.65	4	Cir	0.012	1.00	414.44	31 TO 34
14	6	12.436	-77.097	None	0.00	0.02	0.95	5.0	408.02	0.97	408.14	4	Cir	0.012	1.00	414.43	33 TO 203
15	End	8.884	-90.000	None	0.00	0.04	0.95	5.0	407.00	0.45	407.04	15	Cir	0.012	0.97	412.38	112 TO 111
16	15	22.706	-75.400	None	0.00	0.00	0.00	5.0	407.21	0.53	407.33	15	Cir	0.012	0.29	412.02	113 TO 112
17	16	38.945	-14.411	None	0.00	0.22	0.95	5.0	407.50	0.49	407.69	15	Cir	0.012	1.00	411.64	114 TO 113
18	End	32.379	-90.000	None	0.00	0.00	0.00	5.0	407.00	0.99	407.32	6	Cir	0.012	0.15	414.34	37 TO 38
19	18	1.640	0.000	None	0.00	0.02	0.95	5.0	407.32	1.22	407.34	6	Cir	0.012	1.00	414.45	36 TO 37
20	End	29.208	-90.000	None	0.00	0.00	0.00	5.0	407.00	0.99	407.29	4	Cir	0.012	0.15	414.08	40 TO 41
21	20	3.869	0.000	None	0.00	0.02	0.95	5.0	407.29	1.03	407.33	4	Cir	0.012	1.00	414.65	39 TO 40

Project File: New.stm

Number of lines: 21

Date: 11/4/2024

Storm Sewer Tabulation

Station		Len	Drng Area		Rnoff coeff	Area x C		Tc		Rain (I)	Total flow	Cap full	Vel	Pipe		Invert Elev		HGL Elev		Grnd / Rim Elev		Line ID	
Line	To Line		Incr	Total		Incr	Total	Inlet	Syst					Size	Slope	Dn	Up	Dn	Up	Dn	Up		
			(ft)	(ac)		(ac)	(C)	(min)	(min)					(in)	(%)	(ft)	(ft)	(ft)	(ft)	(ft)	(ft)		
1	End	15.546	0.00	0.56	0.00	0.00	0.53	5.0	5.6	7.6	4.06	11.66	2.34	18	1.03	413.25	413.41	414.76	414.77	414.89	417.61	502 TO 501	
2	1	73.372	0.00	0.56	0.00	0.00	0.53	5.0	5.1	7.8	4.16	26.02	3.43	18	5.12	413.41	417.17	414.83	417.95	417.61	421.44	503 TO 502	
3	2	7.268	0.56	0.56	0.95	0.53	0.53	5.0	5.0	7.8	4.17	0.00	4.11	18	0.00	417.34	417.34	418.12	418.24	421.44	419.98	503 TO 503	
4	End	129.461	0.00	0.00	0.00	0.00	0.00	5.0	5.0	0.0	2.36	5.01	2.55	15	0.52	406.33	407.00	407.58	407.73	409.64	411.68	101 TO 27	
5	End	9.823	0.14	0.42	0.95	0.13	0.40	5.0	7.3	7.1	2.84	4.97	2.32	15	0.51	407.00	407.05	409.47	409.49	0.00	412.48	202 TO 201	
6	5	35.439	0.07	0.28	0.95	0.07	0.27	5.0	6.9	7.2	1.92	4.97	1.57	15	0.51	407.22	407.40	409.55	409.58	412.48	413.37	203 TO 202	
7	6	61.502	0.00	0.19	0.00	0.00	0.18	5.0	6.0	7.5	1.35	4.87	1.10	15	0.49	407.57	407.87	409.62	409.64	413.37	414.33	204 TO 203	
8	7	39.038	0.00	0.19	0.00	0.00	0.18	5.0	5.4	7.7	1.39	4.99	1.13	15	0.51	408.04	408.24	409.66	409.68	414.33	414.44	204A TO 204	
9	8	21.809	0.17	0.17	0.95	0.16	0.16	5.0	5.0	7.8	1.27	4.95	1.03	15	0.50	408.24	408.35	409.69	409.70	414.44	413.50	205 TO 204A	
10	8	25.059	0.00	0.02	0.00	0.00	0.02	5.0	5.2	7.8	0.15	0.22	1.61	4	1.00	408.24	408.49	409.69	409.81	414.44	414.01	32 TO 204A	
11	10	12.776	0.00	0.02	0.00	0.00	0.02	5.0	5.0	7.8	0.15	0.22	1.62	4	1.02	408.49	408.62	409.82	409.88	414.01	414.64	35 TO 32	
12	11	1.078	0.00	0.02	0.00	0.00	0.02	5.0	5.0	7.8	0.15	0.21	1.62	4	0.93	408.62	408.63	409.91	409.92	414.64	414.65	34 TO 35	
13	12	2.657	0.02	0.02	0.95	0.02	0.02	5.0	5.0	7.8	0.15	0.19	1.62	4	0.75	408.63	408.65	409.95	409.96	414.65	414.44	31 TO 34	
14	6	12.436	0.02	0.02	0.95	0.02	0.02	5.0	5.0	7.8	0.15	0.22	1.62	4	0.97	408.02	408.14	409.62	409.68	413.37	414.43	33 TO 203	
15	End	8.884	0.04	0.26	0.95	0.04	0.25	5.0	5.8	7.6	1.87	4.68	1.53	15	0.45	407.00	407.04	409.47	409.48	0.00	412.38	112 TO 111	
16	15	22.706	0.00	0.22	0.00	0.00	0.21	5.0	5.5	7.7	1.60	5.07	1.31	15	0.53	407.21	407.33	409.51	409.52	412.38	412.02	113 TO 112	
17	16	38.945	0.22	0.22	0.95	0.21	0.21	5.0	5.0	7.8	1.64	4.87	1.34	15	0.49	407.50	407.69	409.53	409.55	412.02	411.64	114 TO 113	
18	End	32.379	0.00	0.02	0.00	0.00	0.02	5.0	5.0	7.8	0.15	0.60	0.76	6	0.99	407.00	407.32	409.47	409.49	0.00	414.34	37 TO 38	
19	18	1.640	0.02	0.02	0.95	0.02	0.02	5.0	5.0	7.8	0.15	0.67	0.76	6	1.22	407.32	407.34	409.49	409.49	414.34	414.45	36 TO 37	
20	End	29.208	0.00	0.02	0.00	0.00	0.02	5.0	5.0	7.8	0.15	0.22	1.62	4	0.99	407.00	407.29	409.47	409.60	0.00	414.08	40 TO 41	
21	20	3.869	0.02	0.02	0.95	0.02	0.02	5.0	5.0	7.8	0.15	0.22	1.62	4	1.03	407.29	407.33	409.61	409.63	414.08	414.65	39 TO 40	

Project File: New.stm

Number of lines: 21

Run Date: 11/4/2024

NOTES: Intensity = 44.22 / (Inlet time + 9.10) ^ 0.65; Return period = Yrs. 100 ; c = cir e = ellip b = box

J. VOLUME WORKSHEETS CALCULATIONS



**DYNAMIC
ENGINEERING**

1" (inch) Over Imperious Calculations

Project:	Proposed Chase Bank	Computed By:	SRM
Job #:	1478-99-191	Checked By:	JAG
Location:	Westtown Township, PA	Date:	7/15/2024

§ 144-306B. Infiltration requirements

For regulated activities involving both new development and redevelopment, the volume of a minimum of one inch of runoff from all regulated impervious surfaces shall be infiltrated

Total Impervious (SF) 25354

 0.083333

Required WQ Vol. 2112.833

Volume Management

Project: Proposed Chase Bank

Instructions General Volume Rate Quality

2-Year / 24-Hour Storm Event (NOAA Atlas 14): 3.26 inches Alternative 2-Year / 24-Hour Storm Event inches

Alternative Source:

Pre-Construction Conditions: No. Rows: 3 Exempt from Meadow in Good Condition Automatically Calculate CN, Ia, Runoff and Volume

Land Cover	Area (acres)	Soil Group	CN	Ia (in)	Q Runoff (in)	Runoff Volume (cf)
Impervious Areas: Paved Parking Lots, Roofs, Driveways, Etc. (Excluding ROW)	0.35	B	98	0.041	3.03	3,846
Pervious as Meadow	0.18	B	58	1.448	0.36	237
Impervious as Meadow	0.23	B	58	1.448	0.36	303
TOTAL (ACRES):			0.76	TOTAL (CF):		
TOTAL (ACRES):			0.76	TOTAL (CF):		

Post-Construction Conditions: No. Rows: 2

Land Cover	Area (acres)	Soil Group	CN	Ia (in)	Q Runoff (in)	Runoff Volume (cf)
Impervious Areas: Paved Parking Lots, Roofs, Driveways, Etc. (Excluding ROW)	0.59	B	98	0.041	3.03	6,484
Open Space (Lawns, Parks, Golf Courses, Cemeteries, Etc.) - Good Condition (Grass Cover > 75%)	0.17	B	61	1.279	0.47	289
TOTAL (ACRES):			0.76	TOTAL (CF):		
TOTAL (ACRES):			0.76	TOTAL (CF):		

NET CHANGE IN VOLUME TO MANAGE (CF): 2,387

Non-Structural BMP Volume Credits:

Tree Planting Credit

Other (attach calculations):

Structural BMP Volume Credits:

No. Structural BMPs:

1

Start BMP Numbering at:

DP No.	BMP No.	BMP Name	MRC?	Discharge	Incremental BMP DA (acres)	Volume Routed to BMP (CF)	Infiltration / Vegetated Area (SF)	Infiltration Rate (in/hr)	Infiltration Period (hrs)	Vegetated?	Media Depth (ft)	Storage Volume (CF)	Infiltration Credit (CF)	ET Credit (CF)

Totals:

INFILTRATION & ET CREDITS (CF):

NET CHANGE IN VOLUME TO MANAGE (CF):

2,387

TOTAL CREDITS (CF):

West Chester HydroCAD - REV2

Prepared by Dynamic Engineering

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NOAA 24-hr C 2-Year Rainfall=3.26"

Printed 11/2/2024

Stage-Area-Storage for Pond 8P: Prop. UG Basin 24"

Elevation (feet)	Surface (sq-ft)	Storage (cubic-feet)	Elevation (feet)	Surface (sq-ft)	Storage (cubic-feet)
406.00	3,090	0	406.52	3,090	643
406.01	3,090	12	406.53	3,090	655
406.02	3,090	25	406.54	3,090	668
406.03	3,090	37	406.55	3,090	680
406.04	3,090	49	406.56	3,090	692
406.05	3,090	62	406.57	3,090	705
406.06	3,090	74	406.58	3,090	717
406.07	3,090	87	406.59	3,090	729
406.08	3,090	99	406.60	3,090	742
406.09	3,090	111	406.61	3,090	754
406.10	3,090	124	406.62	3,090	766
406.11	3,090	136	406.63	3,090	779
406.12	3,090	148	406.64	3,090	791
406.13	3,090	161	406.65	3,090	803
406.14	3,090	173	406.66	3,090	816
406.15	3,090	185	406.67	3,090	828
406.16	3,090	198	406.68	3,090	841
406.17	3,090	210	406.69	3,090	853
406.18	3,090	223	406.70	3,090	865
406.19	3,090	235	406.71	3,090	878
406.20	3,090	247	406.72	3,090	890
406.21	3,090	260	406.73	3,090	902
406.22	3,090	272	406.74	3,090	915
406.23	3,090	284	406.75	3,090	927
406.24	3,090	297	406.76	3,090	939
406.25	3,090	309	406.77	3,090	952
406.26	3,090	321	406.78	3,090	964
406.27	3,090	334	406.79	3,090	977
406.28	3,090	346	406.80	3,090	989
406.29	3,090	358	406.81	3,090	1,001
406.30	3,090	371	406.82	3,090	1,014
406.31	3,090	383	406.83	3,090	1,026
406.32	3,090	396	406.84	3,090	1,038
406.33	3,090	408	406.85	3,090	1,051
406.34	3,090	420	406.86	3,090	1,063
406.35	3,090	433	406.87	3,090	1,075
406.36	3,090	445	406.88	3,090	1,088
406.37	3,090	457	406.89	3,090	1,100
406.38	3,090	470	406.90	3,090	1,113
406.39	3,090	482	406.91	3,090	1,125
406.40	3,090	494	406.92	3,090	1,137
406.41	3,090	507	406.93	3,090	1,150
406.42	3,090	519	406.94	3,090	1,162
406.43	3,090	532	406.95	3,090	1,174
406.44	3,090	544	406.96	3,090	1,187
406.45	3,090	556	406.97	3,090	1,199
406.46	3,090	569	406.98	3,090	1,211
406.47	3,090	581	406.99	3,090	1,224
406.48	3,090	593	407.00	3,090	1,236
406.49	3,090	606	407.01	3,090	1,248
406.50	3,090	618	407.02	3,090	1,260
406.51	3,090	630	407.03	3,090	1,271

West Chester HydroCAD - REV2

Prepared by Dynamic Engineering

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NOAA 24-hr C 2-Year Rainfall=3.26"

Printed 11/2/2024

Stage-Area-Storage for Pond 8P: Prop. UG Basin 24" (continued)

Elevation (feet)	Surface (sq-ft)	Storage (cubic-feet)	Elevation (feet)	Surface (sq-ft)	Storage (cubic-feet)
407.04	3,090	1,282	407.56	3,090	2,006
407.05	3,090	1,293	407.57	3,090	2,023
407.06	3,090	1,304	407.58	3,090	2,041
407.07	3,090	1,315	407.59	3,090	2,058
407.08	3,090	1,325	407.60	3,090	2,076
407.09	3,090	1,336	407.61	3,090	2,093
407.10	3,090	1,346	407.62	3,090	2,111
407.11	3,090	1,357	407.63	3,090	2,128
407.12	3,090	1,367	407.64	3,090	2,146
407.13	3,090	1,377	407.65	3,090	2,164
407.14	3,090	1,387	407.66	3,090	2,181
407.15	3,090	1,397	407.67	3,090	2,199
407.16	3,090	1,407	407.68	3,090	2,217
407.17	3,090	1,417	407.69	3,090	2,235
407.18	3,090	1,428	407.70	3,090	2,253
407.19	3,090	1,439	407.71	3,090	2,271
407.20	3,090	1,450	407.72	3,090	2,289
407.21	3,090	1,463	407.73	3,090	2,307
407.22	3,090	1,476	407.74	3,090	2,325
407.23	3,090	1,489	407.75	3,090	2,343
407.24	3,090	1,502	407.76	3,090	2,361
407.25	3,090	1,516	407.77	3,090	2,379
407.26	3,090	1,530	407.78	3,090	2,398
407.27	3,090	1,544	407.79	3,090	2,416
407.28	3,090	1,558	407.80	3,090	2,434
407.29	3,090	1,572	407.81	3,090	2,453
407.30	3,090	1,587	407.82	3,090	2,471
407.31	3,090	1,602	407.83	3,090	2,489
407.32	3,090	1,616	407.84	3,090	2,508
407.33	3,090	1,632	407.85	3,090	2,526
407.34	3,090	1,647	407.86	3,090	2,545
407.35	3,090	1,662	407.87	3,090	2,563
407.36	3,090	1,677	407.88	3,090	2,582
407.37	3,090	1,693	407.89	3,090	2,600
407.38	3,090	1,709	407.90	3,090	2,619
407.39	3,090	1,724	407.91	3,090	2,638
407.40	3,090	1,740	407.92	3,090	2,656
407.41	3,090	1,756	407.93	3,090	2,675
407.42	3,090	1,772	407.94	3,090	2,693
407.43	3,090	1,788	407.95	3,090	2,712
407.44	3,090	1,805	407.96	3,090	2,731
407.45	3,090	1,821	407.97	3,090	2,750
407.46	3,090	1,838	407.98	3,090	2,768
407.47	3,090	1,854	407.99	3,090	2,787
407.48	3,090	1,871	408.00	3,090	2,806
407.49	3,090	1,887	408.01	3,090	2,825
407.50	3,090	1,904	408.02	3,090	2,843
407.51	3,090	1,921	408.03	3,090	2,862
407.52	3,090	1,938	408.04	3,090	2,881
407.53	3,090	1,955	408.05	3,090	2,900
407.54	3,090	1,972	408.06	3,090	2,919
407.55	3,090	1,989	408.07	3,090	2,938

 2YR VOLUME
 INFILTRATED
 2,434 > 2,387
 REQUIRED PER
 DEP
 SPREADSHEET


West Chester HydroCAD - REV2

Prepared by Dynamic Engineering

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NOAA 24-hr C 2-Year Rainfall=3.26"

Printed 11/2/2024

Stage-Area-Storage for Pond 8P: Prop. UG Basin 24" (continued)

Elevation (feet)	Surface (sq-ft)	Storage (cubic-feet)	Elevation (feet)	Surface (sq-ft)	Storage (cubic-feet)
408.08	3,090	2,956	408.60	3,090	3,927
408.09	3,090	2,975	408.61	3,090	3,945
408.10	3,090	2,994	408.62	3,090	3,963
408.11	3,090	3,013	408.63	3,090	3,981
408.12	3,090	3,032	408.64	3,090	3,999
408.13	3,090	3,051	408.65	3,090	4,017
408.14	3,090	3,070	408.66	3,090	4,035
408.15	3,090	3,088	408.67	3,090	4,053
408.16	3,090	3,107	408.68	3,090	4,070
408.17	3,090	3,126	408.69	3,090	4,088
408.18	3,090	3,145	408.70	3,090	4,106
408.19	3,090	3,164	408.71	3,090	4,123
408.20	3,090	3,183	408.72	3,090	4,141
408.21	3,090	3,202	408.73	3,090	4,158
408.22	3,090	3,221	408.74	3,090	4,176
408.23	3,090	3,240	408.75	3,090	4,193
408.24	3,090	3,258	408.76	3,090	4,211
408.25	3,090	3,277	408.77	3,090	4,228
408.26	3,090	3,296	408.78	3,090	4,245
408.27	3,090	3,315	408.79	3,090	4,262
408.28	3,090	3,334	408.80	3,090	4,279
408.29	3,090	3,353	408.81	3,090	4,296
408.30	3,090	3,371	408.82	3,090	4,313
408.31	3,090	3,390	408.83	3,090	4,330
408.32	3,090	3,409	408.84	3,090	4,347
408.33	3,090	3,428	408.85	3,090	4,364
408.34	3,090	3,447	408.86	3,090	4,380
408.35	3,090	3,465	408.87	3,090	4,397
408.36	3,090	3,484	408.88	3,090	4,413
408.37	3,090	3,503	408.89	3,090	4,430
408.38	3,090	3,522	408.90	3,090	4,446
408.39	3,090	3,540	408.91	3,090	4,462
408.40	3,090	3,559	408.92	3,090	4,478
408.41	3,090	3,578	408.93	3,090	4,494
408.42	3,090	3,596	408.94	3,090	4,510
408.43	3,090	3,615	408.95	3,090	4,526
408.44	3,090	3,633	408.96	3,090	4,542
408.45	3,090	3,652	408.97	3,090	4,557
408.46	3,090	3,670	408.98	3,090	4,573
408.47	3,090	3,689	408.99	3,090	4,588
408.48	3,090	3,707	409.00	3,090	4,603
408.49	3,090	3,726	409.01	3,090	4,618
408.50	3,090	3,744	409.02	3,090	4,633
408.51	3,090	3,763	409.03	3,090	4,648
408.52	3,090	3,781	409.04	3,090	4,663
408.53	3,090	3,800	409.05	3,090	4,677
408.54	3,090	3,818	409.06	3,090	4,692
408.55	3,090	3,836	409.07	3,090	4,706
408.56	3,090	3,854	409.08	3,090	4,720
408.57	3,090	3,873	409.09	3,090	4,733
408.58	3,090	3,891	409.10	3,090	4,747
408.59	3,090	3,909	409.11	3,090	4,760

West Chester HydroCAD - REV2

Prepared by Dynamic Engineering

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NOAA 24-hr C 2-Year Rainfall=3.26"

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Stage-Area-Storage for Pond 8P: Prop. UG Basin 24" (continued)

Elevation (feet)	Surface (sq-ft)	Storage (cubic-feet)	Elevation (feet)	Surface (sq-ft)	Storage (cubic-feet)
409.12	3,090	4,773	409.64	3,090	5,383
409.13	3,090	4,785	409.65	3,090	5,395
409.14	3,090	4,797	409.66	3,090	5,408
409.15	3,090	4,809	409.67	3,090	5,420
409.16	3,090	4,820	409.68	3,090	5,432
409.17	3,090	4,830	409.69	3,090	5,445
409.18	3,090	4,840	409.70	3,090	5,457
409.19	3,090	4,850	409.71	3,090	5,469
409.20	3,090	4,860	409.72	3,090	5,482
409.21	3,090	4,870	409.73	3,090	5,494
409.22	3,090	4,880	409.74	3,090	5,507
409.23	3,090	4,890	409.75	3,090	5,519
409.24	3,090	4,901	409.76	3,090	5,531
409.25	3,090	4,911	409.77	3,090	5,544
409.26	3,090	4,922	409.78	3,090	5,556
409.27	3,090	4,932	409.79	3,090	5,568
409.28	3,090	4,943	409.80	3,090	5,581
409.29	3,090	4,954	409.81	3,090	5,593
409.30	3,090	4,965	409.82	3,090	5,605
409.31	3,090	4,977	409.83	3,090	5,618
409.32	3,090	4,988			
409.33	3,090	5,000			
409.34	3,090	5,012			
409.35	3,090	5,024			
409.36	3,090	5,037			
409.37	3,090	5,049			
409.38	3,090	5,062			
409.39	3,090	5,074			
409.40	3,090	5,086			
409.41	3,090	5,099			
409.42	3,090	5,111			
409.43	3,090	5,123			
409.44	3,090	5,136			
409.45	3,090	5,148			
409.46	3,090	5,160			
409.47	3,090	5,173			
409.48	3,090	5,185			
409.49	3,090	5,197			
409.50	3,090	5,210			
409.51	3,090	5,222			
409.52	3,090	5,235			
409.53	3,090	5,247			
409.54	3,090	5,259			
409.55	3,090	5,272			
409.56	3,090	5,284			
409.57	3,090	5,296			
409.58	3,090	5,309			
409.59	3,090	5,321			
409.60	3,090	5,333			
409.61	3,090	5,346			
409.62	3,090	5,358			
409.63	3,090	5,371			

K. BASIN DEWATERING CALCULATIONS

West Chester HydroCAD - REV2

Prepared by Dynamic Engineering

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NOAA 24-hr C 2-Year Rainfall=3.26"

Printed 11/4/2024

Hydrograph for Pond 8P: Prop. UG Basin 24"

Time (hours)	Inflow (cfs)	Storage (cubic-feet)	Elevation (feet)	Outflow (cfs)	Discarded (cfs)	Primary (cfs)
0.00	0.00	0	406.00	0.00	0.00	0.00
5.00	0.02	44	406.04	0.01	0.01	0.00
10.00	0.06	347	406.28	0.01	0.01	0.00
15.00	0.06	2,525	407.85	0.06	0.01	0.05
20.00	0.03	2,471	407.82	0.03	0.01	0.01
25.00	0.00	2,406	407.78	0.01	0.01	0.00
30.00	0.00	2,149	407.64	0.01	0.01	0.00
35.00	0.00	1,891	407.49	0.01	0.01	0.00
40.00	0.00	1,634	407.33	0.01	0.01	0.00
45.00	0.00	1,376	407.13	0.01	0.01	0.00
50.00	0.00	1,119	406.91	0.01	0.01	0.00
55.00	0.00	861	406.70	0.01	0.01	0.00
60.00	0.00	604	406.49	0.01	0.01	0.00
65.00	0.00	346	406.28	0.01	0.01	0.00
70.00	0.00	89	406.07	0.01	0.01	0.00
75.00	0.00	0	406.00	0.00	0.00	0.00
80.00	0.00	0	406.00	0.00	0.00	0.00
85.00	0.00	0	406.00	0.00	0.00	0.00
90.00	0.00	0	406.00	0.00	0.00	0.00
95.00	0.00	0	406.00	0.00	0.00	0.00
100.00	0.00	0	406.00	0.00	0.00	0.00
105.00	0.00	0	406.00	0.00	0.00	0.00
110.00	0.00	0	406.00	0.00	0.00	0.00
115.00	0.00	0	406.00	0.00	0.00	0.00
120.00	0.00	0	406.00	0.00	0.00	0.00
125.00	0.00	0	406.00	0.00	0.00	0.00
130.00	0.00	0	406.00	0.00	0.00	0.00
135.00	0.00	0	406.00	0.00	0.00	0.00
140.00	0.00	0	406.00	0.00	0.00	0.00
145.00	0.00	0	406.00	0.00	0.00	0.00
150.00	0.00	0	406.00	0.00	0.00	0.00
155.00	0.00	0	406.00	0.00	0.00	0.00
160.00	0.00	0	406.00	0.00	0.00	0.00
165.00	0.00	0	406.00	0.00	0.00	0.00
170.00	0.00	0	406.00	0.00	0.00	0.00
175.00	0.00	0	406.00	0.00	0.00	0.00
180.00	0.00	0	406.00	0.00	0.00	0.00
185.00	0.00	0	406.00	0.00	0.00	0.00
190.00	0.00	0	406.00	0.00	0.00	0.00

 2YR VOLUME
DEWATERS WITHIN
96 HOURS


L. TIME OF CONCENTRATION CALCULATIONS

STANDARD E&S WORKSHEET #9
 Determination of Time of Concentration (T_c)
 (FOR SCS METHOD)

PROJECT NAME: Paramount West Chester
 LOCATION: Westtown Township PA
 PREPARED BY: MSW
 LAST REVISED BY:

DATE: 7/1/24
 DATE:

FEATURE/STRUCTURE ##

Two-year 24-hour Rainfall, P_2 : 2.99

OVERLAND FLOW:

PATH NUMBER	Length (ft)	TYPE OF COVER	"n"	Avg. Slope (S) (ft/ft)	TIME (minutes)
A-B	44	Dense Grasses	0.24	0.21	3.00
B-C	56	Smooth Surfaces	0.011	0.038	0.25

$$T_c = \frac{0.007(nL)^{0.8}}{(P_2)^{0.5} S^{0.4}}$$

SHALLOW CONCENTRATED FLOW:

PATH NUMBER	Length (ft)	TYPE OF COVER	Avg. Slope (ft/ft)	V (ft/sec)	TIME (minutes)
C-D	419	Paved	0.01	2.03	3.44

CHANNEL FLOW:

PATH NUMBER	Length (ft)	AREA (sq. ft.)	Avg. Slope (ft/ft)	WETTED PERIMETER (ft)	HYDRAULIC RADIUS (ft)	MANNING'S n	V (ft/sec)	CHANNEL TIME (minutes)
		0.00		#DIV/0!	#DIV/0!		#DIV/0!	#DIV/0!

CHANNEL DIMENSIONS:

PATH NUMBER	BOTTOM WIDTH (ft)	TOTAL DEPTH (ft)	RIGHT SIDE SLOPE (H:V)	LEFT SIDE SLOPE (H:V)	TOP WIDTH (ft)	CALC. FLOW DEPTH (ft)

PIPE FLOW:

PATH NUMBER	Length (ft)	AREA (sq. ft.)	Avg. Slope (ft/ft)	WETTED PERIMETER (ft)	HYDRAULIC RADIUS (ft)	MANNING'S n	V (ft/sec)	PIPE TIME (minutes)
		0.00		0.00	#DIV/0!		#DIV/0!	#DIV/0!

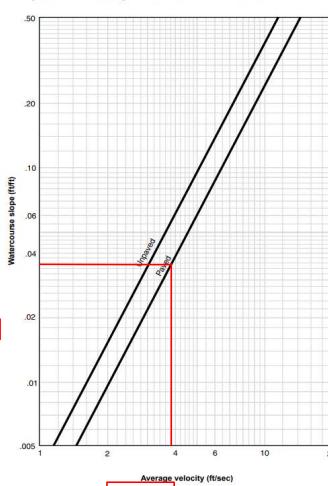
PIPE DIMENSIONS:

PATH NUMBER	PIPE DIAM. (in)	PIPE MATERIAL

Total Time of Concentration: 6.68

FEATURE/STRUCTURE ##

Figure 3-1 Average velocities for estimating travel time for shallow concentrated flow



STANDARD E&S WORKSHEET #9
 Determination of Time of Concentration (T_c)
 (FOR SCS METHOD)

PROJECT NAME: Paramount West Chester
 LOCATION: Westtown Township PA
 PREPARED BY: MSW
 LAST REVISED BY:

DATE: 7/1/24

DATE:

FEATURE/STRUCTURE ##

Two-year 24-hour Rainfall, P_2 : 2.99

OVERLAND FLOW:

PATH NUMBER	Length (ft)	TYPE OF COVER	"n" VALUE	AVG. SLOPE (S) (ft/ft)	TIME (minutes)
A-B	37	Dense Grasses	0.24	0.28	2.33
B-C	63	Smooth Surfaces	0.011	0.05	0.62

$$T_c = \frac{0.007(nL)^{0.8}}{(P_2)^{0.5} S^{0.4}}$$

SHALLOW CONCENTRATED FLOW:

PATH NUMBER	Length (ft)	TYPE OF COVER	Avg. Slope (ft/ft)	V (ft/sec)	TIME (minutes)
B-C	566	Paved	0.02	2.87	3.28

PATH NUMBER	Length (ft)	AREA (sq. ft.)	Avg. Slope (ft/ft)	WETTED PERIMETER (ft)	HYDRAULIC RADIUS (ft)	MANNING'S n	V (ft/sec)	CHANNEL TIME (minutes)
		0.00		#DIV/0!	#DIV/0!		#DIV/0!	#DIV/0!

CHANNEL DIMENSIONS:

PATH NUMBER	BOTTOM WIDTH (ft)	TOTAL DEPTH (ft)	RIGHT SIDE SLOPE (H:V)	LEFT SIDE SLOPE (H:V)	TOP WIDTH (ft)	CALC. FLOW DEPTH (ft)

PIPE FLOW:

PATH NUMBER	Length (ft)	AREA (sq. ft.)	Avg. Slope (ft/ft)	WETTED PERIMETER (ft)	HYDRAULIC RADIUS (ft)	MANNING'S n	V (ft/sec)	PIPE TIME (minutes)
		0.00		0.00	#DIV/0!		#DIV/0!	#DIV/0!

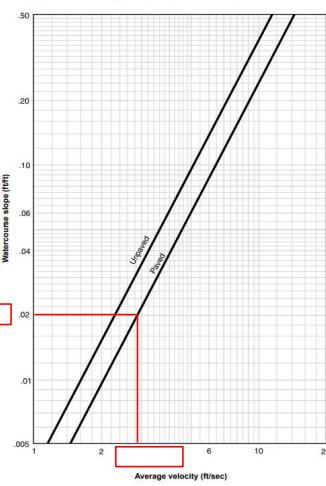
PIPE DIMENSIONS:

PATH NUMBER	PIPE DIAM. (in)	PIPE MATERIAL

Total Time of Concentration: 6.22

FEATURE/STRUCTURE ##

Figure 3-1 Average velocities for estimating travel time for shallow concentrated flow



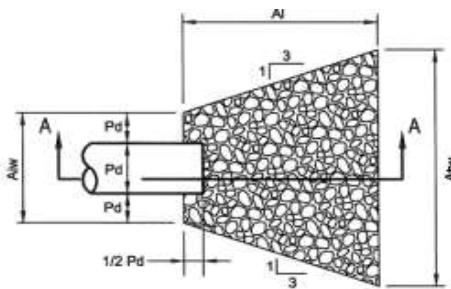
M. RIP RAP CALCULATIONS

EROSION AND SEDIMENTATION CONTROL PLAN

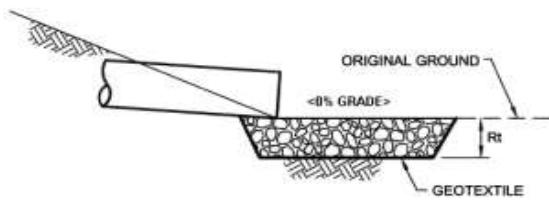
STANDARD WORKSHEET #20 Riprap Apron Outlet Protection

PROJECT NAME:
LOCATION:
PREPARED BY:
CHECKED BY:

Proposed Chase Bank
Westtown Township, PA
MSW DATE: 9/27/2024
SRM DATE: 9/27/2024



PLAN VIEW



SECTION A - A

NO.	PIPE DIA. Do (in.)	TAIL WATER COND.(Ma x or Min)	MAN. "n" FOR PIPE	PIPE SLOPE (FT/FT)	Q (CFS)	V* (FPS)	RIPRAP SIZE	Rt (in)	Al (ft)	Aiw (ft)	Atw (ft)
HW #501	18	MIN	0.012	0.01	4.06	2.34	R-3	9	8	1.5	12.5

* The anticipated velocity (V) should not exceed the maximum permissible shown in Table 6.6 for the proposed riprap protection. Adjust for less than full pipe flow. Use Manning's equation to calculate velocity for pipe slopes ≥ 0.05 ft/ft.

**N. STORMWATER INFILTRATION TESTING
REPORT (BY DYNAMIC EARTH)**

STORMWATER BASIN AREA INVESTIGATION REPORT

PROPOSED CHASE BANK
1506 Pennsylvania State Highway Route 3 (West Chester Pike)
Parcel No. 67-2-42:4
Township of Westtown, Chester County, Pennsylvania

PARAMOUNT REALTY SERVICES, INC
1195 Route 70, Suite 2000
Lakewood, New Jersey 08701



826 Newtown Yardley Road, Suite 201
Newtown, PA 18940



Gregory J. Fritts, P.E.
Principal
PA PE License No. 090904

Project #1478-99-191EC
September 26, 2024

STORMWATER BASIN AREA INVESTIGATION REPORT

PROPOSED CHASE BANK

1506 Pennsylvania State Highway Route 3 (West Chester Pike)
Parcel No. 67-2-42:4

Township of Westtown, Chester County, Pennsylvania

TABLE OF CONTENTS

1.0	INTRODUCTION	1
2.0	SCOPE OF SERVICES	2
3.0	SOIL SURVEY	2
4.0	RESULTS	2
4.1	Subsurface Soil Profile	2
4.2	Subsurface Conditions and Soil Permeability	3
5.0	GENERAL COMMENTS AND LIMITATIONS	3

APPENDICES

- Soil Profile Pit Location Plan
Records of Subsurface Exploration
Infiltration Test Results
NRCS-USDA Custom Soil Survey of Chester County, Pennsylvania

1.0 INTRODUCTION

Dynamic Earth, LLC (Dynamic Earth) has completed a subsurface evaluation for the stormwater management facilities associated with the proposed commercial development to be located at 1506 Pennsylvania State Highway Route 3 (West Chester Pike) in the Township of Westtown, Chester County, Pennsylvania.

The subject site is further identified as Parcel No. 67-2-42-4 and is bound to the north by West Chester Pike with commercial properties beyond; to the east by commercial properties; to the west by the existing retail development with commercial properties beyond; and to the south by the existing retail development with residential properties beyond. The project site is shown on the attached *Soil Profile Pit Location Plan* included in the Appendix of this report.

At the time of Dynamic Earth's investigation, the subject site consisted of a paved parcel located in the northeastern corner of a larger retail development with associated pavements and utilities. Surface cover observed at the time of our investigation included asphalt pavements.

Topographic information was provided on a January 10, 2023 *Partial Topographic Survey, Sheets 1 and 2*, prepared by Dynamic Survey, LLC. Existing site grades generally slope downward toward the southeast and southwest from a high elevation of approximately 424.0 feet along the northeastern property boundary, to low elevations of approximately 405.0 feet and 403.0 feet along the southwestern and southeastern property boundaries. The elevations referenced in the survey, and throughout this report, are given in 1988 North American Vertical Datum (NAVD88), unless otherwise noted.

Based on a July 12, 2024 *Grading Plan* prepared by Dynamic Engineering Consultants, P.C., the proposed site development will include the construction of a one-story Chase Bank with associated drive-up ATM. The proposed building is expected to occupy a footprint area of approximately 3,294 square feet and contain a finished floor elevation of approximately 414.65 feet. Based on the aforementioned grading plan, maximum earth cuts and fills of approximately 0.7 feet and 1.7 feet are expected to be required across the proposed building pad; respectively. Additional site improvements are expected to include pavements, utilities, and stormwater management facilities.

The stormwater management facilities proposed to infiltrate stormwater runoff are anticipated to consist of an underground basin located within the southern portion of the site. The proposed underground basin will reportedly contain an invert elevation of 406.5 feet.

2.0 SCOPE OF SERVICES

Dynamic Earth's scope of services pertaining to this report included evaluating the subsurface conditions by excavating soil profile pits to estimate the apparent seasonal high groundwater levels and performing in-situ permeability testing. A total of two soil profile pits (identified as SPP-1 and SPP-2) were excavated using a track-mounted backhoe. Additionally, two in-situ permeability tests were performed at corresponding soil profile pit locations. The test locations were located within existing asphalt-paved areas, were backfilled to the surface with excavated soil, and were patched superficially with hot mix asphalt upon completion. The soil profile pit locations are shown on the attached *Soil Profile Pit Location Plan*. The Township of Westtown's engineer was informed of the planned test坑ing prior to our mobilization.

The soils encountered were classified in general conformance with U.S. Department of Agriculture (USDA) soil classification. Observations were made for groundwater and/or redoximorphic features indicative of zones of saturation or seasonal high groundwater. Soil logs are included in the Appendix of this report.

Infiltration testing was performed in general accordance with Pennsylvania's *Stormwater Best Management Practices Manual-Appendix C* using double-ring infiltrometer techniques. Detailed results of the infiltration testing are included in the appendix of this report.

Environmental conditions were not evaluated by Dynamic Earth.

3.0 SOIL SURVEY

Based on a review of the United States Department of Agriculture – Natural Resources Conservation Services (USDA-NRCS) soil survey, Urban Land is mapped beneath the site. The *USDA-NRCS Custom Soil Report* is included in the appendix of this report, for reference.

4.0 RESULTS

Detailed descriptions of the subsurface conditions encountered at each location are provided on the *Records of Subsurface Exploration* included herein. A summary of the subsurface conditions encountered is included below.

4.1 Subsurface Soil Profile

Soil profile pits were performed within asphalt-paved areas and encountered approximately four inches of asphalt underlain by approximately four inches of gravel subbase at the surface. Beneath the surficial cover, existing fill materials were encountered that generally consisted of

apparent reworked on-site silty clay loam with variable amounts of gravel and debris. The debris encountered consisted of wood fragments. Where penetrated, this stratum extended to depths ranging between approximately 2.7 feet and 2.9 feet below the ground surface; corresponding to elevations 409.6 feet and 409.3 feet. Beneath the existing fill materials, apparent buried topsoil was encountered within SPP-1 at a depth of approximately 2.7 feet below the ground surface, corresponding to an elevation of 409.3 feet. The apparent buried topsoil extended to a depth of approximately 3.8 feet, corresponding to an elevation of approximately 408.2 feet. Beneath the existing fill material and/or apparent buried topsoil, naturally occurring residual soils were encountered that generally consisted of silt loam with variable amounts of gravel. The natural residual soils extended to termination depths ranging between approximately 12.3 feet and 12.8 feet below the ground surface; corresponding to an elevation of 399.7 feet.

4.2 Subsurface Conditions and Soil Permeability

Evidence of seasonal high groundwater (based on soil mottling) and/or groundwater were not encountered during this investigation. Groundwater is expected to fluctuate seasonally and following periods of significant precipitation.

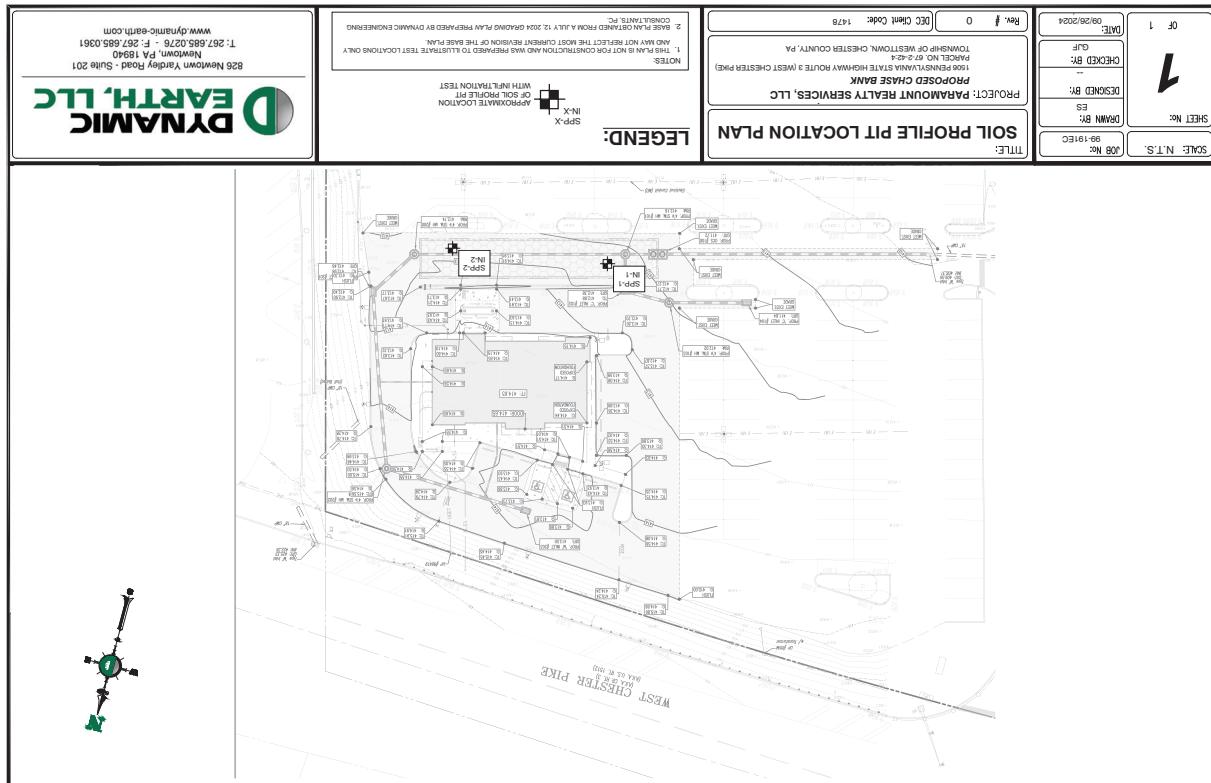
In-situ testing was performed at each soil profile pit location and yielded permeability rates ranging between approximately 0.5 inches per hour (iph) and 0.75 iph. A summary of groundwater and in-situ permeability test results is tabulated below:

SUMMARY OF SUBSURFACE CONDITIONS & FIELD PERMEABILITY TESTING						
Location	Surface Elevation (feet)	Soil Mottling	Groundwater		Infiltration Test Results	Comments
			Depth (feet)	Elevation (feet)		
SPP-1	412.0	Not Encountered		Not Encountered	60	0.75 Fill to 2.7'
SPP-2	412.5	Not Encountered		Not Encountered	72	0.5 Fill to 2.9'

Field Infiltration Rate – does not include factor of safety

5.0 GENERAL COMMENTS AND LIMITATIONS

Supplemental recommendations will be required upon finalization of conceptual site plans or if significant changes are made in the characteristics or location of the proposed stormwater management facilities. Dynamic Earth should be included as a consultant to the design team and should be provided with final plans for review to confirm these criteria apply or to modify recommendations as necessary.



Soil Profile Pit Location Plan

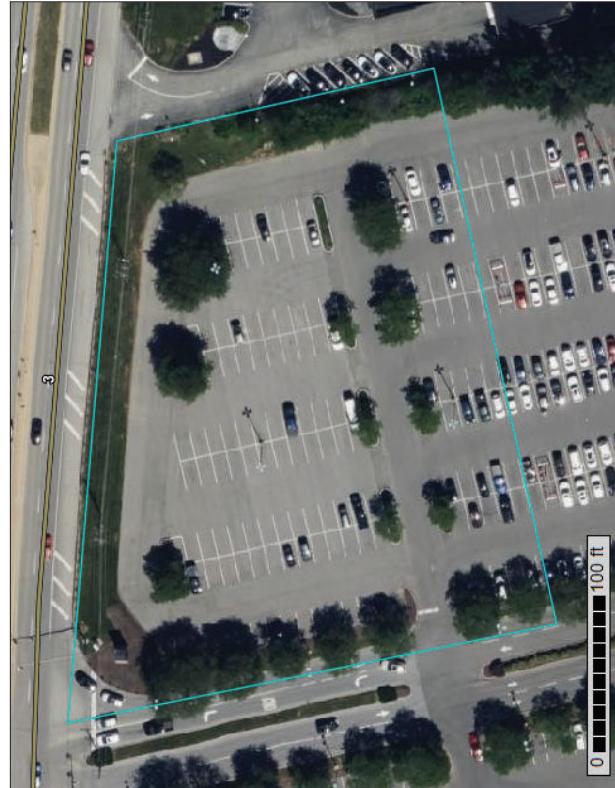
Records of Subsurface Exploration

Soil PROFILE LOG											
Soil Profile Log											
Soil Profile Log											
Soil Type	Color	Texture	Coarse Particles (%)	Fine Particles (%)	Organic Matter (%)	Roots	Boulders	Shrub	Trees	Flora	Fauna
Soil Depth (cm)	Soil Depth (cm)	Soil Depth (cm)	Soil Depth (cm)	Soil Depth (cm)	Soil Depth (cm)	Soil Depth (cm)	Soil Depth (cm)	Soil Depth (cm)	Soil Depth (cm)	Soil Depth (cm)	Soil Depth (cm)
0-5 cm	Dark Brown	Sandy Loam	60	30	10	0	0	0	0	0	0
5-10 cm	Medium Brown	Sandy Loam	60	30	10	0	0	0	0	0	0
10-20 cm	Light Brown	Sandy Loam	60	30	10	0	0	0	0	0	0
20-30 cm	Yellowish Brown	Sandy Loam	60	30	10	0	0	0	0	0	0
30-40 cm	Light Brown	Sandy Loam	60	30	10	0	0	0	0	0	0
40-50 cm	Medium Brown	Sandy Loam	60	30	10	0	0	0	0	0	0
50-60 cm	Dark Brown	Sandy Loam	60	30	10	0	0	0	0	0	0
60-70 cm	Medium Brown	Sandy Loam	60	30	10	0	0	0	0	0	0
70-80 cm	Light Brown	Sandy Loam	60	30	10	0	0	0	0	0	0
80-90 cm	Yellowish Brown	Sandy Loam	60	30	10	0	0	0	0	0	0
90-100 cm	Light Brown	Sandy Loam	60	30	10	0	0	0	0	0	0
100-120 cm	Medium Brown	Sandy Loam	60	30	10	0	0	0	0	0	0
120-140 cm	Dark Brown	Sandy Loam	60	30	10	0	0	0	0	0	0
140-160 cm	Medium Brown	Sandy Loam	60	30	10	0	0	0	0	0	0
160-180 cm	Light Brown	Sandy Loam	60	30	10	0	0	0	0	0	0
180-200 cm	Yellowish Brown	Sandy Loam	60	30	10	0	0	0	0	0	0
200-220 cm	Light Brown	Sandy Loam	60	30	10	0	0	0	0	0	0
220-240 cm	Medium Brown	Sandy Loam	60	30	10	0	0	0	0	0	0
240-260 cm	Dark Brown	Sandy Loam	60	30	10	0	0	0	0	0	0
260-280 cm	Medium Brown	Sandy Loam	60	30	10	0	0	0	0	0	0
280-300 cm	Light Brown	Sandy Loam	60	30	10	0	0	0	0	0	0
300-320 cm	Yellowish Brown	Sandy Loam	60	30	10	0	0	0	0	0	0
320-340 cm	Light Brown	Sandy Loam	60	30	10	0	0	0	0	0	0
340-360 cm	Medium Brown	Sandy Loam	60	30	10	0	0	0	0	0	0
360-380 cm	Dark Brown	Sandy Loam	60	30	10	0	0	0	0	0	0
380-400 cm	Medium Brown	Sandy Loam	60	30	10	0	0	0	0	0	0
400-420 cm	Light Brown	Sandy Loam	60	30	10	0	0	0	0	0	0
420-440 cm	Yellowish Brown	Sandy Loam	60	30	10	0	0	0	0	0	0
440-460 cm	Light Brown	Sandy Loam	60	30	10	0	0	0	0	0	0
460-480 cm	Medium Brown	Sandy Loam	60	30	10	0	0	0	0	0	0
480-500 cm	Dark Brown	Sandy Loam	60	30	10	0	0	0	0	0	0
500-520 cm	Medium Brown	Sandy Loam	60	30	10	0	0	0	0	0	0
520-540 cm	Light Brown	Sandy Loam	60	30	10	0	0	0	0	0	0
540-560 cm	Yellowish Brown	Sandy Loam	60	30	10	0	0	0	0	0	0
560-580 cm	Light Brown	Sandy Loam	60	30	10	0	0	0	0	0	0
580-600 cm	Medium Brown	Sandy Loam	60	30	10	0	0	0	0	0	0
600-620 cm	Dark Brown	Sandy Loam	60	30	10	0	0	0	0	0	0
620-640 cm	Medium Brown	Sandy Loam	60	30	10	0	0	0	0	0	0
640-660 cm	Light Brown	Sandy Loam	60	30	10	0	0	0	0	0	0
660-680 cm	Yellowish Brown	Sandy Loam	60	30	10	0	0	0	0	0	0
680-700 cm	Light Brown	Sandy Loam	60	30	10	0	0	0	0	0	0
700-720 cm	Medium Brown	Sandy Loam	60	30	10	0	0	0	0	0	0
720-740 cm	Dark Brown	Sandy Loam	60	30	10	0	0	0	0	0	0
740-760 cm	Medium Brown	Sandy Loam	60	30	10	0	0	0	0	0	0
760-780 cm	Light Brown	Sandy Loam	60	30	10	0	0	0	0	0	0
780-800 cm	Yellowish Brown	Sandy Loam	60	30	10	0	0	0	0	0	0
800-820 cm	Light Brown	Sandy Loam	60	30	10	0	0	0	0	0	0
820-840 cm	Medium Brown	Sandy Loam	60	30	10	0	0	0	0	0	0
840-860 cm	Dark Brown	Sandy Loam	60	30	10	0	0	0	0	0	0
860-880 cm	Medium Brown	Sandy Loam	60	30	10	0	0	0	0	0	0
880-900 cm	Light Brown	Sandy Loam	60	30	10	0	0	0	0	0	0
900-920 cm	Yellowish Brown	Sandy Loam	60	30	10	0	0	0	0	0	0
920-940 cm	Light Brown	Sandy Loam	60	30	10	0	0	0	0	0	0
940-960 cm	Medium Brown	Sandy Loam	60	30	10	0	0	0	0	0	0
960-980 cm	Dark Brown	Sandy Loam	60	30	10	0	0	0	0	0	0
980-1000 cm	Medium Brown	Sandy Loam	60	30	10	0	0	0	0	0	0
1000-1020 cm	Light Brown	Sandy Loam	60	30	10	0	0	0	0	0	0
1020-1040 cm	Yellowish Brown	Sandy Loam	60	30	10	0	0	0	0	0	0
1040-1060 cm	Light Brown	Sandy Loam	60	30	10	0	0	0	0	0	0
1060-1080 cm	Medium Brown	Sandy Loam	60	30	10	0	0	0	0	0	0
1080-1100 cm	Dark Brown	Sandy Loam	60	30	10	0	0	0	0	0	0
1100-1120 cm	Medium Brown	Sandy Loam	60	30	10	0	0	0	0	0	0
1120-1140 cm	Light Brown	Sandy Loam	60	30	10	0	0	0	0	0	0
1140-1160 cm	Yellowish Brown	Sandy Loam	60	30	10	0	0	0	0	0	0
1160-1180 cm	Light Brown	Sandy Loam	60	30	10	0	0	0	0	0	0
1180-1200 cm	Medium Brown	Sandy Loam	60	30	10	0	0	0	0	0	0
1200-1220 cm	Dark Brown	Sandy Loam	60	30	10	0	0	0	0	0	0
1220-1240 cm	Medium Brown	Sandy Loam	60	30	10	0	0	0	0	0	0
1240-1260 cm	Light Brown	Sandy Loam	60	30	10	0	0	0	0	0	0
1260-1280 cm	Yellowish Brown	Sandy Loam	60	30	10	0	0	0	0	0	0
1280-1300 cm	Light Brown	Sandy Loam	60	30	10	0	0	0	0	0	0
1300-1320 cm	Medium Brown	Sandy Loam	60	30	10	0	0	0	0	0	0
1320-1340 cm	Dark Brown	Sandy Loam	60	30	10	0	0	0	0	0	0
1340-1360 cm	Medium Brown	Sandy Loam	60	30	10	0	0	0	0	0	0
1360-1380 cm	Light Brown	Sandy Loam	60	30	10	0	0	0	0	0	0
1380-1400 cm	Yellowish Brown	Sandy Loam	60	30	10	0	0	0	0	0	0
1400-1420 cm	Light Brown	Sandy Loam	60	30	10	0	0	0	0	0	0
1420-1440 cm	Medium Brown	Sandy Loam	60	30	10	0	0	0	0	0	0
1440-1460 cm	Dark Brown	Sandy Loam	60	30	10	0	0	0	0	0	0
1460-1480 cm	Medium Brown	Sandy Loam	60	30	10	0	0	0	0	0	0
1480-1500 cm	Light Brown	Sandy Loam	60	30	10	0	0	0	0	0	0
1500-1520 cm	Yellowish Brown	Sandy Loam	60	30	10	0	0	0	0	0	0
1520-1540 cm	Light Brown	Sandy Loam	60	30	10	0	0	0	0	0	0
1540-1560 cm	Medium Brown	Sandy Loam	60	30	10	0	0	0	0	0	0
1560-1580 cm	Dark Brown	Sandy Loam	60	30	10	0	0	0	0	0	0
1580-1600 cm	Medium Brown	Sandy Loam	60	30	10	0	0	0	0	0	0
1600-1620 cm	Light Brown	Sandy Loam	60	30	10	0	0	0	0	0	0
1620-1640 cm	Yellowish Brown	Sandy Loam	60	30	10	0	0	0	0	0	0
1640-1660 cm	Light Brown	Sandy Loam	60	30	10	0	0	0	0	0	0
1660-1680 cm	Medium Brown	Sandy Loam	60	30	10	0	0	0	0	0	0
1680-1700 cm	Dark Brown	Sandy Loam	60	30	10	0	0	0	0	0	0
1700-1720 cm	Medium Brown	Sandy Loam	60	30	10	0	0	0	0	0	0
1720-1740 cm	Light Brown	Sandy Loam	60	30	10	0	0	0	0	0	0
1740-1760 cm	Yellowish Brown	Sandy Loam	60	30	10	0	0	0	0	0	0
1760-1780 cm	Light Brown	Sandy Loam	60	30	10	0	0	0	0	0	0
1780-1800 cm	Medium Brown	Sandy Loam	60	30	10	0	0	0	0	0	0
1800-1820 cm	Dark Brown	Sandy Loam	60	30	10	0	0	0	0	0	0
1820-1840 cm	Medium Brown	Sandy Loam	60	30	10	0	0	0	0	0	0
1840-1860 cm	Light Brown	Sandy Loam	60	30	10	0	0	0	0	0	0
1860-1880 cm	Yellowish Brown	Sandy Loam	60	30	10	0	0	0	0	0	0
1880-1900 cm	Light Brown	Sandy Loam	60	30	10	0	0	0	0	0	0
1900-1920 cm	Medium Brown	Sandy Loam	60	30	10	0	0	0	0	0	0
1920-1940 cm	Dark Brown	Sandy Loam	60	30	10	0	0	0	0	0	0
1940-1960 cm	Medium Brown	Sandy Loam	60	30	10	0	0	0	0	0	0
1960-1980 cm	Light Brown	Sandy Loam	60	30	10	0	0	0	0	0	0
1980-2000 cm	Yellowish Brown	Sandy Loam	60	30	10	0	0	0	0	0	0
2000-2020 cm	Light Brown	Sandy Loam	60	30	10	0	0	0	0	0	0
2020-2040 cm	Medium Brown	Sandy Loam	60	30	10	0	0	0	0	0	0
2040-2060 cm	Dark Brown	Sandy Loam	60	30	10	0	0	0	0	0	0
2060-2080 cm	Medium Brown	Sandy Loam	60	30	10	0	0	0	0	0	0
2080-2100 cm	Light Brown	Sandy Loam	60	30	10	0	0	0	0	0	0
2100-2120 cm	Yellowish Brown	Sandy Loam	60	30	10	0	0	0	0	0	0
2120-2140 cm	Light Brown	Sandy Loam	60	30	10	0	0	0	0	0	0
2140-2160 cm	Medium Brown	Sandy Loam	60	30	10	0	0	0	0	0	0
2160-2180 cm	Dark Brown	Sandy Loam	60	30	10	0	0	0	0	0	0
2180-2200 cm	Medium Brown	Sandy Loam	60	30	10	0	0	0	0	0	0
2200-2220 cm	Light Brown	Sandy Loam	60	30	10	0	0	0	0	0	0
2220-2240 cm	Yellowish Brown	Sandy Loam	60	30	10	0	0	0	0	0	0
2240-2260 cm	Light Brown	Sandy Loam	60	30	10	0	0	0	0	0	0
2260-2280 cm	Medium Brown	Sandy Loam	60	30	10	0	0	0	0	0	0
2280-2300 cm	Dark Brown	Sandy Loam	60	30	10	0	0	0	0	0	0
2300-2320 cm	Medium Brown	Sandy Loam	60	30	10	0	0	0	0	0	0
2320-2340 cm	Light Brown	Sandy Loam	60	30	10	0	0	0	0	0	0
2340-2360 cm	Yellowish Brown	Sandy Loam	60	30	10	0	0	0	0	0	0
2360-2380 cm	Light Brown	Sandy Loam	60	30	10	0	0	0	0	0	0
2380-2400 cm	Medium Brown	Sandy Loam	60	30	10	0	0	0	0	0	0
2400-2420 cm	Dark Brown	Sandy Loam	60	30	10	0	0	0	0	0	0
2420-2440 cm	Medium Brown	Sandy Loam	60	30	10	0	0	0	0	0	0
2440-2460											

Infiltration Test Results

**Custom Soil Resource
Report for
Chester County,
Pennsylvania**

A product of the National Cooperative Soil Survey, a joint effort of the United States Department of Agriculture and other Federal agencies, State agencies including the Agricultural Experiment Stations, and local participants



NRCS-USDA Custom Soil Survey
of Chester County, Pennsylvania

July 31, 2024

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Preface

Soil surveys contain information that affects land use planning in survey areas. They highlight soil limitations that affect various land uses and provide information about the properties of the soils in the survey areas. Soil surveys are designed for many different users, including farmers, ranchers, foresters, agronomists, urban planners, community officials, engineers, developers, builders, and home buyers. Also, conservationists, teachers, students, and specialists in recreation, waste disposal, and pollution control can use the surveys to help them understand, protect, or enhance the environment.

Various land use regulations of Federal, State, and local governments may impose special restrictions on land use or land treatment. Soil surveys identify soil properties that are used in making various land use or land treatment decisions. The information is intended to help the land users identify and reduce the effects of soil limitations on various land uses. The landowner or user is responsible for identifying and complying with existing laws and regulations.

Although soil survey information can be used for general farm, local, and wider area planning, onsite investigation is needed to supplement this information in some cases. Examples include soil quality assessments (<http://www.nrcs.usda.gov/wps/portal/nrcs/main/soils/health/>) and certain conservation and engineering applications. For more detailed information, contact your local USDA Service Center (<https://offices.sc.egov.usda.gov/locator/app?agency=nrcs>) or your NRCS State Soil Scientist (http://www.nrcs.usda.gov/wps/portal/nrcs/detail/soils/contactus/?clid=nrcs142p2_053951).

Great differences in soil properties can occur within short distances. Some soils are seasonally wet or subject to flooding. Some are too unstable to be used as a foundation for buildings or roads. Clayey or wet soils are poorly suited to use as septic tank absorption fields. A high water table makes a soil poorly suited to basements or underground installations.

The National Cooperative Soil Survey is a joint effort of the United States Department of Agriculture and other Federal agencies. State agencies including the Agricultural Experiment Stations, and local agencies, The Natural Resources Conservation Service (NRCS) has leadership for the Federal part of the National Cooperative Soil Survey.

Information about soils is updated periodically. Updated information is available through the NRCS Web Soil Survey, the site for official soil survey information.

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How Soil Surveys Are Made

Soil surveys are made to provide information about the soils and miscellaneous areas in a specific area. They include a description of the soils and miscellaneous areas and their location on the landscape and tables that show soil properties and limitations affecting various uses. Soil scientists observed the steepness, length, and shape of the slopes; the general pattern of drainage; the kinds of crops and native plants; and the kinds of bedrock. They observed and described many soil profiles. A soil profile is the sequence of natural layers, or horizons, in a soil. The profile extends from the surface down into the unconsolidated material in which the soil formed or from the surface down to bedrock. The unconsolidated material is devoid of roots and other living organisms and has not been changed by other biological activity.

Currently, soils are mapped according to the boundaries of major land resource areas (MLRAs). MLRAs are geographically associated land resource units that share common characteristics related to physiography, geology, climate, water resources, soils, biological resources, and land uses (USDA, 2006). Soil survey areas typically consist of parts of one or more MLRA.

The soils and miscellaneous areas in a survey area occur in an orderly pattern that is related to the geology, landforms, relief, climate, and natural vegetation of the area. Each kind of soil and miscellaneous area is associated with a particular kind of landform or with a segment of the landform. By observing the soils and miscellaneous areas in the survey area and relating their position to specific segments of the landform, a soil scientist develops a concept, or model, of how they were formed. Thus, during mapping, this model enables the soil scientist to predict with a considerable degree of accuracy the kind of soil or miscellaneous area at a specific location on the landscape.

Commonly, individual soils on the landscape merge into one another as their characteristics gradually change. To construct an accurate soil map, however, soil scientists must determine the boundaries between the soils. They can observe only a limited number of soil profiles. Nevertheless, these observations, supplemented by an understanding of the soil-vegetation-landscape relationship, are sufficient to verify predictions of the kinds of soil in an area and to determine the boundaries.

Soil scientists recorded the characteristics of the soil profiles that they studied. They noted soil color, texture, size and shape of soil aggregates, kind and amount of rock fragments, distribution of plant roots, reaction, and other features that enable them to identify soils. After describing the soils in the survey area and determining their properties, the soil scientist assigned the soils to taxonomic classes (units). Taxonomic classes are concepts. Each taxonomic class has a set of soil characteristics with precisely defined limits. The classes are used as a basis for comparison to classify soils systematically. Soil taxonomy, the system of taxonomic classification used in the United States, is based mainly on the kind and character of soil properties and the arrangement of horizons within the profile. After the soil

scientists classified and named the soils in the survey area, they compared the individual soils with similar soils in the same taxonomic class in other areas so that they could confirm data and assemble additional data based on experience and research.

The objective of soil mapping is not to delineate pure map unit components; the objective is to separate the landscape into landforms or landform segments that have similar use and management requirements. Each map unit is defined by a unique combination of soil components and/or miscellaneous areas in predictable proportions. Some components may be highly contrasting to the other components of the map unit. The presence of minor components in a map unit in no way diminishes the usefulness or accuracy of the data. The delineation of such landforms and landform segments on the map provides sufficient information for the development of resource plans. If intensive use of small areas is planned, onsite investigation is needed to define and locate the soils and miscellaneous areas.

Soil scientists make many field observations in the process of producing a soil map. The frequency of observation is dependent upon several factors, including scale of mapping, intensity of mapping, design of map units, complexity of the landscape, and experience of the soil scientist. Observations are made to test and refine the soil-landscape model and predictions and to verify the classification of the soils at specific locations. Once the soil-landscape model is refined, a significantly smaller number of measurements of individual soil properties are made and recorded. These measurements may include field measurements, such as those for color, depth to bedrock, and texture, and laboratory measurements, such as those for content of sand, silt, clay, salt, and other components. Properties of each soil typically vary from one point to another across the landscape.

Observations for map unit components are aggregated to develop ranges of characteristics for the components. The aggregated values are presented. Direct measurements do not exist for every property presented for every map unit component. Values for some properties are estimated from combinations of other properties.

While a soil survey is in progress, samples of some of the soils in the area generally are collected for laboratory analyses and for engineering tests. Soil scientists interpret the data from these analyses and tests, as well as field-observed characteristics and the soil properties to determine the expected behavior of the soils under different uses. Interpretations for all of the soils are field tested through observation of the soils in different uses and under different levels of management. Some interpretations are modified to fit local conditions, and some new interpretations are developed to meet local needs. Data are assembled from other sources, such as research information, production records, and field experience of specialists. For example, data on crop yields under defined levels of management are assembled from farm records and from field or plot experiments on the same kinds of soil.

Predictions about soil behavior are based not only on soil properties but also on such variables as climate and biological activity. Soil conditions are predictable over long periods of time, but they are not predictable from year to year. For example, soil scientists can predict with a fairly high degree of accuracy that a given soil will have a high water table within certain depths in most years, but they cannot predict that a high water table will always be at a specific level in the soil on a specific date.

After soil scientists located and identified the significant natural bodies of soil in the survey area, they drew the boundaries of these bodies on aerial photographs and

identified each as a specific map unit. Aerial photographs show trees, buildings, fields, roads, and rivers, all of which help in locating boundaries accurately.

Soil Map

The soil map section includes the soil map for the defined area of interest, a list of soil map units on the map, and extent of each map unit, and cartographic symbols displayed on the map. Also presented are various metadata about data used to produce the map, and a description of each soil map unit.



Map Unit Legend

Map Unit Symbol	Map Unit Name	Acres in AOI	Percent of AOI
UfB	Urban land, 0 to 8 percent slopes	2.2	100.0%
Total for Area of Interest			2.2
			100.0%

Map Unit Descriptions

The map units delineated in the detailed soil maps in a soil survey represent the soils or miscellaneous areas in the survey area. The map unit descriptions, along with the maps, can be used to determine the composition and properties of a unit. A map unit delineation on a soil map represents an area dominated by one or more major kinds of soil or miscellaneous areas. A map unit is identified and named according to the taxonomic classification of the dominant soils. Within a taxonomic class there are precisely defined limits for the properties of the soils. On the landscape, however, the soils are natural phenomena, and they have the characteristic variability of all natural phenomena. Thus, the range of some observed properties may extend beyond the limits defined for a taxonomic class. Areas of soils of a single taxonomic class rarely, if ever, can be mapped without including areas of other taxonomic classes. Consequently, every map unit is made up of the soils or miscellaneous areas for which it is named and some minor components that belong to taxonomic classes other than those of the major soils.

Most minor soils have properties similar to those of the dominant soil or soils in the map unit, and thus they do not affect use and management. These are called noncontrasting, or similar, components. They may or may not be mentioned in a particular map unit description. Other minor components, however, have properties and behavioral characteristics divergent enough to affect use or to require different management. These are called contrasting, or dissimilar, components. They generally are in small areas and could not be mapped separately because of the scale used. Some small areas of strongly contrasting soils or miscellaneous areas are identified by a special symbol on the maps. If included in the database for a given area, the contrasting minor components are identified in the map unit descriptions along with some characteristics of each. A few areas of minor components may not have been observed, and consequently they are not mentioned in the descriptions, especially where the pattern was so complex that it was impractical to make enough observations to identify all the soils and miscellaneous areas on the landscape.

The presence of minor components in a map unit in no way diminishes the usefulness or accuracy of the data. The objective of mapping is not to delineate pure taxonomic classes but rather to separate the landscape into landforms or landscape segments that have similar use and management requirements. The delineation of such segments on a map provides sufficient information for the development of resource plans. If intensive use of small areas is planned, however, onsite investigation is needed to define and locate the soils and miscellaneous areas.

1

MAP INFORMATION	
The soil surveys that comprise your AOI were mapped at 1:24,000.	Area of Interest (AOI)
Warning: Soil Map may not be valid at this scale.	Soils
Emergence of maps beyond the scale of mapping can cause misinterpretation of the detail of mapping and accuracy of soil measurements.	Special Features
Please refer to the bar scale on each map sheet for map source of Map.	Streams and Canals
Source of Map: Natural Resources Conservation Service Web Soil Survey URL:	Rails
Corridors in the Web Soil Survey System: Web Mercator (EPSG:3857)	Interstate Highways
Maps from the Web Soil Survey are based on the Web Mercator projection, which preserves direction and shape but distorts distance and area. A projection that preserves area, such as the Albers equal-area conic projection, should be used if more accurate calculations of distance or area are required.	US Routes
This product is generated from the USDA-NRCS certified data as of the version date(s) listed below.	Local Roads
Survey Area: Chester County, Pennsylvania	Lahalli
Soil Survey Date: Version 16, Sep 4, 2023	Gravelly Spot
Soil map units are labeled (as space allows) for map scales 1:50,000 or larger.	Closed Depressions
Details (several images were photographed): Jun 5, 2022-Jul 4, 2022	Miscellaneous Water
The orthophoto of other base maps on which the soil lines were compiled and digitized differs from the background imagery displayed on these maps. As a result, some mirror shifting of map unit boundaries may be evident.	Rock Outcrop
Shaded relief or slope contours are not included on the soil map.	Perennial Water
Soil Survey Area: Survey Area	Seasonal Spot
Soil map units are labeled (as space allows) for map scales 1:50,000 or larger.	Shrubland
Soil Survey Date: Version 16, Sep 4, 2023	Soil
Soil Survey Area: Chester County, Pennsylvania	Soil Map Unit Polygons
Soil Survey Date: Version 16, Sep 4, 2023	Soil Map Unit Lines
Soil Survey Date: Version 16, Sep 4, 2023	Soil Survey Points
Soil Survey Date: Version 16, Sep 4, 2023	Soil Survey Spots
Soil Survey Date: Version 16, Sep 4, 2023	Soil Area
Soil Survey Date: Version 16, Sep 4, 2023	Area of Interest (AOI)
Soil Survey Date: Version 16, Sep 4, 2023	Map Legend

An identifying symbol precedes the map unit name in the map unit descriptions. Each description includes general facts about the unit and gives important soil properties and qualities.

Soils that have profiles that are almost alike make up a *soil series*. Except for differences in texture of the surface layer, all the soils of a series have major horizons that are similar in composition, thickness, and arrangement.

Soils of one series can differ in texture of the surface layer, slope, stoniness, salinity, degree of erosion, and other characteristics that affect their use. On the basis of such differences, a soil series is divided into *soil phases*. Most of the areas shown on the detailed soil maps are phases of soil series. The name of a soil phase commonly indicates a feature that affects use or management. For example, Alpha silt loam, 0 to 2 percent slopes, is a phase of the Alpha series.

Some map units are made up of two or more major soils or miscellaneous areas.

These map units are complexes, associations, or undifferentiated groups.

A complex consists of two or more soils or miscellaneous areas in such an intricate pattern or in such small areas that they cannot be shown separately on the maps. The pattern and proportion of the soils or miscellaneous areas are somewhat similar in all areas. Alpha-Beta complex, 0 to 6 percent slopes, is an example.

An *association* is made up of two or more geographically associated soils or miscellaneous areas that are shown as one unit on the maps. Because of present or anticipated uses of the map units in the survey area, it was not considered practical or necessary to map the soils or miscellaneous areas separately. The pattern and relative proportion of the soils or miscellaneous areas are somewhat similar. Alpha-Beta association, 0 to 2 percent slopes, is an example.

An *undifferentiated group* is made up of two or more soils or miscellaneous areas that could be mapped individually but are mapped as one unit because similar interpretations can be made for use and management. The pattern and proportion of the soils or miscellaneous areas in a mapped area are not uniform. An area can be made up of only one of the major soils or miscellaneous areas, or it can be made up of all of them. Alpha and Beta soils, 0 to 2 percent slopes, is an example.

Some surveys include *miscellaneous areas*. Such areas have little or no soil material and support little or no vegetation. Rock outcrop is an example.

Chester County, Pennsylvania

URB—Urban land, 0 to 8 percent slopes

Map Unit Setting

National map unit symbol: 13nt

Elevation: 800 to 1,500 feet

Mean annual precipitation: 36 to 46 inches

Mean annual air temperature: 41 to 62 degrees F

Frost-free period: 130 to 170 days

Farmland classification: Not prime farmland

Map Unit Composition

Urban land: 90 percent

Minor components: 10 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Urban Land

Setting
Parent material: Pavement, buildings and other artificially covered areas human transported material

Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 8s

Hydric soil rating: No

Minor Components

Udorthents, unstable fill

Percent of map unit: 10 percent

Down-slope shape: Linear

Across-slope shape: Linear

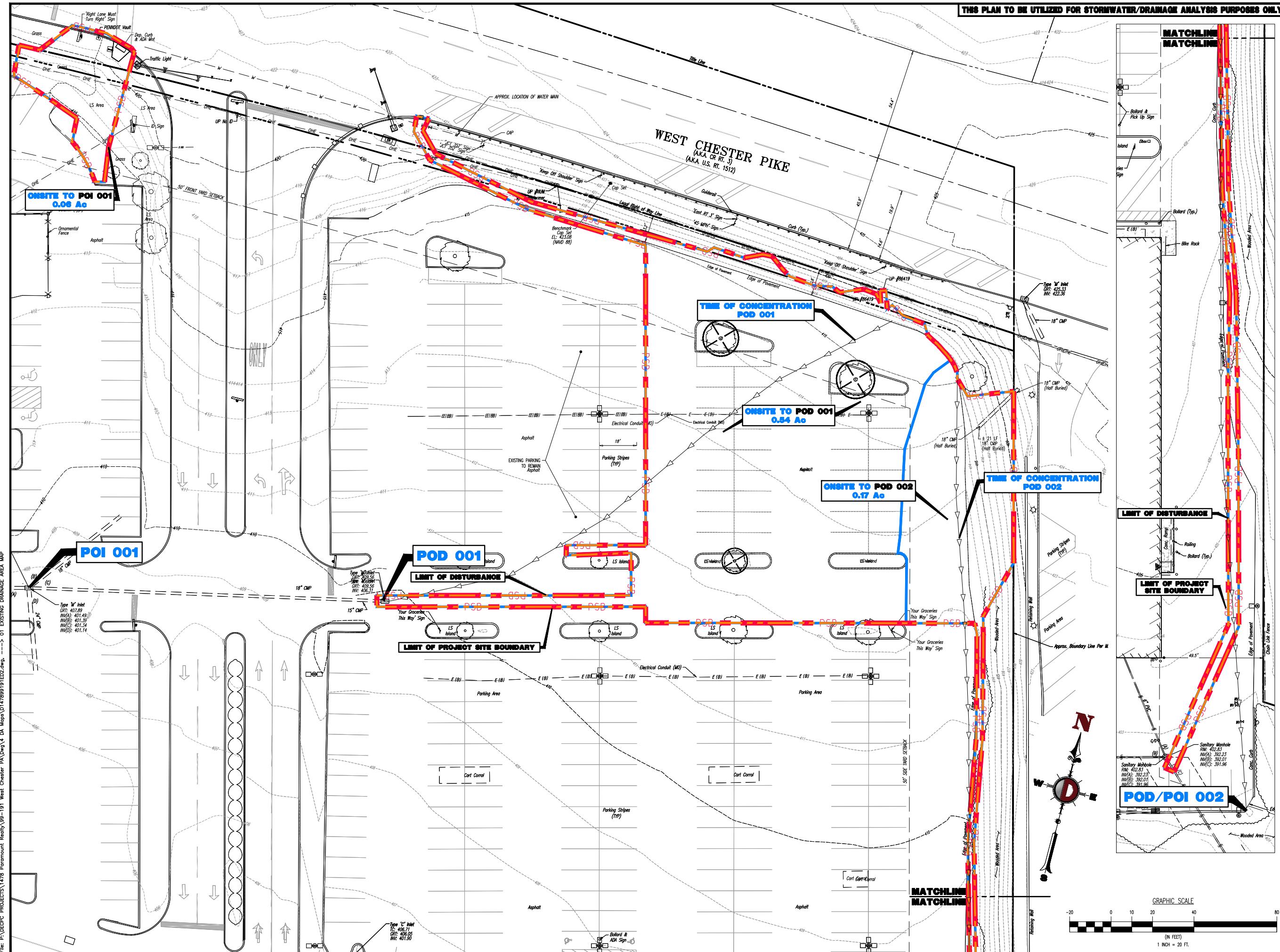
Hydric soil rating: No

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O. DRAINAGE AREA MAPS



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JUSTIN A. GEONNOTTI
PROFESSIONAL ENGINEER

MATTHEW SHARO

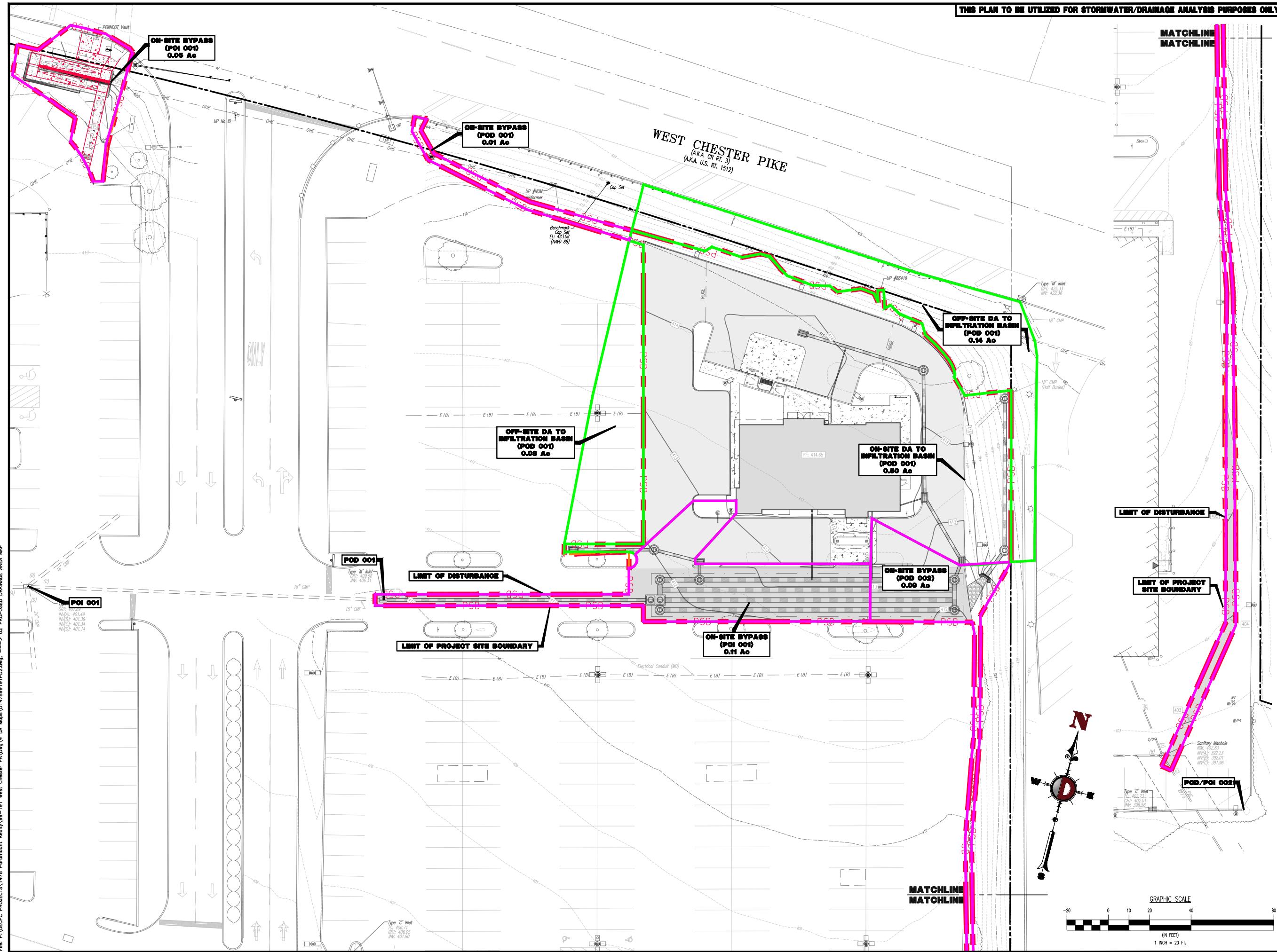
**EXISTING
DRAINAGE AREA
MAP**

1"=20'
DATE:
07/12/2024
No:
78-99-191

No:	1	Rev. #:
	OF 03	2



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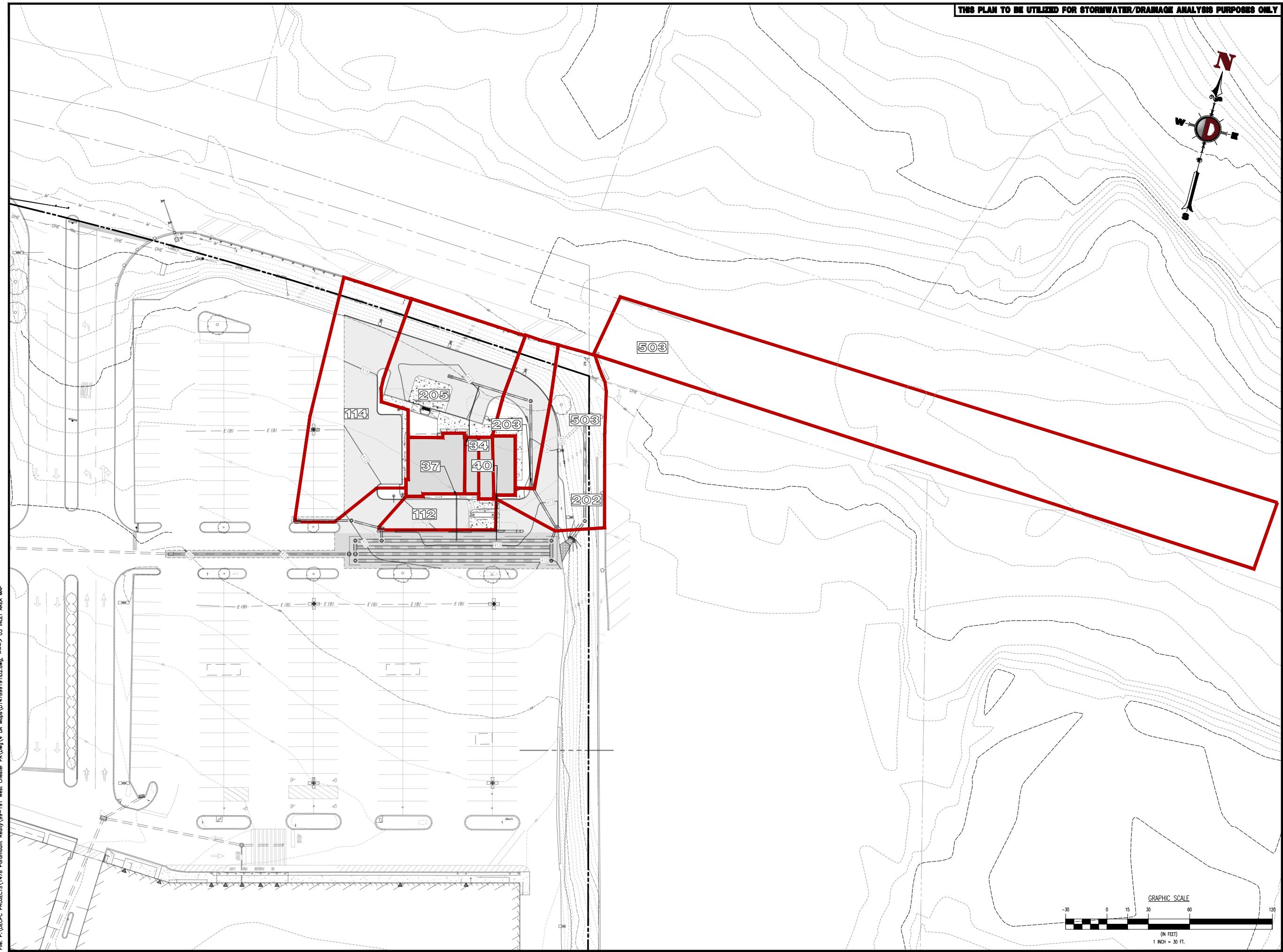
JUSTIN A. GEONNOTTI

MATTHEW SHARO

PROPOSED DRAINAGE AREA MAP

1"=20' 0).	DATE: 07/12/2024
No: 78-99-191	

2
OF 03
2



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REV. DATE	BY
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1 09/20/24 REV. PER TOWNSHIP COMMENTS	AW
COMMENTS	
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TITLE: INLET AREA MAP

SCALE: (H) 1"=20' (V) 07/12/2024
PROJECT #: 1478-99-191
SHEET No: 3 Rev. #: 2
OF 03